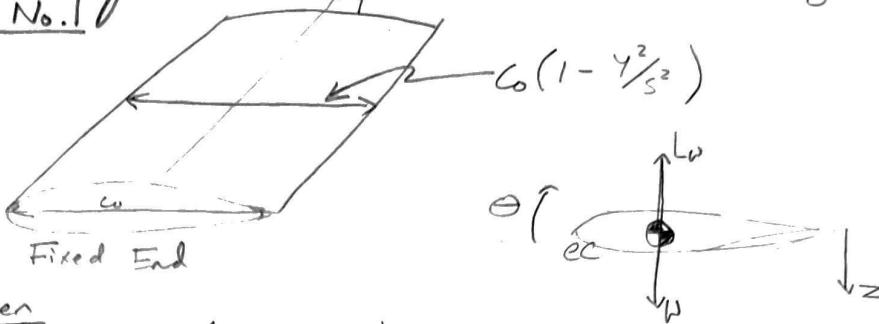


Problem No. 1


Given

$$c(y) = c_0(1 - y^2/s^2)$$

$$\zeta J(y) = (\zeta J)_0 (1 - y^2/s^2)$$

$$dL = q c(y) a_w (x_0 + \theta(y))$$

All forces act at AC

AC : CG same location

AC distance \$e\$ from SC

- a)  $\theta(y) = y/s \theta_T \Rightarrow$  Solve for lift distribution and divergence speed  
Need to solve for trim  $\theta$  using energy methods.

$$U = 2 \left( \frac{1}{2} \int_0^s \zeta J(y) \left( \frac{2\theta}{2y} \right)^2 dy \right) \quad \theta = x_0 + \theta_T y/s$$

$$U = \int_0^s (\zeta J)_0 (1 - y^2/s^2) (\theta_T/s)^2 dy$$

$$\int_0^s (\zeta J)_0 \left( [\theta_T/s]^2 - [\theta_T/s]^2 (y/s)^2 \right) dy$$

$$U = (\zeta J)_0 \left( (\theta_T/s)^2 y - (\theta_T/s)^2 \left(\frac{1}{3}\right) y^3/s^2 \right) \Big|_0^s$$

$$U = (\zeta J)_0 (\theta_T)^2 \left(\frac{2}{3}\right) \left(\frac{1}{s}\right)$$

$$\delta W = \omega \delta z + 2 dL \cdot (ec \delta \theta - \delta z)$$

$$= \omega \delta z + 2 \int_0^s q c_0 a_w (1 - y^2/s^2) (x_0 + \theta_T y/s) (ec \delta \theta - \delta z) dy$$

$$\delta W = \omega \delta z + 2 \int_0^s q c_0 a_w (1 - y^2/s^2) (x_0 + \theta_T y/s) ec \frac{(1 - y^2/s^2)}{s} \delta \theta dy$$

$$\begin{aligned} & x_0 + \theta_T y/s - y^2/s^2 x_0 - \theta_T y^3/s^3 \rightarrow x_0 s + \frac{1}{2} \theta_T s - \frac{1}{3} x_0 s - \frac{1}{4} \theta_T s \\ & \left( \frac{1}{2} - \frac{1}{4} x_0 \right) \rightarrow y/s x_0 - y^3/s^3 x_0 + y^2/s^2 \theta_T - y^4/s^4 \theta_T - y^3/s^3 x_0 \\ & \quad + y^5/s^5 x_0 \\ & \rightarrow \frac{1}{2} x_0 s - \frac{1}{4} x_0 s + \frac{5}{3} \theta_T s - \frac{3}{5} \theta_T s - \frac{1}{4} x_0 s + \frac{1}{6} x_0 s \end{aligned}$$

$$\delta W = \omega \delta z + 2 q c_0^2 e a_w s \left( \frac{1}{6} x_0 + \frac{2}{15} \theta_T \right) \delta \theta$$

$$- 2 q c_0 a_w s \left( \frac{2}{3} x_0 + \frac{1}{4} \theta_T \right) \delta z$$

$$Q_z = \frac{2(8W)}{2(8z)} = \omega - 2g c_0 \omega \text{aws} \left( \frac{2}{3} \kappa_0 + \frac{1}{4} \theta_T \right)$$

$$Q_{\theta_T} = \frac{2(8W)}{2(8\theta_T)} = 2g c_0^2 e \text{aws} \left( \frac{1}{6} \kappa_0 + \frac{2}{15} \theta_T \right)$$

