

# Lecture VI: Constraints and Controllers

Parts Based on Erin Catto's Box2D Tutorial

# Motion Constraints

- In practice, no rigid body is free to move around 'on its own'.
- Movement is **constrained**:
  - wheels on a chair
  - human body parts
  - trigger of a gun
  - opening door
  - actually almost anything you can think of in a game...



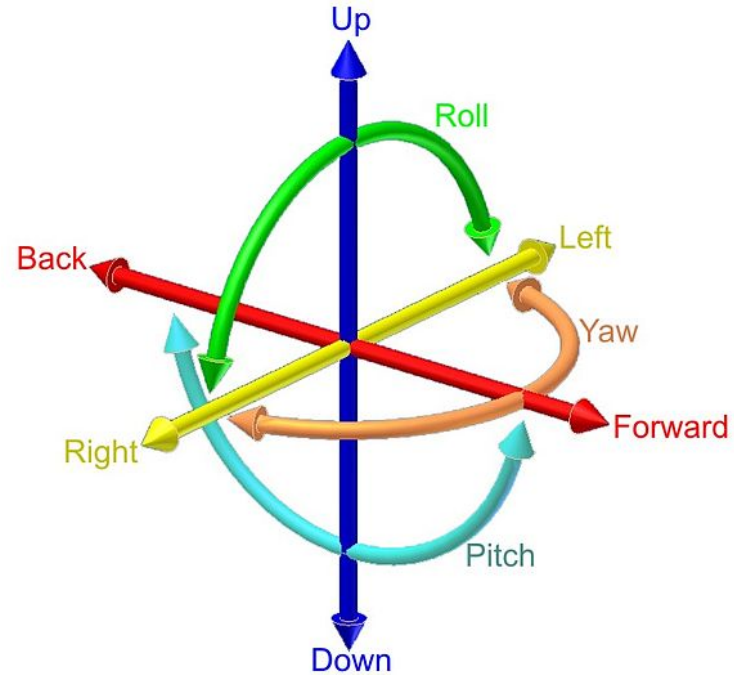
[http://static4.gamespot.com/uploads/scale\\_medium/mig/2/4/7/7/2282477-Garrys\\_13231\\_screen.jpg](http://static4.gamespot.com/uploads/scale_medium/mig/2/4/7/7/2282477-Garrys_13231_screen.jpg)



<http://i2.cdn.turner.com/cnnnext/dam/assets/140813101135-best-biking-cities-utrecht-horizontal-large-gallery.jpg>

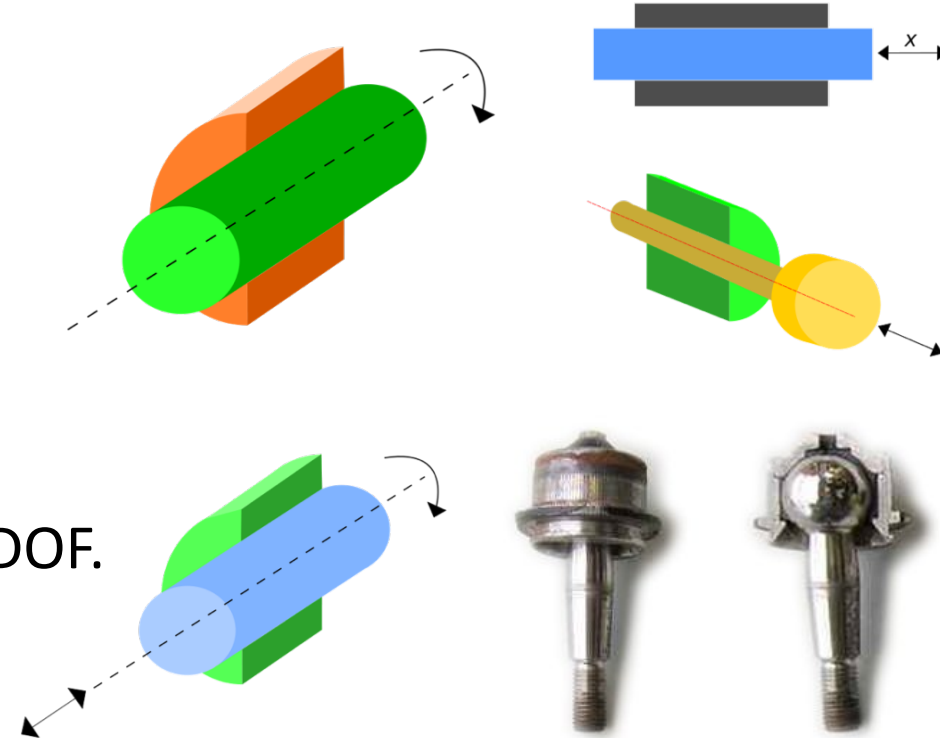
# Degrees of Freedom

- Description of allowed movement by specifying **degrees of freedom (DOF)**
  - Translational (3 DOF max)
  - Rotational (3 DOF max)



# Kinematic Pair

- **Kinematic pair:** connection between two bodies that **imposes constraints** on their relative movement.
  - **Lower pair:** constraint on a point, line or plane
    - Revolute pair, or hinged joint: 1 rotational DOF.
    - Prismatic joint, or slider: 1 translational DOF.
    - Screw pair: 1 coordinated rotation/translation DOF.
    - Cylindrical pair: 1 translational + 1 rotational DOF.
    - Spherical pair, or ball-and-socket joint: 3 rotational DOF.
    - Planar pair: 3 translational DOF.
  - **Higher pair:** constraint on a curve or surface.

