

# 1 Qualitative GSA measures for functions with correlated input parameters

Saltelli et al. (2008)

Lemaire (2013)

Smith (2014)

## 1.1 Qualitative General Sensitivity Analysis

Qualitative Global Sensitivity Analysis (Qualitative GSA) deals with computing measures that can rank random input parameters in terms of their importance on the function output and the variability thereof. If the measures for some input parameters are negligibly small, these parameters can be fixed so that the number of random input parameters decreases for a subsequent quantitative GSA. This pre-selection step is called Factor Fixing. The quantitative GSA then aims to determine the precise effect size of each random input parameter on the function output. The most common measures in quantitative GSA are the so-called Sobol' sensitivity indices. Equation 1 shows the first order index. It is the share of the variance in the function output induced by exclusively one single input parameter  $X_i$  of the variance induced by all random input parameters  $X_1, X_2, \dots, X_k$ .

$$S_i = \frac{\text{Var}_i[Y|X_i]}{\text{Var}[Y]} \quad (1)$$

Equation 2 shows the total order index. This measure is equal to the first order index except of that its numerator includes the variance in the function output that is induced by changes in the other input parameters  $X_{\sim i}$ , caused by interactions with the variation in  $X_i$ .

$$S_i^T = \frac{\mathbb{E}_{\sim i}[\text{Var}_i[Y|\mathbf{X}_{\sim i}]]}{\text{Var}[Y]} \quad (2)$$

Computing these measures requires many function evaluations, even if an estimator is used as a shortcut. The more time-intense one function evaluation is, the more utility provides the aforementioned Factor Fixing based on qualitative measures. The most commonly used measures in qualitative GSA is the Elementary Effect (EE),  $\mu$ , the absolute Elementary Effects,  $\mu^*$ , and the standard deviation of the Elementary Effect,  $\sigma$ . The Elementary Effect is given by the mean of a number of function derivatives with respect to one input parameter. The "change in", or the "step of" the input parameter, denoted by  $\Delta$ , has not to be infinitesimally small. The only restriction is that  $X_i + \Delta$  is in the domain of  $X_i$ .

The derivation, also called the individual Elementary Effect, is denoted by

$$d^{(j)} = \frac{Y(\mathbf{X}_{\sim \mathbf{i}}^{(j)}, X_i^{(j)} + \Delta^{(i,j)})}{\Delta^{(i,j)}}, \quad (3)$$

where  $j$  is an index for the number of observations of  $X_i$ . Then, the Elementary Effect is given by

$$\mu = \frac{1}{r} \sum_{j=1}^r d^{(j)}. \quad (4)$$

The absolute Elementary Effects,  $\mu^*$  is used to prevent observations of opposite sign to cancel each other out.

$$\mu^* = \frac{1}{r} \sum_{j=1}^r |d^{(j)}|. \quad (5)$$

In Equation 4 and 5,  $r$  is the number of parameter draws with index  $j$ . Step  $\Delta^{(j)}$  may or may not vary depending on the sample design that is used to draw the input parameters. These measures (together) are used to proxy the total Sobol' indices that contains the parameter-specific interactions with all other parameter in Equation(2). The total Sobol' index is the relevant one because it also contains interactions that may be important. If the qualitative measures are close to 0 for one particular parameter, its variation can be rendered as irrelevant for the variation in the function output (given there are parameters with measures substantially different from 0).

## 1.2 Sampling Schemes

According to several experiments by Campolongo et al. (2011) using common test functions, the best design is the radial design (Saltelli (2002)) and the most commonly used is the trajectory design (Morris (1991)). Both designs are comprised by a  $(k+1) \times k$ -dimensional matrix. The elements are generated in  $[0, 1]$ . Afterwards, they can be transformed to the distributions of choice. The columns represent the input parameters and each row is a complete input parameter vector. To compute the qualitative measures, a set of multiple matrices, or subsets, of input parameters has to be generated.

A matrix in radial design is generated in the following way: Draw a vector of length  $2k$  from a quasi-random sequence. The first row, or parameter vector, is the first half of the sequence. Then, copy the first row to the remaining  $k$  rows. For each row  $k'$  of the remaining  $2, \dots, k+1$  rows, replace the  $k'$ -th element by the  $k'$ -th element of the second

half of the vector. This generates a matrix of the following form:

$$\mathbf{R}_{(k+1) \times k} = \begin{pmatrix} a_1 & a_2 & \dots & a_k \\ \mathbf{b}_1 & a_2 & \dots & a_k \\ a_1 & \mathbf{b}_2 & \dots & a_k \\ \vdots & \vdots & \vdots & \vdots \\ a_1 & a_2 & \dots & \mathbf{b}_k \end{pmatrix} \quad (6)$$

