NEXT-GENERATION ALL-SOLID-STATE BATTERY

Tuan Vo^{a,b†}, Claas Hüter^b, Stefanie Braun^a, Manuel Torrilhon^a

^aDepartment of Mathematics, Applied and Computational Mathematics (ACoM), RWTH Aachen University, Schinkelstraße 02, 52062 Aachen, Germany ^bInstitute of Energy and Climate Research (IEK-2), Forschungszentrum Jülich, Wilhelm-Johnen-Straße, 52428 Jülich, Germany

Mathematical modelling for the next-generation All-solid-state batteries: Nucleation (SE|SSE)^(*)-interface

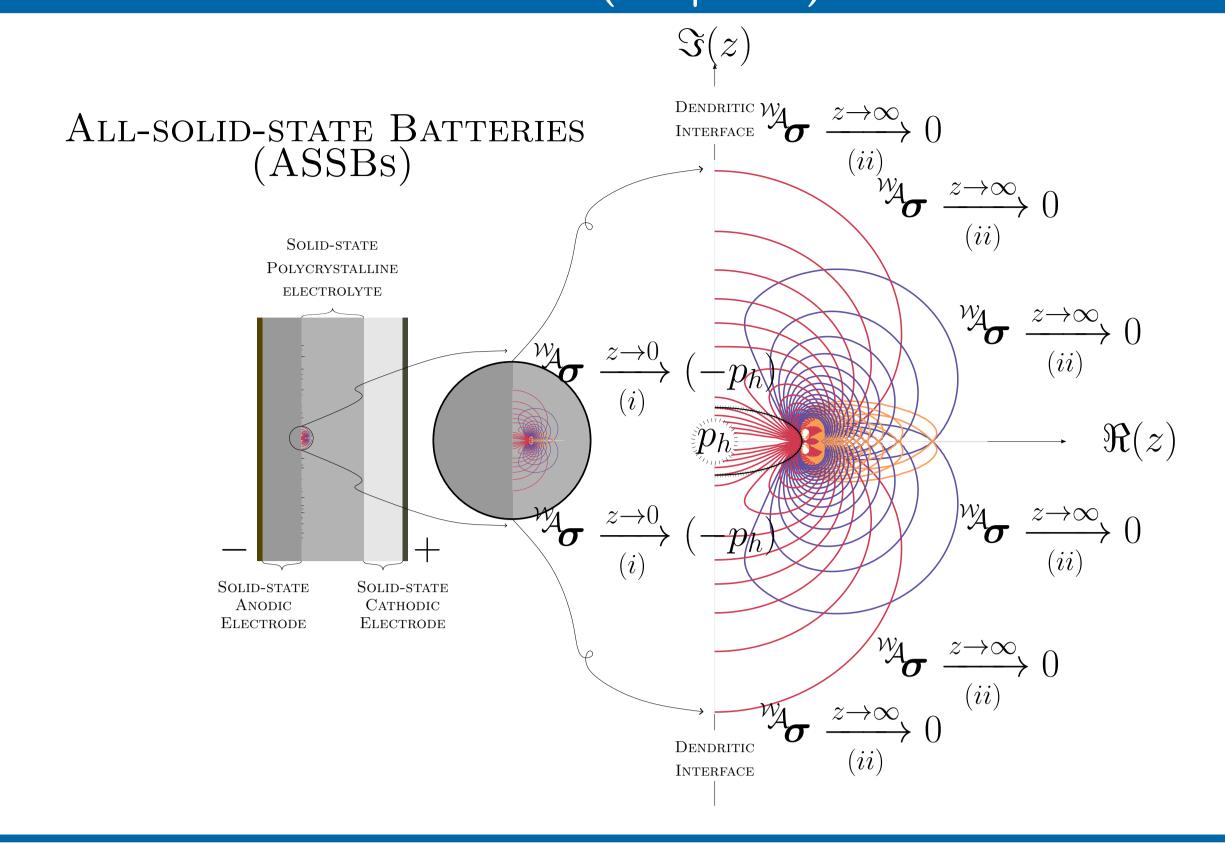
Rechargeable Lithium-ion battery (LIB) is at the heart of every electric vehicle (EV), portable electronic device, and energy storage system [1]. Nowadays, LIBs enable human life more efficient and help to solve global environment issues thanks to EVs' zero emission. However, conventional LIB (c-LIB) is sensible to temperature and pressure, hence, flammable and explosive. This bottleneck is mainly due to liquid-based electrolyte in c-LIBs.