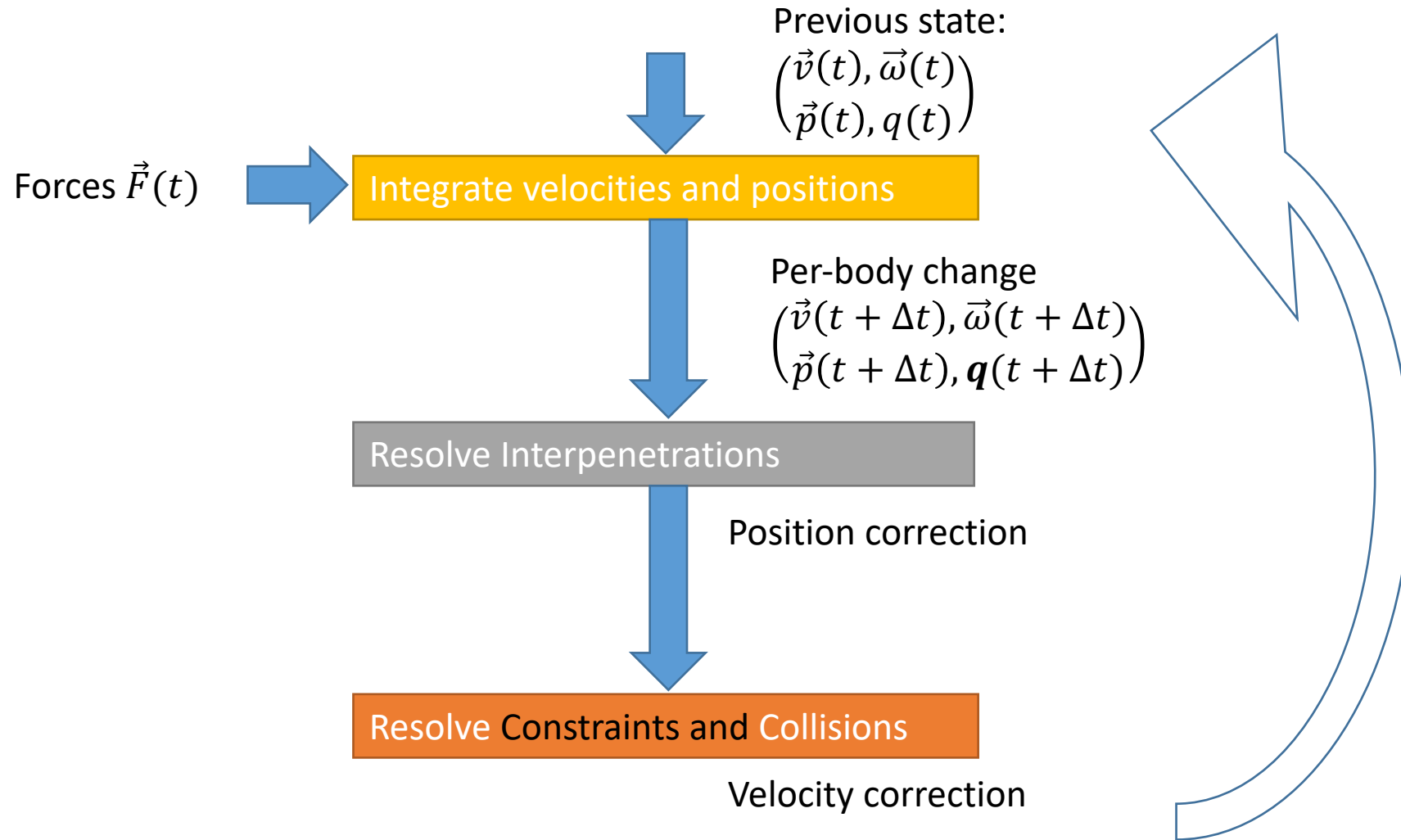


# Constraints Resolution

- Energy of components on constrained d.o.f. can be **lost**.
  - Converted into heat and sound ( $E_o$ )
  - As opposed to **putting pressure** on the joint, causing degradation.
- Project net force on the **unconstrained** degrees of freedom.
- Not true for **soft bodies**!
  - Deforming accordingly...
- (Lagrangian) Approximation: no loss of energy.

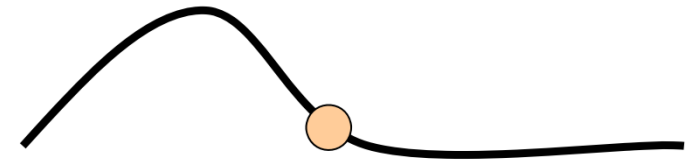
[https://www.youtube.com/watch?v=t\\_ZB0JViW68](https://www.youtube.com/watch?v=t_ZB0JViW68)

# Constrained Game-Engine Loop



# Constraint Representation

- Often with an implicit function  $C(p, p', p'') = 0$ .
- **Example:** position constraint on a curve:  $C(x, y) = 0$ 
  - Constraints dependent only on position are called *holonomic*.



- Equality constraints:  $C(p, p', p'') = 0$
- Inequality constraints:  $C(p, p', p'') \geq 0$ 
  - Examples?

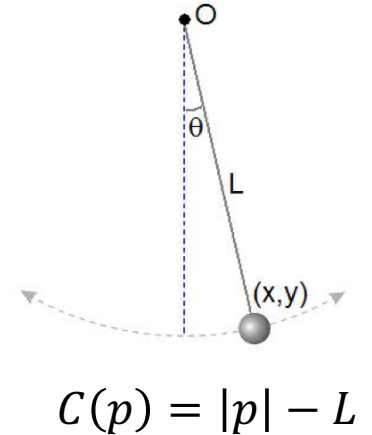
# Differential Equality Constraints

- **Our purpose:** Move from  $\vec{p}(t)$  to  $\vec{p}(t + \Delta t)$  and conserve:

$$C(\vec{p}(t)) = C(\vec{p}(t + \Delta t)) = 0$$

- **Algebraic interpretation:** the following are conserved:

- $C(\vec{p}(t)) = 0$  (**position**)
  - $dC/dt = 0$  (constraint **velocity**)
  - $d^2C/dt^2 = 0$  (constraint **acceleration**)
- Because function should be constant 0!





$$C(p, p', p'') = 0$$

# Velocity Constraint

- Chain rule (single constraint, single bodies):

$$\frac{dc}{dt} = \frac{\partial c}{\partial p} \cdot \frac{dp}{dt} = \frac{\partial c}{\partial p} \cdot \vec{v} = 0$$

