

EX3502

Degree Examination in EX3502 Separation Processes 1

9th May 2025 Time: 14:00 – 17:00

PLEASE NOTE THE FOLLOWING

- (i) You **must not** have in your possession any material other than that expressly permitted in the rules appropriate to this examination. Where this is permitted, such material **must not** be amended, annotated or modified in any way.
- (ii) You **must not** have in your possession any material that could be determined as giving you an advantage in the examination.
- (iii) You **must not** attempt to communicate with any candidate during the exam, either orally or by passing written material, or by showing material to another candidate, nor must you attempt to view another candidate's work.
- (iv) You **must not** take to your examination desk any electronic devices such as mobile phones or other "smart" devices. The only exception to this rule is an approved calculator.

FURTHER REQUIREMENTS SPECIFIC TO THE SCHOOL OF ENGINEERING

- a) Candidates **ARE** permitted to use only an approved calculator.
- b) Candidates **ARE NOT** permitted to use the Engineering Mathematics Examinations Handbook.
- c) Candidates **ARE NOT** permitted to use GREEN or RED pen in their exam booklet.
- d) Data sheets are attached to the paper.
- e) All question papers must be submitted with the exam booklet.

Candidates must attempt **ALL** questions.

Question 1**Evaporator**

A mixture of water and benzoic acid needs to be concentrated from $x_F = 15.0$ wt% to $x_L = 80.0$ wt%. A single stage evaporator is proposed to achieve this as benzoic acid can be approximated as a non-volatile solute in water. The feed temperature is 20 °C and preliminary calculations suggest the most economical evaporator operating pressure is 0.2 bar absolute. You can assume all streams have the thermodynamic properties of water/steam and use the attached steam tables in the datasheet where required.

- a) A liquid flowrate of $L = 394.0 \text{ kg hr}^{-1}$ is desired, what is the required feed flowrate F and vapour flowrate V in kg hr^{-1} ? **[5 marks]**
- b) Calculate the duty of the evaporator in kW. You must assume the Boiling Point Rise (BPR) is given by the following equation:

$$\text{BPR}(\text{°C}) = 15.2x^2 + 8.2x \quad (1)$$

where x is the weight fraction of "solids" in the stream. **[12 marks]**

- c) If saturated steam is available at 30 bara to power the process, what is the steam economy? **[5 marks]**

[Question total: 22 marks]

Question 2**Absorber**

Cream from a dairy must have a odorous taint removed using steam. The cream has a concentration of 0.1 mol% and this must be reduced to below 0.018 mol% to prevent consumer complaints. A stripping column that can process 200.0 mol/s of cream is needed, and the Henrys constant for the system is 80.0 mol%/mol%.

- a) What is the minimum flowrate of steam capable of achieving the desired outlet concentration in mol/s? **[5 marks]**
- b) If a vapour flowrate of 4.0 mol/s is used, how many stages are required? The VLE data is given in Fig. 1 (pg. 11) and you should include this in your solution booklet. **[12 marks]**
- c) Packing is available for the absorber which has a height equivalent to a theoretical stage of 0.5 m/stage. Calculate the height of packing required. Discuss what additional height/space is required around the bed and how the diameter of the column is designed (i.e. what are the key considerations in selecting the diameter). **[5 marks]**

[Question total: 22 marks]

Question 3**Multi-stage distillation with Murphree efficiencies**

A paint factory is purifying a mixture of 40 mol% pentane and 60 mol% hexane. Distillation is to be used and the bottoms product must reach 20 mol% pentane while the top product must be 10 mol% hexane. The feed is preheated so that upon entry equal molar amounts of vapour and liquid are produced. Three VLE diagrams have been provided in Figs. 2, 3, and 4 (pgs. 12, 13, 14) which you should use and include in your solution booklet.

- a) What is the minimum reflux ratio required for this separation? You must submit your graphical construction with your solution booklet. **[6 marks]**
- b) If the reflux ratio is $R = 3.8$, how many theoretical stages are required to carry out the distillation? You must submit your graphical construction with your solution booklet. **[6 marks]**
- c) Assuming a Murphree tray efficiency of 50% what is the real number of trays in the column? You should assume a partial reboiler is fitted. You must submit your graphical construction with your solution booklet. **[10 marks]**

[Question total: 22 marks]

Question 4**Ponchon-Savarit Distillation**

As part of the disposal of old fire-extinguishers, a mixture of carbon-tetrachloride and toluene requires purification before further treatment. The mixture has a concentration of 50.0 mol% CCl_4 and must be purified to 80.0 mol% in the top product while the bottoms product must reach a purity of 20.0 mol% before further processing. You must design a distillation column for this operation.

A VLE chart has been provided in Fig. 5 (pg. 15), while a H - x - y chart is available in Fig. 6 (pg. 16) which you should use and include in your solution booklet.

- a) Under what circumstances does the Ponchon-Savarit method provide a better estimate of the number of theoretical stages required for a given distillation application, when compared to the McCabe-Thiele method? **[4 marks]**
- b) What is the minimum number of stages required to carry out this separation? You must submit your graphical construction with your solution booklet. **[4 marks]**
- c) Assuming that a reflux ratio of 2.4 is used, and the feed has an enthalpy of $h_F = 20000\text{kJ kmol}^{-1}$ use the Ponchon-Savarit method to determine how many ideal stages are required to carry out the separation. You must submit your graphical construction with your solution booklet **[10 marks]**

- d) The column has an overall tray efficiency of 80%. Assuming the column has a thermosyphon (total) reboiler, what is the real number of trays in the column? If you could not solve the previous question please use an estimate of 5 ideal stages.

