Handbook references are given as (p ) for information only.

- 1.  $\ln(4 x^2)$  is defined only if  $4 x^2 > 0$  which gives  $4 > x^2$  or -2 < x < 2 so the answer is C. (p11)
- 2. 2x + xy = (2 + y)x so the variables are separable and P is correct. The equation is also linear so q is correct. The answer is C. (p26)
- 3. Using formula on page 29 of Handbook, cross product is (4+3)i (2+3)j + (-1+2)k = 7i 5j+k so the answer is C.
- 4. The answer is D
- 5. Each string is extended by length l. PE in AB  $=\frac{1}{2}kl^2$ . PE in AC  $=\frac{3}{2}kl^2$ . PE in CB  $=kl^2$ . Total PE is  $3kl^2$ . The answer is C. (p35)
- 6. No solutions as the final line is inconsistent. (p37) The answer is C.

7. 
$$\begin{bmatrix} -1 & 4 \\ 2 & 1 \end{bmatrix} \begin{bmatrix} 2 \\ -1 \end{bmatrix} = \begin{bmatrix} -6 \\ 3 \end{bmatrix} = -3 \begin{bmatrix} 2 \\ -1 \end{bmatrix}$$
. The eigenvalue is -3. (p41) The answer is D.

- 8. The answer is D. (p45)
- 9.  $J(x, y) = \begin{bmatrix} -qy & 2py qx \\ 2rx & 2sy \end{bmatrix}$  so the answer is D. (p47)
- 10.  $[F] = MLT^{-2}[k] = [F]/[e] = MLT^{-2}/L$  so the answer is C. (p53)
- 11. Centre of mass =  $\frac{1 \times 2l_0 + 1 \times 3l_0}{2 + 1 + 1} = \frac{5l_0}{4}$  so the answer is C. (p58)
- 12. The resultant force will be towards the centre so the answer is B. (p59)

- 13. The function is odd so the answer is D. (p60/61)
- 14.  $\mathbf{r.r} = x^2 + y^2 + z^2$  so the answer is B. (p64)
- 15. Mass=  $\int_{B} r dV = \int_{B} r \times r^{2} \sin\theta d \varphi d\theta dr$  (p70) so the answer is B.
- 16. Separating the variables (p26)  $\frac{2y}{1+y^2} \frac{dy}{dx} = \frac{1}{x^2}$  Integrating  $\ln(1+y^2) = -\frac{1}{x} + C$

y(1) = 0 so 0 = -1 + C or C = 1

Giving  $\ln(1+y^2) = 1 - \frac{1}{x} = (x-1)/x$ Taking exponentials  $1 + y^2 = e^{(1-x)/x}$  $y^2 = e^{\frac{1-x}{x}} - 1 \quad y = \sqrt{e^{\frac{1-x}{x}} - 1}$ 

17.  $N_2 = \sqrt{\frac{1}{x}} - \sqrt{\frac{1}{x}}$ 

 $\mathbf{F}_1$  is the frictional force between the floor and the rod.

 $N_1$  is the normal reaction between the floor and the rod.

 $\mathbf{F}_2$  is the frictional force between the cylinder and the rod.

 $N_2$  is the normal reaction between the cylinder and the rod.

**W** is the weight of the rod.

b)  $\mathbf{H}_1 = -k(x - l_0)\mathbf{i}$  (p34)  $\mathbf{H}_2 = -k(4l_0 - x - 2l_0)(-\mathbf{i})$  $= k(2l_0 - x)\mathbf{i}$ 

- c) Equation of motion is  $m\ddot{x}i = \mathbf{H}_1 + \mathbf{H}_2$  (N2)
- (p33) Resolve in the **i**-direction

$$m\ddot{x} = -k(x - l_0) + k(2l_0 - x)$$
  
$$m\ddot{x} + 2kx = 3l_0k$$

19. a) 
$$\begin{bmatrix} 3 & 8 \\ 3 & 1 \end{bmatrix} \begin{bmatrix} 1 \\ 0.5 \end{bmatrix} = \begin{bmatrix} 7 \\ 3.5 \end{bmatrix} = 7 \begin{bmatrix} 1 \\ 0.5 \end{bmatrix}$$
  
$$\begin{bmatrix} 3 & 8 \\ 3 & 1 \end{bmatrix} \begin{bmatrix} 1 \\ -0.75 \end{bmatrix} = \begin{bmatrix} -3 \\ 2.25 \end{bmatrix} = -3 \begin{bmatrix} 1 \\ -0.75 \end{bmatrix}$$