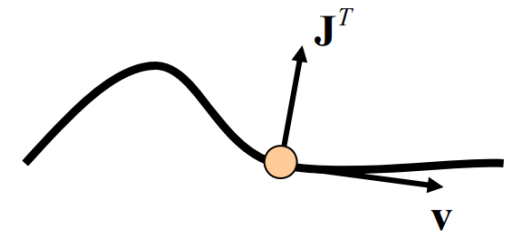
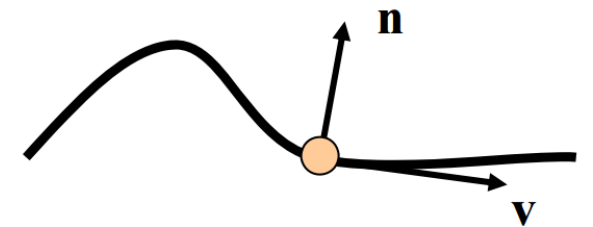
- Multiple constraints, multiple bodies:

$$C = \{c_1, \dots, c_n\}, P = \{p_1, \dots, p_m\}$$

- We get the **Jacobian**  $J_{n \times m} = \left( \frac{\partial c_i}{\partial p_j} \right)$

- **Kinematic** velocity constraint:

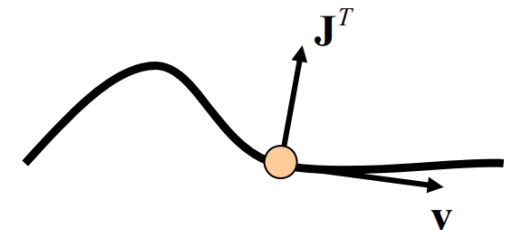
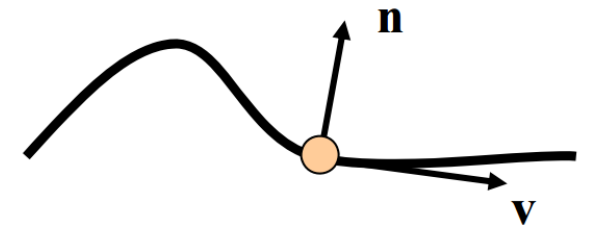
$$J\vec{v} = 0$$



$$C(p, p', p'') = 0$$

# Velocity Constraint

- $J\vec{v} = 0$  means “ $\vec{v}$  is in the **right null space** of  $J$ ”
- Dimension of null space  $\Leftrightarrow$  degrees of valid movement.
- Full rank of  $J \rightarrow$  null space empty  $\rightarrow$  **no allowed movement!**
  - **Physical example:** move on two curves at the same time.
- How do we adhere to allowed velocity all the time?



$$C(p, p', p'') = 0$$

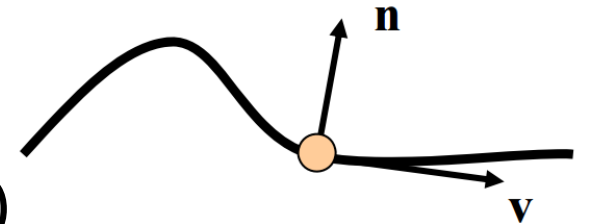
# Acceleration Constraint

- Acceleration constraint:  $\frac{d^2 C}{dt^2} = \frac{dJ}{dt} \vec{v} + J \vec{a} = 0$

- Net external force:  $\vec{F}_E$ .

- Mass matrix:

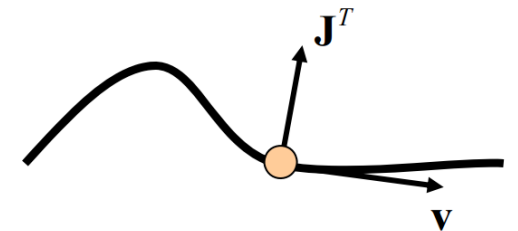
$$M_{3m \times 3m} = \text{diag}(M_1, M_1, M_1, \dots, M_m, M_m, M_m)$$



- To obey the constraint, we need to assume a virtual force  $\vec{F}_C$ .

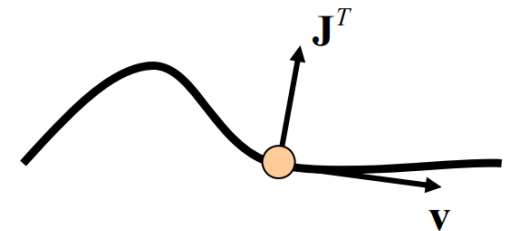
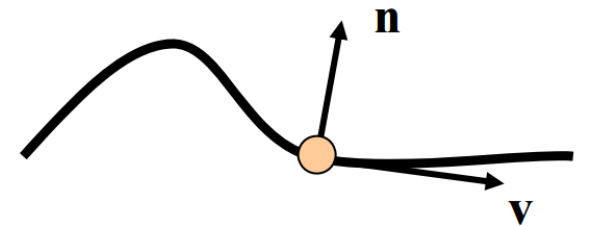
- Dynamic force equation:

$$\frac{dJ}{dt} \vec{v} + JM^{-1}(\vec{F}_E + \vec{F}_C) = 0$$



# The Constraint Force

- The constraint force diverts free (unconstrained) movement to valid movement.
- **Geometric intuition**: constraint force “kills” invalid movement and nothing else.
- Principle of **virtual work**:  $\vec{F}_c$  does no work on  $\vec{v}$ .
- **Motivation**: (energy-wise) lossless constraint.
- **Also**: since it never causes illegal movement!
  - Where have we seen this?

