# Next-generation all-solid-state battery

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## Mathematical modelling for the next-generation All-solid-state batteries: Nucleation (SE|SSE)<sup>(\*)</sup>-interface

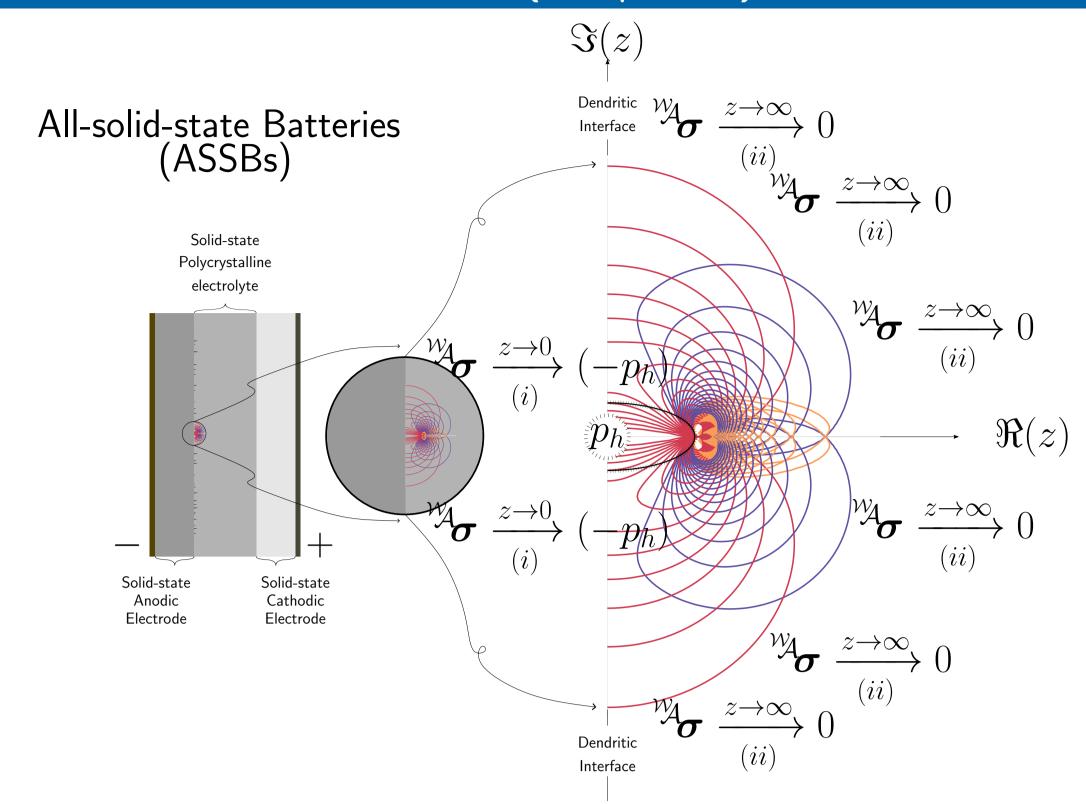
Rechargeable Lithium-ion battery (LIB) is at the heart of every electric vehicle (EV), portable electronic device, and energy storage system [1]. Nowadays, LIBs enable human life more efficient and help to solve global environment issues thanks to EVs' zero emission. However, conventional LIB (c-LIB) is sensible to temperature and pressure, hence, flammable and explosive. This bottleneck is mainly due to liquid-based electrolyte in c-LIBs.

All-solid-state battery (ASSB) is one of promising candidates to overcome bottlenecks of c-LIBs. Thanks to solid-state electrolyte (SSE), ASSB is highly stable towards temperature and pressure. Nevertheless, metallic Li-dendrite triggered at (SE|SSE)-interface is the main drawback as these dendritic threads extrapolate into grain boundary network of SSE, causing crevice, degradation of ionic conductivity, and the probability of short-circuit.

Next-generation All-solid-state battery (ng-ASSB) with a consideration of nucleation criterion defined by

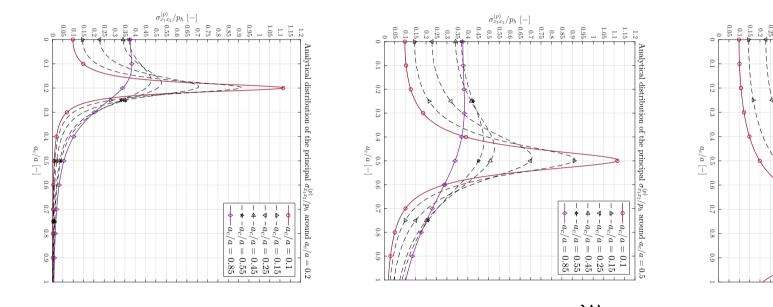
$$a_{\mathsf{Griffith}} := a^* = \arg\min_{a \in \mathbb{R}} \left. \iint_{\Omega} f(a, \boldsymbol{u}; \lambda, \mu, \boldsymbol{d} \otimes \boldsymbol{d}) \, d\Omega - \iint_{\Gamma} f(a; \gamma) \, d\Gamma \right|_{\boldsymbol{u}^0}$$

where, can help to improve ASSB performance.



