MST209 2008

(Handbook references are given as page numbers) 1. ln(x) is defined only for x > 0 (page 11) so f(x) is defined for 2 - x > 0 and 3 + x > 0 giving 2 > x and x > -3. Option C.

- 2. Equation 1 is a linear equation and the variables do not separate. Equation 2 is not linear and the variables separate (page 26). Option C.
- 3. Either using the formula or Sarrus's rule, (page 29) the cross-product is

$$(1-(-2 \times 2))i + (2-2)j + ((2 \times -2) - 1)k$$

= 5i - 5k Option A

4. Using page 31, the angle between **W** and **i** is $\frac{\pi}{2} + \theta$ giving the **i**-component of **W** as

$$|\mathbf{W}|\cos\left(\frac{\pi}{2} + \theta\right) = -|\mathbf{W}|\sin(\theta)$$
. Option D.

- 5. Each spring has length l_0 and natural length $2l_0$ so their length is reduced by l_0 . From page 35 PE in a spring is ½ x stiffness x (deformation)². For left-hand spring PE = $\frac{1}{2}4k(l_0)^2 = 2kl_0^2$ For right-hand spring PE= $\frac{1}{2}2k(l_0)^2 = kl_0^2$ Adding these gives total PE = $3kl_0^2$ Option C.
- 6. From first two bullet points at bottom of page 41, the eigenvalues of A^{-3} are $\frac{1}{\lambda^3}$ so we have option D
- 7. Referring to page 43 the correct option is B.
- 8. The correct option is A. (page 44)
- 9. Referring to page 53, [power] = [energy]/[time] = $\frac{ML^2T^{-2}}{T} = ML^2T^{-3}$ Option D.
- 10. $\begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = -2 \begin{bmatrix} 1 \\ -1 \end{bmatrix}$ so the particles will move in the second normal mode which is phase-opposed (page 57) Option C.
- 11. Mass of 3 kg is at Li, mass of 2 kg is at Li + Lj and mass 1 kg is at Lj so centre of mass (page 58) is

$$\frac{3Li+2Li+2Lj+Lj}{3+2+1} = \frac{5L}{6}i + \frac{3L}{6}j$$
. Option A

12. $\mathbf{r}(t) = 2\mathbf{i} + t\mathbf{k}$ and $\dot{\mathbf{r}}(t) = \mathbf{k}$ From page 60, angular momentum $= \mathbf{r} \times m\dot{\mathbf{r}} = (2\mathbf{i} + t\mathbf{k}) \times m\mathbf{k} = -2m\mathbf{k}$ Option C.

13. From page 64,

grad
$$\phi = \frac{\partial \phi}{\partial x} \mathbf{i} + \frac{\partial \phi}{\partial y} \mathbf{j} + \frac{\partial \phi}{\partial z} \mathbf{k} = yz\mathbf{i} + xz\mathbf{j} + xy\mathbf{k}$$

Option C

14. Using page 71

M of I =
$$\int_B f d^2 dV = \int_B c\rho \rho^2 dV$$

= $\int_0^h \int_{-\pi}^{\pi} \int_0^R c\rho^3 \rho d\rho d\theta dz$

(using page 70 but the integrations are in a different order which is permissible) We need the integral the whole way round the cylinder so the limits for θ are $-\pi$ to π . Option C.

- 15. Using item 22 page 73, the graph is linear so the order is 1. Option A.
- 16. The equation is linear so we can use the integrating factor method ((13) page 26)

$$\frac{dy}{dx} + y \tan x = x \cos x$$

$$p = \exp\left(\int \tan x \, dx\right) = \exp(-\ln(\cos x)) = \frac{1}{\cos x}$$

$$= \sec x$$

Multiply equation by $\sec x$

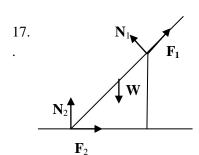
$$\sec x \frac{dy}{dx} + y \sec x \tan x = x$$
$$\frac{d}{dx}(y \sec x) = x$$

Integrating
$$y \sec x = \frac{x^2}{2} + C$$

$$y = \frac{x^2}{2} \cos x + C \cos x$$

$$y(0) = 1 \implies C = 1$$

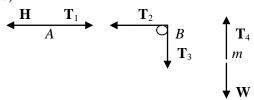
So
$$y = \left(\frac{x^2}{2} + 1\right) \cos x$$
.



