

§1.2 The zeroth law

If two systems are in equilibrium separately with a third system, then they are at equilibrium with each other. (Transitivity)



$$\begin{aligned} f_{AC}(\underline{A}, \underline{C}) &= 0 & \text{We may restate this as} \\ f_{BC}(\underline{B}, \underline{C}) &= 0 & c_1 = F_{AC}(\underline{A}, \underline{c}_2 \dots) \\ && c_1 = F_{BC}(\underline{B}, \underline{c}_2 \dots) \\ && \Rightarrow F_{AC}(\underline{A}, \underline{c}_2 \dots) = F_{BC}(\underline{B}, \underline{c}_2 \dots) \end{aligned} \quad (1)$$

Now invoking the zeroth law.

$$f_{AB}(\underline{A}, \underline{B}) = 0$$

(1) holds for the surface constrained by $f_{AB} = 0$.

$$\Rightarrow F_{AC} = F_{AC}(\underline{A}) = F_{BC}(\underline{B})$$

$$\text{Renaming } \theta_{AC}(\underline{A}) = \theta_{BC}(\underline{B})$$

These specify equation of state

NOTE: The zeroth law severely restricts the types of f 's (of constraint eq')

Temperature Scale (K):

→ Empirically PV is const for volumes of dilute gases.

$$T(K) \equiv 273.16 \times \frac{\frac{d}{dt} (PV)_{\text{sys}}}{\frac{d}{dt} (PV)_{\text{ice-water}}}$$

§1.3 The first law

For adiabatic: $\Delta W = E(x_f) - E(x_i)$

Heat intake: $\Delta Q = \Delta E - \Delta W$

$$dQ = dE - dW$$

NOTE: signs of heat & work are s.t. energy is added to the system.

Quasi Static: Sufficiently slow, s.t. all steps are at equilibrium.

$$dW = \sum J_i dx_i \quad \leftarrow \text{valid only for quasi-static} \quad \begin{matrix} J_i - \text{gen. force} \\ dx_i - \text{gen. displacement} \end{matrix}$$

NOTE: P is calculated from the force exerted on the walls, by the system. Think. Thus we have a minus sign.

Extensive Quantities: proportional to system size (gen. forces)

Intensive Quantities: independent of size (gen. displacements) (eg. relation

→ Temp \leftrightarrow (displacement!)

(lit gen. force)

Response T^n :

Heat capacities: $C_p > C_v$ (physical arg.)

$$C_v = \left. \frac{dQ}{dT} \right|_v = \left. \frac{\partial E}{\partial T} \right|_v ; \quad C_p = \left. \frac{dQ}{dT} \right|_p = \left. \frac{\partial E}{\partial T} \right|_p + P \left. \frac{\partial V}{\partial T} \right|_p$$

True constants: infinitesimal ratio of displacement to force.

$$\text{Isothermal compressibility: } \kappa_T = - \left. \frac{\partial V}{\partial P} \right|_T$$

$$\text{Susceptibility of a magnet: } \chi_T = \left. \frac{\partial M}{\partial B} \right|_T$$

(comes from extensivity)

Thermal Responses: Change of thermodynamic coordinates V with temperature.

$$\alpha_p = \left. \frac{\partial V}{\partial T} \right|_p \quad (= \frac{1}{T} \text{ for ideal gases})$$

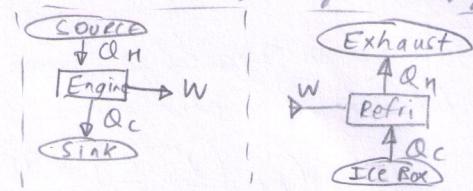
$$\begin{aligned} \text{for ideal gas:} \\ C_p - C_v &= P \left. \frac{\partial V}{\partial T} \right|_p \\ &= PV \alpha_p \\ &= \frac{PV}{T} = \frac{NK}{T} \end{aligned}$$

§1.4 The second law

Remark: Considering efficiencies of heat engines leads to the concept of entropy.

$$\text{Heat Engine Efficiency: } \eta = \frac{W}{Q_H} = \frac{Q_H - Q_C}{Q_H} \leq 1$$

$$\text{Figure of merit of refrigerator: } \omega = \frac{Q_C}{W} = \frac{Q_C}{Q_H - Q_C}$$