#### Interface

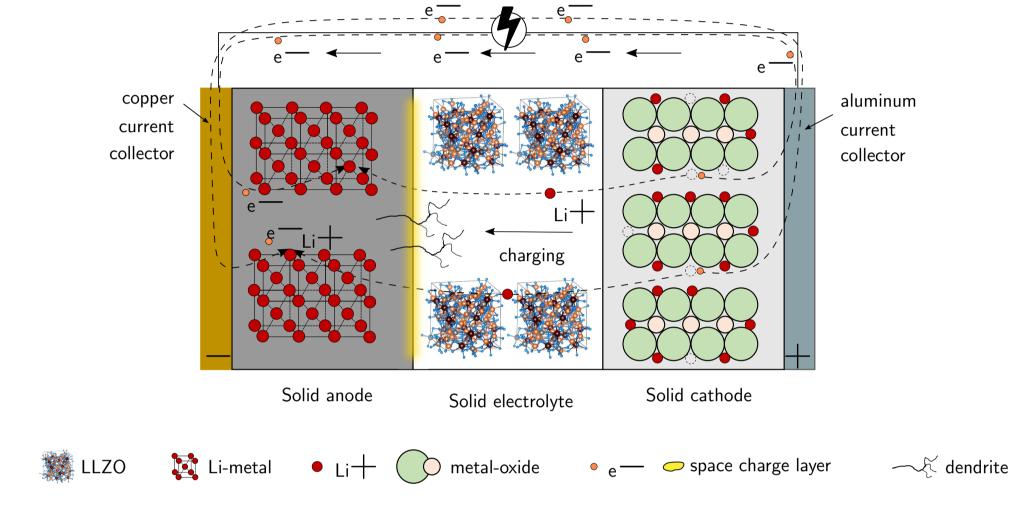
Interface between solid electrode and solid-state electrolyte (SE|SSE) taking place at space charge layer (SCL) [2] found in ASSBs critically exhibits mechanical and electrochemical instability [3]. This evidence points directly to the fact that the soft metallic li anode is erroneously prone to triggering dendrites, under cycles of electric charge & discharge [4].



Distribution: ana. max. shear stress  ${}^{\mathcal{W}}\!\!\sigma_{x_1x_2}^\Pi$  around crack tip  $a_c$ .

# Next-generation All-solid-state battery

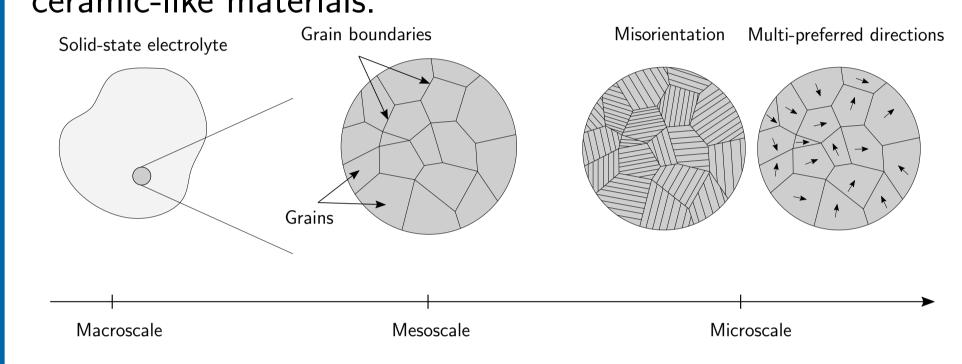
Nucleation taking place at critical dendritic (SE|SSE)-interface



Nucleation taking place at critical dendritic (SE|SSE)-interface Nucleation taking place at critical dendritic (SE|SSE)-interface

### Embedded structural-tensor SSE

Polycrystalline garnet-typed SSE such as LLZO exhibit grain boundaries and various sizes and shapes of grains under microscopic observation. Therefore, this type of microstructure distinctively leads to nuance destruction of ceramic-like materials.