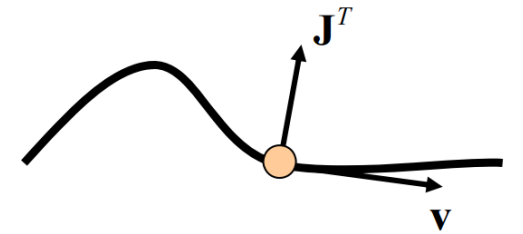
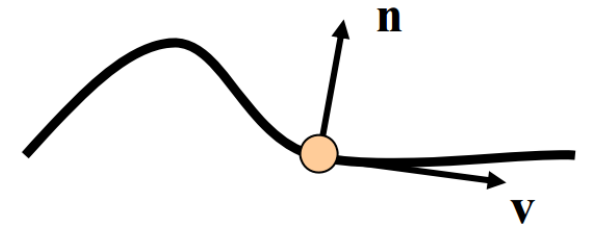


# The Constraint Force

- Principle of **virtual work**:  $\vec{F}_c \cdot \vec{v} = 0$ .
- We have that  $J\vec{v} = 0$ .  
→  $\vec{F}_c$  is **spanned** by the rows of  $J$ :

$$\vec{F}_c = \sum_i \lambda_i J(i, \cdot) = J^T \lambda$$

- $\lambda$  : **Lagrange Multiplier**.
- How do we get  $\lambda$  in order to compute  $\vec{F}_c$ ?



$$\vec{F}_c = J^T \lambda$$

# Direct Solution

- To get :  $\frac{d^2 C}{dt^2} = 0$ , we need to solve for the Lagrange Multiplier:

$$\frac{dJ}{dt} \vec{v} + JM^{-1}(\vec{F}_E + \vec{F}_c) = \frac{dJ}{dt} \vec{v} + JM^{-1}(\vec{F}_E + J^T \lambda)$$

- We get:

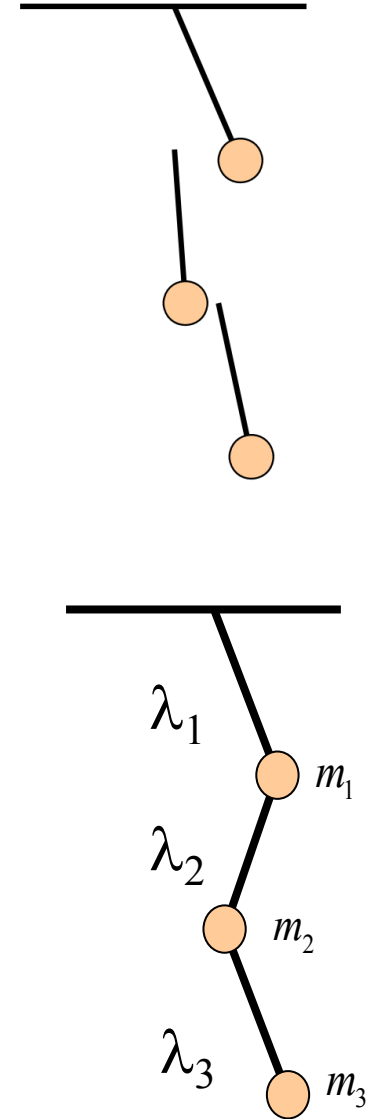
$$\boxed{JM^{-1}J^T} \lambda = \frac{dJ}{dt} \vec{v} + JM^{-1} \vec{F}_E$$

Square  $|C| \times |C|$  matrix

- Disadvantages:
  - Expensive linear solve
  - $J, \frac{dJ}{dt}$  change at each point  $p$  !
  - Might need complicated derivatives:  $\frac{dJ}{dt}$ .
  - Discrete integration combined with this will make an inexact solution.

# Alternative: Sequential impulses

- **Previously:** working with forces to get valid acceleration.
- **Now:** working with impulses to get valid velocity.
- **Sequential impulses (SI)**
  - Applying impulses at each constraint iteratively to correct velocity.
  - Quite stable and converges to a global solution.
- **Pro:**
  - Easier **friction** and **collision handling**.
  - Velocity rather than acceleration.
  - In a time step, **impulse**  $\Leftrightarrow$  **force**.
- **Con:** velocity constraints are not precise  $\rightarrow$  might produce position drift  $\rightarrow$  breaking the constraint.



# Sequential impulses

## Step 1

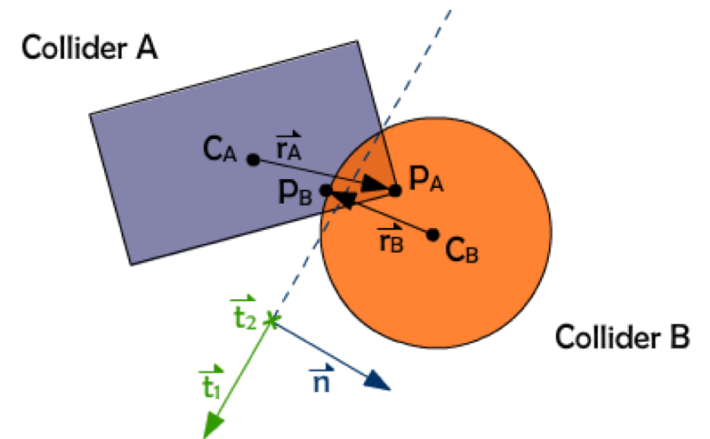
Integrate applied forces, yielding to tentative velocities

## Step 2

Apply impulses sequentially for all constraints to correct the velocity errors

## Step 3

Use the new velocities to update the positions



<http://allenchou.net/wp-content/uploads/2013/12/contacts-figure.png>



# Computing the Impulses

- A single constraint  $i$  currently has  $J_i v \neq 0$ .
  - $J_i$  - row vector, normal to constraint at closest point.
- Change velocity by  $\Delta v$  to get  $J_i(v + \Delta v) = 0$ .
- $\Delta P_i = \int_t^{t+\Delta t} \vec{F}_c dt$ . For infinitesimal time step:
$$\Delta P_i \parallel \vec{F}_c \rightarrow \Delta P_i = J_i^T \lambda_i = M \Delta v$$
  - (a different Lagrange multiplier that we need to compute)
- We compute  $\lambda_i$ :