Kelvin's Statement: No process is possible whose sole result is the complete conversion of heat into work. ($Q_C = 0$)

Clausius's Statement: No process is possible whose sole result is the transfer of heat from a colder to a hotter body. ($W = 0$ in refri)

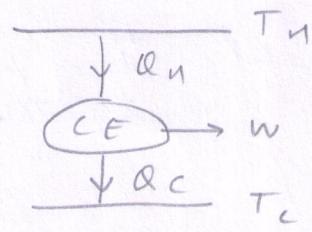
(a) Equivalence of Kelvin's & Clausius's Statements

$$(a) \quad \begin{array}{c} \text{hot} \\ \downarrow Q \\ \text{CE} \\ \downarrow Q_C = Q \end{array} \text{ cold} \quad \begin{array}{c} \downarrow Q_H \\ \text{CE} \\ \downarrow Q_C \end{array} \rightarrow W = \begin{array}{c} \text{hot} \\ \downarrow Q_H - Q_C \\ \text{CE} \\ \downarrow Q_C \end{array} \rightarrow W$$

$$(b) \quad \begin{array}{c} \text{hot} \\ \downarrow Q \\ \text{CE} \\ \rightarrow W \end{array} \quad \begin{array}{c} \downarrow Q_H \\ \text{CE} \\ \downarrow Q_C \end{array} = \begin{array}{c} \text{hot} \\ \downarrow Q_H - Q \\ \text{CE} \\ \downarrow Q_C \end{array} \text{ cold}$$

§1.5 Carnot Engines

A Carnot engine: One that is ① reversible, ② runs in a cycle, ③ with heat exchanges only at a source T_H & a sink T_C .



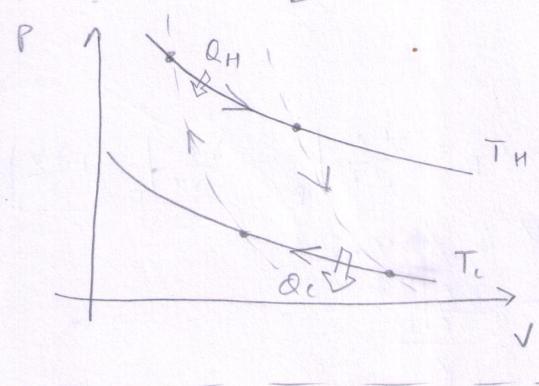
Reversible: One that can run backwards by simply reversing inputs & outputs.

Remark: It's the thermodynamic equivalent of frictionless motion.

Remark: Since heat is not a f' of state, we don't know how to construct adiabats in general.

Internal working substance: ideal gas

$$E = \frac{3}{2} N k_B T = \frac{3}{2} PV \quad \begin{aligned} \delta Q = dE - \delta W \quad \text{for } \delta Q = 0 \quad (\text{as said}) \\ \frac{dP}{P} + \frac{5}{3} \frac{dV}{V} = 0 \Rightarrow PV^{\frac{5}{3}} = \text{const where } r = \frac{5}{3} \end{aligned}$$



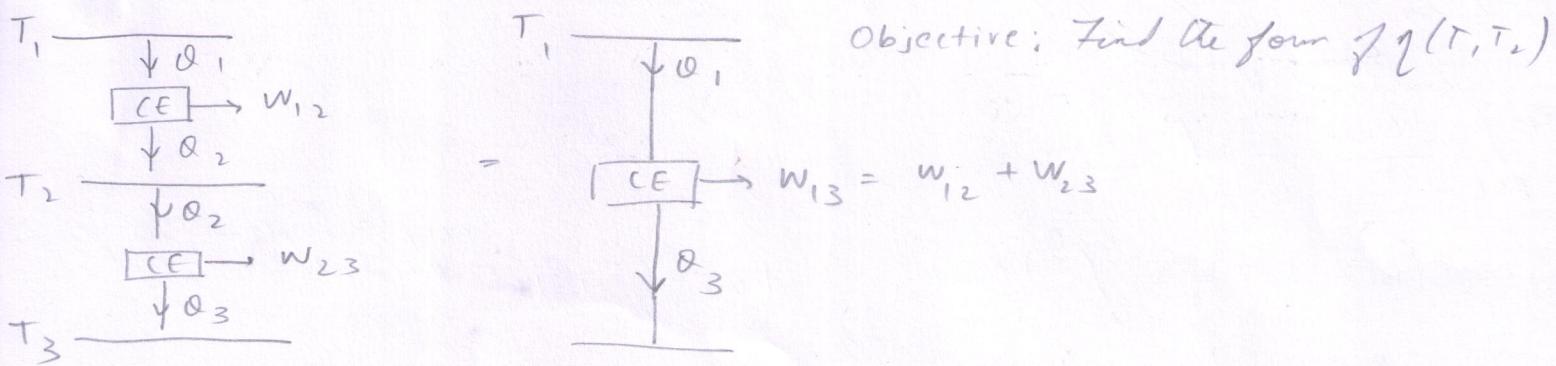
Carnot Theorem: No engine operating b/w two reservoirs (at temperatures T_H & T_C) is more efficient than a Carnot engine operating b/w them.
viz. $\eta_{\text{Carnot}} > \eta_{\text{other engine}}$ (for a given T_H & T_C)

