



A new viscoelastic constitutive model for continuous media at finite thermomechanical changes.

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Motivation and overview

Motivation



Figure 1: Rubber-like materials.

e.g. Melting point of Polypropylene (PP) varies from $130 - 171^{\circ}\text{C}$.

Motivation



Figure 1: Rubber-like materials.

e.g. Melting point of Polypropylene (PP) varies from $130 - 171^{\circ}\text{C}$.
Thermo-visco-elastic model is essential to model rubber-like materials.

Overview (1/2)

Main points from the article:

- Thermomechanical visco-elastic model,
- Highly deformable with viscous dissipation,
- Concept: **internal state variable** and **rational thermodynamics**,
- Goal: constitutive eqns. for **stress**, **entropy** and **internal variables**,
- 2^{nd} law of thermodynamics satisfied,
- Decomposition of deformation into **dilatational** and **deviatoric** part,
- Formulated entirely in **reference configuration**,
- Numerically easy to handle.

Overview (2/2)

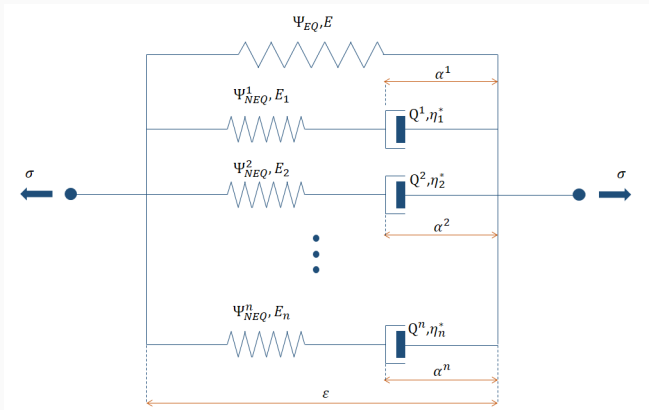


Figure 2: Generalized Maxwell model - 1D rheological interpretation.

where α^i, η_i^*, Q^i is inelastic strain, viscous coefficient and stress of dashpot i^{th} , respectively; E^i is spring stiffness. ($i = 1, 2, ..n$)

Mathematical Model

2nd law of thermodynamics in terms of ref. config. reads:

$$-\rho_0(\dot{\Psi} + \dot{\Theta}\eta) + \mathbf{S} \cdot \dot{\mathbf{E}} - \frac{1}{\Theta} q_0 \text{Grad}\Theta \geq 0 \quad (1)$$

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Time derivative of free energy function $\Psi(\mathbf{E}, \Theta, \text{Grad}\Theta)$ reads:

$$\dot{\Psi} = \frac{\partial \Psi}{\partial \mathbf{E}} \cdot \dot{\mathbf{E}} + \frac{\partial \Psi}{\partial \Theta} \cdot \dot{\Theta} + \frac{\partial \Psi}{\partial \text{Grad}\Theta} \cdot \text{Grad}\dot{\Theta} \quad (2)$$

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Substitution equation (1) into inequality (2) yields:

$$-\rho_0\left(\eta + \frac{\partial \Psi}{\partial \Theta}\right)\dot{\Theta} + \left(\mathbf{S} - \rho_0 \frac{\partial \Psi}{\partial \mathbf{E}}\right) \cdot \dot{\mathbf{E}} - \rho_0 \frac{\partial \Psi}{\partial \text{Grad}\Theta} \cdot \text{Grad}\dot{\Theta} - \frac{1}{\Theta} q_0 \text{Grad}\Theta \geq 0 \quad (3)$$

Preliminary

2nd law of thermodynamics in terms of ref. config. reads:

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Since 2nd law must hold for any admissible process, we conclude:

$\mathbf{S} = \partial_{\mathbf{E}} \Psi$

(4)

$\eta = -\partial_{\Theta} \Psi$

(5)

Mathematical Model (1/5)