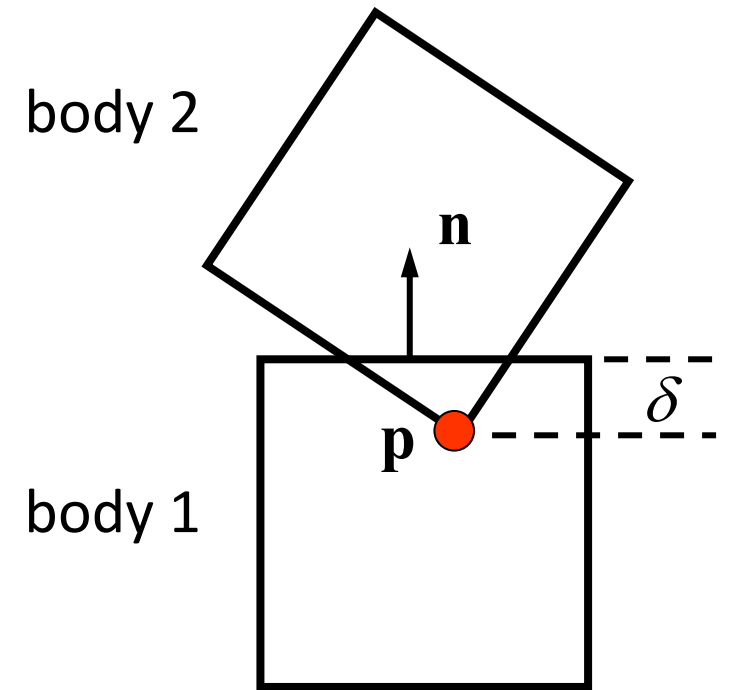
$$J_i(v + M^{-1} J_i^T \lambda_i) = 0$$
$$\lambda_i = \frac{-J_i v}{J_i M^{-1} J_i^T}$$

# Sequential Integration

- As solving a constraint for a body may influence the solving for another one, we need an **iterative process**
  - **while** (!done) {  
    **for** all constraints c **do** solve c;  
}
  - Convergence is usually ensured by reaching either a maximal amount of iterations or a minimal change in every constraints

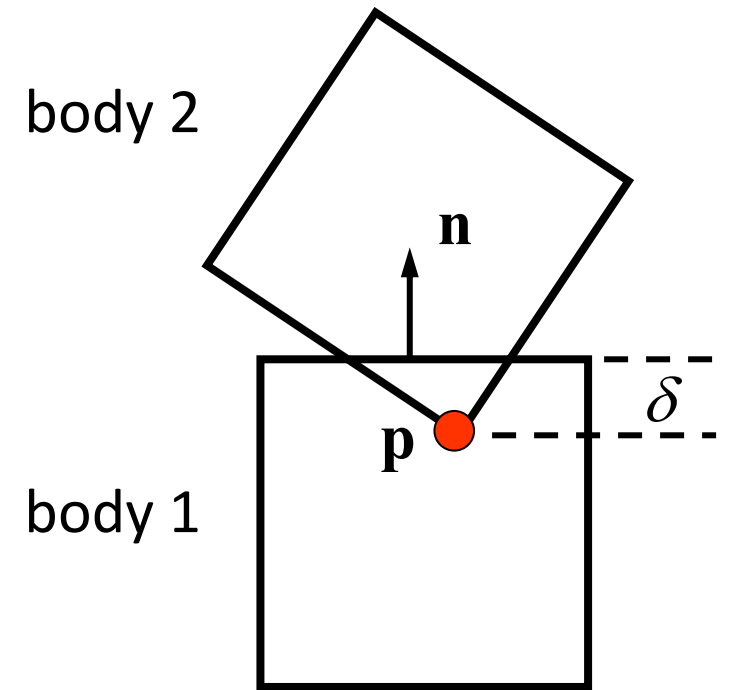
# Inequality Constraints

- Constraints are **inactive** when  $\mathcal{C}(p) > 0$ .
- When they becomes active, solve for them.
  - Otherwise ignore.
- **Example:** collision and interpenetration.



# Collision Constraint

- In **previous** iteration:  $x_i$  is out of the object.
- After position integration:  $x_{i+1}$  is penetrating.
- Penetration normal:  $\hat{n}$  (pointing outwards)
- **Must make sure**: the projected point  $x_{i+1}$  is non-penetrating.
- Constraint:  $C(x_{i+1}) = (x_{i+1} - x_i) \cdot \hat{n} \geq 0$ .
- Velocity constraint:  $\vec{v} \cdot \hat{n} \geq 0$
- **Note**: Can invalidate other constraints.



# Working with rigid bodies

- Constraints depend on chosen center  $x$  and orientation  $q$ :  
 $c(x, q) = 0$ .

- As such, velocity constraints are of the form:  $\frac{dC}{dt}(v, \omega) = 0$

- Mass matrix consequently contains tensors of inertia:

$$M = \text{diag}\{M_1, M_1, M_1, I_1, \dots, M_m, M_m, M_m, I_m\}$$

# Collision Resolution as Constraint Solving

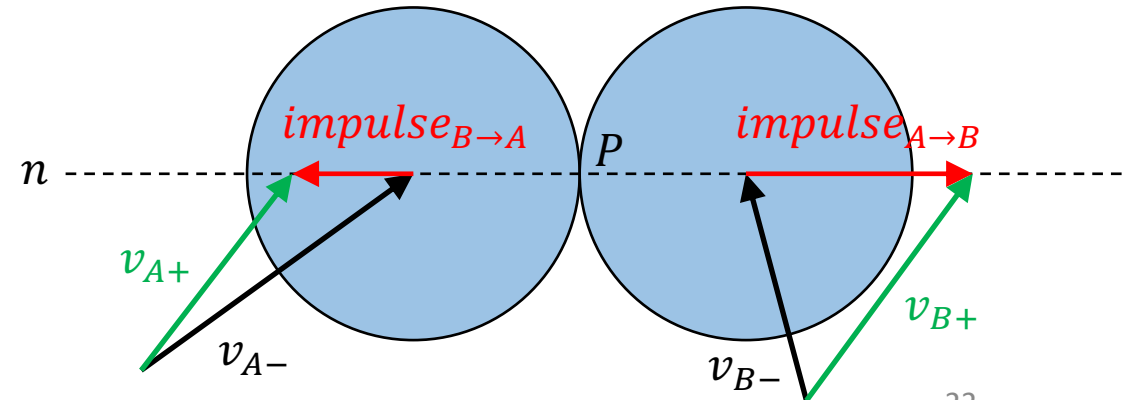
$$\begin{aligned}\frac{dC}{dt} &= (\bar{\mathbf{v}}_{A+} - \bar{\mathbf{v}}_{B+}) \cdot \hat{\mathbf{n}} = \\ &(\vec{\mathbf{v}}_{A+} + \vec{\boldsymbol{\omega}}_{A+} \times \vec{\mathbf{r}}_A - \vec{\mathbf{v}}_{B+} - \vec{\boldsymbol{\omega}}_{B+} \times \vec{\mathbf{r}}_B) \cdot \hat{\mathbf{n}} = \\ &\begin{pmatrix} \hat{\mathbf{n}} \\ \vec{\mathbf{r}}_A \times \hat{\mathbf{n}} \\ -\hat{\mathbf{n}} \\ -\vec{\mathbf{r}}_B \times \hat{\mathbf{n}} \end{pmatrix} \begin{pmatrix} \vec{\mathbf{v}}_{A+} \\ \vec{\boldsymbol{\omega}}_{A+} \\ \vec{\mathbf{v}}_{B+} \\ \vec{\boldsymbol{\omega}}_{B+} \end{pmatrix} = Jv\end{aligned}$$

