

# 1 EE method

$$d_i^{(j)} = \frac{Y(\mathbf{X}_{\sim i}^{(j)}, X_i^{(j)} + \Delta^{(i,j)})}{\Delta^{(i,j)}}, \quad (1)$$

$$\mu_i = \frac{1}{r} \sum_{j=1}^r d_i^{(j)}. \quad (2)$$

$$\sigma_i = \frac{1}{r} \sum_{j=1}^r (d_i^{(j)} - \mu_i) \quad (3)$$

$$\mu_i^* = \frac{1}{r} \sum_{j=1}^r |d_i^{(j)}|. \quad (4)$$

$$\mu_{i,\sigma}^* = \mu_i^* \frac{\sigma_{X_i}}{\sigma_Y}. \quad (5)$$

Scaling provides link from "deterministic effect" to impact on variation of Y. Parameters may have large effects on Y but not on its variation: The impact of  $X$  may be strong but always the same if  $\sigma_x = \epsilon$ . Especially tricky, if Y does also not vary a lot.

Example: linear function with two parameters: high coeff - low SD and low coeff, high SD.

## 2 Sampling schemes

One EE per parameter per subsample.

$$\mathbf{R}_{(k+1) \times k} = \begin{pmatrix} a_1 & a_2 & \dots & a_k \\ \mathbf{b}_1 & a_2 & \dots & a_k \\ a_1 & \mathbf{b}_2 & \dots & a_k \\ \vdots & \vdots & \ddots & \vdots \\ a_1 & a_2 & \dots & \mathbf{b}_k \end{pmatrix} \quad (6)$$

Contains choice of (quasi-random) sequence. Implies share of very high steps.

$$\mathbf{T}_{(k+1) \times k} = \begin{pmatrix} a_1 & a_2 & \dots & a_k \\ \mathbf{b}_1 & a_2 & \dots & a_k \\ \mathbf{b}_1 & \mathbf{b}_2 & \dots & a_k \\ \vdots & \vdots & \ddots & \vdots \\ \mathbf{b}_1 & \mathbf{b}_2 & \dots & \mathbf{b}_k \end{pmatrix} \quad (7)$$

Contains choice of two numerical parameters. Lower bound of step is 0.5 given step function.

### 3 EE method for correlated inputs

1.  $\mathbf{z} = \Phi^{-1}(u)$
2.  $\mathbf{z}_c = \mathbf{Q}^T \mathbf{z}^T$
3.  $\mathbf{x} = \boldsymbol{\mu} + \mathbf{z}_c(\mathbf{i})\sigma(\mathbf{i})$

Transform samples.  $N(3k + 1)$  and  $3Nk$  function evals.

Correlations include step.

$$\mathcal{T}_1(\mathbf{T}_{\mathbf{i}+1,*}; i-1) = \begin{pmatrix} a_k & a_1 & \dots & \dots & a_{k-1} \\ \mathbf{b}_1 & a_2 & \dots & \dots & a_k \\ \mathbf{b}_2 & a_3 & \dots & \dots & \mathbf{b}_1 \\ \vdots & \vdots & \vdots & \ddots & \vdots \\ \mathbf{b}_k & \mathbf{b}_1 & \dots & \dots & \mathbf{b}_{k-1} \end{pmatrix} \quad (8)$$

$$\mathcal{T}_1(\mathbf{T}_{\mathbf{i},*}; i-1) = \begin{pmatrix} a_1 & a_2 & \dots & \dots & a_k \\ a_2 & \dots & \dots & a_k & \mathbf{b}_1 \\ a_3 & \dots & \dots & \mathbf{b}_1 & \mathbf{b}_2 \\ \vdots & \vdots & \vdots & \ddots & \vdots \\ \mathbf{b}_1 & \mathbf{b}_2 & \dots & \dots & \mathbf{b}_k \end{pmatrix} \quad (9)$$

Correlations exclude step.

$$\mathcal{T}_1(\mathbf{T}_{\mathbf{i},*}; i-1) = \begin{pmatrix} a_2 & a_3 & \dots & \dots & a_1 \\ a_3 & \dots & a_k & \mathbf{b}_1 & a_2 \\ a_4 & \dots & \mathbf{b}_1 & \mathbf{b}_2 & a_3 \\ \vdots & \vdots & \vdots & \ddots & \vdots \\ \mathbf{b}_2 & \mathbf{b}_3 & \dots & \dots & \mathbf{b}_1 \end{pmatrix} \quad (10)$$

Trajectory design only.