Lagrange  ~~$\frac{d}{dt} \frac{\partial T}{\partial \dot{\theta}_T}$~~   ~~$- \frac{\partial T}{\partial \theta_T}$~~   ~~$+ \frac{\partial T}{\partial \theta_T}$~~   ~~$+ \frac{\partial U}{\partial \theta_T}$~~  =  $\frac{2(8W)}{2(8\theta_T)}$

$$\frac{d}{dt} \frac{\partial T}{\partial \dot{z}} - \frac{\partial T}{\partial z} + \frac{\partial U}{\partial z} = \frac{2(8W)}{2(8z)}$$

$$\frac{\partial U}{\partial \theta_T} = \frac{4}{3} (\text{GJ})_0 \frac{1}{s} \theta_T$$

$$\frac{4}{3} (\text{GJ})_0 \frac{1}{s} \theta_T + 2g c_0^2 e \text{aws} \left( \frac{1}{6} \kappa_0 + \frac{2}{15} \theta_T \right) = 0$$

$$2g c_0 \omega \text{aws} \left( \frac{2}{3} \kappa_0 + \frac{1}{4} \theta_T \right) = \omega$$

$$\begin{bmatrix} \frac{1}{3} g c_0^2 e \text{aws} & \frac{4}{3} (\text{GJ})_0 \frac{1}{s} + \frac{4}{15} g c_0^2 e \text{aws} \\ \frac{4}{3} g c_0 \omega \text{aws} & \frac{1}{2} g c_0 \omega \text{aws} \end{bmatrix} \begin{bmatrix} \kappa_0 \\ \theta_T \end{bmatrix} = \begin{bmatrix} 0 \\ \omega \end{bmatrix}$$

$$\frac{1}{3} g c_0^2 e \text{aws} \left( \frac{1}{2} g c_0 \omega \text{aws} \right) - \frac{4}{3} g c_0 \omega \text{aws} \left( \frac{4}{3} (\text{GJ})_0 \frac{1}{s} + \frac{4}{15} g c_0^2 e \text{aws} \right)$$

$$\det = \frac{1}{6} g^2 c_0^3 \omega^2 e s^2 - \frac{16}{9} (\text{GJ})_0 g c_0 \omega + \frac{16}{45} g^2 c_0^3 \omega^2 e s^2$$

$$\begin{bmatrix} \kappa_0 \\ \theta_T \end{bmatrix} = \frac{1}{\det} \begin{bmatrix} \frac{1}{2} g c_0 \omega \text{aws} & -\frac{4}{3} (\text{GJ})_0 \frac{1}{s} - \frac{4}{15} g c_0^2 e \text{aws} \\ -\frac{4}{3} g c_0 \omega \text{aws} & \frac{1}{3} g c_0^2 e \text{aws} \end{bmatrix} \begin{bmatrix} 0 \\ \omega \end{bmatrix}$$

$$\kappa_0 = \frac{[-\frac{4}{3} (\text{GJ})_0 \frac{1}{s} - \frac{4}{15} g c_0^2 e \text{aws}] \omega}{\frac{1}{6} g^2 c_0^3 \omega^2 e s^2 - \frac{16}{9} (\text{GJ})_0 g c_0 \omega + \frac{16}{45} g^2 c_0^3 \omega^2 e s^2}$$

$$\theta_T = \frac{\frac{1}{3} g c_0^2 e \text{aws} \omega}{\frac{1}{6} g^2 c_0^3 \omega^2 e s^2 - \frac{16}{9} (\text{GJ})_0 g c_0 \omega + \frac{16}{45} g^2 c_0^3 \omega^2 e s^2}$$

$$dL = q C(y) \alpha_w X(y) dy$$

$$\frac{dL}{dy} = q C_0 (1 - y^2/s^2) (X_0 + \frac{1}{s} \theta_T) \alpha_w$$

$$(-\frac{4}{3}(GJ)_0 \cdot \frac{1}{s} - \frac{4}{15} q C_0^2 e \alpha_w s + \frac{1}{3} q C_0^2 e \alpha_w y) W$$

$$\frac{dL}{dy} = \frac{q C_0 \alpha_w (1 - y^2/s^2) (-\frac{4}{3}(GJ)_0 \cdot \frac{1}{s} - \frac{4}{15} q C_0^2 e \alpha_w s + \frac{1}{3} q C_0^2 e \alpha_w y) W}{\frac{1}{6} q^2 C_0^3 \alpha_w^2 e s^2 - \frac{16}{9}(GJ)_0 q C_0 \alpha_w + \frac{16}{15} q^2 C_0^2 \alpha_w^2 e s^2}$$