Thermoviscoelastic model defined by Helmholtz-free energy function:

$$\Psi = \underbrace{\Psi_{EQ}(\mathbf{C}, \Theta)}_{\text{purely thermoelastic}} + \underbrace{\Psi_{NEQ}(\mathbf{C}, \Theta, \alpha_i)}_{\text{non-equilibrium part}} \quad (6)$$

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Coleman's exploitation yields:

$$\mathbf{S} = \partial_{\mathbf{C}} \Psi = 2\partial_{\mathbf{C}} \Psi_{EQ}(\mathbf{C}, \Theta) + 2\partial_{\mathbf{C}} \Psi_{NEQ}(\mathbf{C}, \Theta, \alpha_i) \quad (7)$$

$$\eta = -\partial_{\Theta} \Psi = -\partial_{\Theta} \Psi_{EQ}(\mathbf{C}, \Theta) - \partial_{\Theta} \Psi_{NEQ}(\mathbf{C}, \Theta, \alpha_i) \quad (8)$$

$$\mathbf{Q}^i = -\partial_{\alpha_i} \Psi = -\partial_{\alpha_i} \Psi_{NEQ}(\mathbf{C}, \Theta, \alpha_i) \quad (9)$$

Reduced local dissipation expression: $\mathcal{D}_{loc}^{red} = \sum_{i=1}^n \mathbf{Q}^i \cdot \dot{\alpha}_i \geq 0$ (10)

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Reduced local dissipation expression: $\mathcal{D}_{loc}^{red} = \sum_{i=1}^n \mathbf{Q}^i \cdot \dot{\alpha}_i \geq 0$ (10)

Propose $\dot{\alpha}_i = \frac{1}{\eta^*} \mathbf{Q}^i$, then inequality (10) becomes:

$$\mathcal{D}_{loc}^{red} = \sum_{i=1}^n \frac{1}{\eta^*} |\mathbf{Q}^i|^2 \geq 0 \quad (11)$$

which satisfies 2nd law of thermodynamics $\forall \eta^* > 0$.

Mathematical Model (2/5)

Recall evolution equation of driving forces \mathbf{Q}^i in viscoelastic theory:

$$\dot{\mathbf{Q}}^i + \frac{\mathbf{Q}^i}{\tau} = E_i \dot{\epsilon} \quad (12)$$

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And

$$E_i \dot{\boldsymbol{\varepsilon}} \equiv \frac{E_i}{E_0} \frac{d}{dt} [\partial_{\boldsymbol{\varepsilon}} \Psi_{EQ}(\boldsymbol{\varepsilon})] \equiv \gamma_i \frac{d}{dt} [\partial_{\boldsymbol{\varepsilon}} \Psi_{EQ}(\boldsymbol{\varepsilon})] \equiv \frac{d}{dt} [\partial_{\boldsymbol{\varepsilon}} \Psi_{EQ}^{\gamma}(\boldsymbol{\varepsilon})] \quad (13)$$

where $\gamma_i \in (0, \infty)$.

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where $\gamma_i \in (0, \infty)$.

$$\therefore \dot{\mathbf{Q}}^i + \frac{\mathbf{Q}^i}{\tau} = E_i \dot{\epsilon} \equiv \frac{d}{dt} [\gamma_i \partial_{\epsilon} \Psi_{EQ}(\epsilon)] \equiv \frac{d}{dt} [\partial_{\epsilon} \Psi_{EQ}^{\Gamma}(\epsilon)] \quad (14)$$

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Here, $\Psi_{EQ}(\epsilon) \rightarrow \Psi_{EQ}(\mathbf{C}, \Theta)$, hence:

$$\dot{\mathbf{Q}}^i + \frac{\mathbf{Q}^i}{\tau} = \frac{d}{dt} [2\partial_{\mathbf{C}} \Psi_{EQ}^{\Gamma}(\mathbf{C}, \Theta)] - \mathbf{Q}_{coupling}^i \quad (15)$$