Activates distortions by numerical parameters and general differences in drawing the elements between schemes.

$$d_i^{full,T} = \frac{f\left(\mathcal{T}(\mathbf{T}_{\mathbf{i}+1,*}; i-1)\right) - f\left(\mathcal{T}(\mathbf{T}_{\mathbf{i},*}; i)\right)}{\Delta}. \quad (11)$$

$$d_i^{ind,T} = \frac{f\left(\mathcal{T}(\mathbf{T}_{\mathbf{i}+1,*}; i)\right) - f\left(\mathcal{T}(\mathbf{T}_{\mathbf{i},*}; i)\right)}{\Delta}. \quad (12)$$

Improvements. Denominator can be written much simpler as  $\mathcal{T}(b_i) - \mathcal{T}(a_i)$ .

$$d_i^{c,T} = \frac{f(\mathcal{T}(\mathbf{T}_{i+1,*}; i-1)) - f(\mathcal{T}(\mathbf{T}_{i-1,*}; i))}{F^{-1}(\Phi^u(b_i)) - F^{-1}(\Phi^u(a_i))} \quad (13)$$

$$d_i^{u,T} = \frac{f(\mathcal{T}(\mathbf{T}_{i+1,*}; i)) - f(\mathcal{T}(\mathbf{T}_{i,*}; i))}{F^{-1}(Q_{k,*k-1}^T(j)T_{i+1,*k-1}^T(j) + Q_{k,k}^T\Phi^u(b_i)) - F^{-1}(Q_{k,*k-1}^T(j)T_{i,*k-1}^T(j) + Q_{k,k}^T\Phi^u(a_i))} \quad (14)$$

## 4 Replication and Validation

Linear function with three parameters and Correlations equal to 0.9, 0.4, 0.01. Numerical parameter lead to re-linearisation of measures in GM'17.

Let  $f(X_1, \dots, X_k) = \sum_{i=1}^k c_i X_i$  be an arbitrary linear function. Let  $\rho_{i,j}$  be the linear correlation between  $X_i$  and  $X_j$ . Then, for all  $i \in 1, \dots, k$ , I expect:<sup>1</sup>

$$d_i^{u,*} = c_i \tag{15}$$

$$d_i^{c,*} = \sum_{j=1}^k \rho_{i,j} c_j \tag{16}$$

Both equations state that, conceptually, the result does not depend on the sampling scheme.

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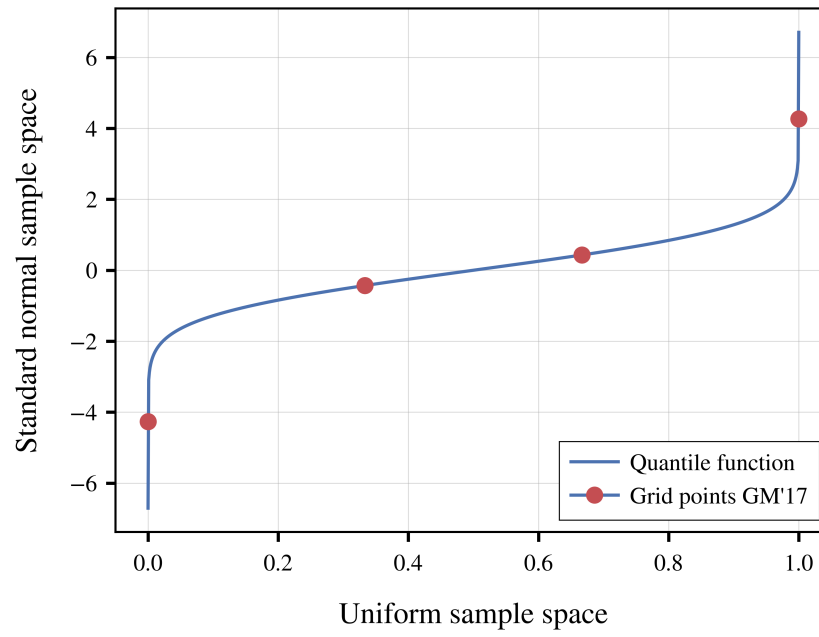
<sup>1</sup>These results correspond to the intuition provided by the example in Saltelli et al. (2008), p. 123.