Consequentially, dendrites contribute to degradation of ionic conductivity and trace along grain boundaries in SSE.

## Nucleation interface: Taking place at the critical dendritic interface

 $ho \, \partial_{t^2}^2 oldsymbol{u}^{(s)} + 
abla \cdot \left( \overset{4}{\mathbb{C}}^{f_{(\lambda,\mu)}^{\mathbb{D}(\Omega)}} : 
abla oldsymbol{u}^{(s)} 
ight) + 
ho 
abla V_e = oldsymbol{0},$ 

s.t. 
$$a_{\mathsf{Griffith}} := a^* = \arg\min_{a \in \mathbb{R}} \left. \iint_{\Omega} f(a, \boldsymbol{u}; \lambda, \mu, \boldsymbol{d} \otimes \boldsymbol{d}) \, d\Omega - \iint_{\Gamma} f(a; \gamma) \, d\Gamma \right|_{\Omega}$$

$$ho \, \partial_{t^2}^2 oldsymbol{u}^{(s)} + 
abla \cdot \left( \overset{4}{\mathbb{C}} f^{\mathbb{D}(\Omega)}_{(\lambda,\mu)} : 
abla oldsymbol{u}^{(s)} 
ight) + 
ho 
abla V_e = oldsymbol{0},$$

s.t. 
$$a_{\mathsf{Griffith}} := a^* = \arg\min_{a \in \mathbb{R}} \left. \iint_{\Omega} f(a, \boldsymbol{u}; \lambda, \mu, \boldsymbol{d} \otimes \boldsymbol{d}) \, d\Omega - \iint_{\Gamma} f(a; \gamma) \, d\Gamma \right|_{\boldsymbol{u}}$$

$$ho \, \partial_{t^2}^2 oldsymbol{u}^{(s)} + 
abla \cdot \left( \overset{4}{\mathbb{C}}^{f_{(\lambda,\mu)}^{\mathbb{D}(\Omega)}} : 
abla oldsymbol{u}^{(s)} 
ight) + 
ho 
abla V_e = oldsymbol{0},$$

$$\text{s.t.} \quad a_{\mathsf{Griffith}} := a^* = \arg\min_{a \in \mathbb{R}} \left. \iint_{\Omega} f(a, \boldsymbol{u}; \lambda, \mu, \boldsymbol{d} \otimes \boldsymbol{d}) \, d\Omega - \left. \iint_{\Gamma} f(a; \gamma) \, d\Gamma \right|_{\boldsymbol{u}}$$

$$ho \, \partial_{t^2}^2 oldsymbol{u}^{(s)} + 
abla \cdot \left( \overset{4}{\mathbb{C}} f^{\mathbb{D}(\Omega)}_{(\lambda,\mu)} : 
abla oldsymbol{u}^{(s)} 
ight) + 
ho 
abla V_e = oldsymbol{0},$$

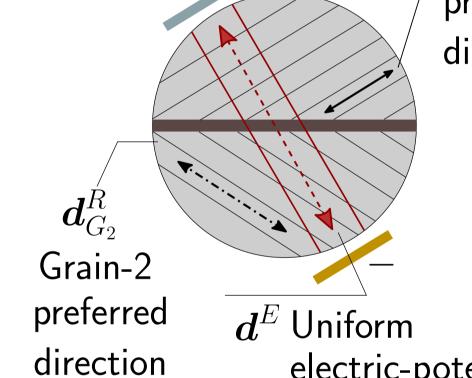
s.t. 
$$a_{\mathsf{Griffith}} := a^* = \arg\min_{a \in \mathbb{R}} \left. \iint_{\Omega} f(a, \boldsymbol{u}; \lambda, \mu, \boldsymbol{d} \otimes \boldsymbol{d}) \, d\Omega - \iint_{\Gamma} f(a; \gamma) \, d\Gamma \right|_{\boldsymbol{u}}$$

$$\rho \, \partial_{t^2}^2 \boldsymbol{u}^{(s)} + \nabla \cdot \left( \mathbb{C}^{f_{(\lambda,\mu)}^{\mathbb{D}(\Omega)}} : \nabla \boldsymbol{u}^{(s)} \right) + \rho \nabla V_e = \boldsymbol{0},$$
s.t.  $a_{\mathsf{Griffith}} := a^* = \arg\min_{a \in \mathbb{R}} \left. \iint_{\Omega} f(a,\boldsymbol{u};\lambda,\mu,\boldsymbol{d}\otimes\boldsymbol{d}) \, d\Omega - \int_{\Gamma} f(a;\gamma) \, d\Gamma \right|$ 