Note here, that each column consists only of the first row element, except of for one row. From this matrix, one individual EE can be obtained for each parameter  $X_i$ . This is achieved by using the  $(i + 1)$ -th row as function argument for the minuend and the first row as subtrahend in the formula for the individual EE. Then,  $\Delta^{(i,j)} = b_i^{(j)} - a_i^{(j)}$ . Tailored to the radial scheme, the derivation can be re-formulated as in Equation (3), where  $j$  is the number of radial subsamples and  $i$  represents the input parameter  $X_i$ .

$$d_i^{(j)} = \frac{Y(\mathbf{a}_{\sim i}^{(j)}, b_i^{(j)}) - Y(\mathbf{a})}{b_i^{(j)} - a_i^{(j)}} = \frac{Y(\mathbf{R}_{i+1,*}) - Y(\mathbf{R}_{1,*})}{b_i^{(j)} - a_i^{(j)}}. \quad (7)$$

If the number of radial subsamples is high, the quasi-random sequence lead to a good and fast coverage of the input space (compared to a random sequence). The quasi-random sequence considered here is the Sobol' sequence. This sequence is comparably succesful in covering the unit hypercube, but also conceptually more involved. Therefore, its presentation is beyond the scope of this work. Since this sequence is quasi-random, the sequence has to be drawn at once for all sets of radial matrices.

Next, I present the trajectory design. As we will see, it leads to a relatively representative coverage for a very small number of subsamples but also to frequent repetitions of similar draws. In this outline, I skip the equations that generate a trajectory and present the method verbally. There are different forms of trajectories. Here, I focus on the version presented in Morris (1991) that yields to equiprobable elements. The first step is to decide the number  $p$  of grid points in interval  $[0, 1]$ . Then, the first row of the trajectory is composed of the lower half value of these grid points. Now, fix  $\Delta = p/[2(p - 1)]$ . This function implies, that adding  $\Delta$  to the lowest point in the lowest half results in the lowest point of the upper half of the grid points, and so on. The rest of the rows is constructed by, first, copying the row one above and, second, by adding  $\Delta$  to the  $k$ -th element of the  $k + 1$ -th row. The implied matrix scheme is depicted below.

$$\mathbf{T}_{(k+1) \times k} = \begin{pmatrix} a_1 & a_2 & \dots & a_k \\ \mathbf{b}_1 & a_2 & \dots & a_k \\ \mathbf{b}_1 & \mathbf{b}_2 & \dots & a_k \\ \vdots & \vdots & \vdots & \vdots \\ \mathbf{b}_1 & \mathbf{b}_2 & \dots & \mathbf{b}_k \end{pmatrix} \quad (8)$$

In contrary to the radial scheme, each  $b_i$  is copied to the subsequent row. Therefore, the EEs have to be determined by comparing each row with the row above instead of with the first row. Importantly, two random transformations are common. These are randomly switching rows and randomly interchanging the  $i$ -th column with the  $(k-i)$ -th column and then reversing the column. The first transformation is skipped as it does not add additional coverage and because we need the stairs-shaped design to facilitate later transformations which account for correlation between input parameters. The second transformation is adapted because it is important to also have negative steps and because it does sustain the stairs shape. Yet, this implies that  $\Delta^{(i,j)}$  is also parameter- and trajectory-specific. Let  $f$  and  $h$  be additional indices representing the input parameters. The derivation formula is adapted to the trajectory design as follows:<sup>1</sup>

$$d_i^{(j)} = \frac{Y(\mathbf{b}_{\mathbf{f} \leq i}^{(j)}, \mathbf{a}_{\mathbf{h} > i}^{(j)}) - Y(\mathbf{b}_{\mathbf{f} < i}^{(j)}, \mathbf{a}_{\mathbf{h} \geq i}^{(j)})}{b_i^{(j)} - a_i^{(j)}} = \frac{Y(\mathbf{T}_{\mathbf{i}+1,*}) - Y(\mathbf{T}_{\mathbf{i},*})}{b_i^{(j)} - a_i^{(j)}}. \quad (9)$$

The trajectory design involves first, a fixed grid, and second and more importantly, a fixed step  $\Delta$ . s.t.  $\{\Delta\} = \{\pm\Delta\}$ . This implies less step variety and less space coverage vis-à-vis the radial design for more than a small number of draws.

So far, we have only considered draws in  $[0,1]$ . For uncorrelated input parameters from arbitrary distributions with well-defined cumulative distribution function,  $\Phi$ , one would simply evaluate each element (of course, potentially including the addition of the step) by the inverse cumulative distribution function,  $\Phi^{-1}$ , of the respective parameter. A bit of intuition is, that  $\Phi$  maps the sample space to  $[0,1]$ . Hence  $\Phi^{-1}$  can be used to transform random draws in  $[0,1]$  to the sample space of the arbitrary distribution. This is a basic example of so-called inverse transform sampling which we will recall in the next section.

