Next-generation all-solid-state battery (#ASSB)

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Mathematical modelling for the next-generation All-solid-state batteries: Nucleation (SE|SSE)$^{(*)}$-interface

Rechargeable Lithium-ion battery (LIB) is at the heart of every electric vehicle (EV), portable electronic device, and energy storage system [1]. Nowadays, LIBs enable human life more efficient and help to solve global environment issues thanks to EVs' zero emission. However, conventional LIB (c-LIB) is sensible to temperature and pressure, hence, flammable and explosive, which is undesirable. This bottleneck is mainly due to liquid-based electrolyte found in c-LIBs.

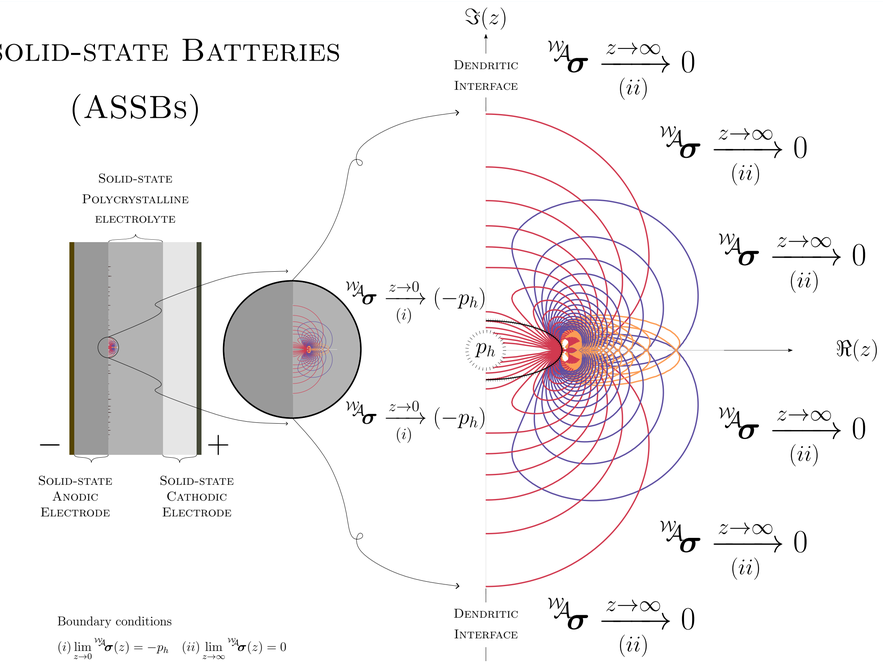
All-solid-state battery (ASSB) is one of promising candidates to overcome bottlenecks of c-LIBs. Thanks to solid-state electrolyte (SSE), ASSB is highly stable towards temperature and pressure. Nevertheless, Li-metal dendrite triggered at (SE|SSE)-interface is the main drawback of ASSB since these dendritic threads extrapolate into SSE grain boundary network, causing crevice, degradation of ionic conductivity, and the probability of short-circuit, which is unfavorable.

Next-generation All-solid-state battery (ng-ASSB) with a consideration of nucleation criterion defined by

$$a_{\text{Griffith}} := a^* = \arg\min_{a\in\mathbb{R}} \iiint_\Omega f(a, \boldsymbol{u}, \theta; \lambda, \mu, \boldsymbol{d}\otimes\boldsymbol{d})\, d\Omega - \iint_\Gamma f(a;\gamma)\, d\Gamma\Big|_{\boldsymbol{u}^{(s)}}$$

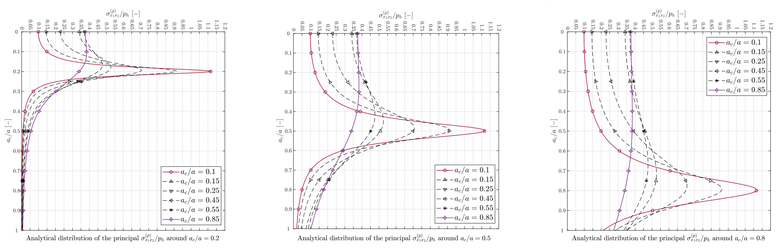
where $\boldsymbol{u}$ displacement field, θ temperature field, a crevice length, λ, μ Lamé constants, $\boldsymbol{d}\otimes\boldsymbol{d}$ embedded misorientation structural tensor, and γ cracking-surface energy density, can help to improve ASSB performance.