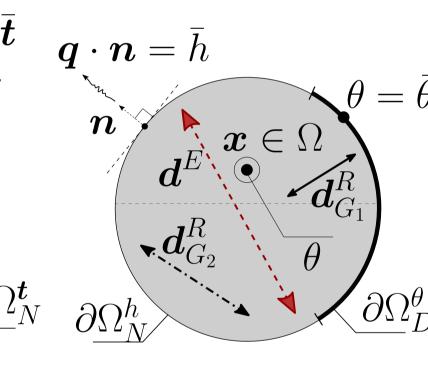
Therefore

$$\therefore \quad a_{\mathsf{Griffith}} := a^* = \arg\min_{a \in \mathbb{R}} \iiint_{\Omega} f(a, \boldsymbol{u}; \lambda, \mu, \boldsymbol{d} \otimes \boldsymbol{d}) \, d\Omega - \iint_{\Gamma} f(a; \gamma) \, d\Gamma \bigg|_{\boldsymbol{u}^{(a)}}$$

Boundary settings



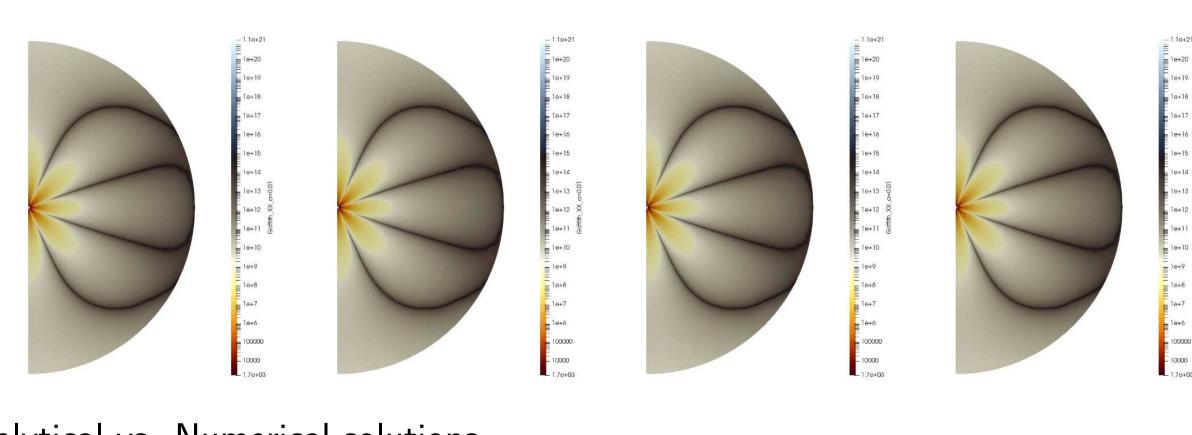
 $oxed{d_{G_1}^R}$  Grain-1  $\partial \Omega^{oldsymbol{u}}_D$   $oldsymbol{\sigma} \cdot oldsymbol{n} = oldsymbol{t}$ preferred direction



displacement field  $oldsymbol{u}$ electric-potential polarizational effect

temperature field  $\theta$ 

The set of boundary conditions is likewise the path of the pressure-centric dendritic crack.



Comparison: Analytical vs. Numerical solutions

#### Contact

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#### References

- [1] **T.Vo**, Modeling the swelling phenomena of li-ion batt. cells based on a numerical chemo-mech. coupled approach. MA, Robert Bosch Battery Systems GmbH, 2018.
- [2] **S.Braun**, C.Yada and A.Latz, *Thermodynamically consistent model for Space-Charge-Layer formation in a solid electrolyte*. Jr. Phys. Chem., 119, 22281-22288, 2015.
- [3] **C.Hüter**, S.Fu, M.Finsterbusch, E.Figgemeier, L.Wells, and R.Spatschek, *Electrode-electrolyte interface stability in solid state electrolyte system: influence of coating* thickness under varying residual stresses. AIMS materials Science, 4(4):867-877, 2017.
- [4] **S.Kim**, J.S.Kim, L.Miara, Y.Wang, S.K.Jung, S.Y.Park, Z.Song, H.King, M.Badding, J.M.Chang, V.Roev, G.Yoon, R.Kim, J.H.Kim, K.Yoon, D.Im, and K.Kang, High-energy and durable li metal batt. using garnet-type solid electrolytes with tailored li-metal compatibility. Nature Communications, 13(1):1883, 2022.