All-solid-state battery (ASSB) is one of promising candidates to overcome bottlenecks of c-LIBs. Thanks to solid-state electrolyte (SSE), ASSB is highly stable towards temperature and pressure. Nevertheless, metallic Li-dendrite triggered at (SE|SSE)-interface is the main drawback as these dendritic threads extrapolate into grain boundary network of SSE, causing crevice, degradation of ionic conductivity, and the probability of short-circuit.

Next-generation All-solid-state battery (ng-ASSB) with a consideration of nucleation criterion defined by

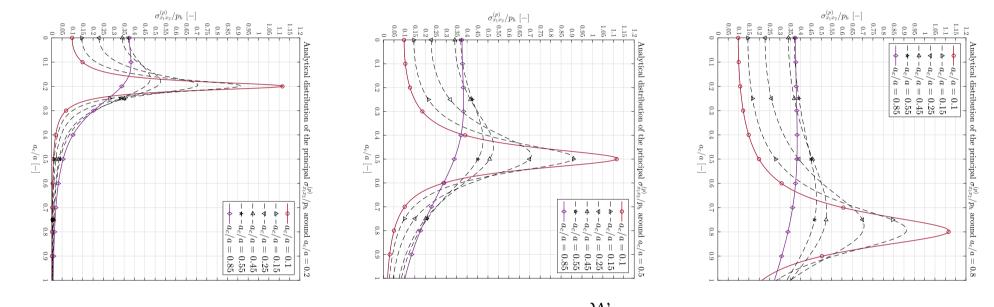
$$a_{\text{Griffith}} := a^* = \arg\min_{a \in \mathbb{R}} \left. \iint_{\Omega} f(a, \boldsymbol{u}; \lambda, \mu, \boldsymbol{d} \otimes \boldsymbol{d}) \, d\Omega - \left. \iint_{\Gamma} f(a; \gamma) \, d\Gamma \right|_{\boldsymbol{u}^{(s)}}$$

where, can help to improve ASSB performance.



Interface

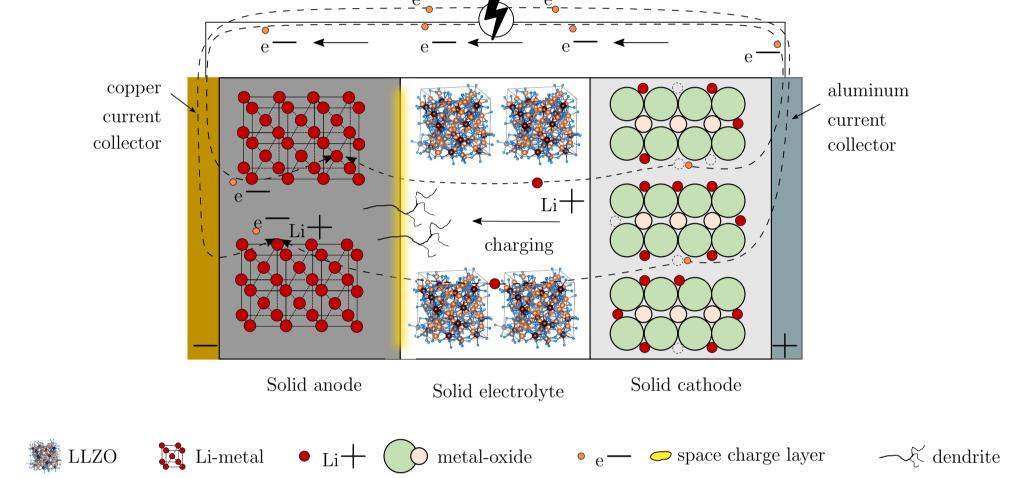
Interface between solid electrode and solid-state electrolyte (SE|SSE) taking place at space charge layer (SCL) [2] found in ASSBs critically exhibits mechanical and electrochemical instability [3]. This evidence points directly to the fact that the soft metallic li anode is erroneously prone to triggering dendrites, under cycles of electric charge & discharge [4].



Distribution: ana. max. shear stress ${}^{\mathcal{W}}\!\!\sigma_{x_1x_2}^{\Pi}$ around crack tip a_c .