N₁ is the normal reaction at the wall
F₁ is the frictional force at the wall
W is the weight of the rod
N₂ is the normal reaction at the floor
F₂ is the frictional force at the floor.

18 a)
$$AB = l - x$$
 and $y + AB = d$
so $y = d - l + x$.

b



 $\mathbf{H} = -k(y-l_0)\mathbf{j}$. By Newton's 3^{rd} law, $|\mathbf{T}_1| = |\mathbf{H}|$ As it is a model pulley, $|\mathbf{T}_2| = |\mathbf{T}_3|$ As it is a model string, $|\mathbf{T}_1| = |\mathbf{T}_2|$ and $|\mathbf{T}_3| = |\mathbf{T}_4|$ So $\mathbf{T}_4 = -k(y-l_0)\mathbf{i}$ $\mathbf{W} = mg\mathbf{i}$ The equation of motion of the mass is $m\ddot{x}\mathbf{i} = \mathbf{W} + \mathbf{T}_4 = mg\mathbf{i} - k(y-l_0)\mathbf{i}$ Resolving in the \mathbf{i} -direction and rearranging gives $m\ddot{x} = mg + kl_0 - k(d-l+x)$

19. (See (11) page 37) The augmented matrix is

$$\begin{pmatrix} 1 & 2 & 0 & 1 \\ 4 & 9 & 3 & 8 \\ -3 & -4 & 8 & 7 \end{pmatrix} \begin{pmatrix} R_1 \\ R_2 \\ R_3 \end{pmatrix}$$

$$\begin{pmatrix} 1 & 2 & 0 & 1 \\ 0 & 1 & 3 & 4 \\ 0 & 2 & 8 & 10 \end{pmatrix} \begin{pmatrix} R_1 \\ R_2 - 4R_1 = R_{2a} \\ R_3 + 3R_1 = R_{3a} \end{pmatrix}$$

$$\begin{pmatrix} 1 & 2 & 0 & 1 \\ 0 & 1 & 3 & 4 \\ 0 & 0 & 2 & 2 \end{pmatrix} \begin{pmatrix} R_1 \\ R_{2a} \\ R_{3a} - 2R_{2a} \\ R_{3a} - 2R_{2a} \end{pmatrix}$$

$$x_1 + 2x_2 = 1$$

$$x_2 + 3x_3 = 1$$

$$2x_3 = 2$$

So $x_3 = 1$, $x_2 = 4 - 3 = 1$ and $x_1 = 1 - 2 = -1$ (Giving $x_1 = -1$, $x_2 = 1$ and $x_3 = 1$) 20. $h_{\text{in}} = 10$, $h_{\text{out}} = 100$, $\kappa = 0.5$, b = 0, $h_a = 10$ $\kappa_l = 0.2$ $b_l = x \times 10^{-3}$

(a) Using the formula from page 51

$$U = \left(\frac{1}{h_{\text{in}}} + \frac{b}{\kappa} + \frac{1}{h_{\text{out}}}\right)^{-1} = \left(\frac{1}{10} + \frac{0.1}{0.5} + \frac{1}{100}\right)^{-1}$$
$$= (0.1 + 0.2 + 0.01)^{-1} = (0.31)^{-1} = \frac{100}{31}$$

b) Adding the lining

$$U_{l} = \left(\frac{1}{h_{in}} + \frac{b}{\kappa} + \frac{1}{h_{a}} + \frac{b_{l}}{\kappa_{l}} + \frac{1}{h_{out}}\right)^{-1}$$

$$U_{l} = \left(0.31 + 0.1 + \frac{0.00x}{0.2}\right)^{-1}$$

$$= (0.41 + .005x)^{-1}$$

(c)
$$U_l = \frac{U}{2}$$
 so $(0.41 + 0.005x)^{-1} = \frac{(0.31)^{-1}}{2}$
 $0.41 + 0.005x = 2(0.31)$
 $0.005x = 0.21$ or $x = 42$ mm