All-solid-state Batteries (ASSBs)



Interface Analysis

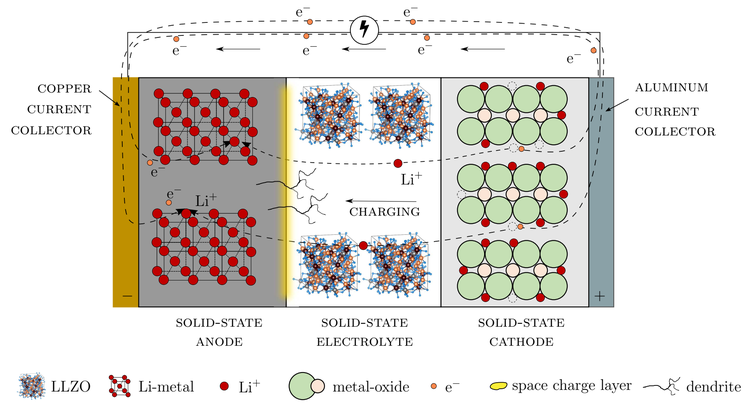
Interface between solid electrode and solid-state electrolyte (SE|SSE) taking place at space charge layer (SCL) [2] found in ASSBs critically exhibits mechanical and electrochemical instability [3]. This evidence points directly to the fact that the soft metallic li anode is erroneously prone to triggering dendrites, under cycles of electric charge & discharge [5].



Distribution: ana. max. shear stress ${}^{\mathcal{M}}\sigma^{\Pi}_{x_1x_2}$ around crack tip a_c.

Next-generation All-solid-state battery

Nucleation criterion governs the instable (SE|SSE)-interface [3]

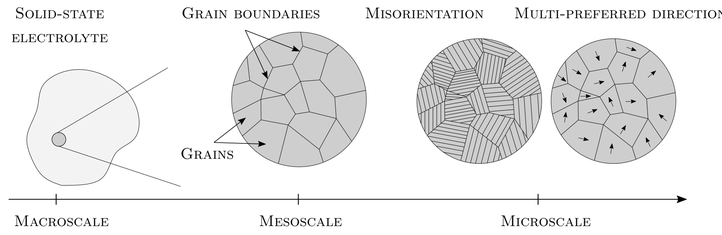


✓ **Thermodynamic consistency** is satisfied, followed by [2].
✓ **Closure** $\bar{\Omega}$ is fulfilled by 15 moments, followed by [4].

Embedded structural-tensor SSE

Polycrystalline garnet-typed SSE such as LLZO exhibit grain boundary network, and grains of various sizes & shapes under microscopic observation. Hence, this type of microstructure is potentially prone to nuance destruction of

$$\boldsymbol{M} := \boldsymbol{d}^R_{G_1} \otimes \boldsymbol{d}^R_{G_2} \quad \text{where} \quad \mathbb{G} := \{\boldsymbol{Q}_{\|_a}, \boldsymbol{Q}_{\perp_a}\} \subset \mathcal{O}(3)$$



Consequentially, dendrites contribute to degradation of ionic conductivity and cracks via tracing along grain boundaries.