The method is direct iteration and converges to the eigenvector with the largest eigenvalue (which is 7) so this will be  $\begin{bmatrix} 1 & 0.5 \end{bmatrix}^T$ . (p24)

- b) No as  $e_0 = 4 \begin{bmatrix} 1 \\ -0.75 \end{bmatrix}$  so it is already an eigenvector.
- 20. a) Using the constant acceleration formulae with  $a_0 = -g$  and  $v_0 = u$ ,  $v^2 u^2 = -2gx$  (p33) but v = 0 when x = h so  $u^2 = 2gh$  or  $u = \sqrt{2gh}$

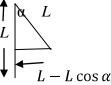
Alternatively you could use conservation of energy.(p35)

- b) Maximum Range =  $u^2/g$  ( Handbook page 49) so maximum range is 2h.
- 21. a) Let u be the speed of the bullet plus wood just after impact. Then by conservation of momentum  $mv_0 = (m+M)u$  or  $u = \frac{mv_0}{m+M}$  (p58)
- b) Taking the datum for the potential energy as the initial height of the block

KE at impact 
$$\frac{=\frac{1}{2}(M+m)(m^2v_0^2)}{(m+M)^2} = \frac{m^2v_0^2}{2(m+M)}$$
 (p35)  
PE at impact = 0

When they come to rest
$$KE = 0$$

$$PE = (m + M)gL(1 - \cos \alpha)$$



By conservation of energy

$$\frac{m^2 v_0^2}{2(m+M)} = (m+M)gL(1-\cos\alpha)$$
So  $v_0^2 = 2(m+M)^2 L(1-\cos\alpha)/m^2$ 

$$\Rightarrow v_0 = \frac{m+M}{m} \sqrt{2gL(1-\cos\alpha)}$$

div 
$$\mathbf{V} = \frac{1}{\rho} \frac{\partial}{\partial \rho} (\rho V_{\rho}) + \frac{1}{\rho} \frac{\partial}{\partial \theta} (V_{\theta}) + \frac{\partial}{\partial z} (V_{z}) \text{ (p67)}$$
  

$$= \frac{1}{\rho} \frac{\partial}{\partial \rho} (\rho^{3} \cos \theta) + \frac{1}{\rho} \frac{\partial}{\partial \theta} (-\sin \theta)$$

$$= 3\rho \cos \theta - \frac{1}{\rho} \cos \theta$$
b) **curl**  $\mathbf{V} = \frac{1}{\rho} \begin{vmatrix} \mathbf{e}_{\rho} & \rho \mathbf{e}_{\theta} & \mathbf{e}_{z} \\ \frac{\partial}{\partial \rho} & \frac{\partial}{\partial \theta} & \frac{\partial}{\partial z} \\ \rho^{2} \cos \theta & -\rho \sin \theta & 0 \end{vmatrix} \text{ (p67)}$ 

$$= \frac{1}{\rho} (0 \mathbf{e}_{\rho} + 0 \mathbf{e}_{\theta} + (-\sin \theta + \rho^{2} \sin \theta) \mathbf{e}_{z})$$

$$\mathbf{Curl} \mathbf{V} = \frac{1}{\rho} (\rho^{2} - 1) \sin \theta \mathbf{e}_{z}$$

- 23. **Note** There is an error in the exam paper and  $Y_N$  for step size 0.01 should be 1.015. This should be obvious from the diagrams.
- a) From the graph the likely order is second order as the graph of  $Y_N$  against  $h^2$  is almost linear.
- b) p = 2 (as  $2^{nd}$  order) (p73)

To achieve 6 dp accuracy we need

$$|Ch^{p}| \le 0.5 \times 10^{-6} \quad (1)$$
And  $Y_{N_{1}} - Y_{N_{2}} \cong C(h_{1}^{p} - h_{2}^{p})$ 
Giving  $1.000 - 1.015 \cong C(0.02^{2} - 0.01^{2})$ 

$$-0.015 \cong C(0.0004 - 0.0001)$$

$$C \cong -\frac{0.015}{0.0003} = -50$$

So substituting in (1)  $50h^2 \le 0.5 \times 10^{-6}$   $\Rightarrow h^2 \le 10^{-8} \Rightarrow h \le 10^{-4}$ The upper bound is  $10^4$ .