21. (a) Acceleration = $-R\dot{\theta}^2 \mathbf{e}_r = -\frac{v_0^2}{R} \mathbf{e}_r$ as we have motion with constant speed. (page 59)

(b) The only force on the car is the tension in the string so $T = -Te_r$ if T is the magnitude of the tension in string. Applying Newton's second law to the car

$$-T\boldsymbol{e}_r = -\frac{mv_0^2}{R}\boldsymbol{e}_r \quad \text{so} \quad T = \frac{mv_0^2}{R}.$$

For mass the force diagram is where $\mathbf{W} = -Mg\mathbf{k}$ and $\mathbf{T}_1 = T\mathbf{k}$ as the string is a model string and so $|\mathbf{T}| = |\mathbf{T}_1|$. As the mass is stationary $\mathbf{W} + \mathbf{T}_1 = \mathbf{0}$.

So
$$T = \frac{mv_0^2}{R} = Mg$$
 or $v_0 = \sqrt{\frac{MRg}{m}}$.

22 (a)

$$\operatorname{div} \mathbf{V} = \frac{\partial V_{\rho}}{\partial \rho} + \frac{1}{\rho} V_{\rho} + \frac{1}{\rho} \frac{\partial V_{\theta}}{\partial \theta} + \frac{\partial V_{z}}{\partial z} \quad (\text{page 66})$$

$$= -\sin \theta - \sin \theta - \sin \theta = -3 \sin \theta$$

(as
$$V_{\rho} = -\rho \sin \theta$$
, $V_{\theta} = \rho \cos \theta$, $V_{z} = 1$)

(b) **curl V**=
$$\frac{1}{\rho}\begin{bmatrix} \mathbf{e}_{\rho} & \rho \mathbf{e}_{\theta} & \mathbf{e}_{z} \\ \frac{\partial}{\partial \rho} & \frac{\partial}{\partial \theta} & \frac{\partial}{\partial z} \\ -\rho \sin \theta & \rho^{2} \cos \theta & 1 \end{bmatrix}$$
 using the

formula from page 67.

$$= \frac{1}{\rho} \Big((0-0)\mathbf{e}_{\rho} - (0-0)\mathbf{e}_{\theta} + (2\rho\cos\theta + \rho\cos\theta)\mathbf{e}_{z} \Big)$$
$$= 3\cos\theta\,\mathbf{e}_{z}$$

23 (a) Surface area S_a is given by (page 71)

$$\int_{S} \sqrt{1 + \left(\frac{\partial f}{\partial x}\right)^2 + \left(\frac{\partial f}{\partial y}\right)^2} dA = \int_{S} \sqrt{1 + (2x)^2 + (2y)^2} dA$$
as $f(x, y) = x^2 + y^2$.

$$S_a = \int_S \sqrt{1 + 4(x^2 + y^2)} \, dA$$

Using polar co-ordinates $x^2 + y^2 = r^2 \le 2$

so $dA = r dr d\theta$ and $0 \le r \le \sqrt{2}$ and $-\pi < \theta \le \pi$

$$S_a = \int_{-\pi}^{\pi} \int_0^{\sqrt{2}} r\sqrt{1 + 4r^2} dr d\theta$$

(b)
$$S_a = \int_0^{\sqrt{2}} \int_{-\pi}^{\pi} r (1 + 4r^2)^{\frac{1}{2}} d\theta dr$$

(as we can swop the order of integration in multiple integrals)

$$S_a = 2\pi \int_0^{\sqrt{2}} r(1+4r^2)^{\frac{1}{2}} dr$$

Integrations can be done by inspection or by using the substitution (page 23). Let $u = 1 + 4r^2$

then
$$\frac{du}{dr} = 8r$$
. If $r = 0$, $u = 1$ and if $r = \sqrt{2}$, $u = 9$ so

$$S_a = 2\pi \int_1^9 \frac{1}{8} u^{\frac{1}{2}} du = \frac{\pi}{4} \left[\frac{2u^{\frac{3}{2}}}{3} \right]_1^9 = \frac{\pi}{6} (27 - 1) = \frac{13\pi}{3}.$$