Solve for divergent speed while trimmed:

Look at  $X_0$  denominator.

$$0 = \cancel{\frac{7.5}{s^2} q^2 C_0^2 \alpha_w f^2} - \cancel{\frac{16/9(GJ)_0 q X_0 \alpha_w}{s^2 e C_0^2 \alpha_w}} + \cancel{\frac{16/15 q^2 C_0^2 \alpha_w f^2}{s^2 e C_0^2 \alpha_w}}$$

$$23.5 q^2 - \frac{80(GJ)_0}{s^2 e C_0^2 \alpha_w} q = 0$$

$$q = 0$$

$$q_A = \frac{3.4(GJ)_0}{s^2 e C_0^2 \alpha_w}$$

$$\cancel{\frac{1}{\rho} V_A^2} = \frac{3.4(GJ)_0}{s^2 e C_0^2 \alpha_w \rho} (2)$$

$$V_A = \sqrt{\frac{6.8(GJ)_0}{s^2 e C_0^2 \alpha_w \rho}}$$

$$b) \theta(y) = y/s \theta_1 + y^2/s^2 \theta_2$$

Solve for  $U$

$$U = \mathcal{Z}(1/s) \int_0^s GJ(y) \left( \frac{2\theta}{2y} \right)^2 dy$$

$$\frac{2\theta}{2y} \rightarrow \frac{\theta_1}{s} + 2 \frac{y}{s^2} \theta_2$$

$$U = \int_0^s GJ \cdot \left( 1 - \frac{y^2}{s^2} \right) \left( \frac{\theta_1}{s} + 2 \frac{y}{s^2} \theta_2 \right)^2 dy$$

$$\left( 1 - \frac{y^2}{s^2} \right) \left( \frac{\theta_1^2}{s^2} + 4 \frac{y}{s^3} \theta_1 \theta_2 + \cancel{2 \frac{y^2}{s^3} \theta_1 \theta_2} + 4 \frac{y^2}{s^4} \theta_2^2 \right)$$

$$\int_0^s \left( \frac{\theta_1^2}{s^2} + 4 \frac{y}{s^3} \theta_1 \theta_2 + 4 \frac{y^2}{s^4} \theta_2^2 - \frac{y^2}{s^4} \theta_1^2 - 4 \frac{y^3}{s^5} \theta_1 \theta_2 - 4 \frac{y^4}{s^6} \theta_2^2 \right) dy$$

$$\frac{\theta_1^2}{s} + \frac{2}{s} \theta_1 \theta_2 + \cancel{\frac{4}{3} \frac{\theta_2^2}{s}} - \cancel{\frac{1}{3} \frac{\theta_1^2}{s}} - \frac{1}{s} \theta_1 \theta_2 - \cancel{\frac{4}{3} \frac{\theta_2^2}{s}}$$

$$U = (GJ) \cdot (1/s) \left( \frac{2}{3} \theta_1^2 + \frac{8}{15} \theta_2^2 + \theta_1 \theta_2 \right)$$

$$\delta W = \omega \delta z + 2dL \cdot (\epsilon_c \delta \theta - \delta z)$$

$$\int_0^s q \mathcal{Z}(y) \omega \times (y) dy$$

$$\delta \theta \rightarrow y/s \delta \theta_1 + y^2/s^2 \delta \theta_2$$

$$-2 \int_0^s q c_0 \left( 1 - \frac{y^2}{s^2} \right) \omega \left( \kappa_0 + \frac{y}{s} \theta_1 + \frac{y^2}{s^2} \theta_2 \right) \delta z$$