$$M = \begin{pmatrix} M_A & & & \\ & I_A & & \\ & & M_B & \\ & & & I_B \end{pmatrix}$$

$$\lambda_i = \frac{-Jv}{JM^{-1}J^T}$$

Handy Identities

$$\begin{aligned}\mathbf{A} \cdot (\mathbf{B} \times \mathbf{C}) &= \\ \mathbf{C} \cdot (\mathbf{A} \times \mathbf{B}) &= \\ \mathbf{B} \cdot (\mathbf{C} \times \mathbf{A}) &= \end{aligned}$$



# Collision Resolution as Constraint Solving

- We get the “well-known”:

$$\lambda = \frac{-(1 + C_R)[(\bar{v}_{A-} - \bar{v}_{B-}) \cdot \hat{n}]}{\left(\frac{1}{m_A} + \frac{1}{m_B}\right) + [(\vec{r}_A \times \hat{n})^T I_A^{-1} (\vec{r}_A \times \hat{n}) + (\vec{r}_B \times \hat{n})^T I_B^{-1} (\vec{r}_B \times \hat{n})]}$$

- ...For  $C_R = 0$ .

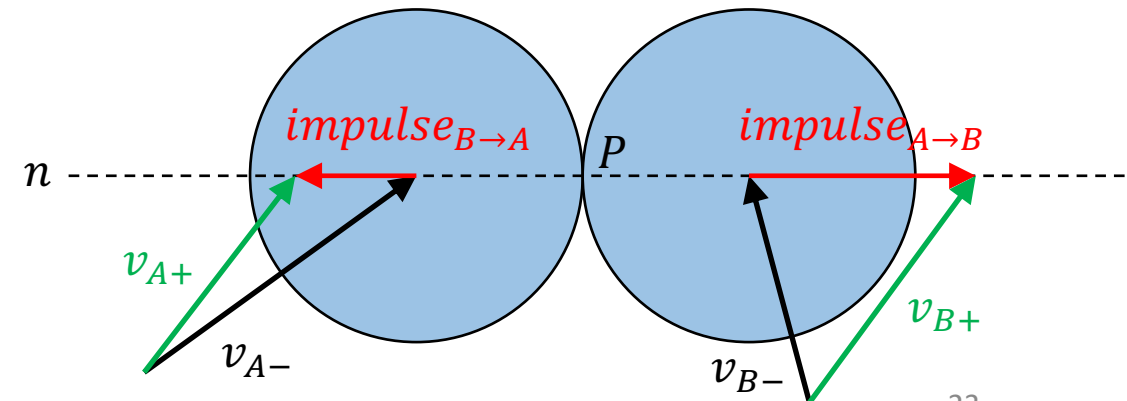
- Explanation: we solved for “minimum velocity to resolve”.

- Elastic restitution is an **extra velocity bias**.

Handy Identities

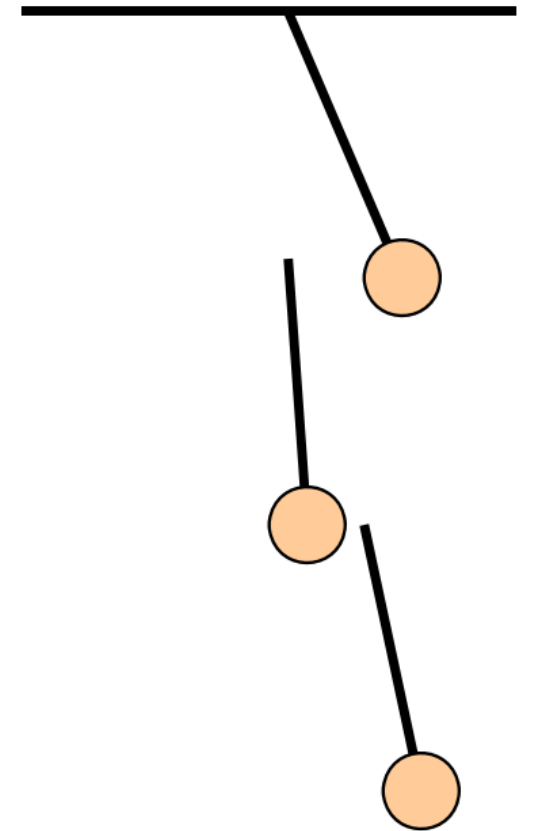
$$\begin{aligned} \mathbf{A} \cdot (\mathbf{B} \times \mathbf{C}) &= \\ \mathbf{C} \cdot (\mathbf{A} \times \mathbf{B}) &= \\ \mathbf{B} \cdot (\mathbf{C} \times \mathbf{A}) &= \end{aligned}$$

$$\lambda_i = \frac{-Jv}{JM^{-1}J^T}$$



# Position Drift

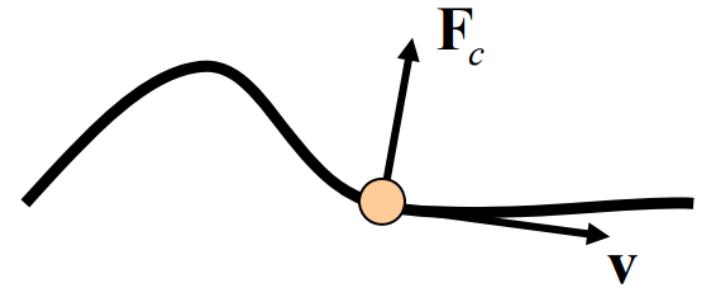
- Even if velocities are fixed, the position integration might drift
  - Since discrete time step.
- Solution: nothing simple
  - Like interpenetration resolution
- Possible easy fix: project positions as well!
  - More on that in position-based dynamics...





