Mathematical modelling for All-solid-state battery

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Mathematical modelling for the next-generation All-solid-state batteries: Nucleation (SE|SSE)^(*)-Interface

Rechargeable Lithium-ion battery (LIB) is at the heart of every electric vehicle (EV), portable electronic device, and energy storage system [5]. Nowadays, LIBs enable human life more efficient and help to solve global environment issues thanks to EVs' zero However, conventional LIB (c-LIB) is emission. sensible to temperature and pressure, hence, flammable and explosive, which is undesirable. This bottleneck is mainly due to liquid-based electrolyte found in c-LIBs.

All-solid-state battery (ASSB) is one of promising candidates to overcome bottlenecks of c-LIBs. Thanks to solid-state electrolyte (SSE), ASSB is highly stable towards temperature and pressure. Nevertheless, Limetal dendrite triggered at (SE|SSE)-Interface is the main drawback of ASSB since these dendritic threads extrapolate into SSE grain boundary network, causing crevice, degradation of ionic conductivity, and the probability of short-circuit, which is unfavorable [10].

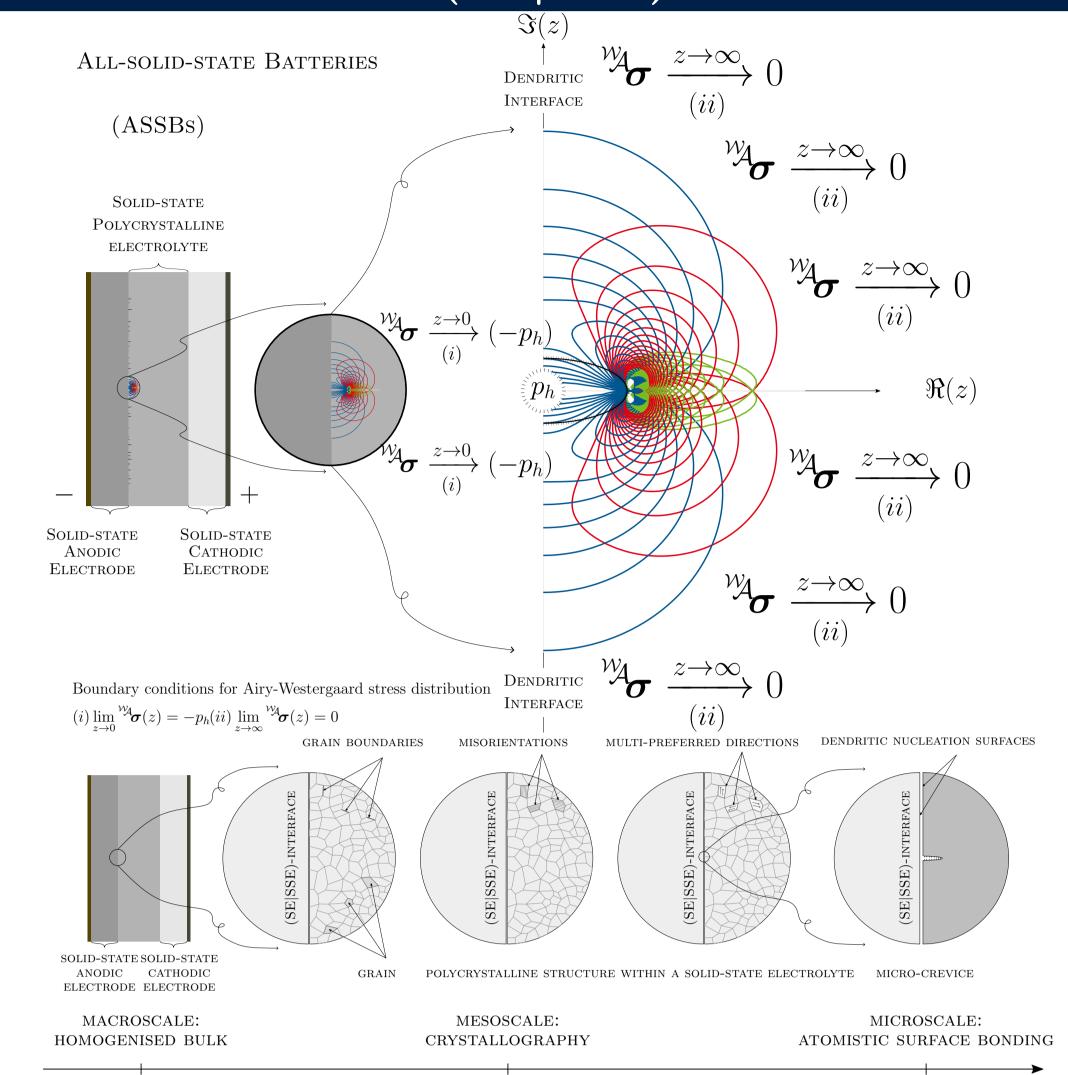
Next-generation All-solid-state battery (ng-ASSB) with a consideration of nucleation criterion defined by