Next-generation All-solid-state battery

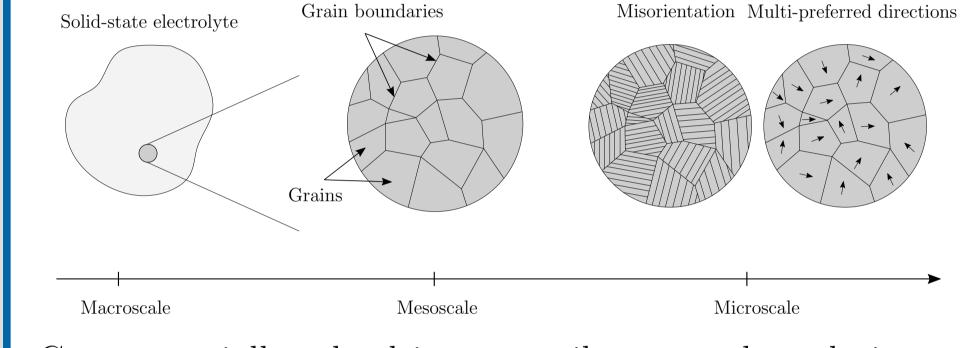
Nucleation taking place at critical dendritic (SE|SSE)-interface



Nucleation taking place at critical dendritic (SE|SSE)-interface Nucleation taking place at critical dendritic (SE|SSE)-interface

Embedded structural-tensor SSE

Polycrystalline garnet-typed SSE such as LLZO exhibit grain boundaries and various sizes and shapes of grains under microscopic observation. Therefore, this type of microstructure distinctively leads to nuance destruction of ceramic-like materials.



Consequentially, dendrites contribute to degradation of ionic conductivity and trace along grain boundaries in SSE.

Nucleation interface: Taking place at the critical dendritic interface

$$ho\,\partial_{t^2}^2oldsymbol{u}^{(s)} +
abla\cdot\left(\mathbb{C}^{4}f^{\mathbb{D}(\Omega)}_{(\lambda,\mu)}:
ablaoldsymbol{u}^{(s)}
ight) +
ho
abla V_e = oldsymbol{0},$$

s.t.
$$a_{\text{Griffith}} := a^* = \arg\min_{a \in \mathbb{R}} \iiint_{\Omega} f(a, \boldsymbol{u}; \lambda, \mu, \boldsymbol{d} \otimes \boldsymbol{d}) d\Omega - \iint_{\Gamma} f(a; \gamma) d\Gamma \Big|_{\boldsymbol{u}}$$

$$ho \, \partial_{t^2}^2 oldsymbol{u}^{(s)} +
abla \cdot \left(\overset{4}{\mathbb{C}} f^{\mathbb{D}(\Omega)}_{(\lambda,\mu)} :
abla oldsymbol{u}^{(s)}
ight) +
ho
abla V_e = oldsymbol{0},$$

s.t.
$$a_{\text{Griffith}} := a^* = \arg\min_{a \in \mathbb{R}} \iiint_{\Omega} f(a, \boldsymbol{u}; \lambda, \mu, \boldsymbol{d} \otimes \boldsymbol{d}) d\Omega - \iint_{\Gamma} f(a; \gamma) d\Gamma$$

$$ho \, \partial_{t^2}^2 oldsymbol{u}^{(s)} +
abla \cdot \left(\overset{4}{\mathbb{C}}^{f_{(\lambda,\mu)}^{\mathbb{D}(\Omega)}} :
abla oldsymbol{u}^{(s)}
ight) +
ho
abla V_e = oldsymbol{0},$$

s.t.
$$a_{\text{Griffith}} := a^* = \arg\min_{a \in \mathbb{R}} \iiint_{\Omega} f(a, \boldsymbol{u}; \lambda, \mu, \boldsymbol{d} \otimes \boldsymbol{d}) d\Omega - \iint_{\Gamma} f(a; \gamma) d\Gamma \Big|_{\boldsymbol{u}}$$

$$ho \, \partial_{t^2}^2 oldsymbol{u}^{(s)} +
abla \cdot \left(\overset{4}{\mathbb{C}}^{f_{(\lambda,\mu)}^{\mathbb{D}(\Omega)}} :
abla oldsymbol{u}^{(s)}
ight) +
ho
abla V_e = oldsymbol{0},$$