[4 marks]

[Question total: 22 marks]

END OF PAPER

DATASHEET

Conversion from Celsius to Fahrenheit:

$$^{\circ}F = ^{\circ}C \times 1.8 + 32$$

Operating lines:

$$y_n = x_{n+1} \frac{R}{R+1} + \frac{x_D}{R+1} \quad \text{Enrichment line} \quad (2)$$

$$y_m = x_{m+1} \frac{L_m}{V_m} - x_W \frac{W}{V_m} \quad \text{Stripping line} \quad (3)$$

$$y = x \frac{q}{q-1} - \frac{x_F}{q-1} \quad q\text{-line} \quad (4)$$

$$\frac{y_{A,n+1}}{1 - y_{A,n+1}} = \frac{L'}{V'} \frac{x_{A,n}}{1 - x_{A,n}} + \frac{y_{A,1}}{1 - y_{A,1}} - \frac{L'}{V'} \frac{x_{A,0}}{1 - x_{A,0}} \quad \text{Absorption} \quad (5)$$

Relative volatility

$$y_A = \frac{\alpha x_A}{1 + (\alpha - 1)x_A} \quad (6)$$

Rayleigh's equation

$$\ln \left(\frac{L_{final}}{L_{initial}} \right) = \int_{x_{initial}}^{x_{final}} \frac{dx}{y - x} \quad (7)$$

If the relative volatility is constant:

$$\ln \left(\frac{L_{final}}{L_{initial}} \right) = (\alpha - 1)^{-1} \ln \left(\frac{x_{final}(1 - x_{initial})}{x_{initial}(1 - x_{final})} \right) + \ln \left(\frac{1 - x_{initial}}{1 - x_{final}} \right) \quad (8)$$

Quadratic equation:

$$ax^2 + bx + c = 0 \quad x = \frac{-b \pm \sqrt{b^2 - 4ac}}{2a} \quad (9)$$

Ponchon-Savarit equations:

$$P_C = (R + 1)(h_V(x = x_D) - h_L(x = x_D)) + h_L(x = x_D) \quad (10)$$

Table 1: Thermodynamic properties of saturated steam by temperature, calculated using the NASA CEA database and the vapour pressure data of Wexler or Wagner and Pruss (1990). The reference state is the triple point of saturated liquid water.

| T (°C) | P (bar) | $C_{p,l}$ (kJ kg $^{-1}$ K $^{-1}$) | $C_{p,v}$ (kJ kg $^{-1}$ K $^{-1}$) | h_l (kJ kg $^{-1}$) | h_{lv} (kJ kg $^{-1}$) | h_v (kJ kg $^{-1}$) | s_l (kJ kg $^{-1}$ K $^{-1}$) | s_v (kJ kg $^{-1}$ K $^{-1}$) |
|-------------|--------------|--|--|------------------------------|---------------------------------|------------------------------|--|--|
| 0.01 | 0.00612 | 4.22 | 1.888 | 0.000611 | 82501.0 | 2501.0 | - 6.161e- 08 | 9.155 |
| 1 | 0.00657 | 4.216 | 1.889 | 4.177 | 2499.0 | 2503.0 | 0.01526 | 9.129 |
| 2 | 0.00706 | 4.213 | 1.89 | 8.392 | 2496.0 | 2505.0 | 0.03061 | 9.103 |
| 3 | 0.00758 | 4.21 | 1.89 | 12.6 | 2494.0 | 2506.0 | 0.04589 | 9.076 |
| 4 | 0.00814 | 4.208 | 1.891 | 16.81 | 2491.0 | 2508.0 | 0.0611 | 9.051 |
| 5 | 0.00873 | 4.205 | 1.892 | 21.02 | 2489.0 | 2510.0 | 0.07625 | 9.025 |
| 6 | 0.00935 | 4.203 | 1.892 | 25.22 | 2487.0 | 2512.0 | 0.09134 | 8.999 |
| 7 | 0.01 | 4.201 | 1.893 | 29.43 | 2484.0 | 2514.0 | 0.1064 | 8.974 |
| 8 | 0.0107 | 4.199 | 1.894 | 33.63 | 2482.0 | 2516.0 | 0.1213 | 8.949 |
| 9 | 0.0115 | 4.197 | 1.895 | 37.82 | 2480.0 | 2517.0 | 0.1362 | 8.924 |
| 10 | 0.0123 | 4.196 | 1.896 | 42.02 | 2477.0 | 2519.0 | 0.1511 | 8.9 |
| 12 | 0.014 | 4.193 | 1.898 | 50.41 | 2472.0 | 2523.0 | 0.1806 | 8.851 |
| 14 | 0.016 | 4.191 | 1.899 | 58.79 | 2468.0 | 2527.0 | 0.2099 | 8.804 |
| 16 | 0.0182 | 4.188 | 1.901 | 67.17 | 2463.0 | 2530.0 | 0.239 | 8.757 |
| 18 | 0.0206 | 4.187 | 1.904 | 75.55 | 2458.0 | 2534.0 | 0.2678 | 8.711 |
| 20 | 0.0234 | 4.185 | 1.906 | 83.92 | 2454.0 | 2537.0 | 0.2965 | 8.666 |
| 25 | 0.0317 | 4.182 | 1.912 | 104.8 | 2442.0 | 2547.0 | 0.3673 | 8.557 |
| 30 | 0.0425 | 4.18 | 1.918 | 125.7 | 2430.0 | 2556.0 | 0.4368 | 8.452 |
| 35 | 0.0563 | 4.179 | 1.925 | 146.6 | 2418.0 | 2565.0 | 0.5052 | 8.352 |
| 40 | 0.0738 | 4.179 | 1.932 | 167.5 | 2406.0 | 2574.0 | 0.5724 | 8.256 |
| 45 | 0.0959 | 4.179 | 1.94 | 188.4 | 2394.0 | 2582.0 | 0.6386 | 8.163 |
| 50 | 0.124 | 4.18 | 1.948 | 209.3 | 2382.0 | 2591.0 | 0.7038 | 8.075 |
| 55 | 0.158 | 4.181 | 1.957 | 230.2 | 2370.0 | 2600.0 | 0.768 | 7.99 |
| 60 | 0.199 | 4.183 | 1.966 | 251.2 | 2358.0 | 2609.0 | 0.8312 | 7.908 |
| 65 | 0.25 | 4.185 | 1.976 | 272.1 | 2345.0 | 2618.0 | 0.8935 | 7.83 |
| 70 | 0.312 | 4.188 | 1.987 | 293.0 | 2333.0 | 2626.0 | 0.955 | 7.754 |
| 75 | 0.386 | 4.192 | 1.999 | 314.0 | 2321.0 | 2635.0 | 1.016 | 7.681 |
| 80 | 0.474 | 4.196 | 2.012 | 334.9 | 2308.0 | 2643.0 | 1.075 | 7.611 |
| 85 | 0.579 | 4.2 | 2.026 | 355.9 | 2295.0 | 2651.0 | 1.134 | 7.543 |
| 90 | 0.702 | 4.205 | 2.042 | 377.0 | 2283.0 | 2660.0 | 1.193 | 7.478 |
| 95 | 0.846 | 4.211 | 2.059 | 398.0 | 2270.0 | 2668.0 | 1.25 | 7.415 |
| 100 | 1.01 | 4.217 | 2.077 | 419.1 | 2256.0 | 2676.0 | 1.307 | 7.354 |
| 110 | 1.43 | 4.23 | 2.121 | 461.4 | 2230.0 | 2691.0 | 1.419 | 7.238 |
| 120 | 1.99 | 4.246 | 2.174 | 503.8 | 2202.0 | 2706.0 | 1.528 | 7.129 |
| 130 | 2.7 | 4.265 | 2.237 | 546.4 | 2174.0 | 2720.0 | 1.635 | 7.026 |
| 140 | 3.62 | 4.286 | 2.311 | 589.2 | 2144.0 | 2733.0 | 1.739 | 6.929 |