**Table 1.** Replication and validation - trajectory design

Measure	GM'17	Repl. $\mu^{*\dagger}$	Repl. $\sigma^{\ddagger}$	S'20
$\mu^{*,ind}$	1.20	1.36	0.83	1.00
	1.30	1.48	0.91	1.00
	3.20	3.11	1.94	1.00
$\sigma^{ind}$	0.55	0.00	0.56	0.00
	0.60	0.00	0.62	0.00
	1.30	0.00	1.32	0.00
$\mu^{*,full}$	14.90	16.20	9.97	2.30
	12.50	13.45	8.31	1.91
	10.00	9.93	6.18	1.41
$\sigma^{full}$	6.50	0.00	6.74	0.00
	5.50	0.00	5.63	0.00
	4.00	0.00	4.20	0.00

 $\dagger 0^{num} = 0.00001$  and  $l = 4$ . $\ddagger 0^{num} = 0.00000001$  and  $l = 24$ .**Table 2.** Replication and validation - radial design

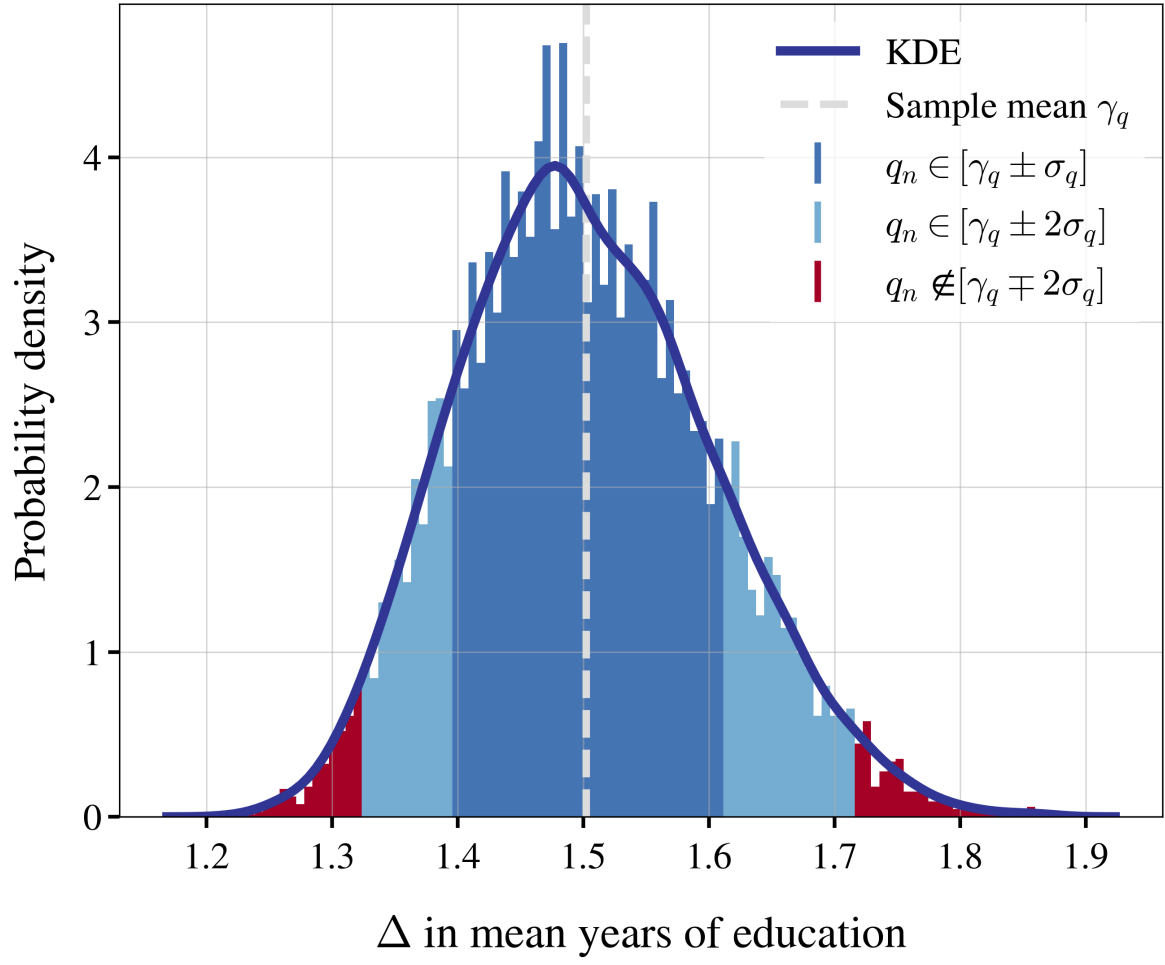
Measure	GM'17	Replication	S'20
$\mu^{*,ind}$	0.60	0.57	1.00
	0.75	0.85	1.00
	1.50	1.31	1.00
$\sigma^{ind}$	0.20	0.10	0.00
	0.30	0.41	0.00
	0.85	0.22	0.00
$\mu^{*,full}$	7.50	6.84	2.30
	6.80	7.77	1.91
	4.75	4.19	1.41
$\sigma^{full}$	2.90	1.15	0.00
	2.65	3.68	0.00
	2.50	0.70	0.00