s.t.
$$a_{\text{Griffith}} := a^* = \arg\min_{a \in \mathbb{R}} \iiint_{\Omega} f(a, \boldsymbol{u}; \lambda, \mu, \boldsymbol{d} \otimes \boldsymbol{d}) d\Omega - \iint_{\Gamma} f(a; \gamma) d\Gamma \Big|_{\boldsymbol{u}^{(s)}}$$

$$ho \, \partial_{t^2}^2 oldsymbol{u}^{(s)} +
abla \cdot \left(\overset{4}{\mathbb{C}}^{f_{(\lambda,\mu)}^{\mathbb{D}(\Omega)}} :
abla oldsymbol{u}^{(s)}
ight) +
ho
abla V_e = oldsymbol{0},$$

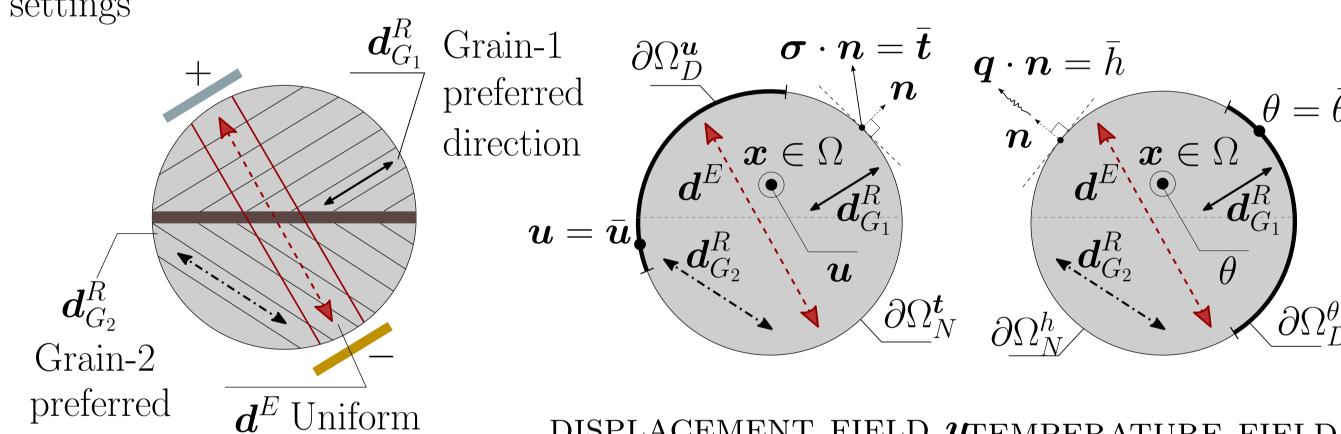
s.t.
$$a_{\text{Griffith}} := a^* = \arg\min_{a \in \mathbb{R}} \iiint_{\Omega} f(a, \boldsymbol{u}; \lambda, \mu, \boldsymbol{d} \otimes \boldsymbol{d}) d\Omega - \iint_{\Gamma} f(a; \gamma) d\Gamma$$

Therefore

$$\therefore \quad a_{\text{Griffith}} := a^* = \arg\min_{a \in \mathbb{R}} \iiint_{\Omega} f(a, \boldsymbol{u}; \lambda, \mu, \boldsymbol{d} \otimes \boldsymbol{d}) \, d\Omega - \iint_{\Gamma} f(a; \gamma) \, d\Gamma \bigg|_{\boldsymbol{u}^{(s)}}$$