Thus using the 2nd law

$$Q_H - Q_H' > 0 \Rightarrow Q_H > Q_H'$$

$$\begin{array}{c} \text{hot} \\ \downarrow Q_H \\ \text{CE} \\ \downarrow Q_C \end{array} \quad \begin{array}{c} \text{hot} \\ \downarrow Q_H' \\ \text{CE} \\ \downarrow Q_C' \end{array} \quad = \quad \begin{array}{c} \text{hot} \\ \downarrow Q_H - Q_H' \\ \text{CE} \\ \downarrow Q_C - Q_C' \end{array} \quad \text{cold}$$

remark: We've shown that max. efficiency is only dependent on the two temperatures; we thus use it to construct a temperature scale.



$$Q_2 = Q_1 - w_{12} = Q_1 [1 - \eta(T_1, T_2)]$$

$$Q_3 = Q_2 - w_{23} = Q_2 [1 - \eta(T_2, T_3)]$$

$$= Q_1 [1 - \eta(T_1, T_2)] [1 - \eta(T_2, T_3)] \quad \text{using}$$

$$Q_3 = Q_1 - w_{13} = Q_1 [1 - \eta(T_1, T_3)]$$

$$\Rightarrow [1 - \eta(T_1, T_3)] = [1 - \eta(T_1, T_2)] [1 - \eta(T_2, T_3)] \quad \text{using}$$

? (convention)

$$\Rightarrow 1 - \eta(T_1, T_2) \text{ is of the form } \frac{f(T_2)}{f(T_1)} = \frac{T_2}{T_1}$$

$$\Rightarrow 1 - \eta(T_1, T_2) = \frac{Q_2}{Q_1} = \frac{T_2}{T_1}$$

$$\Rightarrow \eta(T_H, T_C) = \frac{T_H - T_C}{T_H}$$

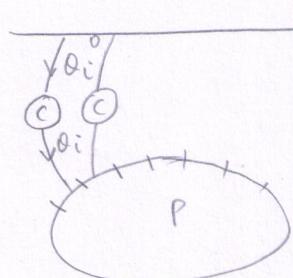
(weak! efficiency for defining Temp upto a prop const)

claim: θ & T can be made equivalent
↑ efficiency based def' of temp.
ideal gas temp

Note: Thus $T > 0$ else Kelvin's statement is violated.

§ 1.6 Entropy

Clausing's Theorem: For any cyclic transformation (reversible or not), $\oint \frac{\partial Q}{T} \leq 0$, where ∂Q is the heat supplied to the system at temperature T .



T°

For the whole system:

$$W_{\text{tot}} = W + \sum (Q_i^\circ - Q_i)$$

$$= \sum Q_i^\circ = \sum \frac{Q_i}{T_i} T^\circ$$

$$\text{also } \frac{Q_i^\circ}{Q_i} = \frac{T^\circ}{T_i} = T^\circ \sum \frac{Q_i}{T_i}$$

for the cyclic process

$$W = \sum Q_i$$

Now from 2nd law

$$W_{\text{tot}} = \sum Q_i^\circ = Q_{\text{tot}} \leq 0$$

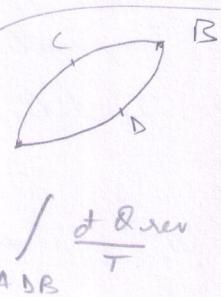
$$\Rightarrow T^\circ \sum \frac{Q_i^\circ}{T_i} \leq 0 \Rightarrow \oint \frac{\partial Q}{T} \leq 0$$