**Figure 1.** Grid points in standard normal sample space for trajectory design with  $l = 4$ 

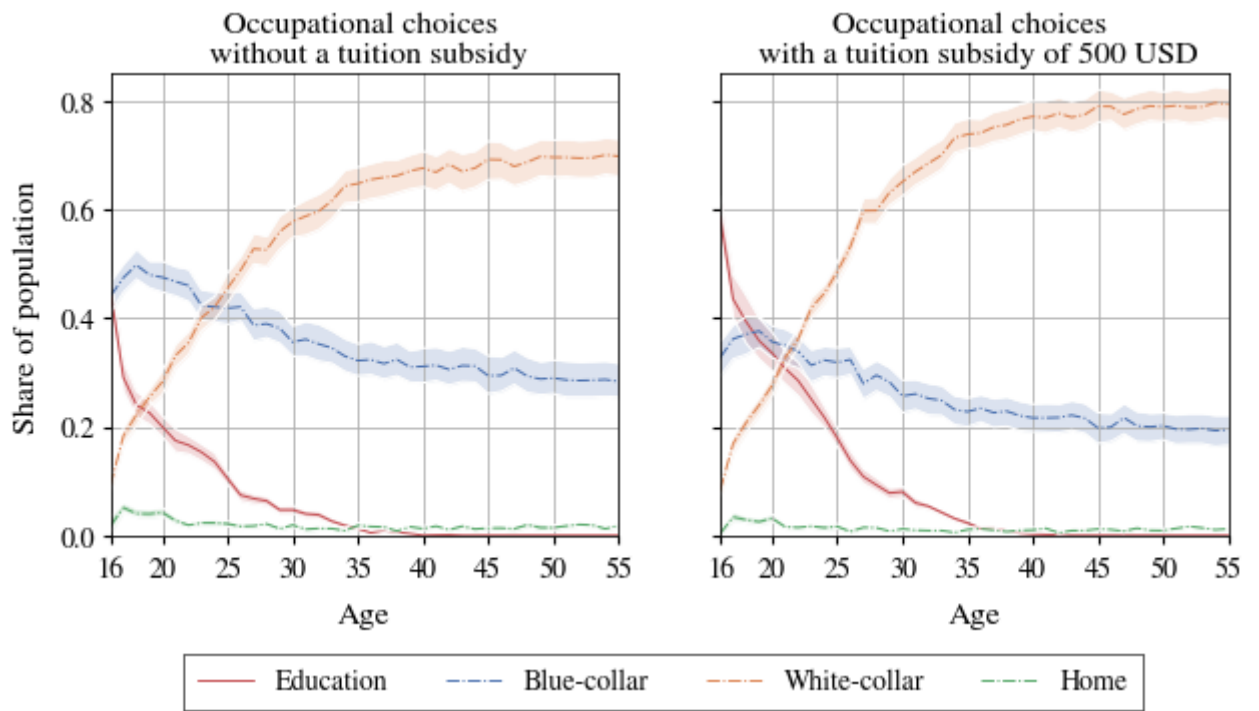


## 5 Results: Uncertainty Analysis

**Figure 2.