24. Auxiliary equation is  $2\lambda^2 + 6\lambda + 5 = 0$  (p26) So  $\lambda = \frac{-6 \pm \sqrt{36 - 40}}{4} = -\frac{3}{2} \mp \frac{1}{2}i$ 

Giving the complementary function as

$$y_c = e^{-\frac{3}{2}t} \left( C\cos\left(\frac{t}{2}\right) + D\sin\left(\frac{t}{2}\right) \right)$$

24. (cont) For particular integral try (p27)

$$y = p\cos\left(\frac{t}{2}\right) + q\sin\left(\frac{t}{2}\right)$$
$$\frac{dy}{dt} = -\frac{1}{2}p\sin\left(\frac{t}{2}\right) + \frac{1}{2}q\cos\left(\frac{t}{2}\right)$$
$$\frac{d^2y}{dt^2} = -\frac{1}{4}p\cos\left(\frac{t}{2}\right) - \frac{1}{4}q\sin\left(\frac{t}{2}\right)$$

Substituting into the equation gives

$$-\frac{1}{2}p\cos\left(\frac{t}{2}\right) - \frac{1}{2}q\sin\left(\frac{t}{2}\right) - 3p\sin\left(\frac{t}{2}\right)$$
$$+3q\cos\left(\frac{t}{2}\right) + 5p\cos\left(\frac{t}{2}\right) + 5q\sin\left(\frac{t}{2}\right)$$
$$= 39\sin\left(\frac{t}{2}\right)$$

Giving

$$\left(\frac{9}{2}p + 3q\right)\cos\left(\frac{t}{2}\right) + \left(\frac{9}{2}q - 3p\right)\sin\left(\frac{t}{2}\right)$$

$$= 39\sin\left(\frac{t}{2}\right)$$

Equating coefficients  $\frac{9}{2}p + 3q = 0 \Rightarrow q = -\frac{3}{2}p$ and  $\frac{9}{2}q - 3p = 39$  or  $\frac{3}{2}q - p = 13$ which becomes  $-\frac{9}{4}p - p = 13$ 

giving 
$$p = -4$$
 and  $q = 6$ 

so 
$$y_p = -4\cos\left(\frac{t}{2}\right) + 6\sin\left(\frac{t}{2}\right)$$

$$y = y_c + y_p \quad (p27)$$

$$y = e^{-\frac{3}{2}t} \left( C\cos\left(\frac{t}{2}\right) + D\sin\left(\frac{t}{2}\right) \right) - 4\cos\left(\frac{t}{2}\right)$$

$$+6\sin\left(\frac{t}{2}\right)$$

b) 
$$\frac{dy}{dt} = -\frac{3}{2}e^{-\frac{3}{2}t}\left(C\cos\left(\frac{t}{2}\right) + D\sin\left(\frac{t}{2}\right)\right) + e^{-\frac{3}{2}t}\left(-\frac{1}{2}C\sin\left(\frac{t}{2}\right) + \frac{1}{2}D\cos\left(\frac{t}{2}\right)\right)$$

$$-4\cos\left(\frac{t}{2}\right) + 6\sin\left(\frac{t}{2}\right)$$

$$y(0) = -1 \Rightarrow C - 4 = -1 \Rightarrow C = 3$$

$$\frac{dy(0)}{dx} = 1 \implies \frac{1}{2}D - \frac{3}{2}C + 3 = 1 \implies D = 5$$

The particular solution is

$$y = e^{-\frac{3}{2}t} (3\cos\left(\frac{t}{2}\right) + 5\sin\left(\frac{t}{2}\right)) - 4\cos\left(\frac{t}{2}\right) + 6\sin\left(\frac{t}{2}\right)$$

25. a)  $i \mid R \mid W$ 

$$\mathbf{R} = -kv^2\mathbf{i}$$
  $\mathbf{W} = -mg\mathbf{i}$ 

b) Equation of motion is ma = R + W (N2) (p33) Resolving in the **i-**direction  $ma = -kv^2 - mg$ 

Using  $a = v \frac{dv}{dx}$  and dividing by m gives

$$v\frac{dv}{dx} = -\frac{k}{m}(v^2 + mg) = -\frac{g}{\lambda^2}(\lambda^2 + v^2)$$
as  $\lambda = \sqrt{\frac{mg}{k}}$ 

c) Separating the variables (p26)

$$\frac{v}{\lambda^2 + v^2} \frac{dv}{dx} = -\frac{g}{\lambda^2}$$

Integrating  $\frac{1}{2}\ln(\lambda^2 + v^2) = -\frac{g}{\lambda^2}x + C$ 

where C is the constant of integration.