24. (a) Auxiliary equation (page 26) is $\lambda^2 + 6\lambda + 9 = 0$ or $(\lambda + 3)^2 = 0$ giving $\lambda = -3$ twice so the complementary function is $y_c = (C + Dt)e^{-3t}$ For particular integral (page 27) a trial solution for $25e^{-2t}$ is ae^{-2t} and a trial solution for 27t is bt + c so we can use the trial solution

$$y = ae^{-2t} + bt + c$$

$$\frac{dy}{dx} = -2ae^{-2t} + b \qquad \frac{d^2y}{dx^2} = 4ae^{-2t}$$

Substituting in the equation and collecting up the terms $ae^{-2t} + 9bt + 6b + 9c = 25e^{-2t} + 27t$

Comparing coefficients gives

$$a = 25$$
, $9b = 27$ and $6b + 9c = 0$
so $b = 3$ and $c = -2$

The particular integral is $y_p = 25e^{-2t} + 3t - 2$

The general solution is

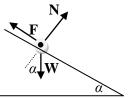
$$y = y_c + y_p = (C + Dt)e^{-3t} + 25e^{-2t} + 3t - 2$$

(b)
$$\dot{y} = -3(C+Dt)e^{-3t} + De^{-3t} - 50e^{-2t} + 3$$

 $y(0) = 0 \implies C + 25 - 2 = 0 \text{ so } C = -23$
 $\dot{y}(0) = 0 \implies -3C + D - 50 + 3 = 0 \implies -3C + D = 47$
So $D = 47 + 3C = 47 - 69 = -22$
 $y = -(23 + 22t)e^{-3t} + 25e^{-2t} + 3t - 2$

(c) As $t \to \infty$ $y \to 3t - 2$ so y increases linearly with t for large t.

25. (a)



 $W = mg \sin \alpha i - mg \cos \alpha j \quad \mathbf{N} = |\mathbf{N}|$ $\mathbf{F} = -|\mathbf{F}|i = -kvi$

(b) $m\mathbf{a} = \mathbf{W} + \mathbf{N} + \mathbf{F}$

Resolving in the i-direction gives

$$ma = mg \sin \alpha - kv$$

or
$$m\frac{dv}{dt} = mg \sin \alpha - kv$$
 (1) as $a = \frac{dv}{dt}$

(c) Terminal speed (page 34) occurs when a = 0 so $mg \sin \alpha$

$$v_T = \frac{mg\sin\alpha}{k}$$

(d) Separating the variables of (1) (page 26) (or could use integrating factor)

$$\frac{1}{mg\sin\alpha - kv}\frac{dv}{dt} = \frac{1}{m}$$

Integrating

$$\int 1/(mg\sin\alpha - kv)dv = \frac{t}{m} + C$$
$$-\frac{1}{k}\ln(mg\sin\alpha - kv) = \frac{t}{m} + C$$

as
$$v = v_0 < v_T = \frac{mg \sin \alpha}{k}$$
 at $t = 0$ and so

$$mg\sin\alpha - kv > 0$$

Also $C = \frac{1}{k} \ln(mg \sin \alpha - kv_0)$, so

$$\frac{t}{m} = \frac{1}{k} \left(\ln(mg \sin \alpha - kv_0) - \ln(mg \sin \alpha - kv) \right)$$
$$\frac{kt}{m} = \ln\left(\frac{mg \sin \alpha - kv_0}{ma \sin \alpha - kv}\right)$$

$$\frac{mg\sin\alpha - kv_0}{mg\sin\alpha - kv} = e^{\frac{kt}{m}}$$

$$mg \sin \alpha - kv = (mg \sin \alpha - kv_0)e^{-\frac{kt}{m}}$$
$$v = \frac{1}{k} \left(mg \sin \alpha - (mg \sin \alpha - kv_0)e^{-\frac{kt}{m}} \right)$$