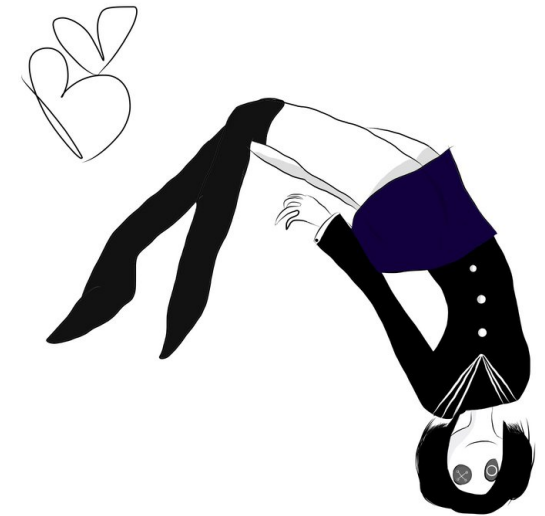
# Alternative: Reduced Coordinate Simulation

- Instead of breaking & correcting => only produce force / torque along a specific DOF.
  - Reducing possible movement.
- impulse-based is a full coordinate simulation.
- **Pro:** faster simulation.
  - less calculations.
  - less tuning.
- **Con:** more vulnerable to numerical instability.
  - might be difficult to parameterize the DOF system.
- For instance:  $Jv = 0$  => use only null space of  $J$ !



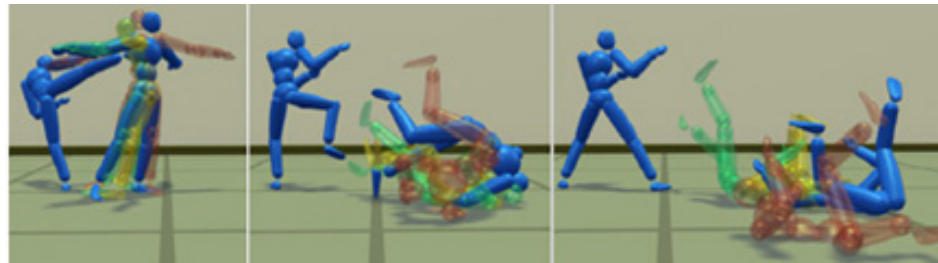
# Motion control

- Imagine you have rigid bodies moving and constrained correctly according to the forces you apply.
- Letting them 'live' on their own is fine for **passive** objects.
  - projectile, furniture, environmental objects *etc.*
- Living beings **produce motion!**
  - Otherwise they will just fall onto the ground at the beginning of the game



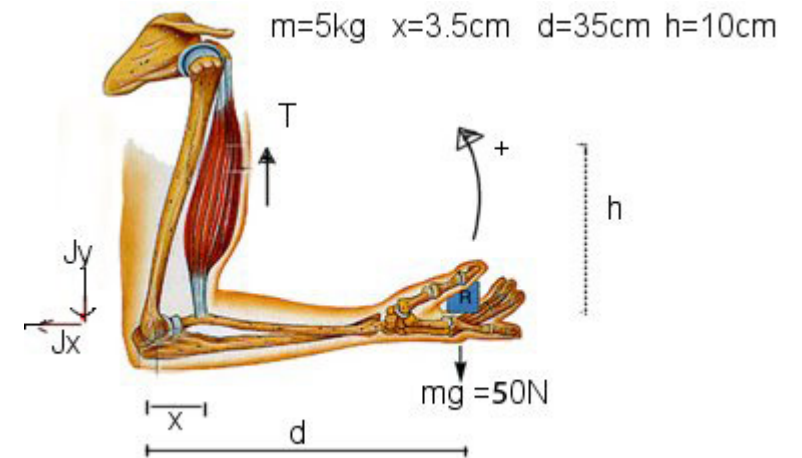
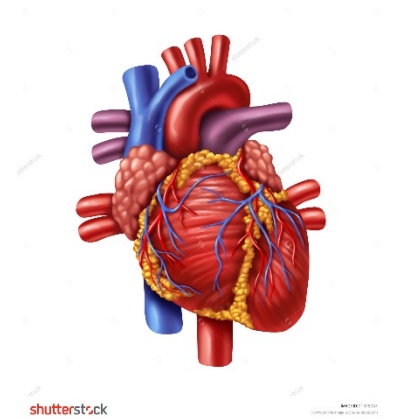
# Motion Control

- Animated bodies are controlled using a mix of **kinematics** and **dynamics**.
- **Kinematics**: replay and slightly adapt pre-recorded motions.
- **Dynamics**: passively animate objects reacting to external forces (*e.g.* human ragdoll).
- A real-time controller switches from one to the other according to events, forces, poses *etc.*



# Motion Control

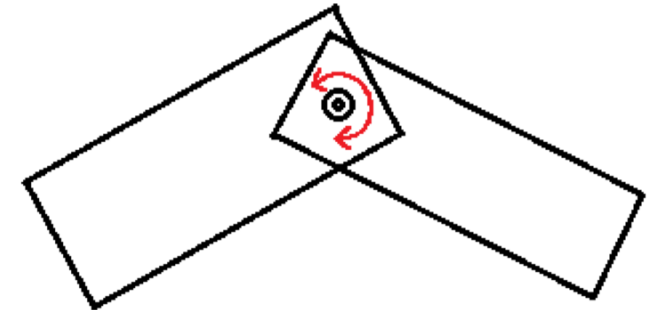
- Imagine that you want to **actively actuate** rigid bodies using forces and torques.
  - not yet in games but will probably in a near future...
- Actuators **generate** motion from within the bodies
  - Joint torques
  - External forces
  - Virtual forces
  - Muscle forces
  - *contractile elements*



[continuummechanics.org/cm/index.html](http://continuummechanics.org/cm/index.html)

# Joint Torques

- Most straightforward actuation model.
- Joint torques directly generate torques for each actuated DOF.
- Assuming that there is a 'fake' motor at the location of the joint that can produce torque.
- e.g. increase a joint angle  $\Leftrightarrow$  positive torque.
- Very useful for tracking pre-recorded motions or any other error-based poses (e.g. balance pose)
  - Amount of applied torque depends directly on the error



<http://files.maartenbaert.be/extremephysics/illustration-hinge-joint.png>

# External Forces

- Applying external forces on the right object, local position, and for the right amount of time.
  - Difficult to produce **realistic motions**.
  - Does not really fit natural motions.
    - Motion originates from **inside**!
- Similar to a **puppetry technique**.
  - System control must be mastered.
- But very useful for the control of the global orientation and position of a complex system (root node).



