Next-generation all-solid-state battery (#ASSB)

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Mathematical modelling for the next-generation All-solid-state batteries: Nucleation (SE|SSE)^(*)-interface

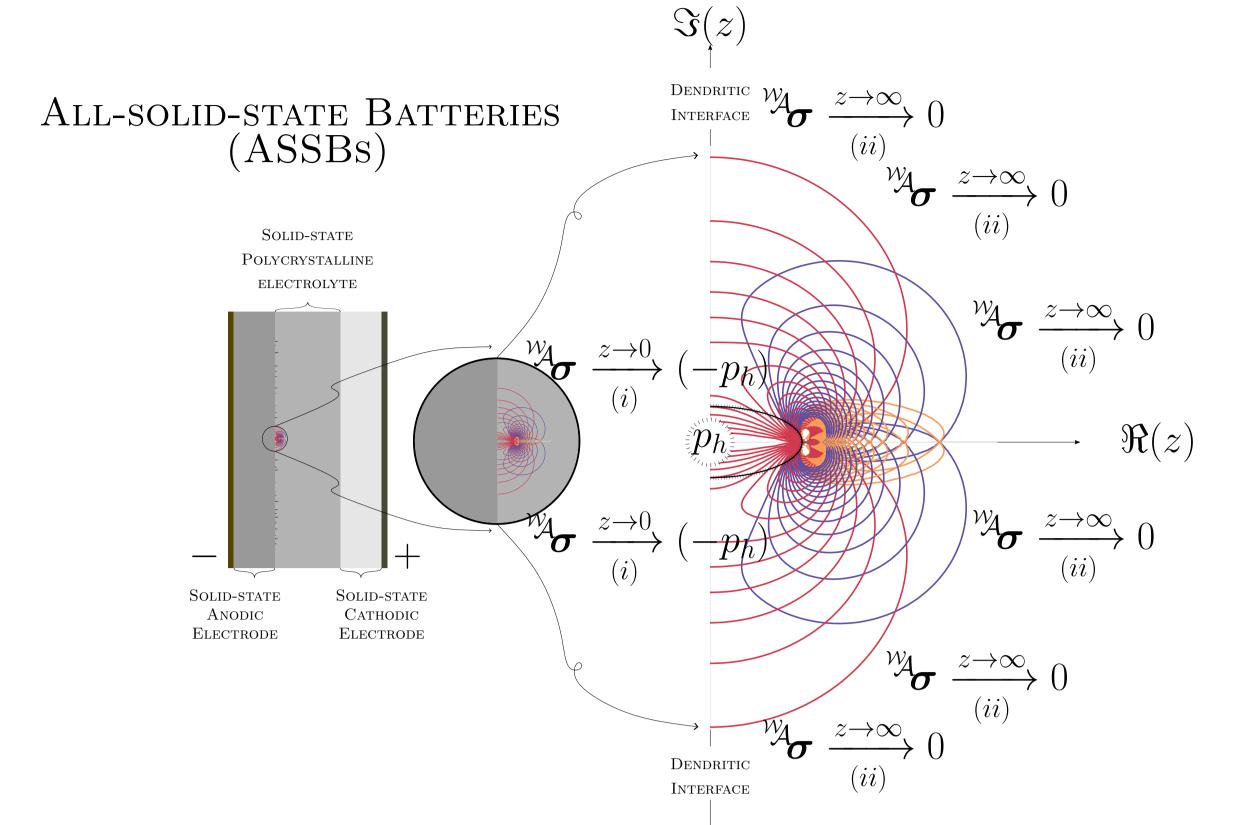
Rechargeable Lithium-ion battery (LIB) is at the heart of every electric vehicle (EV), portable electronic device, and energy storage system [1]. Nowadays, LIBs enable human life more efficient and help to solve global environment issues thanks to EVs' zero emission. However, conventional LIB (c-LIB) is sensible to temperature and pressure, hence, flammable and explosive, which is undesirable. This bottleneck is mainly due to liquid-based electrolyte found in c-LIBs.

All-solid-state battery (ASSB) is one of promising candidates to overcome bottlenecks of c-LIBs. Thanks to solid-state electrolyte (SSE), ASSB is highly stable towards temperature and pressure. Nevertheless, Limetal dendrite triggered at (SE|SSE)-interface is the main drawback of ASSB since these dendritic threads extrapolate into SSE grain boundary network, causing crevice, degradation of ionic conductivity, and the probability of short-circuit, which is unfavorable.