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$$\dot{\mathbf{Q}}^i + \frac{\mathbf{Q}^i}{\tau} = \frac{d}{dt} [2\partial_{\mathbf{C}} \Psi_{EQ}^{\Gamma}(\mathbf{C}, \Theta)] - \mathbf{Q}_{coupling}^i \quad (15)$$

The term $\mathbf{Q}_{coupling}^i$ is subtracted because:

$$\underbrace{\Psi_{EQ}^{\Gamma}(\mathbf{C}, \Theta)}_{\text{purely thermoelastic}} = \underbrace{\Psi_{EQ}^{\Gamma}(\mathbf{C})}_{\text{elastic}} + \underbrace{\Psi_{EQ}^{\Gamma}(\mathbf{C}, \Theta)}_{\text{thermoelastic coupling}} + \underbrace{\Psi_{EQ}^{\Gamma}(\Theta)}_{\text{rigid heat conduction}} \quad (16)$$

Mathematical Model (3/5)

Therefore, we have:

$$\dot{\mathbf{Q}}^i + \frac{\mathbf{Q}^i}{\tau} = \frac{d}{dt} [2\partial_{\mathbf{C}} \psi_{EQ}^{\Gamma}(\mathbf{C}, \Theta)] - \mathbf{Q}_{coupling}^i \quad (17)$$

$$\mathbf{Q}^i|_{t=0} = 2\partial_{\mathbf{C}} \psi_{EQ}^{\Gamma}(\mathbf{C}_0, \Theta_0) \quad (18)$$

Mathematical Model (3/5)

Therefore, we have:

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$$\mathbf{Q}^i|_{t=0} = 2\partial_{\mathbf{C}} \Psi_{EQ}^{\Gamma}(\mathbf{C}_0, \Theta_0) \quad (18)$$

which can be rewritten into convolution representation by using integration:

$$\mathbf{Q}^i = e^{\frac{-t}{\tau}} \mathbf{Q}_0^i + \int_{0^+}^t e^{\frac{-(t-s)}{\tau}} \left\{ \frac{d}{ds} [2\partial_{\mathbf{C}} \Psi_{EQ}^{\Gamma}(\mathbf{C}, \Theta)] - \mathbf{Q}_{coupling}^i \right\} ds \quad (19)$$

Convolution representation (19) is **the most compact** form, hence it is of **easy** to perform numerical implementation.

Mathematical Model (4/5)

$$\Psi = \underbrace{\Psi_{EQ}(\mathbf{C}, \Theta)}_{\text{purely thermoelastic}} + \underbrace{\Psi_{NEQ}(\mathbf{C}, \Theta, \alpha_i)}_{\text{non-equilibrium part}} \quad (20)$$

$$\Psi_{NEQ}(\mathbf{C}, \Theta, \alpha_i) = \sum_{i=1}^n \left[E_i |\alpha_i|^2 - 2 \partial_{\mathbf{C}} \Psi_{EQ}^{\Gamma}(\mathbf{C}, \Theta) : \alpha_i + \Psi_{EQ}^{\Gamma}(\mathbf{C}, \Theta) \right] \quad (21)$$

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How to get expression (21) ?

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How to get expression (21) ?

Brief answer:

Because, we have proposed (22), motivated by (23) and (24):

$$\dot{\alpha}_i = \frac{1}{\eta^*} \mathbf{Q}^i \quad (22)$$

$$\mathbf{Q}^i = -\partial_{\alpha_i} \Psi = -\partial_{\alpha_i} \Psi_{NEQ}(\mathbf{C}, \Theta, \alpha_i) \quad (23)$$

$$\partial_{\alpha_i \alpha_i}^2 \Psi_{NEQ} = E_i(\Theta) \quad (24)$$

Therefore, by integration (24) twice, time derivative (23) with substitution of (22), expression (21) is achieved.