$$+ 2 \int_0^s q c_0 \left( 1 - \frac{y^2}{s^2} \right) \omega \left( \kappa_0 + \frac{y}{s} \theta_1 + \frac{y^2}{s^2} \theta_2 \right) (\epsilon c_0) \left( 1 - \frac{y^2}{s^2} \right) \left( \frac{y}{s} \delta \theta_1 + \frac{y^2}{s^2} \delta \theta_2 \right)$$

$$----- \\ \left( 1 - \frac{y^2}{s^2} \right) \left( \kappa_0 + \frac{y}{s} \theta_1 + \frac{y^2}{s^2} \theta_2 \right)$$

$$\textcircled{1} \quad \kappa_0 + \frac{y}{s} \theta_1 + \frac{y^2}{s^2} \theta_2 - \frac{y^2}{s^2} \kappa_0 - \frac{y^3}{s^3} \theta_1 - \frac{y^4}{s^4} \theta_2$$

$$\textcircled{2} \quad \left( \frac{y}{s} - \frac{y^3}{s^3} \right) \left( \right) \rightarrow \kappa_0 \frac{y}{s} + \frac{y^2}{s^2} \theta_1 + \frac{y^3}{s^3} \theta_2 - \frac{y^3}{s^3} \kappa_0 - \frac{y^4}{s^4} \theta_1 - \frac{y^5}{s^5} \theta_2 \\ - \frac{y^3}{s^3} \kappa_0 - \frac{y^4}{s^4} \theta_1 - \frac{y^5}{s^5} \theta_2 + \frac{y^5}{s^5} \kappa_2 + \frac{y^6}{s^6} \theta_1 + \frac{y^7}{s^7} \theta_2$$

$$\textcircled{3} \quad \left( \frac{y^2}{s^2} - \frac{y^4}{s^4} \right) \left( \right) \rightarrow \kappa_0 \frac{y^2}{s^2} + \frac{y^3}{s^3} \theta_1 + \frac{y^4}{s^4} \theta_2 - \frac{y^4}{s^4} \kappa_0 - \frac{y^5}{s^5} \theta_1 - \frac{y^6}{s^6} \theta_2 \\ - \frac{y^4}{s^4} \kappa_0 - \frac{y^5}{s^5} \theta_1 - \frac{y^6}{s^6} \theta_2 + \frac{y^6}{s^6} \kappa_0 + \frac{y^7}{s^7} \theta_1 + \frac{y^8}{s^8} \theta_2$$

$$\textcircled{1} \rightarrow \int_0^s (\quad) dy$$

$$s(\frac{K_o s}{3} + \frac{1}{2}\theta_1 s + \frac{5}{3}\theta_2 s - \frac{1}{3}K_o s - \frac{1}{4}\theta_1 s - \frac{3}{5}\theta_2 s)$$

$$\textcircled{2} \rightarrow \int_0^s (\quad) dy \quad \frac{F}{3} - \frac{\theta_1}{5} + \frac{1}{7} \rightarrow -\frac{1}{15} + \frac{1}{7.5} \rightarrow \frac{2}{35}$$

$$s(\frac{1}{2}K_o + \frac{1}{3}\theta_1 + \frac{1}{4}\theta_2 - \frac{1}{3}K_o - \cancel{\frac{1}{4}\theta_1} - \frac{1}{2}\theta_2 - \frac{1}{4}K_o - \cancel{\frac{1}{5}\theta_1} - \frac{1}{6}\theta_2$$

$$s(\frac{1}{6}K_o + \frac{1}{35}\theta_1 + \frac{1}{24}\theta_2) \quad \frac{2}{2.4} - \frac{1}{3} + \frac{1}{8} \rightarrow \frac{3.3}{8} - \frac{1.8}{3}$$

$$\textcircled{3} \rightarrow \int_0^s (\quad) dy \quad \frac{1.7}{5.7} - \frac{2.5}{7.5} + \frac{1}{9} \rightarrow -\frac{3}{35} + \frac{1}{9} \rightarrow -\frac{27}{315} + \frac{35}{315}$$

$$s(\frac{1}{3}K_o + \frac{1}{4}\theta_1 + \frac{1}{5}\theta_2 - \frac{1}{5}K_o - \cancel{\frac{1}{6}\theta_1} - \frac{1}{7}\theta_2 - \cancel{\frac{1}{5}K_o} - \cancel{\frac{1}{6}\theta_1}$$