For reversible

$$\oint \frac{dQ_{rev}}{T} = 0$$

(you reverse therm calc.)

$$\Rightarrow \int_{ACB} \frac{dQ_{rev}}{T} = \int_{ADB} \frac{dQ_{rev}}{T}$$



and you again get

$$\oint \frac{dQ'}{T} \leq 0; \text{ now since } dQ' = -dQ \text{ (you reverse)} \\ \text{thus } \oint \frac{dQ}{T} \geq 0.$$

$$② S(B) - S(A) = \int_A^B \frac{dQ_{rev}}{T} \quad | \quad dQ_{rev} = T dS \quad \text{using this } ds=0, \text{ we find} \\ \text{defined upto an arbitrary const.} \quad | \quad \text{Thus}$$

Remark: after 1.24 is subtle in the text.

$$③ dF = T dS + \sum_j J_j dx_j \\ (\text{true even when non-reversible!})$$

④ # independent variables are $n+i$ if $\exists n$ conjugate pairs (for doing work)

$$\text{e.g. } (E, \{x_i\}) \text{ Then } \frac{\partial E}{\partial x_i} = \frac{1}{T}, \quad \frac{\partial S}{\partial x_i} \Big|_{E, x_{j \neq i}} = -J_i \frac{1}{T}$$

$$⑤ \int_A^B \frac{dQ}{T} + \int_B^A \frac{dQ_{rev}}{T} \leq 0 \Rightarrow \int_A^B \frac{dQ}{T} \leq S(B) - S(A)$$

$$\Rightarrow \boxed{dS \geq \frac{dQ}{T}} \quad | \quad \text{Entropy increases to equilibrium.} \\ \text{if } dQ > 0 \text{ then } dS > 0, \quad \text{if } dQ < 0 \text{ then } dS < 0,$$

§ 1.7 Approaches to equilibrium and thermodynamic Potentials

Enthalpy: $dQ=0$, eq. to const. external force (T)

$$\frac{\partial W}{\partial x} \leq J_i \cdot \delta x \quad (T = J_i \text{ for quasi static, in general there'll be a} \\ \text{work input to the system} \quad | \quad \text{external force} \quad \text{work done by 'us' } \quad \text{dissipation loss})$$

Now since $dQ=0$, we have

$$dE = dW \leq T \cdot \delta x$$

$$\Rightarrow dH \leq 0 \quad \text{where } H = E - T \cdot x$$

At equilibrium then, $\langle \text{TODO: fill} \rangle$

Helmholtz free energy

Isothermal in absence of mechanical work

$$T = \text{const.} \quad dW = 0$$

$$TS \leq dQ \Rightarrow dE = dQ + dW \leq TS$$

$$\Rightarrow dF \leq 0 \quad \text{where } F = E - TS$$

At eq. $\langle \text{TODO: fill} \rangle$

Gibbs free energy +

(const T) $\delta Q = \text{thermal work at constant temperature}$

$$\delta W \leq T \cdot \delta x \quad \& \quad \delta Q \leq T \delta S$$

$$\delta E \leq T \cdot \delta S + T \cdot \delta x$$

$$\Rightarrow \delta G \leq 0 \quad \text{where} \quad G = E - TS - Tx$$

Grand Potential

$$G = E - TS - \mu \cdot N$$

$\mu = \{\mu_1, \mu_2, \dots\}$ chemical pot.

