Next-generation all-solid-state battery (#ASSB)

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Mathematical modelling for the next-generation All-solid-state batteries: Nucleation (SE|SSE)$^{(*)}$-interface

Rechargeable Lithium-ion battery (LIB) is at the heart of every electric vehicle (EV), portable electronic device, and energy storage system [1]. Nowadays, LIBs enable human life more efficient and help to solve global environment issues thanks to EVs' zero emission. However, conventional LIB (c-LIB) is sensible to temperature and pressure, hence, flammable and explosive, which is undesirable. This bottleneck is mainly due to liquid-based electrolyte found in c-LIBs.

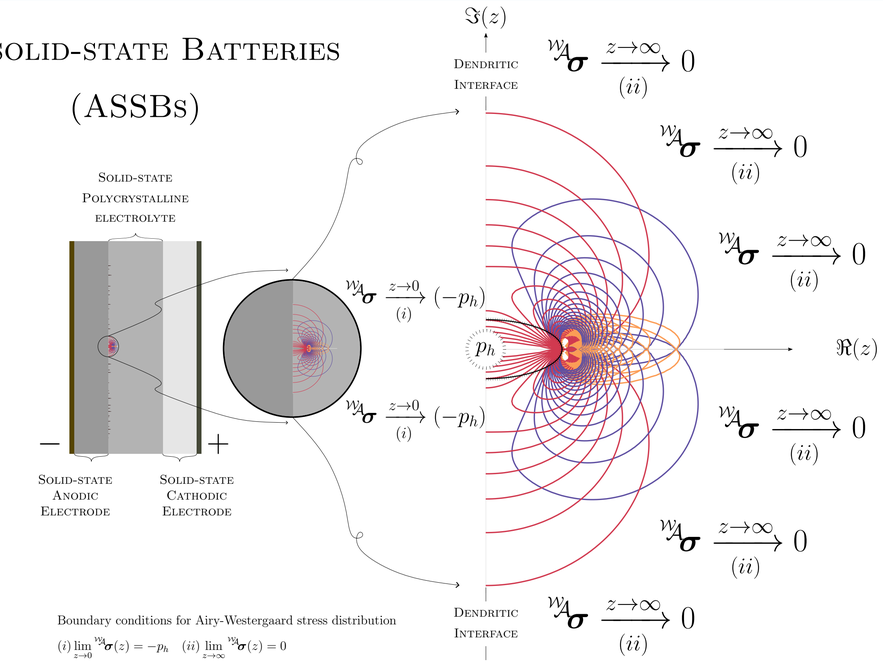
All-solid-state battery (ASSB) is one of promising candidates to overcome bottlenecks of c-LIBs. Thanks to solid-state electrolyte (SSE), ASSB is highly stable towards temperature and pressure. Nevertheless, Li-metal dendrite triggered at (SE|SSE)-interface [5] is the main drawback of ASSB since these dendritic threads extrapolate into SSE grain boundary network, causing crevice, degradation of ionic conductivity, and the probability of short-circuit, which is unfavorable.

Next-generation All-solid-state battery (ng-ASSB) with a consideration of nucleation criterion defined by

$$a_{\text{Griffith}} := a^* = \arg\min_{a\in\mathbb{R}} \iiint_\Omega f(a, \boldsymbol{u}, \theta; \lambda, \mu, \boldsymbol{d}^R \otimes \boldsymbol{d}^R)\, d\Omega - \iint_\Gamma f(a;\gamma)\, d\Gamma \Big|_{\boldsymbol{u}^{(s)}}$$

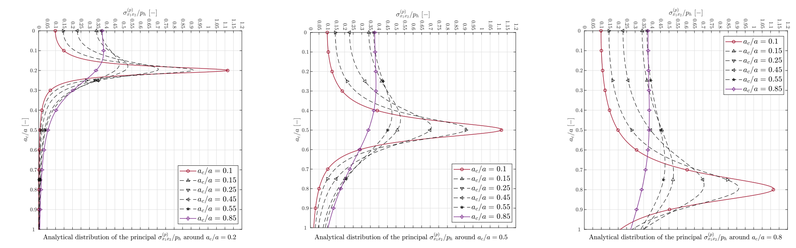
where $\boldsymbol{u}$ displacement field, θ temperature field, a crevice length, λ, μ Lamé constants, $\boldsymbol{d}^R \otimes \boldsymbol{d}^R$ embedded misorientation structural tensor, and γ cracking-surface energy density, can help to improve ASSB performance.