Next-generation All-solid-state battery (ng-ASSB) with a consideration of nucleation criterion defined by

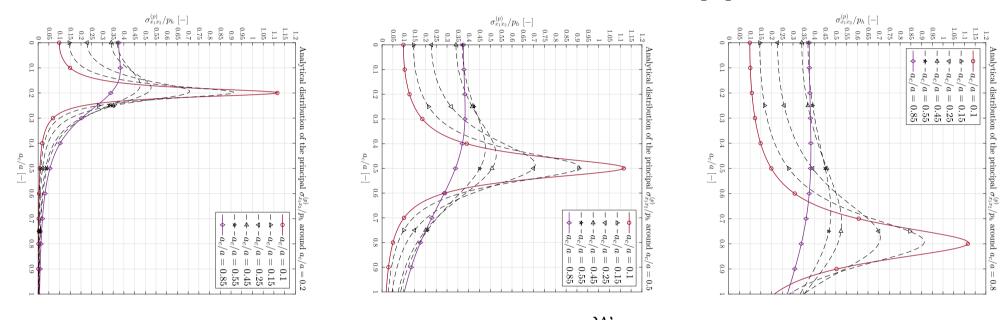
$$a_{ ext{Griffith}} := a^* = \arg\min_{a \in \mathbb{R}} \left. \iint_{\Omega} f(a, \boldsymbol{u}; \lambda, \mu, \boldsymbol{d} \otimes \boldsymbol{d}) \, d\Omega - \left. \iint_{\Gamma} f(a; \gamma) \, d\Gamma \right|_{\boldsymbol{u}^{(s)}}$$

where, can help to improve ASSB performance. can help to improve ASSB performance. can help to improve ASSB performance.



Interface

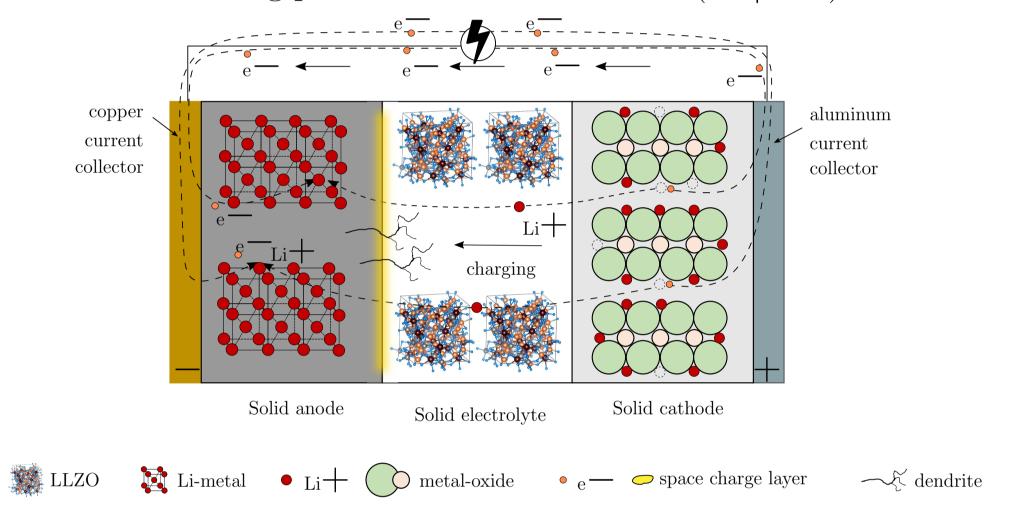
Interface between solid electrode and solid-state electrolyte (SE|SSE) taking place at space charge layer (SCL) [2] found in ASSBs critically exhibits mechanical and electrochemical instability [3]. This evidence points directly to the fact that the soft metallic li anode is erroneously prone to triggering dendrites, under cycles of electric charge & discharge [4].



<u>Distribution</u>: ana. max. shear stress ${}^{\mathcal{W}}\!\!\sigma_{x_1x_2}^{\Pi}$ around crack tip a_c .