When 
$$x = 0$$
  $v = v_0$  so  $C = \frac{1}{2} \ln(\lambda^2 + v_0^2)$  so

$$\frac{1}{2}\ln(\lambda^2 + v^2) - \frac{1}{2}\ln(\lambda^2 + v_0^2) = -\frac{g}{\lambda^2}x$$

or 
$$\ln((\lambda^2 + v^2)/(\lambda^2 + v_0^2)) = -2gx/\lambda^2$$
 (1)

Taking exponentials gives  $\frac{\lambda^2 + v^2}{\lambda^2 + v_0^2} = e^{-\frac{2gx}{\lambda^2}}$ 

So 
$$v = \sqrt{(\lambda^2 + v_0^2)e^{-\frac{2gx}{\lambda^2}} - \lambda^2}$$
.

At greatest height v = 0 so from (1)

$$x = -\frac{\lambda^2}{2g} \ln \left( \frac{\lambda^2}{\lambda^2 + v_0^2} \right) = \frac{\lambda^2}{2g} \ln \left( \frac{\lambda^2 + v_0^2}{\lambda^2} \right) (2)$$

 $\mathbf{i} \downarrow \qquad \mathbf{R} \qquad \mathbf{R} = -kv^2\mathbf{i}$   $\mathbf{W} \qquad \mathbf{W} = mg\mathbf{i}$ 

The equation of motion is ma = R + WResolving in the **i**-direction gives

$$ma = -kv^2 + mg$$

e) At terminal speed a = 0 (Handbook page 34)

so 
$$v_T^2 = \frac{mg}{k}$$
 or  $v_T = \sqrt{\frac{mg}{k}} = \lambda$ 

f) The equation of motion becomes

$$v\frac{dv}{dx} = \frac{g}{\lambda^2}(\lambda^2 - v^2)$$

Separating the variables

$$\frac{v}{\lambda^2 - v^2} \frac{dv}{dx} = \frac{g}{\lambda^2}$$

Integrating  $-\frac{1}{2}\ln(\lambda^2 - v^2) = \frac{g}{\lambda^2}x + D$ 

When x = 0 v = 0 and so  $D = -\frac{1}{2} \ln \lambda^2$ 

$$x = -\frac{\lambda^2}{2g} \ln \left( \frac{\lambda^2 - v^2}{\lambda^2} \right)$$
 (3)

From (2) and using  $v_0 = \lambda$  the particle will return to its original position when  $x = \frac{\lambda^2}{2g} \ln \frac{\lambda^2 + \lambda^2}{\lambda^2} = \frac{\lambda^2}{2g} \ln 2$ 

Substituting in (3) gives  $\ln\left(\frac{\lambda^2 - \nu^2}{\lambda^2}\right) = -\ln 2$ 

Giving 
$$\frac{\lambda^2 - v^2}{\lambda^2} = \frac{1}{2}$$
 or  $v^2 = \frac{\lambda^2}{2} \Rightarrow v = \frac{\lambda}{\sqrt{2}} = \frac{v_T}{\sqrt{2}}$ 

26.a) 
$$\begin{bmatrix} \dot{x} \\ \dot{y} \end{bmatrix} = \begin{bmatrix} -3 & 1 \\ 3 & -5 \end{bmatrix} \begin{bmatrix} x \\ y \end{bmatrix} + \begin{bmatrix} 36t \\ 0 \end{bmatrix}$$

b) For eigenvalues 
$$\begin{vmatrix} -3 - \lambda & 1 \\ 3 & -5 - \lambda \end{vmatrix} = 0$$

so 
$$\lambda^2 + 8\lambda + 12 = 0$$
 which factorises to

$$(\lambda + 6)(\lambda + 2) = 0$$

So the eigenvalues are  $\lambda = -6$  and  $\lambda = -2$ 

When  $\lambda = -6$  the eigenvectors are given by

$$\begin{bmatrix} 3 & 1 \\ 3 & 1 \end{bmatrix} \begin{bmatrix} x \\ y \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \end{bmatrix} \text{ or } 3x + y = 0 \text{ so a possible}$$
 eigenvector is  $\begin{bmatrix} 1 & -3 \end{bmatrix}^T$ 

When  $\lambda = -2$  the eigenvectors are given by

$$\begin{bmatrix} -1 & 1 \\ 3 & -3 \end{bmatrix} \begin{bmatrix} x \\ y \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \end{bmatrix} \text{ or } x - y = 0 \text{ so a possible}$$
 eigenvector is  $\begin{bmatrix} 1 & 1 \end{bmatrix}^T$ .