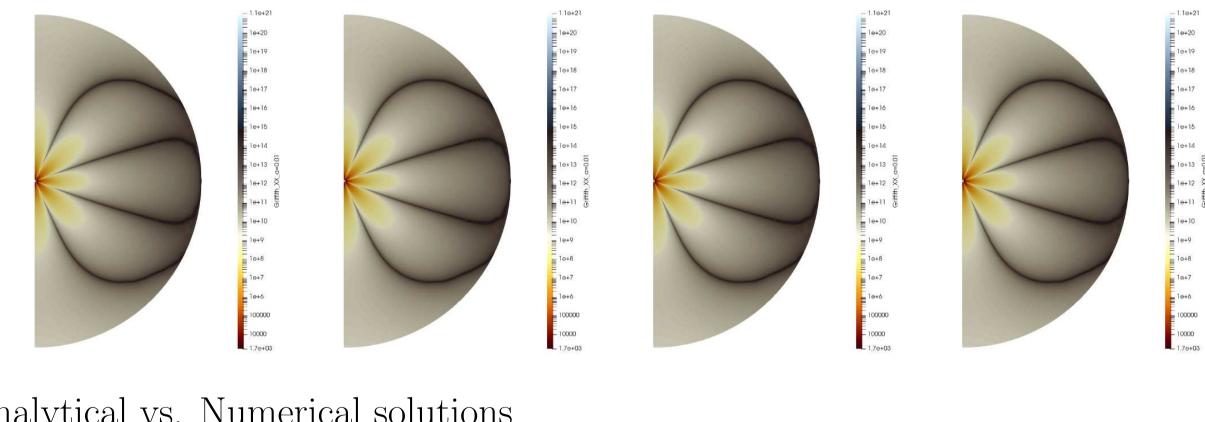
Boundary settings

direction

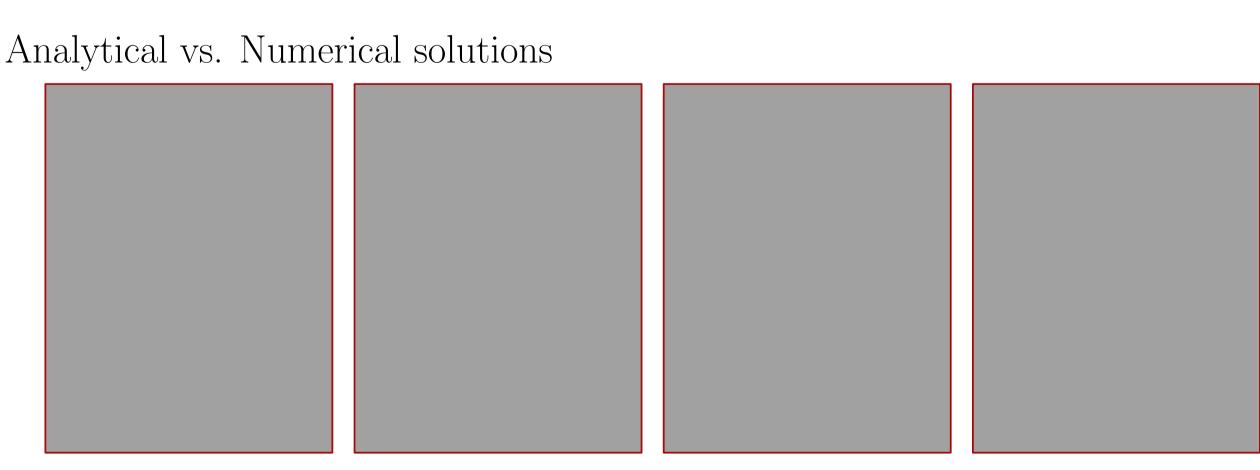


electric-potential polarizational effect

The set of boundary conditions is likewise the path of the pressure-centric dendritic crack.



Comparison: Analytical vs. Numerical solutions



Contact

Tuan Vo vo@acom.rwth-aachen.de



Scan me

References

 $[1] \textbf{T.Vo}, \textit{Modeling the swelling phenomena of li-ion batt. cells based on a numerical chemo-mech. coupled approach. MA, Robert Bosch Battery Systems GmbH, 2018.$

- [2] S.Braun, C. Yada and A. Latz, Thermodynamically consistent model for Space-Charge-Layer formation in a solid electrolyte. Ir. Phys. Chem., 119, 22281-22288, 2015.
- [3] **C.Hüter**, S.Fu, M.Finsterbusch, E.Figgemeier, L.Wells, and R.Spatschek, *Electrode-electrolyte interface stability in solid state electrolyte system: influence of* coating thickness under varying residual stresses. AIMS materials Science, 4(4):867-877, 2017.
- 4 S.Kim, J.S.Kim, L.Miara, Y.Wang, S.K.Jung, S.Y.Park, Z.Song, H.King, M.Badding, J.M.Chang, V.Roev, G.Yoon, R.Kim, J.H.Kim, K.Yoon, D.Im, and K.Kang, High-energy and durable li metal batt. using garnet-type solid electrolytes with tailored li-metal compatibility. Nature Communications, 13(1):1883, 2022.