$N = \{N_1, N_2, \dots\}$ # particle of each species

$$dG = -SdT + T \cdot dx - N \cdot d\mu$$

$dW \cdot \mu \cdot dN$ specifies change in internal energy upon the addition of molecular species

§ 1.8 Useful mathematical results

(1) Extensivity

$$\rightarrow dF = T \cdot dS + J \cdot dx + \mu \cdot dN$$

For fixed intensive co-ordinates, the extensive coordinates are mapped to sys. size (particle #)
i.e. $E(\lambda s, \lambda x, \lambda N) = \lambda E(s, x, N)$

Evaluating the derivatives w.r.t. λ we have
& putting $\lambda = 1$

$$\frac{\partial E}{\partial \lambda} \Big|_{s, x, N} = \sum \frac{\partial E}{\partial s_i} \Big|_{s, x, N} + \sum \frac{\partial E}{\partial x_\alpha} \Big|_{s, x, N} + \sum \frac{\partial E}{\partial N_\alpha} \Big|_{s, x, N} = F$$

The partials from are T, J_i & μ_α respectively

$$\text{thus } F = TS + J \cdot x + \mu \cdot N$$

differentiate & use to get

$$dT + x \cdot dJ + N \cdot d\mu = 0$$

called ^{the} Gibbs-Duhem relation

$$\begin{aligned} \text{side note} \\ \text{let } \lambda s = x(\lambda) \\ \lambda x = y(\lambda) \\ \lambda N = z(\lambda) \\ \text{then} \\ \frac{dF}{d\lambda} &= \frac{\partial E}{\partial x} \frac{\partial x}{\partial \lambda} + \\ &\quad \frac{\partial E}{\partial y} \frac{\partial y}{\partial \lambda} + \\ &\quad \frac{\partial E}{\partial z} \frac{\partial z}{\partial \lambda} \\ &= \frac{\partial E}{\partial (x)} \frac{\partial x}{\partial \lambda} + \\ &\quad \frac{\partial E}{\partial (y)} \frac{\partial y}{\partial \lambda} + \frac{\partial E}{\partial (z)} \frac{\partial z}{\partial \lambda} \end{aligned}$$

It's sometimes called the "fundamental eq" of thermodynamics. It holds only when extensivity holds!

Kardas page 37, Feb 3, 2014

$$\langle F(x) \rangle = \int_{-\infty}^{\infty} p(x) F(x) dx$$

$\lim F(x)$ itself is a random variable with PDF

$$p_F(f) df = \text{prob}(F(x) \in [f, f+df])$$

$F(x) = f$ may have multiple solns. let the solns be x_i :

$$\begin{aligned} p_F(f) df &= \sum_i p(x_i) dx_i \Rightarrow p_F(f) = \sum_i p(x_i) \frac{dx_i}{df} \\ &= \sum_i p(x_i) \left. \frac{dx}{dF} \right|_{x=x_i} \end{aligned}$$

$\left| \frac{dx}{dF} \right|$ are the Jacobians associated with change of variables from x to F .

Eg. $p(x) = \lambda e^{-\frac{\lambda|x|}{2}}$

$$f(x) = x^2 \quad f(x) = f \text{ has 2 solns} \quad x_{\pm} = \pm \sqrt{f}$$

with the Jacobian $\left| \pm \frac{f^{-1/2}}{2} \right|$

$$\therefore p_F(f) = \frac{\lambda}{2} e^{-\lambda \sqrt{f}} \left(\left| \frac{1}{2\sqrt{f}} \right| + \left| -\frac{1}{2\sqrt{f}} \right| \right) = \frac{\lambda e^{-\lambda \sqrt{f}}}{2\sqrt{f}}$$

$$\text{for } f > 0 \quad \text{and} \quad p_F(f) = 0 \quad \text{for } f \leq 0.$$

* The n^{th} moment is

$$\text{Def} \quad m_n = \langle x^n \rangle = \int dx p(x) x^n$$

* The characteristic f is the generator of moments of the distribution.

In the Fourier transform of the PDF

$$\tilde{f}(k) = \langle e^{-ikx} \rangle = \int dx p(x) e^{-ikx}$$

The PDF can be recovered as

$$\begin{aligned} p(x) &= \frac{1}{2\pi} \int dk \tilde{f}(k) e^{ikx} &= \frac{1}{2\pi} \int dk \int dx p(x) e^{-ikx} e^{ikx} \\ &= \frac{1}{2\pi} \int dk e^{ikx} \int dx' p(x') e^{-ikx'} \end{aligned}$$

* Moments of the dist are obtained by expanding $\tilde{f}(k)$ in powers of k .

$$\tilde{f}(k) = \left\langle \sum_{n=0}^{\infty} \frac{(-ik)^n}{n!} x^n \right\rangle = \sum_{n=0}^{\infty} \frac{(-ik)^n}{n!} \langle x^n \rangle$$