(e)
$$v = \frac{dx}{dt} = \frac{1}{k} \left(mg \sin \alpha - (mg \sin \alpha - kv_0) e^{-\frac{kt}{m}} \right)$$

Integrating

$$x = \frac{mgt}{k}\sin\alpha + \frac{m}{k^2}(mg\sin\alpha - kv_0)e^{-\frac{kt}{m}} + D$$
When $t = 0$, $x = 0$ so $D = -\frac{m}{k^2}((mg\sin\alpha - kv_0))$

$$x = \frac{mgt}{k}\sin\alpha + \frac{m}{k^2}(mg\sin\alpha - kv_0)\left(e^{-\frac{kt}{m}} - 1\right)$$

26. (a)

$$\begin{bmatrix} \dot{x} \\ \dot{y} \end{bmatrix} = \begin{bmatrix} 5 & -2 \\ -10 & 4 \end{bmatrix} \begin{bmatrix} x \\ y \end{bmatrix}$$
 This is of the correct form if $\mathbf{x} = \begin{bmatrix} x \\ y \end{bmatrix}$ and $\mathbf{A} = \begin{bmatrix} 5 & -2 \\ -10 & 4 \end{bmatrix}$.

(b) Eigenvalues of A (page 41) are given by

$$\begin{vmatrix} 5 - \lambda & -2 \\ -10 & 4 - \lambda \end{vmatrix} = 0$$
 or $(5 - \lambda)(4 - \lambda) - 20 = 0$

Giving $-9\lambda + \lambda^2 = 0$ or $\lambda(\lambda - 9) = 0$

The eigenvalues are $\lambda = 0$ and $\lambda = 9$

For the eigenvectors

$$(5 - \lambda)x - 2y = 0$$
$$-10x + (4 - \lambda)y = 0$$

With $\lambda = 0$ these reduce to

$$5x - 2y = 0$$
 and $-10x + 4y = 0$

Both give $y = \frac{5}{2}x$ and so an eigenvalue is $\begin{bmatrix} 2 & 5 \end{bmatrix}^T$.

With $\lambda = 9$ these reduce to

$$-4x - 2y = 0$$
 and $-10x - 5y = 0$.

Both give y = -2x and so an eigenvalue is $\begin{bmatrix} 1 \\ -2 \end{bmatrix}^T$

From page 43 the solution becomes

$$\mathbf{x} = C_1 \begin{bmatrix} 2 \\ 5 \end{bmatrix} + C_2 \begin{bmatrix} 1 \\ -2 \end{bmatrix} e^{9t}$$

(c) As x = 6 and y = 6 when t = 0, we get

$$6 = 2C_1 + C_2$$
 (1) and $6 = 5C_1 - 2C_2$ (2)

(1) times 2 plus (2) gives $9C_1 = 18$ or $C_1 = 2$

From (1) $C_2 = 6 - 4 = 2$ giving

$$x = 4 + 2e^{9t}$$
 and $y = 10 - 4e^{9t}$

(d) The chemical Y reduces to zero when $10 = 4e^{9t}$ or

$$t = \frac{1}{9} \ln \left(\frac{5}{2} \right)$$

(e) At this time $x = 4 + 2 \times \frac{5}{2} = 9$ as $e^{9t} = \frac{5}{2}$. This is an increase of 50% from 6.

27. (a) At equilibrium (page 47)

$$x\left(1 - \frac{x}{X} - \frac{y}{Y}\right) = 0 \qquad (1)$$

$$y\left(1 - \frac{x}{2X} - \frac{2y}{Y}\right) = 0 \qquad (2)$$

From (1) x = 0 or $x = X\left(1 - \frac{y}{Y}\right)$ Substituting x = 0 in (2) gives $y\left(1 - \frac{2y}{Y}\right) = 0$ So y = 0 or $y = \frac{Y}{2}$ giving points (0,0) and $\left(0, \frac{Y}{2}\right)$. Substituting $x = X\left(1 - \frac{y}{Y}\right)$ (3) into (2) gives $y\left(\frac{1}{2} - \frac{3y}{2Y}\right) = 0$ or y = 0 and $y = \frac{Y}{3}$ Using (3) when y = 0 x = X and when $y = \frac{Y}{3}$ $x = \frac{2X}{3}$ giving points (X, 0) and $\left(\frac{2X}{3}, \frac{Y}{3}\right)$ The equilibrium points are (0,0) $\left(0, \frac{Y}{2}\right)$ $\left(X, 0\right)$ $\left(\frac{2X}{3}, \frac{Y}{3}\right)$