Mathematical Model (5/5) IN SHORT

$$\Psi = \underbrace{\Psi_{EQ}(\mathbf{C}, \Theta)}_{\text{purely thermoelastic}} + \underbrace{\Psi_{NEQ}(\mathbf{C}, \Theta, \alpha_i)}_{\text{non-equilibrium part}} \quad (25)$$

$$\Psi_{NEQ}(\mathbf{C}, \Theta, \alpha_i) = \sum_{i=1}^n \left[E_i |\alpha_i|^2 - 2\partial_{\mathbf{C}} \Psi_{EQ}^{\Gamma}(\mathbf{C}, \Theta) : \alpha_i + \Psi_{EQ}^{\Gamma}(\mathbf{C}, \Theta) \right]$$

Mathematical Model (5/5) IN SHORT

$$\Psi = \underbrace{\Psi_{EQ}(\mathbf{C}, \Theta)}_{\text{purely thermoelastic}} + \underbrace{\Psi_{NEQ}(\mathbf{C}, \Theta, \alpha_i)}_{\text{non-equilibrium part}} \quad (25)$$

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$$\mathbf{S} = 2\partial_{\mathbf{C}} \Psi_{EQ}(\mathbf{C}, \Theta) + \sum_{i=1}^n \left[2\partial_{\mathbf{C}} \Psi_{EQ}^{\Gamma}(\mathbf{C}, \Theta) - 4\partial_{\mathbf{C}\mathbf{C}}^2 \Psi_{EQ}^{\Gamma}(\mathbf{C}, \Theta) \alpha_i \right]$$

$$\eta = -\partial_{\Theta} \Psi_{EQ}(\mathbf{C}, \Theta)$$

$$+ \sum_{i=1}^n \left[-\partial_{\Theta} \Psi_{EQ}^{\Gamma}(\mathbf{C}, \Theta) + 2\partial_{\mathbf{C}\Theta} \Psi_{EQ}^{\Gamma}(\mathbf{C}, \Theta) : \alpha_i - \partial_{\Theta} E_i(\Theta) |\alpha_i|^2 \right]$$

$$\mathbf{Q}^i = e^{\frac{-t}{\tau}} \mathbf{Q}_0^i + \int_{0^+}^t e^{\frac{-(t-s)}{\tau}} \left\{ \frac{d}{ds} [2\partial_{\mathbf{C}} \Psi_{EQ}^{\Gamma}(\mathbf{C}, \Theta)] - 2\partial_{\Theta} E_i(\Theta) \alpha_i \frac{d\Theta}{ds} \right\} ds$$

$$\alpha_i = \frac{1}{E_i} 2\partial_{\mathbf{C}} \Psi_{EQ}^{\Gamma}(\mathbf{C}, \Theta) - \frac{\mathbf{Q}^i}{2E_i}; \quad \boxed{\Psi_{EQ}^{\Gamma}(\mathbf{C}, \Theta) = \gamma_i \Psi_{EQ}(\mathbf{C}, \Theta)} \quad (26)$$

Dilatational-Deviatoric Multiplicative Split

Dilatational-Deviatoric Multiplicative Split (1/2)

- Motivation: Polymeric materials behave strongly in shear, weakly in dilatation (Malvern [1969]).
- Proposed by Flory [1966]:

$$\mathbf{F} = (J^{1/3}\mathbf{I})\tilde{\mathbf{F}} \quad (27)$$

$$\text{with } \det(\tilde{\mathbf{F}}) \equiv 1 \quad (28)$$

where \mathbf{F} is deformation gradient, J Jacobian, $\tilde{\mathbf{F}}$ deviatoric part and $(J^{1/3}\mathbf{I})$ dilatational part.

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where \mathbf{F} is deformation gradient, J Jacobian, $\tilde{\mathbf{F}}$ deviatoric part and $(J^{1/3}\mathbf{I})$ dilatational part.