Also,

$$e^{ikx_0} \tilde{p}(k) = \langle e^{-ik(x-x_0)} \rangle = \sum_{n=0}^{\infty} \frac{(-ik)^n}{n!} \langle (x-x_0)^n \rangle$$

²⁴ The cumulant generating $f^ = \ln(\text{characteristic } f^*)$

& its expansion generates cumulants.

$$\ln(\tilde{p}(k)) \equiv \sum_{n=1}^{\infty} \frac{(-ik)^n}{n!} \langle x^n \rangle_c \quad \left| \begin{array}{l} \text{Op.} \\ \langle x^n \rangle_c \end{array} \right| \quad \ln x = \frac{1}{x} \Big|_0 \quad \text{opp.} \\ \ln(1) = x$$

$$\ln \left(1 + \sum_{n=1}^{\infty} \frac{(-ik)^n}{n!} \langle x^n \rangle \right) \\ = \sum_{m=1}^{\infty} (-1)^{m+1} \left[\sum_{n=1}^{\infty} \frac{(-ik)^n}{n!} \langle x^n \rangle \right]^m$$

= (from Defⁿ of $\ln(\tilde{p}(x))$)

$$\sum_{n=1}^{\infty} \frac{(-ik)^n}{n!} \langle x^n \rangle_c$$

$$\langle x \rangle_c = \langle x \rangle$$

$$\langle x^2 \rangle_c = \langle x^2 \rangle - \langle x \rangle^2 \dots$$

\downarrow Known of K
Not clear on
what is x compared

$$\ln(1+x) = \ln(1) + \frac{1}{1+x} \Big|_{x=0} x \quad \left| \begin{array}{l} e^x = y \\ \ln e^x = x = \ln y \\ e^x = 1 \quad |x=0 \end{array} \right.$$

$$\frac{d}{dx} (1+x)^{-1} = \frac{-1 \cdot 1}{(1+x)^2}$$

$$\frac{d}{dx} (1+x)^{-2} = \frac{-2}{(1+x)^3} \cdot 1$$

$$\ln(1+\epsilon) = \sum_{n=1}^{\infty} (-1)^{n+1} \frac{\epsilon^n}{n} \quad \checkmark$$

§ 2.3 Some Important prob. distributions

$$(1) \text{ Normal} \quad p(x) = \frac{1}{\sqrt{2\pi\sigma^2}} \left[e^{-\frac{(x-\lambda)^2}{2\sigma^2}} \right]$$

$$\tilde{p}(x) = \int dx \frac{1}{\sqrt{2\pi\sigma^2}} e^{-\frac{(x-\lambda)^2}{2\sigma^2} - ikx}$$

$$\stackrel{?}{=} e^{-ik\lambda - \frac{k^2\sigma^2}{2}}$$

$$\ln \tilde{p}(k) = -ik\lambda - \frac{k^2\sigma^2}{2}$$

$$= \sum_{n=1}^{\infty} \frac{(-ik)^n}{n!} \langle x^n \rangle_c$$

$$\int_A e^{-ikx} dx \\ \int e^{-ikx} dx =$$

$$\Rightarrow \langle x \rangle_c = \lambda \quad \langle x^2 \rangle_{xc} = \sigma^2 \quad \left| \langle x^3 \rangle_c = \langle x^4 \rangle_c = \dots = 0 \right.$$

Binomial 1/2 $p_N(N_A) = \binom{N}{N_A} P_A^{N_A} P_B^{N-N_A}$

$$\tilde{p}_N(k) = \langle e^{-ikN_A} \rangle = \sum_{N_A=0}^N \frac{N!}{N_A!(N-N_A)!} P_A^N P_B^{N-N_A} e^{-ikN_A} \\ = (P_A \cdot e^{-ik} + P_B)^N$$