Next-generation All-solid-state battery

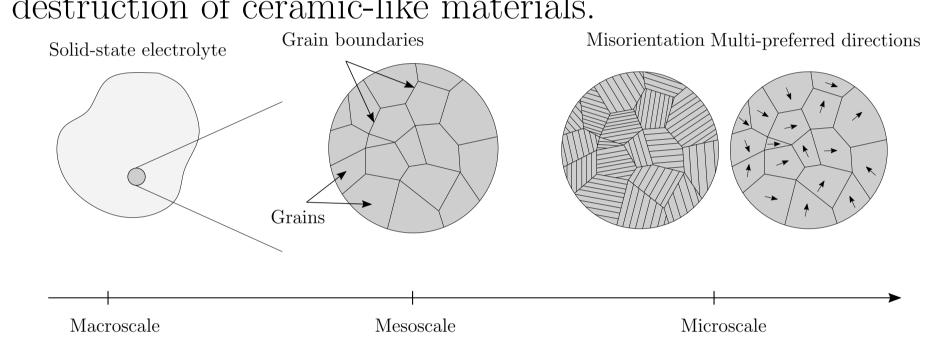
Nucleation taking place at critical dendritic (SE|SSE)-interface



Nucleation taking place at critical dendritic (SE|SSE)-interface Nucleation taking place at critical dendritic (SE|SSE)-interface

Embedded structural-tensor SSE

Polycrystalline garnet-typed SSE such as LLZO exhibit a network of grain boundaries, and grains with various sizes and shapes under microscopic observation. Therefore, this type of microstructure is potentially prone to nuance destruction of ceramic-like materials.



Consequentially, dendrites contribute to degradation of ionic conductivity and cracks via tracing along grain boundaries.

Nucleation interface: Taking place at the critical dendritic interface

Coupled fields: Displacement vector field and temperature scalar field

$$m{u}: egin{cases} \Omega imes \mathbb{R}_+ o \mathbb{R}^3, \ (m{x},t) \mapsto m{u}(m{x},t), \end{cases} \qquad ext{and} \qquad heta: egin{cases} \Omega imes \mathbb{R}_+ o \mathbb{R}, \ (m{x},t) \mapsto heta(m{x},t), \end{cases}$$

Governing conservation equations

$$\frac{d}{dt} \int_{\Omega} (\cdot) \ d\Omega = \int_{\Omega} (\cdot)^{\text{action}} \ d\Omega + \int_{\partial\Omega} (\cdot)^{\text{action}} \ d\partial\Omega + \int_{\Omega} (\cdot)^{\text{production/source/sink}} \ d\Omega$$

 $\rho(\boldsymbol{x},t)$ is mass density per unit volume (puv); $\boldsymbol{b}(\boldsymbol{x},t)$ body force puv; $\boldsymbol{v}(\boldsymbol{x},t)$ velocity; $e(\boldsymbol{x},t)$ internal energy puv; $\boldsymbol{q}(\boldsymbol{x},t)$ heat flux; $r(\boldsymbol{x},t)$ heat source puv; $\boldsymbol{\sigma}$ Cauchy stress and $\boldsymbol{\varepsilon}$ infinitesimal strain.

$$ho \, \partial_{t^2}^2 oldsymbol{u}^{(s)} +
abla \cdot \left(\overset{4}{\mathbb{C}} f^{\mathbb{D}(\Omega)}_{(\lambda,\mu)} :
abla oldsymbol{u}^{(s)}
ight) +
ho
abla V_e = \mathbf{0},$$

s.t.
$$a_{\text{Grifflith}} := a^* = \arg\min_{a \in \mathbb{R}} \iiint_{\Omega} f(a, \boldsymbol{u}; \lambda, \mu, \boldsymbol{d} \otimes \boldsymbol{d}) d\Omega - \iint_{\Gamma} f(a; \gamma) d\Gamma \Big|_{\boldsymbol{u}^{(1)}}$$

Thermodynamic consistency: satisfied. Closure problem: fulfilled.

$$ho \, \partial_{t^2}^2 oldsymbol{u}^{(s)} +
abla \cdot \left(\overset{4}{\mathbb{C}}^{f_{(\lambda,\mu)}^{\mathbb{D}(\Omega)}} :
abla oldsymbol{u}^{(s)}
ight) +
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abla V_e = oldsymbol{0},$$

s.t.
$$a_{\text{Griffith}} := a^* = \arg\min_{a \in \mathbb{R}} \iiint_{\Omega} f(a, \boldsymbol{u}; \lambda, \mu, \boldsymbol{d} \otimes \boldsymbol{d}) d\Omega - \iint_{\Gamma} f(a; \gamma) d\Gamma \Big|_{\boldsymbol{u}^{(a)}}$$