It follows:

$$\tilde{\mathbf{C}} = \tilde{\mathbf{F}}^T \tilde{\mathbf{F}} = (J^{-2/3}\mathbf{I})\mathbf{C} \quad (29)$$

$$\partial_{\mathbf{C}}\tilde{\mathbf{C}} = J^{-2/3}(\mathbb{I} - \frac{1}{3}\mathbf{C} \otimes \mathbf{C}^{-1}) \quad (30)$$

$$2\partial_{\mathbf{C}}J = J\mathbf{C}^{-1} \quad (31)$$

Dilatational-Deviatoric Multiplicative Split (2/2)

$$\boxed{\Psi = \Psi_{EQ}(\mathbf{C}, \Theta) + \Psi_{NEQ}(\mathbf{C}, \Theta, \alpha_i)} \quad (32)$$

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Dilatational-Deviatoric Multiplicative Split (2/2)

$$\boxed{\Psi = \Psi_{EQ}(\mathbf{C}, \Theta) + \Psi_{NEQ}(\mathbf{C}, \Theta, \alpha_i)} \quad (32)$$

Consideration of specific Helmholtz free energy function $\Psi_{EQ}(\mathbf{C}, \Theta)$:

$$\Psi_{EQ}(\mathbf{C}, \Theta) = \Psi_{EQ}^{vol}(J, \Theta) + \Psi_{EQ}^{iso}(\tilde{\mathbf{C}}, \Theta) + T(\Theta) \quad (33)$$

where

$\Psi_{EQ}^{vol}(J, \Theta)$: convex volumetric response,

$\Psi_{EQ}^{iso}(\tilde{\mathbf{C}}, \Theta)$: poly-convex deviatoric response,

$T(\Theta)$: purely thermal contribution.

which can be recast into:

$$\boxed{\Psi_{EQ}(\mathbf{C}, \Theta) = \zeta \Psi_{EQ}^{iso}(\tilde{\mathbf{C}}, \Theta)} \quad (34)$$

where $\zeta \in (0, \infty)$.

Dilatational-Deviatoric Multiplicative Split (2/2)

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where $\zeta \in (0, \infty)$.

Next step: Rewrite $\Psi_{EQ}(\mathbf{C}, \Theta) \rightarrow \Psi_{EQ}^{iso}(\tilde{\mathbf{C}}, \Theta)$ for $\Psi, \mathbf{S}, \eta, \mathbf{Q}$ and α_i .

Summary and conclusion

Summary 1/3

(i) Helmholtz free energy function:

$$\Psi = \Psi_{EQ}(\mathbf{C}, \Theta) + \Psi_{NEQ}(\mathbf{C}, \Theta, \alpha_i) \quad (35)$$

$$\Psi_{NEQ}(\mathbf{C}, \Theta, \alpha_i) = \sum_{i=1}^n \left[E_i |\alpha_i|^2 - 2 \partial_{\mathbf{C}} \Psi_{EQ}^{\Gamma}(\mathbf{C}, \Theta) : \alpha_i + \Psi_{EQ}^{\Gamma}(\mathbf{C}, \Theta) \right] \quad (36)$$

$$\Psi_{EQ}(\mathbf{C}, \Theta) = \Psi_{EQ}^{vol}(J, \Theta) + \Psi_{EQ}^{iso}(\tilde{\mathbf{C}}, \Theta) + T(\Theta) \quad (37)$$

and

$$\Psi_{EQ}^{\Gamma}(\mathbf{C}, \Theta) = \gamma_i \Psi_{EQ}(\mathbf{C}, \Theta) \equiv \gamma_i \zeta \Psi_{EQ}^{iso}(\tilde{\mathbf{C}}, \Theta) \equiv \beta \Psi_{EQ}^{iso}(\tilde{\mathbf{C}}, \Theta) \quad (38)$$

where free energy factor $\beta = \gamma_i \zeta$ and $\beta \in (0, \infty)$.