### 1.3 The approach for correlated input parameters in Ge and Menendez (2017)

This section describes the incomplete approach by Ge and Menendez (2017) to extend the EE-based measures to input parameters that are correlated. Their main achievement is to outline a transformation of samples in radial and trajectory design that incorporates the correlation between the input parameters. This implies, that the trajectory and radial samples cannot be written as in Equation (6) and Equation (8). The reason is that the correlations of parameter  $X_i$ , to which step  $\Delta^i$  is added, implies that all other parameters  $\mathbf{X}_{\sim i}$  in the same row with non-zero correlation are changed as well. Therefore, the rows

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<sup>1</sup>In contrary to most authors, I also denote the step as a subtraction instead of  $\Delta$  when referring to the trajectory design. This provides additional clarity.

cannot be denoted and compared as easily by  $a$ 's and  $b$ 's as in Equation (6) and (8). Transforming these matrices allows to re-define the EE-based measures accordingly, such that they sustain the main properties of the ordinary measures for uncorrelated parameters. The property is to be a function of the mean derivative. Yet, Ge and Menendez (2017) fail to fully develop these measures. I will explain how their measures lead to arbitrary results for correlated input parameters. This section covers their approach in a simplified form, focussing on normally distributed input parameters, and presents their measures.

The next paragraph deals with developing a recipe for transforming draws  $\mathbf{u} = \{u_1, u_2, \dots, u_k\}$  from  $[0, 1]$  for an input parameter vector to draws  $\mathbf{x} = \{x_1, x_2, \dots, x_k\}$  from an arbitrary joint normal distribution. We will do this in three steps.

For this purpose, let  $\Sigma$  be a non-singular variance-covariance matrix and let  $\boldsymbol{\mu}$  be the mean vector. The  $k$ -variate normal distribution is denoted by  $\mathcal{N}_k(\boldsymbol{\mu}, \Sigma)$ .

Creating potentially correlated draws  $\mathbf{x}$  from  $\mathcal{N}_k(\boldsymbol{\mu}, \Sigma)$  is simple. Following Gentle (2006), page 197, this can be done the following way: Draw a  $k$ -dimensional row vector of i.i.d standard normal deviates from the *univariate*  $N_1(0, 1)$  distribution, such that  $\mathbf{z} = \{z_1, z_2, \dots, z_k\}$ , and compute the Cholesky decomposition of  $\Sigma$ , such that  $\Sigma = \mathbf{T}^T \mathbf{T}$ . The lower triangular matrix is denoted by  $\mathbf{T}'$ . Then apply the operation in Equation (10) to obtain the correlated deviates from  $\mathcal{N}_k(\boldsymbol{\mu}, \Sigma)$ .

$$\mathbf{x} = \boldsymbol{\mu} + \mathbf{T}^T \mathbf{z}^T \quad (10)$$

Intuition for the mechanics that underlie is provided in Appendix A (not in this draft).

The next step is to understand that we can split the operation in Equation (10) into two subsequent operations. For this, let  $\boldsymbol{\sigma}$  be the vector of standard deviations and let  $\mathbf{R}$  be the correlation matrix of  $\mathbf{x}$ .

The first operation is to transform the standard deviates  $\mathbf{z}$  to correlated standard deviates  $\mathbf{z}_c$  by using  $\mathbf{z}_c = \mathbf{Q}^T \mathbf{z}^T$ . In this equation,  $\mathbf{Q}^t$  is the lower matrix from the Cholesky decomposition  $\mathbf{R} = \mathbf{Q}^T \mathbf{Q}$ . This is equivalent to the above approach in Gentle (2006) for the specific case of the multivariate standard normal distribution  $\mathcal{N}_k(0, R)$ . This is true because for multivariate standard normal deviates, the correlation matrix is equal to the covariance matrix.

The second operation is to scale the correlated standard normal deviates:  $\mathbf{z} = \mathbf{z}_c \boldsymbol{\sigma} + \boldsymbol{\mu}$ .

The last step is to recall the inverse transform sampling method. Therewith we can transform the input parameter draws  $\mathbf{u}$  to uncorrelated standard normal draws  $\mathbf{z}$ . Then we will continue with the two operation in the above paragraph. The transformation from  $\mathbf{u}$  to  $\mathbf{z}$  is summarized by the following three points:

1.  $\mathbf{z} = \Phi^{-1}(u)$

2.  $\mathbf{z}_c = \mathbf{z}\mathbf{Q}^T$

3.  $\mathbf{x} = \boldsymbol{\mu} + \mathbf{z}_c\boldsymbol{\sigma}.$

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