** Probability distribution of quantity of interest  $q$



**Figure 3.** Comparison of shares of occupation decision over time between scenarios with cone plots

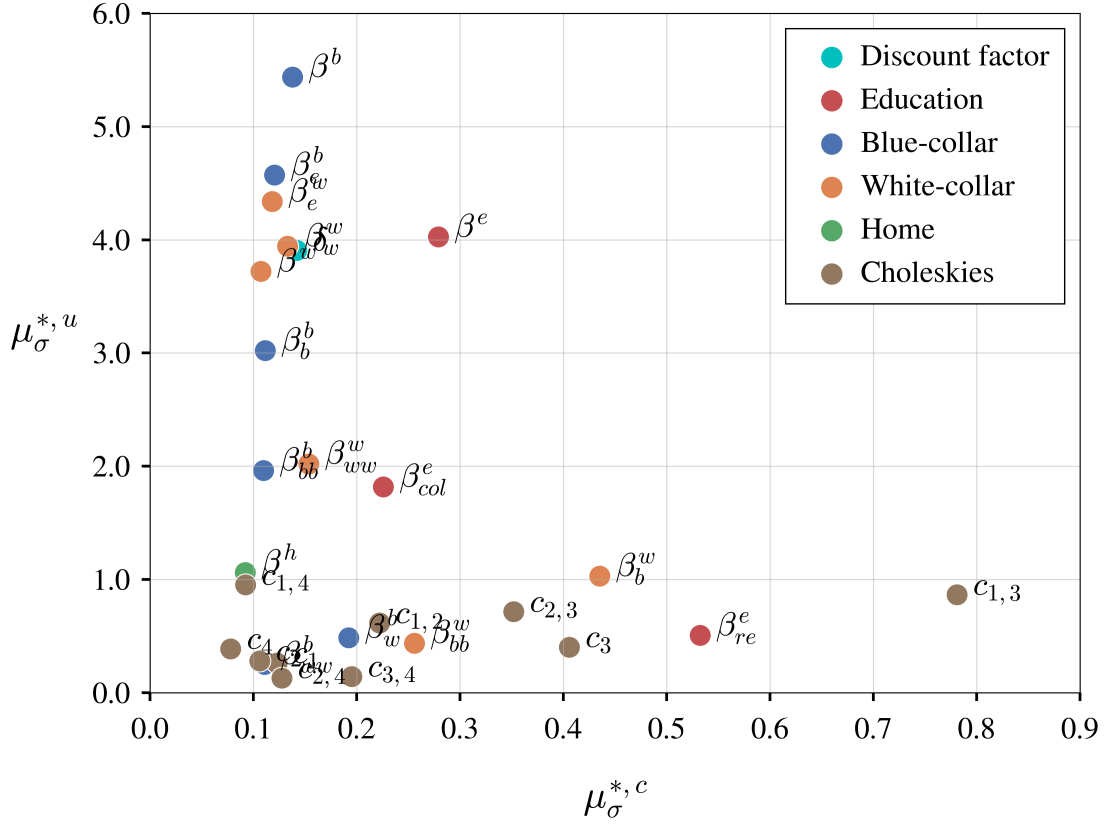
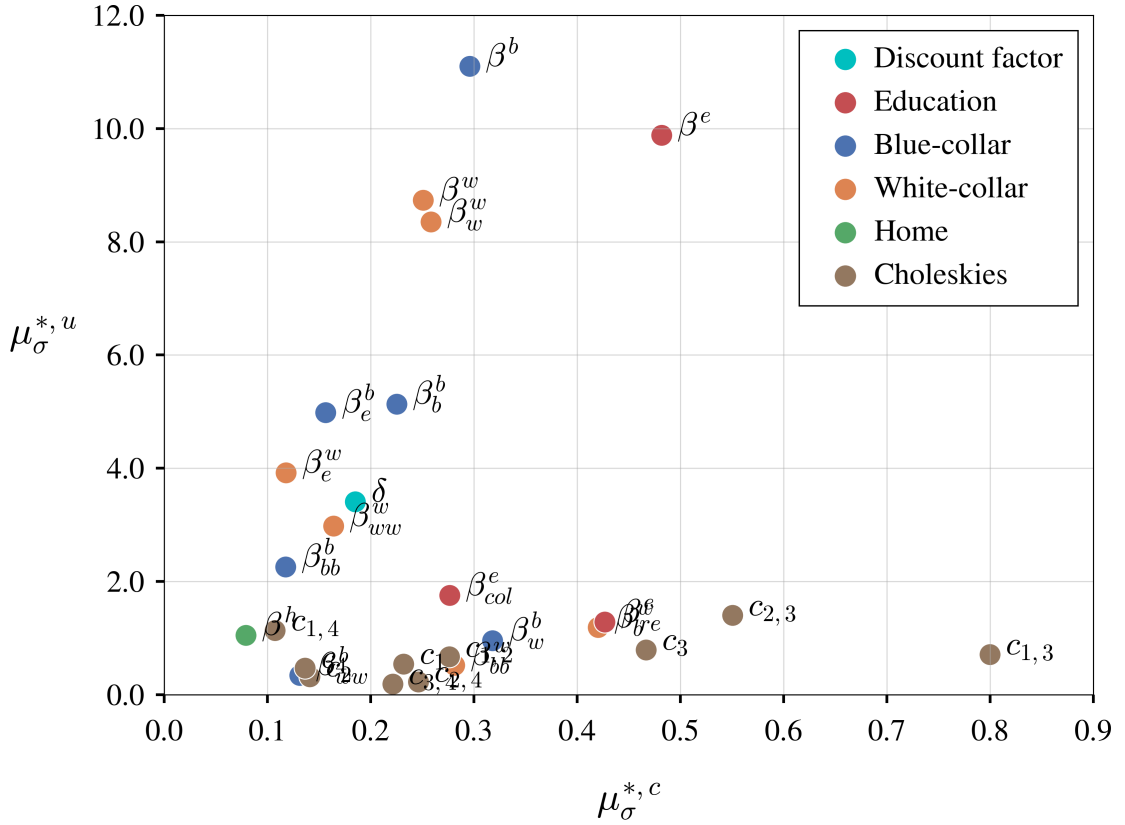


## 5.1 Results: Qualitative Sensitivity Analysis

Be cautious!