$$s(\frac{2}{35}K_o + \frac{1}{24}\theta_1 + \frac{8}{315}\theta_2)$$

Put it all together:

$$\delta W = \omega \delta z + q c_o^2 e a w s (\frac{1}{3}K_o + \frac{4}{35}\theta_1 + \frac{1}{12}\theta_2) \delta \theta_1$$

$$+ q c_o^2 e a w s (\frac{4}{35}K_o + \frac{1}{12}\theta_1 + \frac{16}{315}\theta_2) \delta \theta_2$$

$$- q c_o a w s (\frac{4}{35}K_o + \frac{1}{12}\theta_1 + \frac{4}{15}\theta_2) \delta z$$

$$Q_z = \frac{2(\delta W)}{2(\delta z)} = \omega - q c_o a w s \left( \frac{1}{3}K_o + \frac{1}{2}\theta_1 + \frac{4}{15}\theta_2 \right)$$

$$Q_{\theta_1} = \frac{2(\delta W)}{2(\delta \theta_1)} = q c_o^2 e a w s \left( \frac{1}{3}K_o + \frac{4}{35}\theta_1 + \frac{1}{12}\theta_2 \right)$$

$$Q_{\theta_2} = \frac{2(\delta W)}{2(\delta \theta_2)} = q c_o^2 e a w s \left( \frac{4}{35}K_o + \frac{1}{12}\theta_1 + \frac{16}{315}\theta_2 \right)$$

Lagrange  $\overset{\text{Eq}}{\rightarrow}$ : (generically)

$$\frac{d}{dt} \frac{\partial T}{\partial \dot{q}} - \frac{\partial T}{\partial q} + \frac{\partial U}{\partial q} = \frac{\partial (\delta W)}{\partial \dot{q}}$$

$$\frac{\partial (\delta W)}{\partial \dot{q}} = \frac{\partial U}{\partial q}$$

$$\frac{\partial U}{\partial z} = 0$$

$$\frac{\partial U}{\partial \theta_1} = (45)_o \frac{1}{5} \left[ \left( \frac{4}{3} \right) \theta_1 + \theta_2 \right]$$

$$\frac{\partial U}{\partial \theta_2} = (45)_o \frac{1}{5} \left[ \left( \frac{16}{15} \right) \theta_2 + \theta_1 \right]$$

Put together:

$$q_{coaws} \left( \frac{4}{3}K_0 + \frac{1}{2}\Theta_1 + \frac{4}{15}\Theta_2 \right) = \omega$$

$$q_{c^2eaws} \left( \frac{1}{3}K_0 + \frac{4}{35}\Theta_1 + \frac{1}{12}\Theta_2 \right) = (GJ)_0 \cdot \frac{1}{s} \left( \frac{4}{3}\Theta_1 + \Theta_2 \right)$$

$$q_{c^2eaws} \left( \frac{4}{35}K_0 + \frac{1}{12}\Theta_1 + \frac{16}{15}\Theta_2 \right) = (GJ)_0 \cdot \frac{1}{s} \left( \frac{16}{15}\Theta_2 + \Theta_1 \right)$$

$$\begin{bmatrix} \frac{4}{3}q_{coaws} & \frac{1}{2}q_{coaws} & \frac{4}{15}q_{coaws} \\ \frac{1}{3}q_{c^2eaws} & \frac{4}{35}q_{c^2eaws} - (GJ)_0 \cdot \frac{4}{3}s & \frac{1}{12}q_{c^2eaws} - (GJ)_0 \cdot \frac{1}{s} \\ \frac{4}{35}q_{c^2eaws} & \frac{1}{12}q_{c^2eaws} - (GJ)_0 \cdot \frac{1}{s} & \frac{16}{15}q_{c^2eaws} - (GJ)_0 \cdot \frac{16}{15}s \end{bmatrix} \begin{bmatrix} K_0 \\ \Theta_1 \\ \Theta_2 \end{bmatrix} = \begin{bmatrix} \omega \\ 0 \\ 0 \end{bmatrix}$$

↳ This would be a hard matrix to inverse so...  
call the matrix, P.

$$\begin{bmatrix} K_0 \\ \Theta_1 \\ \Theta_2 \end{bmatrix} = P^{-1} \begin{bmatrix} \omega \\ 0 \\ 0 \end{bmatrix}$$

$$\frac{dL}{dy} = q_{coaws} \left( 1 - \frac{4^2}{s^2} \right) \begin{bmatrix} 1 & \frac{4}{s} & \frac{4^2}{s^2} \end{bmatrix} \begin{bmatrix} K_0 \\ \Theta_1 \\ \Theta_2 \end{bmatrix}$$

I used Matlab to solve  $\frac{dL}{dy}$  and  $V_A$ .