Table 2 continued: Thermodynamic properties of saturated steam by temperature.

| T (°C) | P (bar) | $C_{p,I}$ (kJ kg ⁻¹ K ⁻¹) | $C_{p,V}$ (kJ kg ⁻¹ K ⁻¹) | h_I (kJ kg ⁻¹) | h_{IV} (kJ kg ⁻¹) | h_V (kJ kg ⁻¹) | s_I (kJ kg ⁻¹ K ⁻¹) | s_V (kJ kg ⁻¹ K ⁻¹) |
|-------------|--------------|--|--|------------------------------------|---------------------------------------|------------------------------------|--|--|
| 150 | 4.76 | 4.31 | 2.396 | 632.3 | 2114.0 | 2746.0 | 1.842 | 6.837 |
| 160 | 6.18 | 4.338 | 2.492 | 675.6 | 2082.0 | 2757.0 | 1.943 | 6.749 |
| 170 | 7.92 | 4.369 | 2.599 | 719.2 | 2049.0 | 2768.0 | 2.042 | 6.665 |
| 180 | 10.0 | 4.406 | 2.716 | 763.2 | 2014.0 | 2777.0 | 2.14 | 6.584 |
| 190 | 12.6 | 4.447 | 2.846 | 807.6 | 1978.0 | 2785.0 | 2.236 | 6.506 |
| 200 | 15.5 | 4.494 | 2.99 | 852.4 | 1940.0 | 2792.0 | 2.331 | 6.43 |
| 250 | 39.8 | 4.865 | 4.012 | 1086.0 | 1715.0 | 2801.0 | 2.793 | 6.072 |
| 300 | 85.9 | 5.752 | 6.223 | 1345.0 | 1405.0 | 2750.0 | 3.255 | 5.706 |

Table 2: Thermodynamic properties of saturated steam by pressure, calculated using the NASA CEA database and the vapour pressure data of Wexler or Wagner and Pruss (1990). The reference state is the triple point of saturated liquid water.

| P (bar) | T (°C) | $C_{p,I}$ (kJ kg ⁻¹ K ⁻¹) | $C_{p,V}$ (kJ kg ⁻¹ K ⁻¹) | h_I (kJ kg ⁻¹) | h_{IV} (kJ kg ⁻¹) | h_V (kJ kg ⁻¹) | s_I (kJ kg ⁻¹ K ⁻¹) | s_V (kJ kg ⁻¹ K ⁻¹) |
|--------------|-------------|--|--|------------------------------------|---------------------------------------|------------------------------------|--|--|
| 0.01 | 6.97 | 4.201 | 1.893 | 29.3 | 2484.0 | 2514.0 | 0.1059 | 8.975 |
| 0.015 | 13.0 | 4.192 | 1.898 | 54.69 | 2470.0 | 2525.0 | 0.1956 | 8.827 |
| 0.02 | 17.5 | 4.187 | 1.903 | 73.43 | 2459.0 | 2533.0 | 0.2606 | 8.723 |
| 0.025 | 21.1 | 4.184 | 1.907 | 88.43 | 2451.0 | 2539.0 | 0.3119 | 8.642 |
| 0.03 | 24.1 | 4.183 | 1.91 | 101.0 | 2444.0 | 2545.0 | 0.3543 | 8.577 |
| 0.035 | 26.7 | 4.181 | 1.914 | 111.8 | 2438.0 | 2550.0 | 0.3907 | 8.521 |
| 0.04 | 29.0 | 4.181 | 1.917 | 121.4 | 2432.0 | 2554.0 | 0.4224 | 8.473 |
| 0.045 | 31.0 | 4.18 | 1.919 | 130.0 | 2427.0 | 2557.0 | 0.4507 | 8.431 |
| 0.05 | 32.9 | 4.18 | 1.922 | 137.8 | 2423.0 | 2561.0 | 0.4763 | 8.394 |
| 0.055 | 34.6 | 4.179 | 1.924 | 144.9 | 2419.0 | 2564.0 | 0.4995 | 8.36 |
| 0.06 | 36.2 | 4.179 | 1.927 | 151.5 | 2415.0 | 2567.0 | 0.5209 | 8.329 |
| 0.065 | 37.6 | 4.179 | 1.929 | 157.6 | 2412.0 | 2569.0 | 0.5407 | 8.301 |
| 0.07 | 39.0 | 4.179 | 1.931 | 163.4 | 2408.0 | 2572.0 | 0.5591 | 8.275 |
| 0.075 | 40.3 | 4.179 | 1.933 | 168.8 | 2405.0 | 2574.0 | 0.5763 | 8.25 |
| 0.08 | 41.5 | 4.179 | 1.935 | 173.9 | 2402.0 | 2576.0 | 0.5925 | 8.227 |
| 0.085 | 42.7 | 4.179 | 1.936 | 178.7 | 2400.0 | 2578.0 | 0.6078 | 8.206 |
| 0.09 | 43.8 | 4.179 | 1.938 | 183.3 | 2397.0 | 2580.0 | 0.6223 | 8.186 |
| 0.095 | 44.8 | 4.179 | 1.94 | 187.6 | 2394.0 | 2582.0 | 0.6361 | 8.167 |
| 0.12 | 49.4 | 4.18 | 1.947 | 206.9 | 2383.0 | 2590.0 | 0.6963 | 8.085 |
| 0.14 | 52.5 | 4.18 | 1.953 | 220.0 | 2376.0 | 2596.0 | 0.7366 | 8.031 |
| 0.16 | 55.3 | 4.181 | 1.958 | 231.6 | 2369.0 | 2601.0 | 0.772 | 7.985 |
| 0.18 | 57.8 | 4.182 | 1.962 | 241.9 | 2363.0 | 2605.0 | 0.8035 | 7.944 |
| 0.2 | 60.1 | 4.183 | 1.966 | 251.4 | 2358.0 | 2609.0 | 0.832 | 7.907 |
| 0.22 | 62.1 | 4.184 | 1.971 | 260.1 | 2352.0 | 2613.0 | 0.8579 | 7.874 |