All-solid-state Batteries (ASSBs)



Interface Analysis

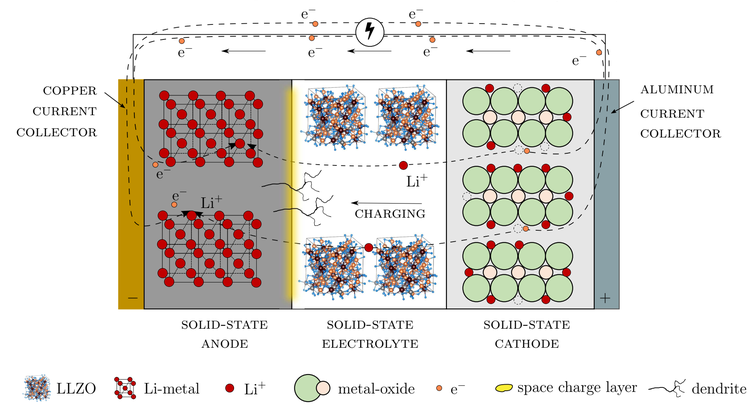
Interface between solid electrode and solid-state electrolyte (SE|SSE) taking place at space charge layer (SCL) [2] found in ASSBs critically exhibits mechanical and electrochemical instability [3]. This evidence points directly to the fact that the soft metallic li anode is erroneously prone to triggering dendrites, under cycles of electric charge & discharge [5].



Distribution: ana. max. shear stress $^{w_{\mathcal{A}}}\Pi_{x_1x_2}$ around crack tip a_c.

Next-generation All-solid-state battery

Nucleation criterion governs the instable (SE|SSE)-interface [3]

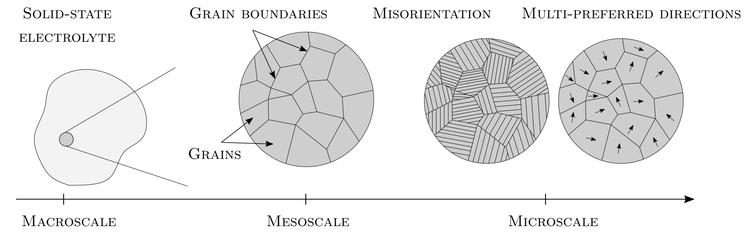


✓ **Thermodynamic consistency** is satisfied, followed by [2].
✓ **Closure** $\bar{\Omega}$ is fulfilled by 15 moments, followed by [4].

Embedded structural-tensor in SSE

Polycrystalline garnet-type SSE [5] such as LLZO exhibit grain boundary network, and grains with variation of {size, shape} under microscopic observation. Hence, this microstructure is potentially prone to nuances of destruction.

$\boldsymbol{M} = \boldsymbol{d}^R_{G_1} \otimes \boldsymbol{d}^R_{G_2}$ given by $\mathbb{G} := \{\boldsymbol{Q}_{||_d}, \boldsymbol{Q}_{\perp_d}\} \subset \mathcal{O}(3)$.



Consequentially, dendrites contribute to degradation of ionic conductivity and tiny-cracks tracing along grain boundaries.

Nucleation interface: Taking place at the critical dendritic interface

Coupled fields: Displacement field $\boldsymbol{u}$ and temperature field θ; structural tensor $\boldsymbol{M}$

$$\boldsymbol{u} : \begin{cases} \Omega \times \mathbb{R}_+ \to \mathbb{R}^3, \\ (\boldsymbol{x}, t) \mapsto \boldsymbol{u}(\boldsymbol{x}, t), \end{cases} \quad \theta : \begin{cases} \Omega \times \mathbb{R}_+ \to \mathbb{R}, \\ (\boldsymbol{x}, t) \mapsto \theta(\boldsymbol{x}, t), \end{cases} \quad \boldsymbol{M}^{\{RR,RE\}}_{i=1,\dots,N} : \begin{cases} \boldsymbol{d}^R_{\text{Grain i}} \otimes \boldsymbol{d}^R_{\text{Grain i}} \\ \boldsymbol{d}^R_{\text{Grain i}} \otimes \boldsymbol{d}^E \end{cases}$$