There would be no way for me to do these calculations by hand without mistakes.

$R = C_{oaws}$  ↳ To simplify matrix

$$M = (GJ)_0$$

See attachment for calculations...

$$\frac{dL}{dy} = \frac{-(15W)(s^2 - y^2)(-223440M^2s + 12152MRcgs^2 - 127680MRcgsy + 95760MRcgsy^2 + 603R^2c^2g^2s^2 + 3920R^2c^2g^2s^2y - 7788R^2c^2g^2s^2y^2)}{4s^4(1117200M^2 + 82880MRcgs - 2577R^2c^2g^2s^2)}$$

$$V_A = \sqrt{\frac{280M(\sqrt{23450S} + 296)}{2577Rcgs}}$$

$$R = C_0 \alpha_w s$$

$$M = (GJ)_0$$

## Hw #2 - Aeroelasticity - ME597/AAE556

Victoria Nagorski - 9/19/22

### Contents

- Problem 1b

#### Problem 1b

```
syms q R c M s W y rho

% Solve for lift
P = [4/3*q*R 1/2*q*R 4/15*q*R;
      1/3*R*c*q (4/35*q*c*R-4/3*M/s) (1/12*q*c*R-M/s);
      4/35*q*c*R (1/12*q*c*R-M/s) (16/315*q*c*R-16/15*M/s)];
theta = P^-1 * [W;0;0]

dL_dy = q * R/s * (1 - y^2/s^2) * [1 y/s y^2/s^2]*theta

% Solve for V_d
alpha0 = theta(1);
[~,D] = numden(alpha0)
q = simplify(solve(D,q))

q_A = q(2)
V_A = sqrt(2/rho * q_A)

theta =
-(15*W*(- 223440*M^2 + 12152*M*R*c*q*s + 603*R^2*c^2*q^2*s^2))/(4*(1117200*M^2*R*q + 82880*M*R^2*c*q^2*s - 2577*R^3*c^2*q^3*s^2))
-(2100*W*s*(- 7*R*q*s*c^2 + 228*M*c))/(1117200*M^2 + 82880*M*R*c*q*s - 2577*R^2*c^2*q^2*s^2)
-(45*W*s*(- 649*R*q*s*c^2 + 7980*M*c))/(1117200*M^2 + 82880*M*R*c*q*s - 2577*R^2*c^2*q^2*s^2)

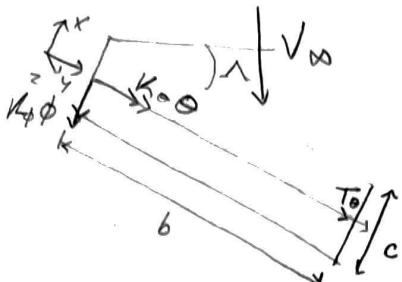
dL_dy =
(15*R*W*q*(y^2/s^2 - 1)*(- 223440*M^2 + 12152*M*R*c*q*s + 603*R^2*c^2*q^2*s^2))/(4*s*(1117200*M^2*R*q + 82880*M*R^2*c*q^2*s - 2577*R^3*c^2*q^3*s^2)) - (2100*R*W*q*y
468800*M^2*R*q + 331520*M*R^2*c*q^2*s - 10308*R^3*c^2*q^3*s^2

D =
q =
(140*M*(234505^(1/2) + 296))/(2577*R*c*s)
-(140*M*(234505^(1/2) - 296))/(2577*R*c*s)

q_A =
(140*M*(234505^(1/2) + 296))/(2577*R*c*s)

V_A =
((280*M*(234505^(1/2) + 296))/(2577*R*c*rho*s))^(1/2)
```

## Problem No. 2



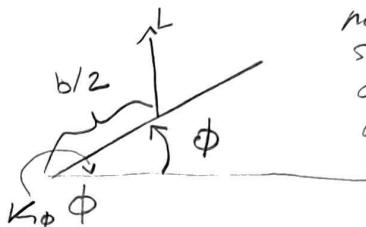
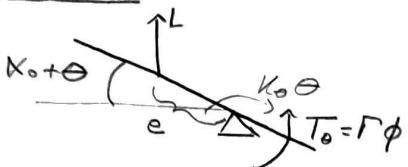
$\phi \rightarrow$  bending slope  
 $T_0 = r\phi$

Has a  $K_0$ .