Table 2 continued: Thermodynamic properties of saturated steam by pressure.

| P (bar) | T (°C) | $C_{p,I}$ (kJ kg ⁻¹ K ⁻¹) | $C_{p,v}$ (kJ kg ⁻¹ K ⁻¹) | h_I (kJ kg ⁻¹) | h_{lv} (kJ kg ⁻¹) | h_v (kJ kg ⁻¹) | s_I (kJ kg ⁻¹ K ⁻¹) | s_v (kJ kg ⁻¹ K ⁻¹) |
|--------------|-------------|--|--|------------------------------------|---------------------------------------|------------------------------------|--|--|
| 0.24 | 64.1 | 4.185 | 1.974 | 268.1 | 2348.0 | 2616.0 | 0.8818 | 7.844 |
| 0.26 | 65.8 | 4.186 | 1.978 | 275.6 | 2343.0 | 2619.0 | 0.904 | 7.817 |
| 0.28 | 67.5 | 4.187 | 1.982 | 282.6 | 2339.0 | 2622.0 | 0.9246 | 7.791 |
| 0.3 | 69.1 | 4.188 | 1.985 | 289.2 | 2335.0 | 2625.0 | 0.9439 | 7.767 |
| 0.32 | 70.6 | 4.189 | 1.989 | 295.5 | 2332.0 | 2627.0 | 0.9621 | 7.745 |
| 0.34 | 72.0 | 4.19 | 1.992 | 301.4 | 2328.0 | 2630.0 | 0.9793 | 7.725 |
| 0.36 | 73.3 | 4.19 | 1.995 | 307.0 | 2325.0 | 2632.0 | 0.9956 | 7.705 |
| 0.38 | 74.6 | 4.191 | 1.998 | 312.4 | 2322.0 | 2634.0 | 1.011 | 7.686 |
| 0.4 | 75.9 | 4.192 | 2.001 | 317.6 | 2318.0 | 2636.0 | 1.026 | 7.669 |
| 0.42 | 77.0 | 4.193 | 2.004 | 322.5 | 2316.0 | 2638.0 | 1.04 | 7.652 |
| 0.44 | 78.2 | 4.194 | 2.007 | 327.2 | 2313.0 | 2640.0 | 1.054 | 7.636 |
| 0.46 | 79.3 | 4.195 | 2.01 | 331.8 | 2310.0 | 2642.0 | 1.067 | 7.621 |
| 0.48 | 80.3 | 4.196 | 2.013 | 336.2 | 2307.0 | 2644.0 | 1.079 | 7.607 |
| 0.5 | 81.3 | 4.197 | 2.016 | 340.5 | 2305.0 | 2645.0 | 1.091 | 7.593 |
| 0.55 | 83.7 | 4.199 | 2.022 | 350.5 | 2299.0 | 2649.0 | 1.119 | 7.561 |
| 0.6 | 85.9 | 4.201 | 2.029 | 359.8 | 2293.0 | 2653.0 | 1.145 | 7.531 |
| 0.65 | 88.0 | 4.203 | 2.035 | 368.5 | 2288.0 | 2656.0 | 1.169 | 7.504 |
| 0.7 | 89.9 | 4.205 | 2.041 | 376.7 | 2283.0 | 2659.0 | 1.192 | 7.479 |
| 0.75 | 91.8 | 4.207 | 2.047 | 384.4 | 2278.0 | 2662.0 | 1.213 | 7.456 |
| 0.8 | 93.5 | 4.209 | 2.053 | 391.6 | 2274.0 | 2665.0 | 1.233 | 7.434 |
| 0.85 | 95.1 | 4.211 | 2.059 | 398.5 | 2269.0 | 2668.0 | 1.252 | 7.413 |
| 0.9 | 96.7 | 4.213 | 2.065 | 405.1 | 2265.0 | 2670.0 | 1.269 | 7.394 |
| 0.95 | 98.2 | 4.214 | 2.07 | 411.4 | 2261.0 | 2673.0 | 1.286 | 7.376 |
| 1 | 99.6 | 4.216 | 2.076 | 417.4 | 2258.0 | 2675.0 | 1.303 | 7.359 |
| 1.1 | 102.0 | 4.22 | 2.087 | 428.8 | 2250.0 | 2679.0 | 1.333 | 7.327 |
| 1.2 | 105.0 | 4.223 | 2.097 | 439.3 | 2244.0 | 2683.0 | 1.361 | 7.298 |
| 1.3 | 107.0 | 4.226 | 2.108 | 449.1 | 2238.0 | 2687.0 | 1.387 | 7.271 |
| 1.4 | 109.0 | 4.229 | 2.118 | 458.4 | 2232.0 | 2690.0 | 1.411 | 7.246 |
| 1.5 | 111.0 | 4.232 | 2.128 | 467.1 | 2226.0 | 2693.0 | 1.434 | 7.223 |
| 1.6 | 113.0 | 4.235 | 2.138 | 475.3 | 2221.0 | 2696.0 | 1.455 | 7.201 |
| 1.7 | 115.0 | 4.238 | 2.147 | 483.2 | 2216.0 | 2699.0 | 1.475 | 7.181 |
| 1.8 | 117.0 | 4.241 | 2.157 | 490.7 | 2211.0 | 2701.0 | 1.494 | 7.162 |
| 1.9 | 119.0 | 4.244 | 2.166 | 497.8 | 2206.0 | 2704.0 | 1.513 | 7.144 |
| 2 | 120.0 | 4.247 | 2.175 | 504.7 | 2202.0 | 2706.0 | 1.53 | 7.127 |
| 2.5 | 127.0 | 4.26 | 2.22 | 535.4 | 2181.0 | 2717.0 | 1.607 | 7.052 |
| 3 | 134.0 | 4.272 | 2.262 | 561.5 | 2163.0 | 2725.0 | 1.672 | 6.992 |
| 3.5 | 139.0 | 4.283 | 2.302 | 584.3 | 2148.0 | 2732.0 | 1.727 | 6.94 |
| 4 | 144.0 | 4.294 | 2.34 | 604.7 | 2133.0 | 2738.0 | 1.777 | 6.895 |
| 4.5 | 148.0 | 4.305 | 2.377 | 623.2 | 2120.0 | 2743.0 | 1.821 | 6.856 |
| 5 | 152.0 | 4.315 | 2.413 | 640.2 | 2108.0 | 2748.0 | 1.861 | 6.821 |