Governing conservation equations

$$\frac{d}{dt}\int_\Omega (\cdot)\, d\Omega = \int_\Omega (\cdot)^{\text{action}}\, d\Omega + \int_{\partial\Omega} (\cdot)^{\text{action}}\, d\partial\Omega + \int_\Omega (\cdot)^{\text{production (+/-)}}\, d\Omega$$

$\rho(\boldsymbol{x}, t)$ is mass density per unit volume (puv); $\boldsymbol{b}(\boldsymbol{x}, t)$ body force puv; $\boldsymbol{v}(\boldsymbol{x}, t)$ velocity; $e(\boldsymbol{x}, t)$ internal energy puv; $\boldsymbol{q}(\boldsymbol{x}, t)$ heat flux; $r(\boldsymbol{x}, t)$ heat source puv; $\boldsymbol{\sigma}$ Cauchy stress and $\boldsymbol{\varepsilon}$ infinitesimal strain. Helmholtz energy functional

$$a_{\text{Griffith}} := a^* = \arg\min_{a\in\mathbb{R}} \iiint_\Omega f(a, \boldsymbol{u}; \lambda, \mu, \boldsymbol{d} \otimes \boldsymbol{d})\, d\Omega - \iint_\Gamma f(a;\gamma)\, d\Gamma \Big|_{\boldsymbol{u}^{(s)}}$$

Governing PDE

$$a_{\text{Griffith}} := a^* = \arg\min_{a\in\mathbb{R}} \iiint_\Omega f(a, \boldsymbol{u}; \lambda, \mu, \boldsymbol{d} \otimes \boldsymbol{d})\, d\Omega - \iint_\Gamma f(a;\gamma)\, d\Gamma \Big|_{\boldsymbol{u}^{(s)}}$$

abc

Strain energy: Interface between solid electrode and solid-state electrolyte (SE|SSE) taking place at space charge

$$\iiint_\Omega f(a, \boldsymbol{u}; \lambda, \mu, \boldsymbol{d} \otimes \boldsymbol{d})\, d\Omega$$

Surface energy: Interface between solid electrode and solid-state electrolyte (SE|SSE) taking place

$$\iint_\Gamma f(a;\gamma)\, d\Gamma$$

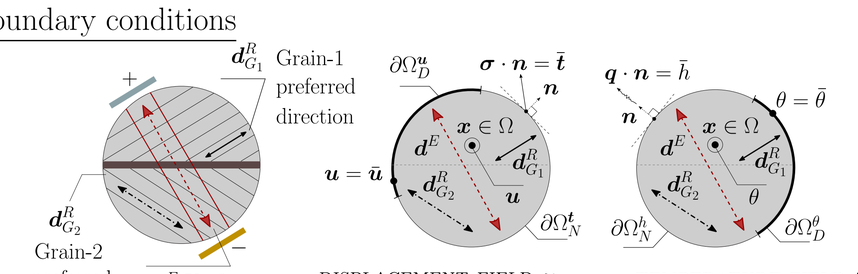
Therefore, the governing problem of dendritic nucleation at (SE|SSE) takes the form

$$\partial_t \boldsymbol{u} + \nabla \cdot \left(\mathbb{C}^4 f_{\text{alocation}}(\lambda, \mu, \boldsymbol{d}^R_{G_i, i=1,\dots,N}, \boldsymbol{d}^E; \boldsymbol{x}) : \nabla \boldsymbol{u}^{(s)} \right) + \rho \boldsymbol{b} = -\rho \nabla V_e,$$