**Table 3.** Mean absolute correlated and uncorrelated elementary effects (based on 150 subsamples in trajectory and radial design)

Parameter	$\mu_T^{*,c}$	$\mu_R^{*,c}$	$\mu_T^{*,u}$	$\mu_R^{*,u}$
<i>General</i>				
$\delta$	17	23	476	415
<i>Blue-collar</i>				
$\beta^b$	1	3	43	88
$\beta_e^b$	11	14	406	443
$\beta_b^b$	25	51	688	1169
$\beta_{bb}^b$	871	934	15 540	17 860
$\beta_w^b$	29	48	73	143
$\beta_{ww}^b$	389	460	869	1183
<i>White-collar</i>				
$\beta^w$	1	3	50	117
$\beta_e^w$	26	28	943	852
$\beta_w^w$	24	47	718	1521
$\beta_{ww}^w$	933	997	12 257	18 069
$\beta_b^w$	131	127	309	356
$\beta_{bb}^w$	120	1352	2088	2477
<i>Education</i>				
$\beta^e$	0.0008	0.0002	0.001	0.003
$\beta_{he}^e$	0.0001	0.0002	0.001	0.001
$\beta_{re}^e$	0.0003	0.0002	0.0003	0.0006
<i>Home</i>				
$\beta^h$	0.0003	0.0003	0.000 02	0.000 02
<i>Lower Triangular Cholesky Matrix</i>				
$c_1$	8	16	18	37
$c_2$	8	11	22	24
$c_3$	0.0004	0.0004	0.0004	0.0007
$c_4$	0.0004	0.000 08	0.0002	0.0003
$c_{1,2}$	4	4	10	10
$c_{1,3}$	0.0005	0.0006	0.0006	0.0005
$c_{2,3}$	0.0003	0.0005	0.0006	0.001
$c_{1,4}$	0.000 04	0.000 05	0.0004	0.0005
$c_{2,4}$	0.0001	0.0002	0.0001	0.0002
$c_{3,4}$	0.0001	0.0001	0.000 08	0.0001

**Figure 4.** Sigma-normalized mean absolute Elementary Effects for trajectory design**Figure 5.** Sigma-normalized mean absolute Elementary Effects for radial design

## 5.2 Review: Estimation Results

**Table 4.** Estimates for the distribution of input parameters

Parameter	Mean	Standard error (SE)	SE in KW94
<i>General</i>			
$\delta$	0.95	0.000 84	-
<i>Blue-collar</i>			
$\beta^b$	9.21	0.013	0.014
$\beta_e^b$	0.038	0.0011	0.0015
$\beta_b^b$	0.033	0.000 44	0.000 79
$\beta_{bb}^b$	-0.0005	0.000 013	0.000 019
$\beta_w^b$	0.0	0.000 67	0.0024
$\beta_{ww}^b$	0.0	0.000 029	0.000 096
<i>White-collar</i>			
$\beta^w$	8.48	0.0076	0.0123
$\beta_e^w$	0.07	0.000 47	0.000 96
$\beta_w^w$	0.067	0.000 55	0.000 90
$\beta_{ww}^w$	-0.001	0.000 017	0.000 070
$\beta_b^w$	0.022	0.000 33	0.0010
$\beta_{bb}^w$	-0.0005	0.000 021	0.000 030
<i>Education</i>			
$\beta^e$	0.0	330	459
$\beta_{he}^e$	0.0	155	410
$\beta_{re}^e$	-4000	202	660
<i>Home</i>			
$\beta^h$	17 750	390	1442
<i>Lower Triangular Cholesky Matrix</i>			
$c_1$	0.2	0.0015	0.0056
$c_2$	0.25	0.0013	0.0046
$c_3$	1500	108	350
$c_4$	1500	173	786
$c_{1,2}$	0.0	0.0064	0.023
$c_{1,3}$	0.0	143	0.412
$c_{2,3}$	0.0	116	0.379
$c_{1,4}$	0.0	232	0.911
$c_{2,4}$	0.0	130	0.624
$c_{3,4}$	0.0	177	0.870

### 5.3 Improvement: Sampling scheme tailored to Sobol' indices

Similar to trajectory design to have interactions still included. Base row is expectation. Shuffle row. Add random value between  $[0, 0.5]$ . Take square root of squared difference and divide by step.

## References

Saltelli, A., M. Ratto, T. Andres, F. Campolongo, J. Cariboni, D. Gatelli, M. Saisana, and S. Tarantola (2008). *Global Sensitivity Analysis: The Primer*. John Wiley & Sons.