(b) Taking $u = x - \frac{x^2}{x} - xy$ and $v = -y + \frac{xy}{2x} + \frac{2y^2}{y}$ $\frac{\partial u}{\partial x} = 1 - \frac{2x}{X} - \frac{y}{Y} \qquad \frac{\partial v}{\partial x} = \frac{y}{2X}$ $\frac{\partial u}{\partial y} = -\frac{x}{Y} \quad \frac{\partial v}{\partial y} = -1 + \frac{x}{2X} + \frac{4y}{Y}$ $J(x, y) = \begin{bmatrix} 1 - \frac{2x}{X} - \frac{y}{Y} & -\frac{x}{Y} \\ \frac{y}{2X} & -1 + \frac{x}{2X} + \frac{4y}{Y} \end{bmatrix}$

$$\mathbf{J}(0,0) = \begin{bmatrix} 1 & 0 \\ 0 & -1 \end{bmatrix}$$

has eigenvalues 1 and -1. (The eigenvalues of a triangular matrix are the diagonal matrix. Page 41) These are real and distinct and of opposite sign and so (0,0) is a saddle point. (page 47)

$$\mathbf{J}\left(0, \frac{Y}{2}\right) = \begin{bmatrix} \frac{1}{2} & 0\\ \frac{Y}{4Y} & 1 \end{bmatrix}$$

has eigenvalues $\frac{1}{2}$ and 1. These are real and distinct and both positive and so $\left(0, \frac{Y}{2}\right)$ is a source.

$$\mathbf{J}(X,0) = \begin{bmatrix} -1 & -\frac{X}{Y} \\ 0 & -\frac{1}{2} \end{bmatrix}$$

has eigenvalues -1 and $-\frac{1}{2}$. These are real and distinct and both negative so (X, 0) is a sink.

$$J\left(\frac{2X}{3}, \frac{Y}{3}\right) = \begin{bmatrix} -\frac{2}{3} & -\frac{2X}{3Y} \\ \frac{Y}{6X} & \frac{2}{3} \end{bmatrix}$$

The characteristic equation is

$$\left(-\frac{2}{3} - \lambda\right)\left(\frac{2}{3} - \lambda\right) + \frac{1}{9} = 0$$
. This simplifies to $\lambda^2 = \frac{1}{3}$ so $\lambda = \pm \frac{1}{\sqrt{3}}$. These are real and distinct and of opposite sign and so $\left(\frac{2X}{3}, \frac{Y}{3}\right)$ is a saddle point.

28 (a)
$$\mathbf{W} = mg\mathbf{i}$$

$$\mathbf{H} = -k(x - l_0)\mathbf{i} \text{ (page 34)}$$

$$\mathbf{R} = -r(\dot{l})(-\mathbf{i}) = r(\dot{y} - \dot{x})\mathbf{i}$$
 as the length of the damper is $l = y - x$. (page 54) (b) The equation of motion is

mii – W + H + D

$$m\ddot{x}\mathbf{i} = \mathbf{W} + \mathbf{H} + \mathbf{R}$$

Resolving in the i-direction gives

$$m\ddot{x} = mg - k(x - l_0) + r(\dot{y} - \dot{x})$$
 So $m\ddot{x} + r\dot{x} + kx = mg + kl_0 + r\dot{y}$