The complementary function is

$$\begin{bmatrix} x \\ y \end{bmatrix} = C_1 \begin{bmatrix} 1 \\ 1 \end{bmatrix} e^{-2t} + C_2 \begin{bmatrix} 1 \\ -3 \end{bmatrix} e^{-6t}$$

c) For particular integral try  $\begin{bmatrix} x \\ y \end{bmatrix} = \begin{bmatrix} at + b \\ ct + d \end{bmatrix}$ 

Substituting in the equations

$$a = -3(at + b) + ct + d + 36t$$
$$c = 3(at + b) - 5(ct + d)$$

Collecting terms

$$(3a - c - 36)t + a + 3b - d = 0$$
$$(5c - 3a)t + c - 3b + 5d = 0$$

Equating coefficients of t gives

$$3a - c = 36$$
 (1) and  $5c - 3a = 0$  (2)

Substituting (1) into (2) gives  $3a - \frac{3a}{5} = 36$ 

$$\Rightarrow a = 15 \Rightarrow c = 9$$

Equating the constants gives

$$a + 3b - d = 0$$
 or  $3b - d = -15$  (3)

$$c - 3b + 5d = 0$$
 or  $3b - 5d = 9$  (4)

Subtracting (4) from (3) gives 4d = -24 or d = -6 and substituting in (3) gives b = -7 Giving the particular solution

$$\begin{bmatrix} x_p \\ y_p \end{bmatrix} = \begin{bmatrix} 15t - 7 \\ 9t - 6 \end{bmatrix}$$

And a general solution

$$\begin{bmatrix} x \\ y \end{bmatrix} = C_1 \begin{bmatrix} 1 \\ 1 \end{bmatrix} e^{-2t} + C_2 \begin{bmatrix} 1 \\ -3 \end{bmatrix} e^{-6t} + \begin{bmatrix} 15t - 7 \\ 9t - 6 \end{bmatrix}$$

d) Using x(0) = 3 and y(0) = 0 gives

$$\begin{bmatrix} 3 \\ 0 \end{bmatrix} = C_1 \begin{bmatrix} 1 \\ 1 \end{bmatrix} + C_2 \begin{bmatrix} 1 \\ -3 \end{bmatrix} + \begin{bmatrix} -7 \\ -6 \end{bmatrix}$$

Or 
$$C_1 + C_2 = 10$$
 and  $C_1 - C_2 = 6$ 

Subtracting  $4C_2 = 4$  so  $C_2 = 1$ 

Substituting in the first equation gives  $C_1 = 9$ 

$${x \brack y} = 9 \begin{bmatrix} 1 \\ 1 \end{bmatrix} e^{-2t} + \begin{bmatrix} 1 \\ -3 \end{bmatrix} e^{-6t} + \begin{bmatrix} 15t - 7 \\ 9t - 6 \end{bmatrix}$$

e) In the long term the exponentials tend to zero and the population will grow linearly in the proportion 15:9.

27. Let  $\theta_{in}$  be the temperature inside the pipe

 $\theta_1$  the temperature on the inside surface of the pipe  $\theta_2$  the temperature on the outside surface of the pipe  $\theta_3$  the temperature on the outside surface of the lagging

 $\theta_{\rm out}$  the temperature of the air around the pipe. Using the formula given in the question for the pipe  $q=-\kappa A\frac{d\theta}{dr}$ , replacing A by  $2\pi rL$  and rearranging we get

$$\frac{d\theta}{dr} = -\frac{q}{2\kappa L\pi r}$$

Integrating assuming q is constant

$$\theta = -\frac{q}{2\kappa L\pi} \ln r + C$$

$$\theta = \theta_2$$
 when  $r = R$  so  $C = \theta_2 + \frac{q}{2\kappa L\pi} \ln R$ 