(ii) Second Piola-Kirchhoff stress:

$$\begin{aligned} S = & 2\partial_{\mathbf{C}} \Psi_{EQ}(\mathbf{C}, \Theta) \\ & + \sum_{i=1}^m \beta \left\{ J^{\frac{-2}{3}} \text{Dev} \left[2\partial_{\tilde{\mathbf{C}}} \Psi_{EQ}^{iso}(\tilde{\mathbf{C}}, \Theta) \right] - 2\partial_{\mathbf{C}} \left\{ J^{\frac{-2}{3}} \text{Dev} \left[2\partial_{\tilde{\mathbf{C}}} \Psi_{EQ}^{iso}(\tilde{\mathbf{C}}, \Theta) \right] \right\} \right\} \end{aligned} \quad (39)$$

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(iii) Entropy:

$$\begin{aligned} \eta = & -\partial_{\Theta} \Psi_{EQ}(\mathbf{C}, \Theta) \\ & + \sum_{i=1}^n \left[\beta \left(-\partial_{\Theta} \Psi_{EQ}^{iso}(\tilde{\mathbf{C}}, \Theta) + 2\partial_{\mathbf{C}\Theta} \Psi_{EQ}^{iso}(\tilde{\mathbf{C}}, \Theta) : \alpha_i \right) - \partial_{\Theta} E_i |\alpha_i|^2 \right] \end{aligned} \quad (40)$$

Summary 3/3

(iv) Dissipation:

$$\mathcal{D}_{loc}^{red} = \sum_{i=1}^n \frac{1}{\tilde{\eta}_i^*} \left| \tilde{\mathbf{Q}}^i \right|^2 \geq 0 \quad (41)$$

with $\tilde{\mathbf{Q}}^i = e^{\frac{-t}{\tilde{\tau}_i}} \tilde{\mathbf{Q}}_0^i$ (42)

$$+ \int_{0^+}^t e^{\frac{-(t-s)}{\tilde{\tau}_i}} \left\{ \frac{d}{ds} [2\partial_{\mathbf{C}} \Psi_{EQ}^{iso}(\tilde{\mathbf{C}}, \Theta)] - 2\partial_{\Theta} E_i \alpha_i \frac{d\Theta}{ds} \right\} ds$$

and $\alpha_i = \frac{1}{E_i} \beta_i J^{\frac{-2}{3}} \text{Dev}[\partial_{\tilde{\mathbf{C}}} \Psi_{EQ}^{iso}(\tilde{\mathbf{C}}, \Theta)] - \frac{1}{2E_i} \tilde{\mathbf{Q}}^i$ (43)

Summary 3/3

(iv) Dissipation:

$$\mathcal{D}_{loc}^{red} = \sum_{i=1}^n \frac{1}{\tilde{\eta}_i^*} |\tilde{\mathbf{Q}}^i|^2 \geq 0 \quad (41)$$

with $\tilde{\mathbf{Q}}^i = e^{\frac{-t}{\tilde{\tau}_i}} \tilde{\mathbf{Q}}_0^i$ (42)

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and $\alpha_i = \frac{1}{E_i} \beta_i J^{\frac{-2}{3}} \text{Dev}[\partial_{\tilde{\mathbf{c}}} \Psi_{EQ}^{iso}(\tilde{\mathbf{C}}, \Theta)] - \frac{1}{2E_i} \dot{\tilde{\mathbf{Q}}}^i$ (43)

(v) Evolution equation:

$$\dot{\tilde{\mathbf{Q}}}^i + \frac{\tilde{\mathbf{Q}}^i}{\tilde{\tau}_i} = \beta_i \frac{d}{dt} \left\{ J^{\frac{-2}{3}} \text{Dev} \left[2\partial_{\tilde{\mathbf{c}}} \Psi_{EQ}^{iso}(\tilde{\mathbf{C}}, \Theta) \right] \right\} - 2\partial_{\Theta} E_i \alpha_i \frac{d\Theta}{dt} \quad (44)$$

$$\tilde{\mathbf{Q}}^i|_{t=0} = \tilde{\mathbf{Q}}_0^i \quad (45)$$

Conclusion

Goals:

- To develop a constitutive model compatible with 2nd law of thermodynamics and to suit FEM numerical treatment. → Satisfied
- 3D frame for viscoelastic constitutive model at finite thermomechanical changes. → Satisfied

Remarks:

- Free energy function is decomposed into purely thermoelastic part and non-equilibrium part. → Applied
- Volumetric/Deviatoric multiplicative decomposition on deformation gradient. → Applied

Suggested future work:

- A numerical realization/implementation.

Questions

Backup slide 1: Dilatational part $J^{1/3}$.I

Stretches λ_i ($i = 1, 2, 3$) of a 3D-body in 3 directions x, y, z are:

$$\lambda_1 = \frac{|dx|}{|d\mathbf{X}|} \quad (46)$$

$$\lambda_2 = \frac{|dy|}{|d\mathbf{Y}|} \quad (47)$$

$$\lambda_3 = \frac{|dz|}{|d\mathbf{Z}|} \quad (48)$$

$$\Rightarrow \lambda_1 \lambda_2 \lambda_3 = \frac{|dx|}{|d\mathbf{X}|} \frac{|dy|}{|d\mathbf{Y}|} \frac{|dz|}{|d\mathbf{Z}|} \equiv \frac{dv}{dV} \equiv \det(\mathbf{F}) \equiv J \quad (49)$$

Consideration of **isotropy**, we have $\lambda_1 = \lambda_2 = \lambda_3 \equiv \lambda$, hence:

$$\lambda^3 = J \quad (50)$$

$$\therefore \boxed{\lambda = J^{1/3}} \quad (51)$$

Backup slide 2: Why $\partial_{\epsilon}\Psi(\epsilon, \Theta) = 2\partial_{\mathbf{C}}\Psi(\mathbf{C}, \Theta)$?

$$\partial_{\epsilon}\Psi(\epsilon, \Theta) = 2\partial_{\mathbf{C}}\Psi(\mathbf{C}, \Theta) \quad (52)$$

Example:

$$\Psi(e) = 5e + 1 \quad (53)$$

$$\therefore \partial_e \Psi(e) = 5 \quad (54)$$

$$\because e = \frac{1}{2}(c - 1) \quad (55)$$

$$\Rightarrow \Psi(c) = \frac{5}{2}c - \frac{3}{2} \quad (56)$$

$$\therefore \partial_c \Psi(c) = \frac{5}{2} \quad (57)$$

Comparison equations (54) and (57) yields:

$$\partial_e \Psi = 2\partial_c \Psi \quad (58)$$

$$\therefore \partial_{\epsilon}\Psi(\epsilon, \Theta) = 2\partial_{\mathbf{C}}\Psi(\mathbf{C}, \Theta) \quad (59)$$

Backup slide 3: Driving forces Q^i in viscoelastic theory

Constitutive expression reads:

$$\sigma = \partial_\varepsilon \hat{\Psi} = E_0 \varepsilon + \sum_{i=1}^n E_i (\varepsilon - \alpha_i) \quad (60)$$

$$Q_i = -\partial_{\alpha_i} \hat{\Psi} = E_i (\varepsilon - \alpha_i) \quad (61)$$

$$\dot{\alpha}_i = \frac{1}{\eta_i} Q_i \quad (62)$$

Consider the evolution equation, i.e. time derivative of (61):

$$\dot{Q}_i = E_i (\dot{\varepsilon} - \dot{\alpha}_i) \quad (63)$$

Insertion (62) to (63) yield:

$$\therefore \dot{Q}_i + \frac{1}{\tau_i} Q_i = E_i \dot{\varepsilon} \quad (64)$$