\* Note: Drawing

on problem statement  
is wrong... prof  
no respond on intent  
so I solved based  
on problem statement  
wording

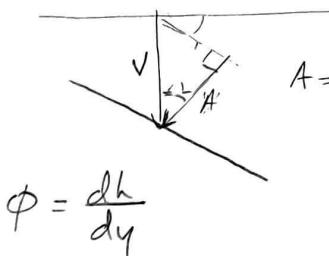
FBDs



a) Derive static equilibrium eq using energy.

$$U = \frac{1}{2} K_\phi \phi^2 + \frac{1}{2} K_\theta \theta^2$$

Need to derive angles for  $\Lambda, \bar{\Lambda}$ :



$$\Lambda = \cos^{-1} V_n$$

$$z = h(\bar{y}) - \bar{x} \theta(\bar{y})$$

$$\begin{bmatrix} \bar{y} \\ \bar{x} \end{bmatrix} = \begin{bmatrix} C_\Lambda & S_\Lambda \\ -S_\Lambda & C_\Lambda \end{bmatrix} \begin{bmatrix} y \\ x \end{bmatrix}$$

$$K_s = - \left. \frac{dz}{dx} \right|_{\bar{x}} = \frac{V_h}{V} \rightarrow V_n = -V \left[ \frac{dz}{dx} \frac{d\bar{x}}{dx} + \frac{dz}{d\bar{y}} \frac{d\bar{y}}{dx} \right]$$

$$\begin{aligned} \bar{y} &= C_\Lambda y + S_\Lambda x \\ \bar{x} &= -S_\Lambda y + C_\Lambda x \end{aligned}$$

$$\begin{aligned} \frac{d\bar{y}}{dx} / \frac{d\bar{x}}{dx} &\rightarrow \sin \Lambda \\ \frac{d\bar{y}}{dx} / \frac{d\bar{x}}{dx} &\rightarrow \cos \Lambda \quad \frac{dz}{d\bar{x}} / \frac{d\bar{x}}{dx} \rightarrow -\theta(\bar{y}) \\ \frac{dz}{d\bar{y}} / \frac{d\bar{x}}{dx} &\rightarrow h'(\bar{y}) \end{aligned}$$

$$K_s = \frac{V_h}{V} = \theta(\bar{y}) \cos \Lambda - h'(\bar{y}) \sin \Lambda$$

$$\frac{V_h}{V \cos \Lambda} \Rightarrow \frac{K_o}{\cos \Lambda} + \Theta - \phi \tan \Lambda$$

$$X_c = \frac{X_0}{\cos \Lambda} + \theta - \phi \tan \Lambda$$

Two different sources produce work  
 $\rightarrow$  Lift  
 $\rightarrow$  Tension

We have the following equation:

$$\frac{\partial U}{\partial \phi} \delta \phi + \frac{\partial U}{\partial \theta} \delta \theta = \delta W$$

Solve for  $\delta W$ :

$$L = g_n S C_{Lx} X_c$$

$$\delta W = (L \cdot \frac{b}{2}) \delta \phi + (L \cdot e + T \phi) \delta \theta$$

$$\frac{\partial U}{\partial \phi} \rightarrow K_\phi \phi$$

$$\frac{\partial U}{\partial \theta} \rightarrow K_\theta \theta$$

We now have 2 equations if we break up by  $\delta \phi$  and  $\delta \theta$

$$(L \cdot \frac{b}{2}) = K_\phi \phi$$

$$(L \cdot e + T \phi) = K_\theta \theta$$

$$g_n S C_{Lx} \left( \frac{b}{2} \right) \left( \frac{X_0}{\cos \Lambda} + \theta - \phi \tan \Lambda \right) = K_\phi \phi$$