$$\ln \tilde{P}_N(k) = N \ln (P_A e^{-ik} + P_B) = N \ln (\tilde{P}_1(k))$$

From the def' of expectation &

$$N_A = 0 \quad \text{with prob } P_B$$

$$N_A = 1 \quad \text{with prob } P_A, \text{ we have}$$

$$\langle N_A^l \rangle = P_A \quad \forall l > 0$$

In general then

$$\langle N_A \rangle_c = N P_A$$

$$\langle N_A^2 \rangle_c = N (P_A - P_A^2)$$

$$\langle N_A^2 \rangle_c = \langle N_A \rangle_c^2 - \langle N_A \rangle_c^2$$

$$\ln \tilde{P}(k) = \sum_{n=1}^{\infty} \frac{(-ik)^n}{n!} \langle x^n \rangle_c$$

$$\ln \tilde{P}_N(k) = \sum_{n=1}^{\infty} \frac{(-ik)^n}{n!} \langle (N_A^n) \rangle_c = N \ln (\tilde{P}_1(k)) = -ik P_A N$$

$$\langle N_A^1 \rangle_c = N P_A$$

$$\langle N_A^2 \rangle_c = 0$$

$$P_N(N_A) = \binom{N}{N_A} P_A^{N_A} P_B^{1-N_A}$$

$$\tilde{P}_N(k) = \langle e^{-ik N_A} \rangle = \sum_{N_A=0}^N \frac{N!}{N_A! (N-N_A)!} P_A^{N_A} P_B^{N-N_A} e^{-ik N_A}$$

$$= (P_A e^{-ik} + P_B)^N$$

$$\ln \tilde{P}_N(k) = N (P_A e^{-ik} + P_B) = N \tilde{P}_1(k)$$

$$\star \langle \ln \tilde{P}_N(k) \rangle = N \langle \tilde{P}_1(k) \rangle = N \langle (P_A e^{-ik} + P_B) \rangle \text{ Not helping}$$

$$\tilde{P}_1(k) = \langle e^{-i N_A k} \rangle = P_A e^{-ik} + P_B$$

$$P_1(N_A) = P_A$$



$$\ln \tilde{P}_N(k) = N \tilde{p}_1(k)$$

This shows that we need to calc. anything only for 1 trial & the cumulants will become N times that of the 1 trial case.

Now for 1 trial

$$\langle N_A \rangle = 0 \cdot P_B + 1 \cdot P_A = P_A$$

$$\langle N_A^2 \rangle = 0 \cdot P_B + 1^2 \cdot P_A = P_A$$

!

$$\langle N_A^l \rangle = P_A$$

$$\text{Thus, } \langle N_A \rangle_c = \langle N_A \rangle = P_A$$

$$\begin{aligned} \text{for 1 trial } \langle N_A^2 \rangle_c &= \langle N_A^2 \rangle - (\langle N_A \rangle)^2 \\ &= P_A - P_A^2 \end{aligned}$$

$$\text{Thus } \langle N_A \rangle_c = N P_A$$

$$\text{for } N \text{ trials } \langle N_A^2 \rangle_c = N (P_A - P_A^2)$$

(3) The Poisson Distribution

- (a) Prob. of one & only one event (decay) in the interval $[t, t+dt]$ is proportional to dt as $dt \rightarrow 0$.
- (b) The prob. of events at different intervals are independent of each other.

The prob. of observing exactly M decays in the interval T is given by the Poisson distribution.

It is obtained by dividing the interval into $N = T/dt \gg 1$, as a limit of the binomial distribution.

In each segment, an event occurs with the prob. $P_A dt$ & no event with $q = 1 - \alpha dt$.

$$\begin{aligned} \tilde{p}(k) &= (pe^{-ik} + q)^N = \lim_{dt \rightarrow 0} [p \times dt e^{-ik} + 1 - \alpha dt]^N \\ &= \lim_{dt \rightarrow 0} [(e^{-ik}-1) \times dt + 1]^{T/dt} \\ &= e^{-\alpha(e^{-ik}-1)T} \end{aligned}$$

The gaussian PDF is obtained as

$$\begin{aligned}
 p(x) &= \int \frac{dk}{2\pi} e^{\alpha(e^{-ik}-1)\tau + ikx} \\
 &= e^{-\alpha\tau} \left/ \frac{dk}{2\pi} e^{ikx} e^{\alpha\tau e^{-ik}} \right. \\
 &= e^{-\alpha\tau} \int \frac{dk}{2\pi} e^{ikx} \sum_{M=0}^{\infty} \frac{(\alpha\tau)^M}{M!} e^{-ikM} \\
 &\quad \int \frac{dk}{2\pi} e^{ik(x-M)} = \delta(x-M)
 \end{aligned}$$

$$\Rightarrow P_{\alpha\tau}(x) = \sum_{M=0}^{\infty} e^{-\alpha\tau} \frac{(\alpha\tau)^M}{M!} \delta(x-M)$$