Table 2 continued: Thermodynamic properties of saturated steam by pressure.

| P (bar) | T (°C) | $C_{p,I}$ (kJ kg ⁻¹ K ⁻¹) | $C_{p,v}$ (kJ kg ⁻¹ K ⁻¹) | h_I (kJ kg ⁻¹) | h_{lv} (kJ kg ⁻¹) | h_v (kJ kg ⁻¹) | s_I (kJ kg ⁻¹ K ⁻¹) | s_v (kJ kg ⁻¹ K ⁻¹) |
|--------------|-------------|--|--|------------------------------------|---------------------------------------|------------------------------------|--|--|
| 6 | 159.0 | 4.335 | 2.48 | 670.5 | 2086.0 | 2756.0 | 1.931 | 6.759 |
| 7 | 165.0 | 4.353 | 2.543 | 697.1 | 2066.0 | 2763.0 | 1.992 | 6.707 |
| 8 | 170.0 | 4.371 | 2.603 | 721.0 | 2047.0 | 2768.0 | 2.046 | 6.662 |
| 9 | 175.0 | 4.388 | 2.66 | 742.7 | 2030.0 | 2773.0 | 2.094 | 6.621 |
| 10 | 180.0 | 4.405 | 2.715 | 762.7 | 2014.0 | 2777.0 | 2.138 | 6.585 |
| 15 | 198.0 | 4.485 | 2.964 | 844.7 | 1946.0 | 2791.0 | 2.315 | 6.443 |
| 20 | 212.0 | 4.562 | 3.19 | 908.6 | 1890.0 | 2798.0 | 2.447 | 6.339 |
| 25 | 224.0 | 4.638 | 3.404 | 962.0 | 1840.0 | 2802.0 | 2.554 | 6.256 |
| 30 | 234.0 | 4.714 | 3.612 | 1008.0 | 1795.0 | 2803.0 | 2.646 | 6.186 |
| 35 | 243.0 | 4.791 | 3.817 | 1050.0 | 1753.0 | 2803.0 | 2.725 | 6.125 |
| 40 | 250.0 | 4.869 | 4.022 | 1087.0 | 1713.0 | 2801.0 | 2.797 | 6.07 |
| 45 | 257.0 | 4.949 | 4.228 | 1122.0 | 1676.0 | 2798.0 | 2.861 | 6.02 |
| 50 | 264.0 | 5.032 | 4.438 | 1155.0 | 1640.0 | 2794.0 | 2.921 | 5.974 |
| 60 | 276.0 | 5.208 | 4.877 | 1214.0 | 1571.0 | 2785.0 | 3.027 | 5.89 |
| 70 | 286.0 | 5.4 | 5.354 | 1267.0 | 1505.0 | 2773.0 | 3.122 | 5.815 |
| 80 | 295.0 | 5.614 | 5.883 | 1317.0 | 1442.0 | 2759.0 | 3.208 | 5.745 |
| 90 | 303.0 | 5.854 | 6.476 | 1364.0 | 1379.0 | 2743.0 | 3.287 | 5.679 |
| 100 | 311.0 | 6.127 | 7.147 | 1408.0 | 1318.0 | 2725.0 | 3.36 | 5.616 |
| 120 | 325.0 | 6.813 | 8.819 | 1491.0 | 1194.0 | 2686.0 | 3.496 | 5.494 |

Data sheet handout.

Submit this graph as part of your solution book.

Student ID:

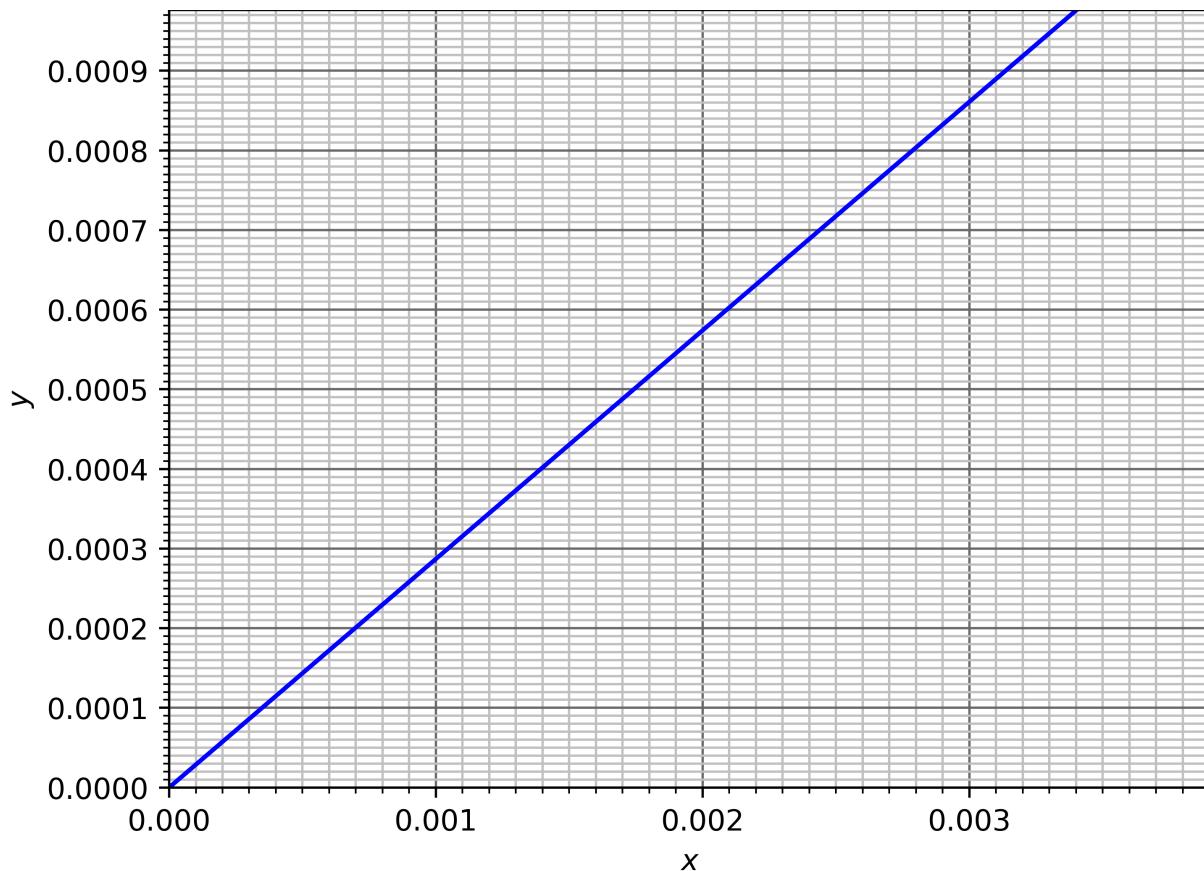


Figure 1: A blank VLE chart for use in Q. 2

Data sheet handout.
Submit this graph as part of your solution book.

Student ID:

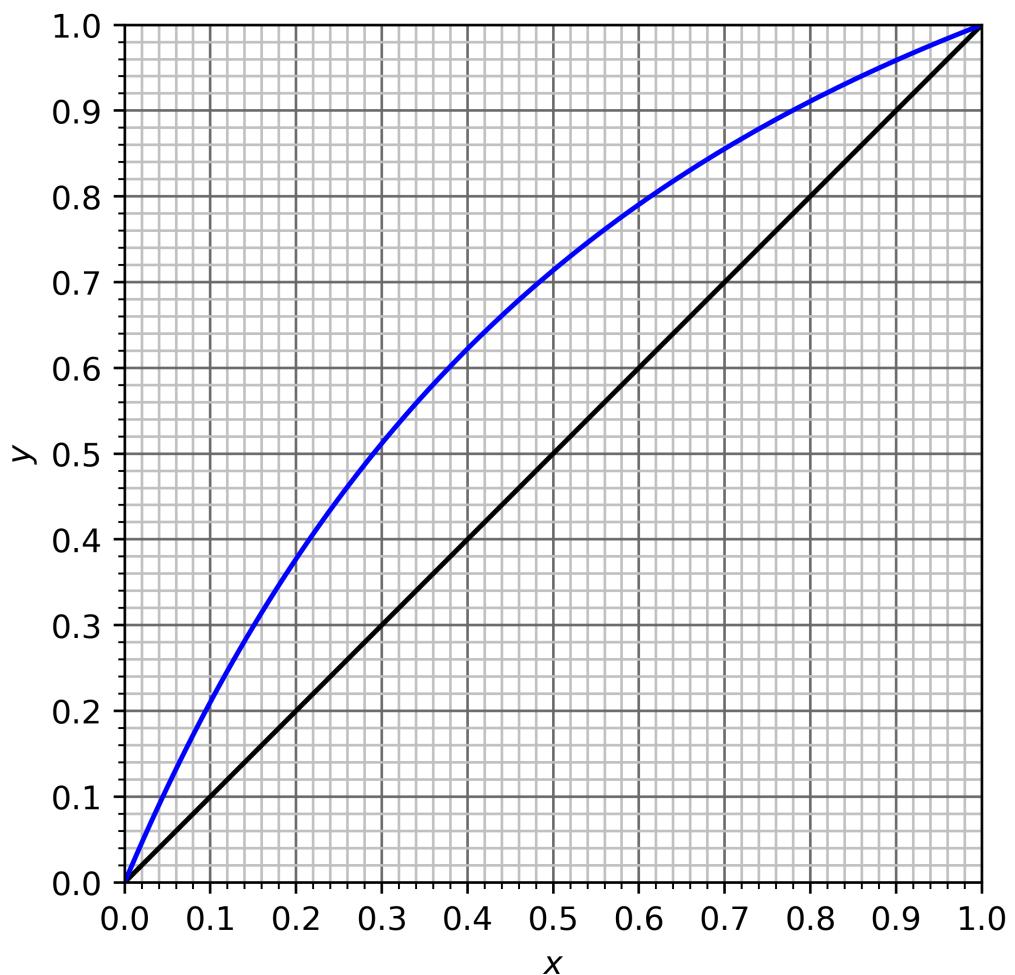


Figure 2: VLE data for the benzene-toluene system. For use in Q. 3

Data sheet handout.
Submit this graph as part of your solution book.

Student ID:

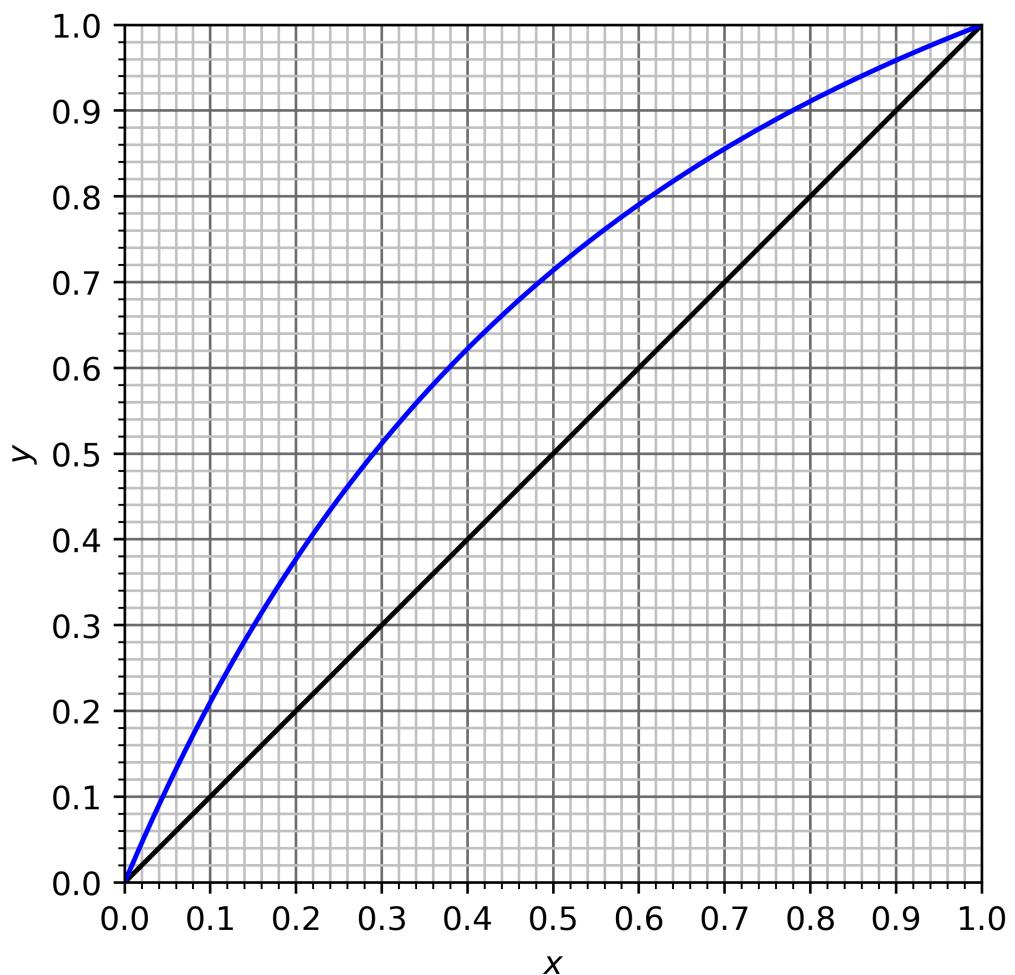


Figure 3: VLE data for the benzene-toluene system. For use in Q. 3

Data sheet handout.
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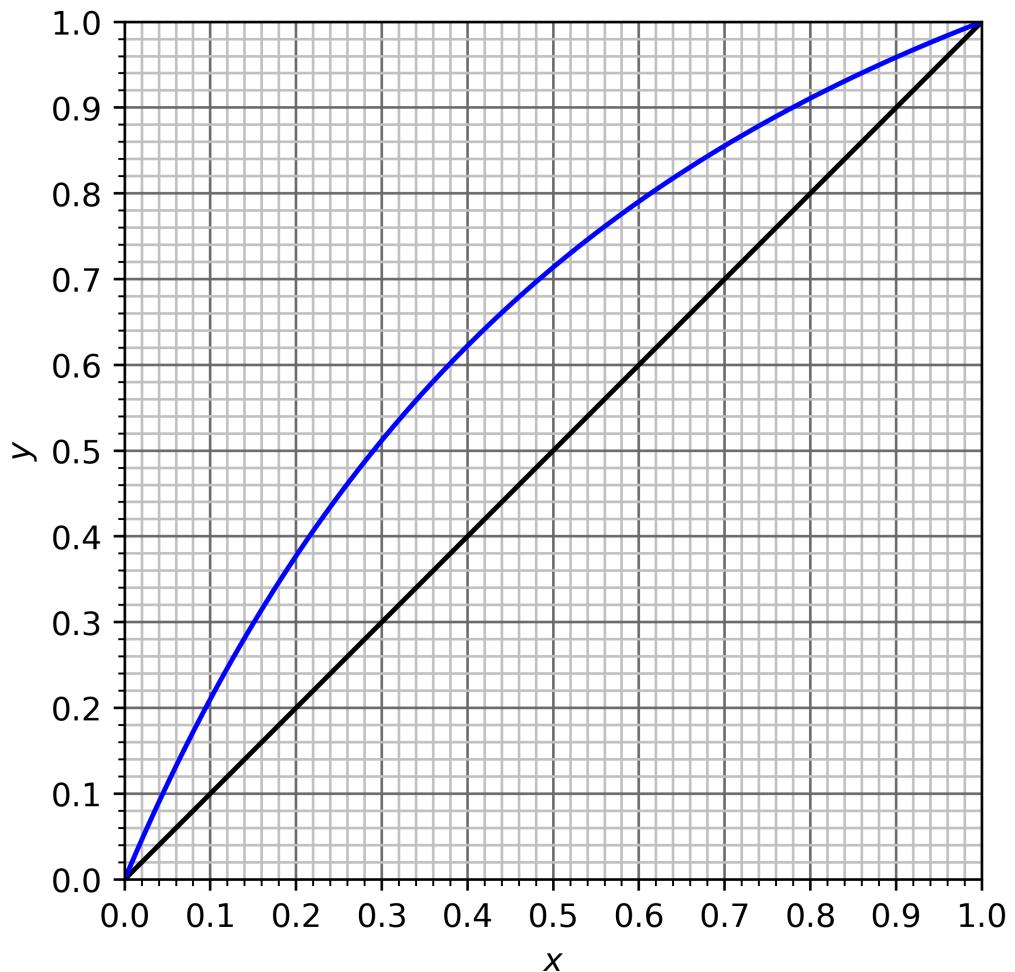


Figure 4: VLE data for the benzene-toluene system. For use in Q. 3

Data sheet handout.
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Student ID:

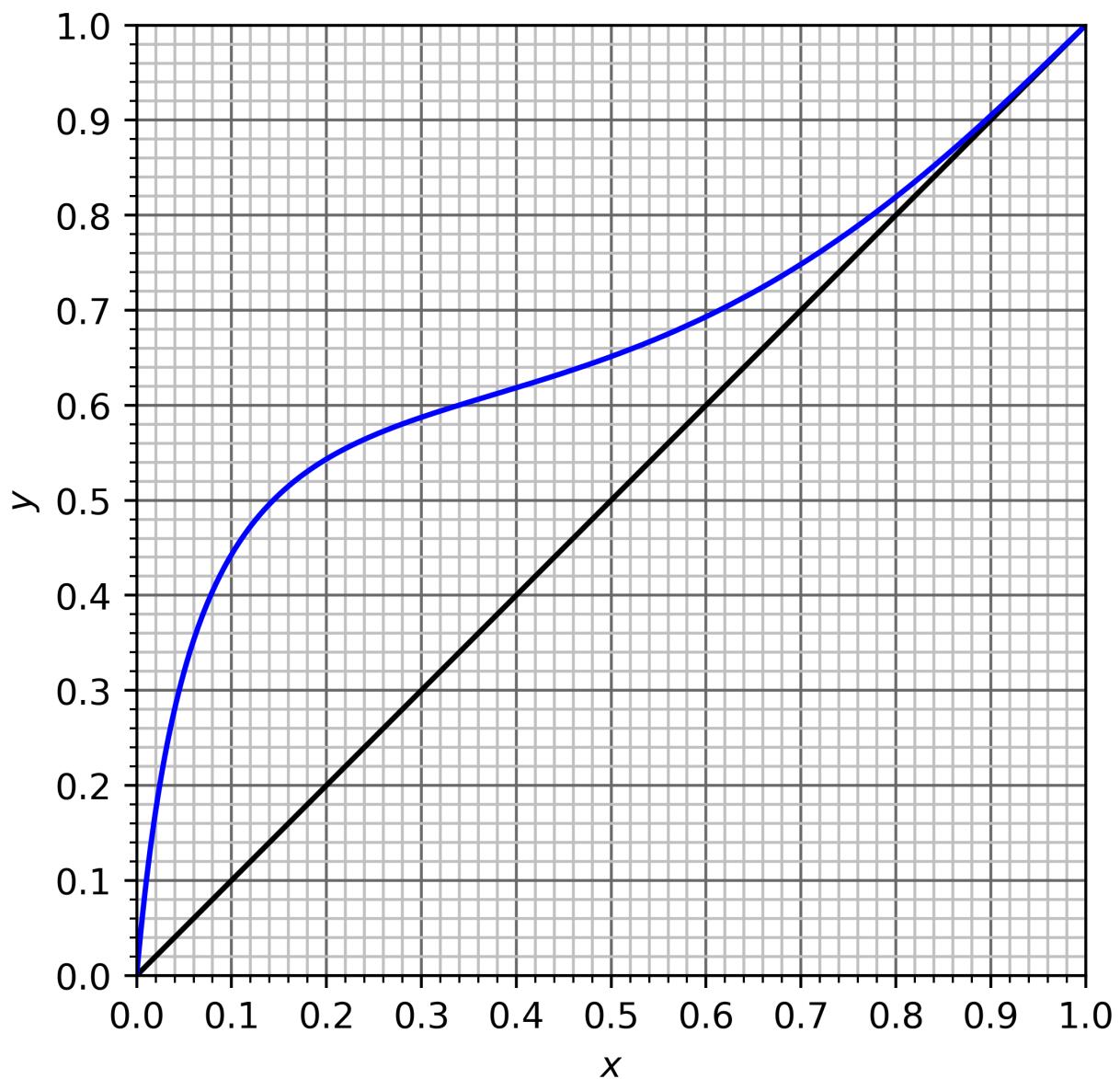


Figure 5: VLE data for the carbon-tetrachloride/toluene system. For use in Q. 4

Data sheet handout.

Submit this graph as part of your solution book.

Student ID:

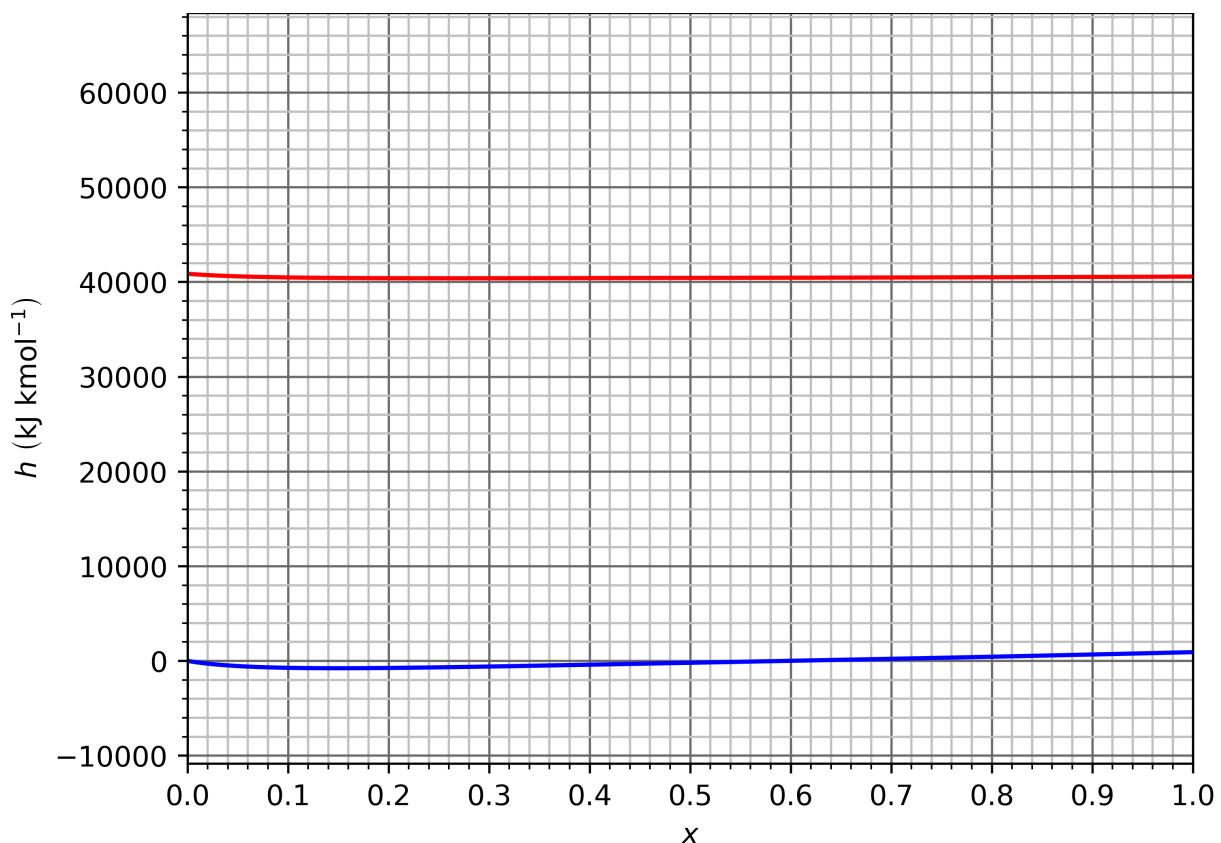


Figure 6: H - x - y data for the carbon-tetrachloride/toluene water system. For use in Q. 4