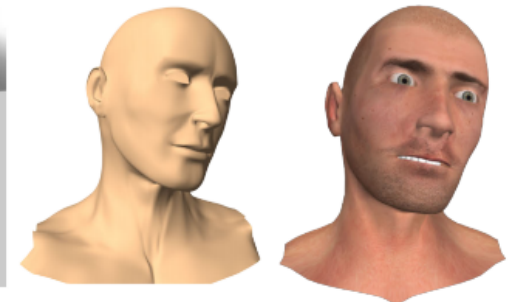
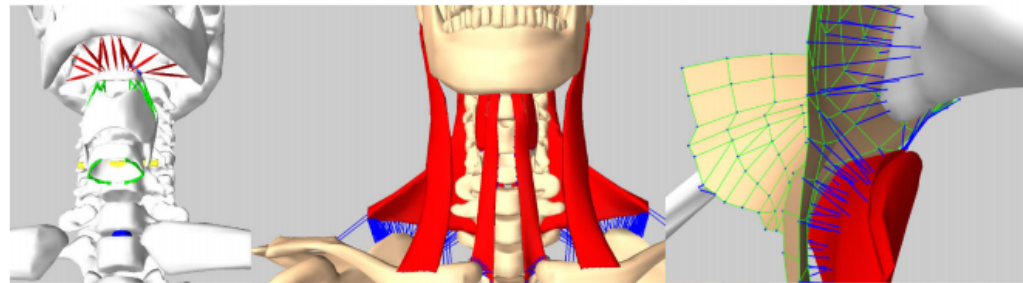
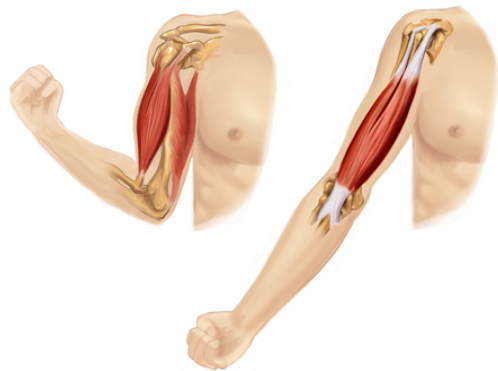
<http://previews.123rf.com/images/pkdinkar/pkdinkar1109/pkdinkar110900022/10551395-employee-as-a-puppet-on-strings-Stock-Vector-puppet-man-marionette.jpg>

# Virtual Forces

- Not really an actuation method.
- Emulate the effect of applying an external force by computing the equivalent joint torque.
- Use the relation between **joint rotation** and **position** where a force is applied (by the Jacobian of the system).

# Muscle Forces

- Motion actually comes from the **contraction of muscles**.
  - they also produce torques at joints, but not in a ‘fake motor’ way.
- Emulating physical behavior to the model => “realistic” actuation of rigid bodies.
  - commonly used in biomechanics / motion analysis
  - the muscle model is usually a combination of **non-linear springs** and **dampers**.



[Lou *et al.* 2013] “Physics-based Human Neck Simulation”

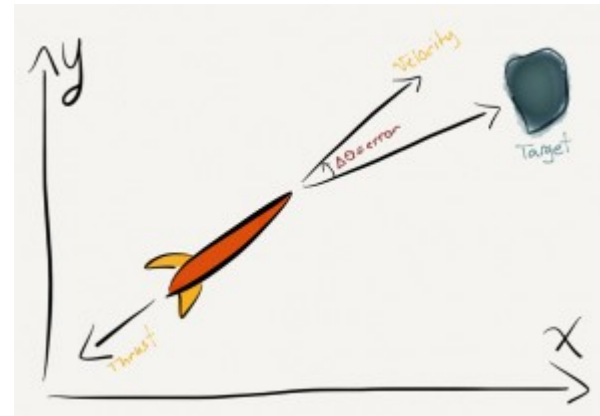


# Controller design

- Joint-space motion control.
  - defines and tracks kinematics target.
- Stimulus-response network control
  - genetically evolves controllers according to objectives.
- Constrained dynamics optimization control.
  - finds optimal torques through online optimization.

# PD Controller

- Proportional Derivative (PD) controller
  - Used to compute joint torques linearly proportional to the difference between the current state and the target state.
  - Based on joint orientation and angular velocity.



[http://www.gamedev.net/uploads/monthly\\_10\\_2014/ccs-224713-0-48143500-1414694390.jpg](http://www.gamedev.net/uploads/monthly_10_2014/ccs-224713-0-48143500-1414694390.jpg)

# PD Controller

$$\tau = k_p(\theta_d - \theta) + k_v(\dot{\theta}_d - \dot{\theta})$$

Where:

- $\tau$  is the generated joint torque.
- $\theta_d$  and  $\theta$  the desired and current **joint angles**.
- $\dot{\theta}_d$  and  $\dot{\theta}$  the desired and current joint **angular velocity**.
- $k_p$  and  $k_v$  are the **controller gain**.
  - Regulating how responsive the controller is to deviation.

# PD Controller

- Con: The motion-controller designer needs to carefully define the gain values.
  - too high  $k_p$ : producing stiff unresponsive motions.
  - too low  $k_p$ : not track target correctly.
  - too high  $k_v$ : converging too slowly to the target.
  - too low  $k_v$ : producing oscillations.
- ...Expect to spend time fine tuning gains!

$$\tau = k_p(\theta_d - \theta) + k_v(\dot{\theta}_d - \dot{\theta})$$