$\Rightarrow x$ are integers only. Thus for $n = \text{some int say } M$

$$P_{\alpha\tau}(M) = e^{-\alpha\tau} \frac{(\alpha\tau)^M}{M!}$$

Cumulants are obtained.

$$\ln \tilde{P}_{\alpha\tau}(k) = \alpha\tau(e^{-ik}-1) = \alpha\tau \sum_{n=1}^{\infty} \frac{(-ik)^n}{n!}$$

$$\Rightarrow \langle M^n \rangle_c = \alpha\tau$$

| Many Random Variables | § 2-4

- The joint PDF $p(\vec{x})$ is prob. density of an outcome in the vol. element

$$d^N \vec{x} = \prod_{i=1}^N dx_i \quad \text{around} \quad \vec{x} = \{x_1, x_2, \dots, x_N\}$$

- Normalized s.t.

$$P_{\vec{x}}(S) = \int d^N \vec{x} p(\vec{x}) = 1$$

If events are independent,

$$p(\vec{x}) = \prod_{i=1}^N p_i(x_i)$$

→ Unconditional PDF : describes subset of random variables

$$p(x_1, \dots, x_m) = \int \prod_{i=m+1}^N dx_i p(x_1, \dots, x_N)$$

→ Conditional PDF :

$$p(x_1, \dots, x_m | x_{m+1}, \dots, x_N) = \frac{p(x_1, \dots, x_N)}{p(x_{m+1}, \dots, x_N)}$$

$$p(\vec{v} | \vec{x}) = \frac{p(\vec{x}, \vec{v})}{p(\vec{x})}$$

if \vec{v} & \vec{x} are independent then

$$p(\vec{v} | \vec{x}) \text{ should be } p(\vec{v})$$

$$\therefore p(\vec{x}, \vec{v}) = p(\vec{x}) p(\vec{v})$$

$$\text{then } p(\vec{v} | \vec{x}) = \frac{p(\vec{x}, \vec{v})}{p(\vec{x})} = p(\vec{v})$$

→ expectation

$$\langle F(\vec{x}) \rangle = \int d^N \vec{x} p(\vec{x}) F(\vec{x})$$

→ Joint characteristic f'

$$\tilde{p}(\vec{x}) = \left\langle e^{i \sum_{j=1}^N k_j x_j} \right\rangle$$

(Missing stuff)

§ 2.5 Sums of random variables & the central limit theorem.

$$x = \sum_{i=1}^N x_i$$

$$\begin{aligned} p_x(\vec{x}) &= \int d^N \vec{x} p(\vec{x}) \delta(x - \sum x_i) \\ &= \int d\vec{x} \prod_{i=1}^{N-1} p(x_1, x_2, \dots, x - x_1 - x_2 - \dots - x_{N-1}) \end{aligned}$$

$$\tilde{p}_x(k) = \left\langle e^{-ik \sum x_i} \right\rangle$$

$$= \tilde{p} \cdot (k_1 = k_2 = \dots = k_N = k)$$

$$\ln \cdot \tilde{p} = -\langle k \rangle \sum_{i=1}^N \langle x_i \rangle_c + \frac{(-ik)^2 \sum_{i_1 i_2} \langle x_{i_1} x_{i_2} \rangle_c}{2}$$

+ ...

$$\text{as } \langle x \rangle_c = \langle \sum x_i \rangle = \sum \langle x_i \rangle$$

$$\langle x^2 \rangle_c = \langle (\sum x_i)^2 \rangle = \sum_{i,j} \langle x_i x_j \rangle$$

If the random variables are ~~random~~, independent, then

$$p(\vec{x}) = \prod p_i(x_i)$$

$$\tilde{p}_x(k) = \prod \tilde{p}_i(k)$$

The cross terms in $\ln \tilde{p}$'s expansion vanish. Thus

$$\langle x^n \rangle_c = \sum_{i=1}^N \langle x_i^{**n} \rangle_c$$