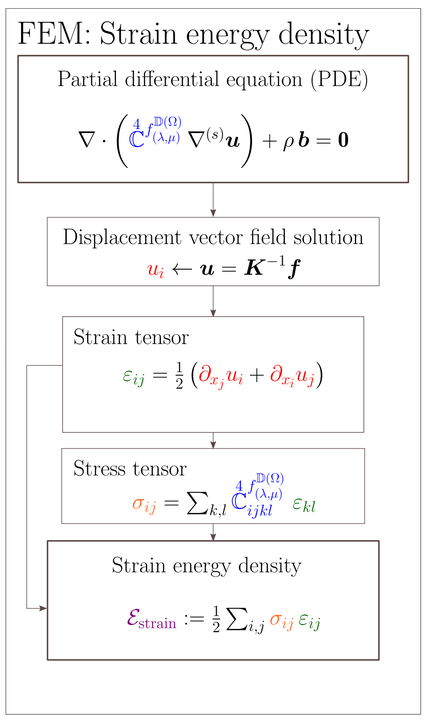
$$\text{s.t.} \quad a_{\text{Griffith}} := a^* = \arg\min_{a\in\mathbb{R}} \iiint_\Omega f(a, \boldsymbol{u}, \theta; \lambda, \mu, \boldsymbol{d} \otimes \boldsymbol{d})\, d\Omega - \iint_\Gamma f(a;\gamma)\, d\Gamma \Big|_{\bar{\boldsymbol{u}}}$$

where

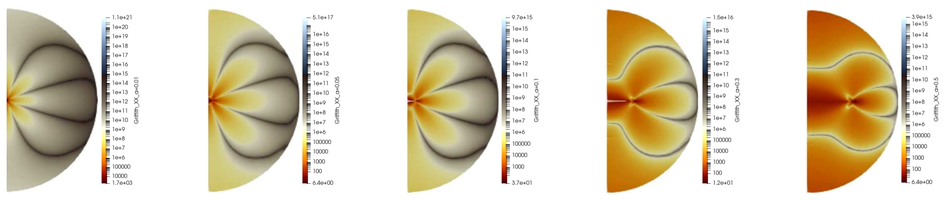
Boundary conditions



FEM: Strain energy density



Numerical spectral of *Griffith* criterion in x-direction at (SE|SSE) yields



(a) Case 1 $a_{\text{crevice}} = 0.01$ (b) Case 2 $a_{\text{crevice}} = 0.05$ (c) Case 3 $a_{\text{crevice}} = 0.1$ (d) Case 4 $a_{\text{crevice}} = 0.3$ (e) Case 5 $a_{\text{crevice}} = 0.5$

where a sample of 5 cases with various prescribed crevice length is studied.

Analysis: Airy-Westergaard function used for stress analysis: (i) max. shear stress and (ii) principal stresses

$$w_{\mathcal{A}} : \begin{cases} \mathbb{C} \to \mathbb{C}, \\ z \mapsto {}^{w_{\mathcal{A}}}(z) := \Re\left(\oiint_\Gamma \mathcal{K}^{(\star)}\, dz\right) + x_2\, \Im\left(\oint_\Gamma \mathcal{K}^{(\star)}\, dz\right), \end{cases} \quad \mathcal{K}^{(\star)} : \begin{cases} \mathbb{C} \to \mathbb{C}, \\ z \mapsto \mathcal{K}^{(\star)} := -p_h + p_h/\sqrt{1 - a^2/z^2}, \end{cases}$$

where a the crevice length, p_h pressure at the opening crevice on dendritic interface, and $\forall\, \{p_h, a\} \in \mathbb{R}_+$.

Numerics → FEM: element matrix $\boldsymbol{K}^e$ approx. by *Gauss quadrature*; indices imply $4 + 2 = 6$ *for-loop*:

$$K^{e\,\alpha\beta}_{ik} = \int_{\Omega^\xi} \left(\mathcal{L}^\alpha_1\, \mathbb{C}^{fGL}_{i1k1}(\boldsymbol{x})\, \mathcal{R}^\beta_1 + \mathcal{L}^\alpha_1\, \mathbb{C}^{fGL}_{i1k2}(\boldsymbol{x})\, \mathcal{R}^\beta_2 + \mathcal{L}^\alpha_2\, \mathbb{C}^{fGL}_{i2k1}(\boldsymbol{x})\, \mathcal{R}^\beta_1 + \mathcal{L}^\alpha_2\, \mathbb{C}^{fGL}_{i2k2}(\boldsymbol{x})\, \mathcal{R}^\beta_2 \right) \det(\boldsymbol{J})\, d\Omega^\xi$$

where $\mathcal{L}^\alpha_j$ and $\mathcal{R}^\beta_l$ are gradients of basis functions at node α^{th} and β^{th}, respectively.

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