27. (cont)

Giving 
$$\theta - \theta_2 = \frac{q}{2\kappa L\pi} \ln\left(\frac{R}{r}\right)$$

Now if we take  $\theta = \theta_1$  at radius r, we have

$$\theta_1 - \theta_2 = \frac{q}{2\kappa L\pi} \ln\left(\frac{R}{r}\right) \tag{1}$$

Similarly for the lagging

$$\theta_2 - \theta_3 = \frac{q}{2\kappa_{lag}L\pi} \ln\left(\frac{R+d}{R}\right)$$
 (2)

Using the given formula for the heat transfer at the surface of the pipe applied to the inside of the pipe with the above definitions of temperatures,

$$\theta_{\rm in} - \theta_1 = \frac{q}{2\pi Lr h_{\rm in}} \tag{3}$$

And the outside of the pipe

$$\theta_3 - \theta_{\text{out}} = \frac{q}{2\pi L(R+d)h_{\text{out}}}$$
 (4)

Adding (3), (1), (2) and (4) we get

$$\theta_{\rm in} - \theta_{\rm out} = \frac{q}{2\pi L} \left( \frac{1}{rh_{\rm in}} + \frac{1}{\kappa} \ln\left(\frac{R}{r}\right) + \frac{1}{\kappa_{lag}} \ln\left(\frac{R+d}{R}\right) + \frac{1}{(R+d)h_{\rm out}} \right)$$

which rearranges to give the required result.

b) For maximum q we need to minimise

$$U = \left(\frac{1}{rh_{\text{in}}} + \frac{1}{\kappa} \ln \left(\frac{R}{r}\right) + \frac{1}{\kappa_{lag}} \ln \left(\frac{R+d}{R}\right) + \frac{1}{(R+d)h_{\text{out}}}\right)$$

with respect to d.

$$\frac{dU}{dd} = \frac{1}{\kappa_{\text{lag}}} \frac{1}{R+d} - \frac{1}{(R+d)^2 h_{\text{out}}}$$
$$= \frac{\left(\frac{R+d}{\kappa_{\text{lag}}} - \frac{1}{h_{\text{out}}}\right)}{(R+d)^2}$$

For a minimum and therefore q a maximum this needs to be zero so  $d = \frac{\kappa_{\text{lag}}}{h_{\text{out}}} - R$  (which is valid because of the inequality given in the question.)

28. a) 
$$\mathbf{H}_{3}$$
  $\mathbf{H}_{3}$   $\mathbf{H}_{3}$   $\mathbf{W}_{1}$   $\mathbf{H}_{2}$   $\mathbf{W}_{2}$   $\mathbf{H}_{4}$ 

b) Using the delta forces (p57)

$$\Delta H_1 = -k_1 x_1 i$$
  
 $\Delta H_2 = -k_2 (x_2 - x_1)(-i) = k_2 (x_2 - x_1) i$ 

$$\Delta H_3 = -\Delta H_2 = -k_2(x_2 - x_1)i$$
 (N3)

$$\Delta H_4 = -k_3(-x_2)(-i) = -k_3x_2i$$

Equation of motion for  $m_1$  is  $m_1\ddot{x}_1\mathbf{i} = \Delta\mathbf{H}_1 + \Delta\mathbf{H}_2$ 

Resolving in the **i**-direction gives

$$m_1\ddot{x}_1 = -k_1x_1 + k_2(x_2 - x_1) \quad (1)$$

Equation of motion for  $m_2$  is  $m_2\ddot{x}_2\mathbf{i} = \Delta\mathbf{H}_3 + \Delta\mathbf{H}_4$ 

Resolving in the i-direction gives

$$m_2\ddot{x}_2 = -k_2(x_2 - x_1) - k_3x_2$$
 (2)

c) (1) becomes 
$$\ddot{x}_1 = -\frac{k_1 + k_2}{m_1} x_1 + \frac{k_2}{m_2} x_2$$

after collecting terms and dividing by  $m_1$ 

Similarly (2) becomes 
$$\ddot{x}_2 = \frac{k_2}{m_2} x_1 - \frac{k_2 + k_3}{m_2} x_2$$