$$(a) \quad K_\phi \phi + g_n S C_{Lx} \left( \frac{b}{2} \right) \tan \Lambda \phi - g_n S C_{Lx} \left( \frac{b}{2} \right) \theta = g_n S C_{Lx} \left( \frac{b}{2} \right) \frac{X_0}{\cos \Lambda}$$

$$g_n S C_{Lx} e \left( \frac{X_0}{\cos \Lambda} + \theta - \phi \tan \Lambda \right) + T \phi = K_\theta \theta$$

$$(b) \quad K_\theta \theta - g_n S C_{Lx} e \theta + g_n S C_{Lx} e \tan \Lambda \phi - T \phi = g_n S C_{Lx} e \frac{X_0}{\cos \Lambda}$$

Write into Matrix form:

$$[\theta \quad \phi]^T$$

$-\frac{g_n S C_{Lx} (b/2)}{K_\phi}$	$K_\phi + g_n S C_{Lx} (b/2) \tan \Lambda$
$\frac{g_n S C_{Lx} e}{K_\theta}$	$g_n S C_{Lx} e \tan \Lambda - T$

$$\begin{bmatrix} \theta \\ \phi \end{bmatrix} = g_n S C_{Lx} \frac{X_0}{\cos \Lambda} \begin{bmatrix} b/2 \\ e \end{bmatrix}$$

b) Derive characteristic eq. Solve for divergent dynamic pressure

$$\begin{aligned} & \left[ -q_n SC_{Lx}(b/2) \frac{K_\phi + q_n SC_{Lx}(b/2) \tan \Lambda}{K_\theta - q_n SC_{Lx} e} \right] \\ & - q_n SC_{Lx}(b/2) (q_n SC_{Lx} e \tan \Lambda - \Gamma) \\ & - (K_\theta - q_n SC_{Lx} e) (K_\phi + q_n SC_{Lx}(b/2) \tan \Lambda) = 0 \\ & - (q_n SC_{Lx})^2 \frac{(b/2)^2}{e} \tan \Lambda + q_n SC_{Lx}(b/2) \Gamma - K_\theta K_\phi \\ & - K_\theta q_n SC_{Lx}(b/2) \tan \Lambda + (q_n SC_{Lx})^2 \frac{(b/2)^2}{e} \tan \Lambda \\ & + K_\phi q_n SC_{Lx}(e) = 0 \end{aligned}$$

$q_n SC_{Lx}(b/2) \Gamma - K_\theta K_\phi - K_\theta q_n SC_{Lx}(b/2) \tan \Lambda + K_\phi q_n SC_{Lx}(e) = 0$

Solve for  $q_n$ :

$$q_n SC_{Lx} e \left( \frac{\Gamma b}{2e} - K_\theta \frac{b}{2e} \tan \Lambda + K_\phi \right) = K_\theta K_\phi$$

$$q_n = \frac{K_\theta K_\phi}{SC_{Lx} e} \left( \frac{\Gamma}{K_\phi} \frac{b}{2e} - \frac{K_\theta}{K_\phi} \frac{b}{2e} \tan \Lambda + 1 \right)$$

$q_n = \frac{K_\theta}{SC_{Lx} e} \left( \frac{\Gamma}{K_\phi} \frac{b}{2e} - \frac{K_\theta}{K_\phi} \frac{b}{2e} \tan \Lambda + 1 \right)$

c) Critical value of gain  $\Gamma$  above which wing divergence cannot occur

When  $q_d < 0$ , then divergence won't occur because then airspeed is an imaginary number

$$\frac{K\theta}{S C_{L\infty} e} \left( \frac{\Gamma}{K\phi} \frac{b}{2e} - \frac{K\theta}{K\phi} \frac{b}{2e} \tan \Lambda + 1 \right) < 0 - 1 \\ + \frac{K\theta}{K\phi} \frac{b}{2e} \tan \Lambda$$

$$\frac{\Gamma}{K\phi} \frac{b}{2e} < \left( \frac{K\theta}{K\phi} \frac{b}{2e} \tan \Lambda - 1 \right) \frac{2e}{b} K\phi$$

$$\boxed{\Gamma < K\theta \tan \Lambda - \frac{2e}{b} K\phi}$$