$$\partial_{t} \boldsymbol{u} + \nabla \cdot \left(\overset{4}{\mathbb{C}} f_{\text{alocation}}(\lambda, \mu, \boldsymbol{d}_{G_{i}, i=1, \dots, N}^{R}, \boldsymbol{d}^{E}; \boldsymbol{x}) : \nabla \boldsymbol{u}^{(s)} \right) + \rho \boldsymbol{b} = -\rho \nabla V_{e}, \tag{1}$$

s.t.
$$a_{\text{Griffith}}^{\text{generalised}} := a^* = \arg\min_{a \in \mathbb{R}} \iiint_{\Omega} f(a, \boldsymbol{u}, \theta; \lambda, \mu, \boldsymbol{d}^{(\star)} \otimes \boldsymbol{d}^{(\star)}) d\Omega - \iint_{\Gamma} f(a; \gamma) d\Gamma \Big|_{\bar{\boldsymbol{u}}}$$
 (2)

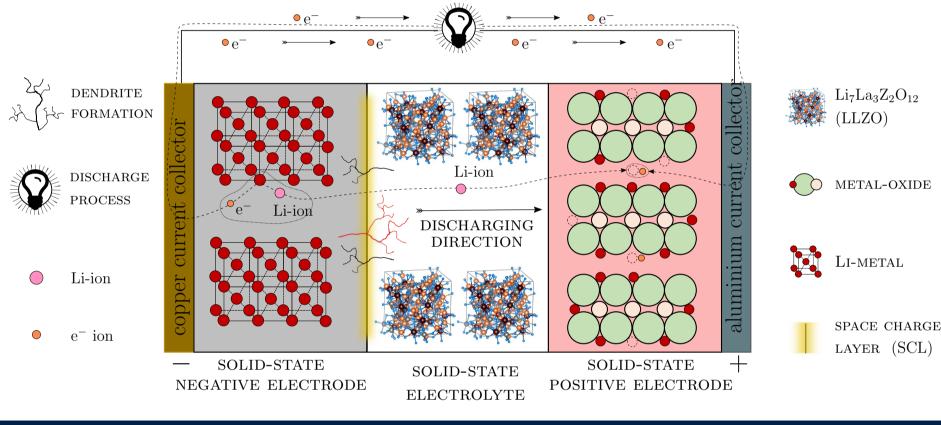
where $V_e: \mathbb{R}^3 \to \mathbb{R}$ is the electric potential applied globally on ASSB. Due to nature setting of ASSB taking the form (SE|SSE|SE) the electric potential becomes uniform. Additionally, \boldsymbol{u} is the displacement field, θ temperature field, a crevice length, λ , μ Lamé constants, $\mathbf{d}^{(\star)} \otimes \mathbf{d}^{(\star)}$ embedded misorientation structural tensor, and γ cracking-surface energy density, can help to improve ASSB performance [1][2].

Aim: The study is with the purpose of gaining a better insight into dendrite nucleation and formation in ASSB.



Next-generation All-solid-state battery

Griffith nucleation criterion governs (SE|SSE)-Interface.



Space-charge Layer

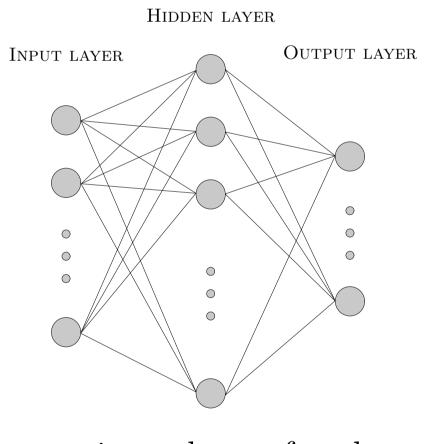
SCL presents in ASSB [8], and likewise in Semiconductors. UCLEATION

Energy density landscape

ASSB enables energy demand thanks to (i), and followed by (ii). Energy density: ASSB versus LIB versus Petroi THEORETICAL CAPACITY OF CHARGE: PURE METALLIC LITHIUM (Li) VERSUS GRAPHITE (C₆) $(4 \, h \, l^{-1})^{[?][?]} \, | \, [mAh \, cm^{-3}]^{[?]}$ $3800^{[?]}|3860^{[?][?][?][?]}|3861^{[?]}$

Artificial Neural Networks

Application: Steel property prediction.



An augmentation scheme for the prediction of the bainitic transformation temperature is validated by means of ANNs [9].

Semiconductor

Application: Start/Stop Starter Motor.