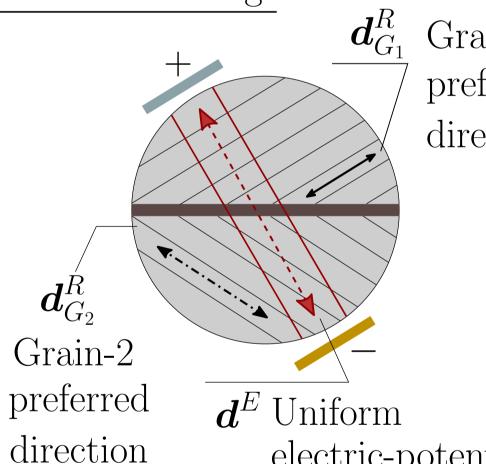
Helmholtz energy functional

$$a_{ ext{Griffith}} := a^* = \arg\min_{a \in \mathbb{R}} \iiint_{\Omega} f(a, \boldsymbol{u}; \lambda, \mu, \boldsymbol{d} \otimes \boldsymbol{d}) \, d\Omega - \iint_{\Gamma} f(a; \gamma) \, d\Gamma \bigg|_{\boldsymbol{u}^{(s)}}$$

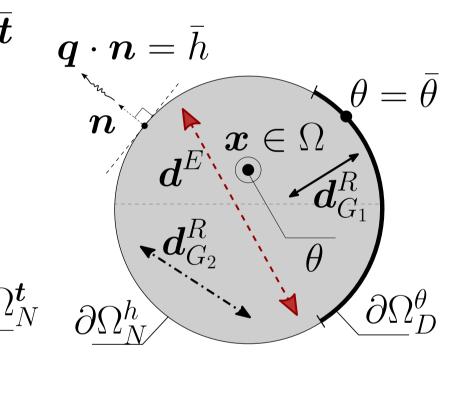
Governing PDE Therefore

$$\therefore \quad a_{\text{Griffith}} := a^* = \arg\min_{a \in \mathbb{R}} \iiint_{\Omega} f(a, \boldsymbol{u}; \lambda, \mu, \boldsymbol{d} \otimes \boldsymbol{d}) \, d\Omega - \iint_{\Gamma} f(a; \gamma) \, d\Gamma \bigg|_{\boldsymbol{u}^{(s)}}$$

Boundary condition settings

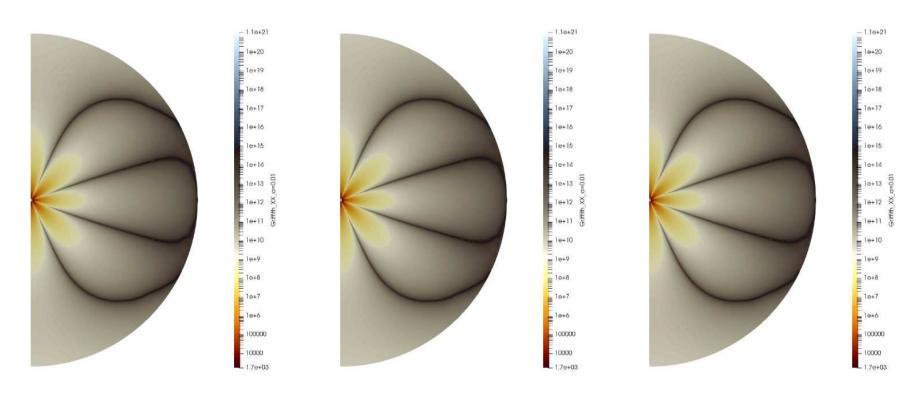


Grain-1 $\partial \Omega_D^{\boldsymbol{u}} \quad \boldsymbol{\sigma} \cdot \boldsymbol{n} = 0$ preferred direction $\boldsymbol{u} = \bar{\boldsymbol{u}} \quad \boldsymbol{d}^R \quad \boldsymbol{d}$



Uniform displacement field utemperature field θ electric-potential polarizational effect

The set of boundary conditions is likewise the path of the pressure-centric dendritic crack.



Comparison: Analytical vs. Numerical solutions

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