Putting them in matrix form

$$\begin{bmatrix} \ddot{x}_1 \\ \ddot{x}_2 \end{bmatrix} = \begin{bmatrix} -\frac{k_1 + k_2}{m_1} & \frac{k_2}{m_1} \\ \frac{k_2}{m_2} & -\frac{k_2 + k_3}{m_2} \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix}$$

which gives the required dynamic matrix. (p56)

d) The dynamic matrix becomes  $\begin{bmatrix} -2 & 1 \\ 1 & -2 \end{bmatrix}$ 

For the eigenvalues  $\begin{vmatrix} -2 - \lambda & 1 \\ 1 & -2 - \lambda \end{vmatrix} = 0$  (p41)

so 
$$\lambda^2 + 4\lambda + 3 = 0$$

Factorising  $(\lambda + 3)(\lambda + 1) = 0$ 

The eigenvalues are  $\lambda = -3$  and  $\lambda = -1$ 

So the normal mode angular frequencies are

1 and  $\sqrt{3}$ 

e) For eigenvectors for  $\lambda = -3$ 

$$\begin{bmatrix} 1 & 1 \\ 1 & 1 \end{bmatrix} \begin{bmatrix} u \\ v \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \end{bmatrix} \text{ so } u + v = 0$$

A typical eigenvector is  $\begin{bmatrix} 1 \\ -1 \end{bmatrix}^T$ 

For eigenvectors for  $\lambda = -1$ 

$$\begin{bmatrix} -1 & 1 \\ 1 & -1 \end{bmatrix} \begin{bmatrix} u \\ v \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \end{bmatrix} \text{ so } u - v = 0$$

A typical eigenvector is  $[1 1]^T$ 

28. e) The general solution is

$$\begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = \begin{bmatrix} 1 \\ 1 \end{bmatrix} (A\cos t + B\sin t) 
+ \begin{bmatrix} 1 \\ -1 \end{bmatrix} (C\cos\sqrt{3}t + D\sin\sqrt{3}t) 
= \begin{bmatrix} 1 \\ 1 \end{bmatrix} C_1 \cos(t + \varphi_1) + \begin{bmatrix} 1 \\ -1 \end{bmatrix} C_2 \cos(\sqrt{3}t + \varphi_1)$$
(p57)

28. (cont)

f) As the vector  $\begin{bmatrix} 0.1\\ -0.1 \end{bmatrix}$  is an eigenvector corresponding to  $\lambda=-3$ , the particles will oscillate with angular frequency  $\sqrt{3}$  out of phase.

29. a) 
$$u(x,y) = X(x)Y(y)$$
So  $\frac{\partial^2 u}{\partial x^2} = X''(x)Y(y)$  and  $\frac{\partial^2 u}{\partial y^2} = X(x)Y''(y)$ 

Substituting in the equation X''Y + XY'' = 0

Divide by XY and rearrange  $\frac{X''}{X} = -\frac{Y''}{Y} = -\mu$  where  $\mu$  is a constant.

So 
$$X'' + \mu X = 0$$
 and  $Y'' - \mu Y = 0$  (as required)  
 $u(x, 0) = 0 \Rightarrow X(x)Y(0) = 0 \Rightarrow Y(0) = 0$ 

Similarly  $u(x, a) = 0 \Rightarrow Y(a) = 0$ 

b) If  $\mu > 0$  let  $\mu = k^2$  where k > 0 so  $Y'' - k^2Y = 0$  which has solution  $Y = Ae^{ky} + Be^{-ky}$ 

$$Y(0) = 0 \Rightarrow A + B = 0 \Rightarrow B = -A$$

$$Y(a) = 0 \Rightarrow Ae^{ka} + Be^{-ka} = 0 \Rightarrow A(e^{ka} - e^{-ka}) = 0$$

$$k \neq 0 \text{ so the breeket is not zero} \Rightarrow A = 0 \Rightarrow B = 0$$

 $k \neq 0$  so the bracket is not zero  $\Rightarrow A = 0 \Rightarrow B = 0$  so only trivial solution.

If 
$$\mu = 0$$
  $Y'' = 0$  and  $Y = Cy + D$ 

$$Y(0) = 0 \Rightarrow D = 0$$
 and  $Y(a) = 0 \Rightarrow Ca = 0 \Rightarrow C = 0$   
So only trivial solution.