Nucleation interface: Taking place at the critically dendritic (SE|SSE)-Interface

Coupled fields are Displacement field \boldsymbol{u} and temperature field $\boldsymbol{\theta}$;

$$m{u}: egin{cases} \Omega imes \mathbb{R}_+ & \to \mathbb{R}^3, \\ (m{x},t) & \mapsto m{u}(m{x},t), \end{cases} \quad heta: egin{cases} \Omega imes \mathbb{R}_+ & \to \mathbb{R}, \\ (m{x},t) & \mapsto m{\theta}(m{x},t), \end{cases}$$

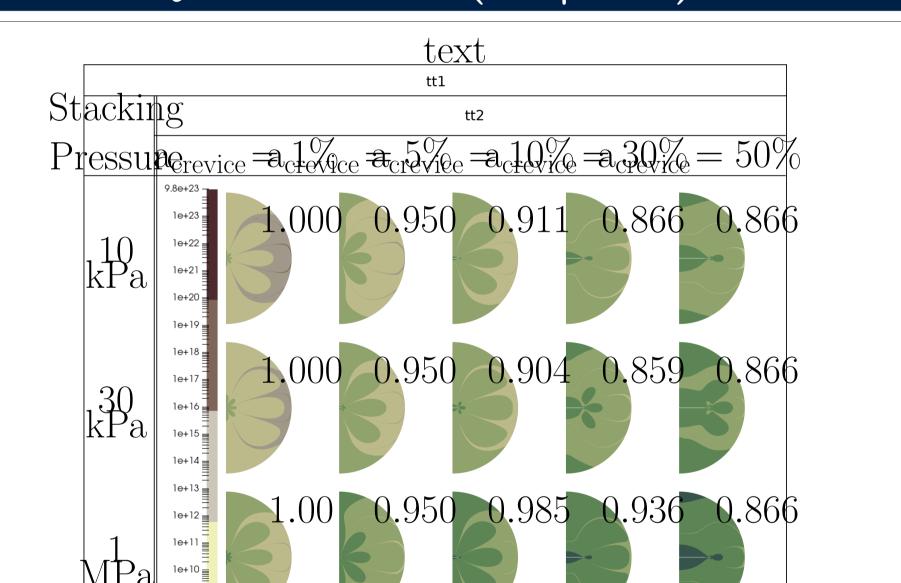
Governing conservation equations used to describe balance of mass, conservation of linear momentum, conservation of angular momentum, and conservation of energy with $\rho(\boldsymbol{x},t)$ is mass density per unit volume (puv); $\boldsymbol{b}(\boldsymbol{x},t)$ body force puv; $\boldsymbol{v}(\boldsymbol{x},t)$ velocity; $e(\boldsymbol{x},t)$ internal energy puv; $\boldsymbol{q}(\boldsymbol{x},t)$ heat flux; $r(\boldsymbol{x},t)$ heat source puv; σ Cauchy stress and ε infinitesimal strain.

the deformation of SSE due to dendrite formation at (SE|SSE)interface

$$\iiint_{\Omega} f(a, \boldsymbol{u}; \lambda, \mu, \boldsymbol{d} \otimes \boldsymbol{d}) d\Omega$$

Strain energy is based on Surface energy is analysised based on the open crevice cracking at (SE|SSE)-interface affected by prescribed pressure

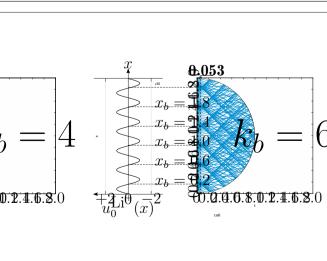
$$\iint_{-}^{T} f(a;\gamma) \, d\Gamma$$

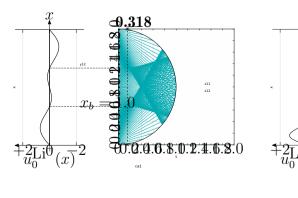


(i) Theoretical capacity of charge

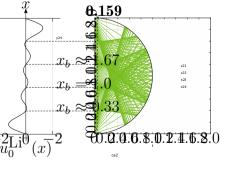
0.899 0.854 1.000 0.950 0.866 0.948 0.900 1.000 0.950 0.866

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Dr. R. Speck,



Acknowledgments

T. Vo expresses sincere gratitude to the JARA-

CSD research project, led by Dr. S. Braun and

Dr. C. Hüter, for their crucial support. Special thanks to

Prof. Dr. R. Spatschek for hosting at IEK-2, FZ Jülich.

Moreover, T. Vo's role as a teaching assistant in the

courses of Mathematische Grundlagen I, II, III, IV, and

NumPDE at Computational Engineering Science (CES)

RWTH Aachen University (2019-2023), was accomplished

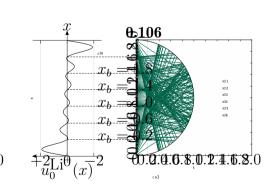
and enriched thanks to the guidance and mentorship of

Prof. Dr. M. Torrilhon, Prof. Dr. M. Schlottke-Lakemper,

Prof. Dr. B. Berkels,

Prof. Dr. J. Kowalski, Dr. A. Jha, Prof. Dr. B. Stamm,

Dr. A. Litvinenko, and Dr. M. Kirchhart.



Dr. S. Braun.

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