(c) Using the given values

$$\ddot{x} + 4\dot{x} + 13x = g + 13 + 4\dot{y}$$

and with $\dot{y} = \sin t$, we get

$$\ddot{x} + 4\dot{x} + 13x = g + 13 + 4\sin t$$

A possible trial solution for the particular integral is (using page 27) $x = a + b \sin t + c \cos t$

$$\dot{x} = b \cos t - c \sin t$$
 $\ddot{x} = -b \sin t - c \cos t$
Substituting in the equation

$$-b \sin t - c \cos t + 4b \cos t - 4c \sin t + 13a$$

$$+ 13b \sin t + 13c \cos t$$

$$= g + 13 + 4 \sin t$$

$$13a + (12b - 4c) \sin t + (12c + 4b) \cos t$$

$$= g + 13 + 4 \sin t$$

Equating coefficients $a = \frac{g}{13} + 1$

$$12b - 4c = 4$$
 $12c + 4b = 0 \implies b = -3c$
Substituting in the other equation gives $-40c = 4$
So $c = -\frac{1}{10}$ and $b = \frac{3}{10}$ giving

$$x = \frac{3}{10}\sin t - \frac{1}{10}\cos t + 1 + \frac{g}{13}$$

The amplitude (page 35) is given by

$$\sqrt{\left(\frac{3}{10}\right)^2 + \left(\frac{1}{10}\right)^2} = \frac{1}{\sqrt{10}}$$

29. (a)

As
$$\mu > 0$$
 let $\mu = k^2$ $k > 0$ then the equation becomes
$$\frac{d^2X}{dx^2} + k^2X = 0 \; ,$$

which has general solution (page 35)

$$X = B\cos(kx) + A\sin(kx)$$

$$X' = -kB\sin(kx) + kA\cos(kx)$$

$$X(0) = 0 \Rightarrow B = 0 \quad \frac{dX}{dx}(L) = 0 \Rightarrow kA\cos(kL) = 0$$
As $k \neq 0$ and $A = 0$ gives the trivial solution,
$$\cos(kL) = 0 \quad \text{so } k = \frac{(2n-1)\pi}{2L} \quad \text{giving } \mu = \frac{(2n-1)^2\pi^2}{4L^2}$$
And $X(x) = A_n \sin\left(\frac{(2n-1)\pi x}{2L}\right) \quad n = 1,2,3,...$

b) Using the value for μ above the equation for T is

$$\frac{d^2T}{dt^2} + \frac{(2n-1)^2\pi^2c^2}{4L^2}T = 0$$

Let $b = \frac{(2n-1)\pi c}{2L}$ for convenience then $\frac{d^2T}{dt^2} + b^2T = 0$

This has general solution $T = C \cos(bt) + D \sin(bt)$

$$\frac{dT}{dt} = -bC\sin(bt) + bD\cos(bt)$$

$$\frac{dT}{dt}(0) = 0 \implies D = 0 \text{ so } T(t) = C \cos(bt)$$
$$u(x, t) = X(x)T(t)$$

$$= A_n \sin\left(\frac{(2n-1)\pi x}{2L}\right) \cos\left(\frac{(2n-1)\pi ct}{2L}\right)$$

incorporating the C into A_n .

Adding solutions of this type (page 63 (d))

$$u = \sum_{n=1}^{\infty} A_n \sin\left(\frac{(2n-1)\pi x}{2L}\right) \cos\left(\frac{(2n-1)\pi ct}{2L}\right)$$

c) Initially the string has profile

$$f(x) = \begin{cases} \frac{2dx}{L} & 0 \le x \le \frac{L}{2} \\ d & \frac{L}{2} < x \le L \end{cases}$$

When
$$t = 0$$
 $u = f(x) = \sum_{n=1}^{\infty} A_n \sin\left(\frac{(2n-1)\pi x}{2L}\right)$

The right-hand side is a Fourier sine series (page 61) with some of the terms missing but we can use a similar formula for A_n .