If 
$$\mu < 0$$
 let  $\mu = -k^2$  where  $k > 0$  so  $Y'' + k^2 Y = 0$ 

which has solution  $Y = E \cos ky + F \sin ky$ 

$$Y(0) = 0 \Rightarrow E = 0 \text{ and } Y(a) = 0 \Rightarrow F \sin ka = 0$$

F = 0 gives the trivial solution so

$$\sin ka = 0 \implies ka = r\pi \implies k = \frac{r\pi}{a} \implies \mu = -\frac{r^2\pi^2}{a^2}$$

The solution is  $Y = E \sin \frac{r\pi y}{a}$ 

c) 
$$X'' - \mu X = 0 \Rightarrow X'' - \frac{r^2 \pi^2}{a^2} X = 0$$

$$\Rightarrow X = Ge^{\frac{r\pi x}{a}} + He^{-\frac{r\pi x}{a}}$$

$$u(x,y) \to 0 \text{ as } x \to \infty \text{ so } X(x) \to 0 \text{ as } x \to \infty$$

$$\Rightarrow G = 0 \Rightarrow X = He^{\frac{-r\pi x}{a}}.$$

For each r  $u_r(x,y) = XY = B_r e^{-\frac{r\pi x}{a}} \sin \frac{r\pi y}{a}$  where  $B_r = FH$ .

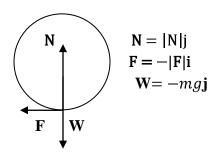
Using the principle of superposition

$$u(x,y) = \sum_{r=1}^{\infty} B_r e^{-\frac{r\pi x}{a}} \sin \frac{r\pi y}{a}$$

d) 
$$u(0, y) = f(y) = \sum_{r=1}^{\infty} B_r \sin \frac{r\pi y}{g}$$

Using the Fourier sine series of f(y) (Handbook 61)  $B_r = \frac{2}{a} \int_0^a f(y) \sin \frac{r\pi y}{a} dy.$ 

30. a)



b) The equation of motion of the centre of mass is  $M\ddot{\mathbf{x}} = \mathbf{N} + \mathbf{F} + \mathbf{W}$ . Resolving in the **j**-direction  $|\mathbf{N}| - Mg = 0 \Rightarrow |\mathbf{N}| = Mg$ 

As we have kinetic friction  $|F| = \mu |N| = \mu Mg$ Substituting in the equation of motion and cancelling M we get  $\ddot{x} = -\mu gi$  (1)

c) As suggested we use the equation of relative rotational motion (Handbook 75)  $I\ddot{\theta} = \Gamma_a^{rel}$  (2) and  $\Gamma^{rel} = -R\mathbf{j} \times \mathbf{F} = -R\mathbf{j} \times -\mu Mg\mathbf{i} = -\mu RMg\mathbf{k}$   $I = \frac{2}{5}MR^2$  (Handbook 74)

Substituting in (2)  $\frac{2}{5}MR^2\ddot{\theta} = -\mu RMg$  or  $\ddot{\theta} = -\frac{5\mu g}{2R}$ 

d)Resolving (1) in the **i**-direction gives  $\ddot{x} = -\mu g$ Integrating  $\dot{x} = -\mu gt + C$  but  $\dot{x} = v_0$  when t = 0 $\Rightarrow C = v_0 \Rightarrow \dot{x} = -\mu gt + v_0$  (3).

Integrating  $\ddot{\theta} = -\frac{5\mu g}{2R}$  gives  $\dot{\theta} = -\frac{5\mu g}{2R}t + D$  and

 $\dot{\theta} = 0$  when  $t = 0 \Rightarrow D = 0$ 

 $\dot{x} + R\dot{\theta} = -\frac{7\mu gt}{2} + v_0$  and  $\dot{x} + R\dot{\theta} = 0$  when

 $t = \frac{2v_0}{7\mu g}$ 

e) Integrating (3) using x = 0 when t = 0 gives

$$x = -\frac{\mu g t^2}{2} + v_0 t$$
. At  $t = \frac{2v_0}{7\mu g} x = \frac{12v_0^2}{49\mu g}$ 

At 
$$t = \frac{2v_0}{7\mu g}$$
  $\dot{\theta} = -\frac{5\mu g}{2R} \frac{2v_0}{7\mu g} = -\frac{5v_0}{7R}$ 

Angular speed is  $\frac{5v_0}{7R}$  as required and the distance the sphere slips is  $\frac{12v_0^2}{49\mu g}$ .