$$A_n = \frac{2}{L} \int_0^L f(x) \sin\left(\frac{(2n-1)\pi x}{2L}\right) dx$$

$$= \frac{2}{L} \left\{ \int_0^L \frac{2dx}{L} \sin\left(\frac{(2n-1)\pi x}{2L}\right) dx + \int_L^L d\sin\left(\frac{(2n-1)\pi x}{2L}\right) dx \right\}$$

$$\begin{split} A_n \\ &= \frac{4d}{L^2} \int_0^{l/2} x \sin\left(\frac{(2n-1)\pi x}{2L}\right) dx \\ &+ \frac{2d}{L} \left[-\frac{2L}{(2n-1)\pi} \cos\left(\frac{(2n-1)\pi x}{2L}\right) \right]_{L/2}^L \\ &= \frac{4d}{L^2} \left[\frac{4L^2}{(2n-1)^2 \pi^2} \sin\left(\frac{(2n-1)\pi x}{2L}\right) - \frac{2Lx}{(2n-1)\pi} \cos\left(\frac{(2n-1)\pi x}{2L}\right) \right]_0^{\frac{L}{2}} \\ &+ \frac{4d}{(2n-1)\pi} \cos\left(\frac{(2n-1)\pi}{4}\right) \end{split}$$

(using the given integral)

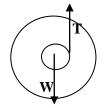
$$= \frac{16d}{(2n-1)^2\pi^2} \sin\left(\frac{(2n-1)\pi}{4}\right)$$

$$-\frac{4d}{(2n-1)\pi} \cos\left(\frac{(2n-1)\pi}{4}\right)$$

$$+\frac{4d}{(2n-1)\pi} \cos\left(\frac{(2n-1)\pi}{4}\right)$$

$$= \frac{16d}{(2n-1)^2\pi^2} \sin\left(\frac{(2n-1)\pi}{4}\right) n = 1,2,3,...$$







c)
$$\mathbf{W} = (2M + m)g\mathbf{i}$$
 $\mathbf{T} = -|\mathbf{T}|\mathbf{i}$

The equation of motion is

$$(2M+m)a = W+T$$

Resolving in the i-direction gives

$$(2M + m)\ddot{x} = (2M + m)g - |T|$$

(Write down means you down have to derive it)

- d) Polar coordinates with the origin at the centre of the axle and θ measured anticlockwise from the horizontal.
- e) The equation of rotational motion is $I\ddot{\theta}\mathbf{k} = \mathbf{r}_T \times \mathbf{T}$ where $\mathbf{r}_T = r\mathbf{j}$ and I is the moment of inertia of the toy about the axle. (page 75) Or $I\ddot{\theta} = (\mathbf{r}_T \times \mathbf{T}) \cdot \mathbf{k}$

f) $x = r\theta$ (as the amount of string unravelled when the toy has rotated an angle θ is $r\theta$)

g)
$$\mathbf{r}_{T} \times \mathbf{T} = r\mathbf{j} \times -|\mathbf{T}|\mathbf{i} = r|\mathbf{T}|\mathbf{k}$$

From e) $I\ddot{\theta} = r|\mathbf{T}|$

From f)
$$\ddot{x} = r\ddot{\theta}$$
 so $|\mathbf{T}| = \frac{I\ddot{x}}{r^2}$

Substitute in c)

$$(2M+m)\ddot{x} = (2M+m)g - I\frac{\ddot{x}}{r^2}$$
 (1)

I = Moment of inertia of discs + Moment of inertia of axle (page 74)

$$I = 2 \times \frac{I}{2}MR^2 + \frac{1}{2mr^2} = MR^2 + \frac{1}{2}mr^2$$

Substituting in (1) and rearranging

$$(2M+m)\ddot{x} + \frac{MR^2 + \frac{1}{2}mr^2}{r^2}\ddot{x} = (2M+m)g$$

$$\left(2Mr^2 + mr^2 + MR^2 + \frac{1}{2}mr^2\right)\ddot{x} = g(2M+m)r^2$$

$$\left(M(R^2 + 2r^2) + \frac{3}{2}mr^2\right)\ddot{x} = g(2M+m)r^2$$

$$\ddot{x} = \frac{g(2M+m)r^2}{\left(M(R^2 + 2r^2) + \frac{3}{2}mr^2\right)}$$