Nucleation interface: Taking place at the critical dendritic interface

Coupled fields: Displacement vector field and temperature scalar field

$$\boldsymbol{u} : \begin{cases} \Omega\times\mathbb{R}_+ \to \mathbb{R}^3, \\ (\boldsymbol{x}, t) \mapsto \boldsymbol{u}(\boldsymbol{x}, t), \end{cases} \quad \theta : \begin{cases} \Omega\times\mathbb{R}_+ \to \mathbb{R}, \\ (\boldsymbol{x}, t) \mapsto \theta(\boldsymbol{x}, t), \end{cases} \quad \theta : \begin{cases} \Omega\times\mathbb{R}_+ \to \mathbb{R}, \\ (\boldsymbol{x}, t) \mapsto \theta(\boldsymbol{x}, t), \end{cases}$$

Governing conservation equations

$$\frac{d}{dt}\int_\Omega (\cdot)\, d\Omega = \int_\Omega (\cdot)^{\text{action}}\, d\Omega + \int_{\partial\Omega} (\cdot)^{\text{action}}\, d\partial\Omega + \int_\Omega (\cdot)^{\text{production/source/sink}}\, d\Omega$$

$\rho(\boldsymbol{x}, t)$ is mass density per unit volume (puv); $\boldsymbol{b}(\boldsymbol{x}, t)$ body force puv; $\boldsymbol{v}(\boldsymbol{x}, t)$ velocity; $e(\boldsymbol{x}, t)$ internal energy puv; $\boldsymbol{q}(\boldsymbol{x}, t)$ heat flux; $r(\boldsymbol{x}, t)$ heat source puv; $\boldsymbol{\sigma}$ Cauchy stress and $\boldsymbol{\varepsilon}$ infinitesimal strain. Helmholtz energy functional

$$a_{\text{Griffith}} := a^* = \arg\min_{a\in\mathbb{R}} \iiint_\Omega f(a, \boldsymbol{u}; \lambda, \mu, \boldsymbol{d}\otimes\boldsymbol{d})\, d\Omega - \iint_\Gamma f(a;\gamma)\, d\Gamma\Big|_{\boldsymbol{u}^{(s)}}$$

Governing PDE

$$a_{\text{Griffith}} := a^* = \arg\min_{a\in\mathbb{R}} \iiint_\Omega f(a, \boldsymbol{u}; \lambda, \mu, \boldsymbol{d}\otimes\boldsymbol{d})\, d\Omega - \iint_\Gamma f(a;\gamma)\, d\Gamma\Big|_{\boldsymbol{u}^{(s)}}$$

abc

Strain energy: Interface between solid electrode and solid-state electrolyte (SE|SSE) taking place at space charge

$$\iiint_\Omega f(a, \boldsymbol{u}; \lambda, \mu, \boldsymbol{d}\otimes\boldsymbol{d})\, d\Omega$$

Surface energy: Interface between solid electrode and solid-state electrolyte (SE|SSE) taking place

$$\iint_\Gamma f(a;\gamma)\, d\Gamma$$

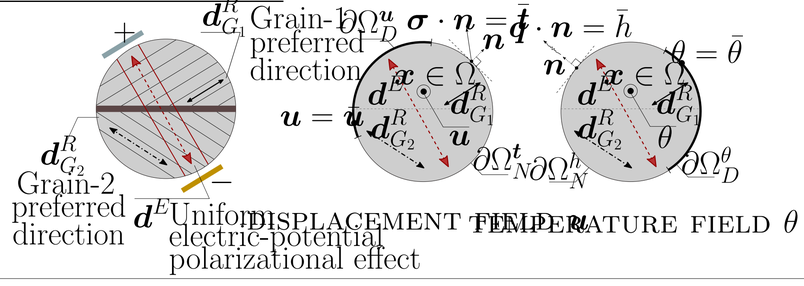
Therefore

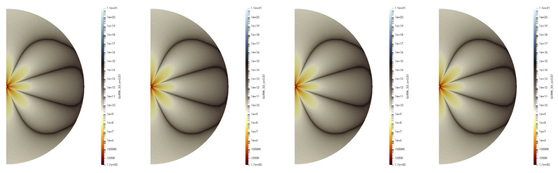
$$\rho\,\partial^2_{t^2}\boldsymbol{u}^{(s)} + \nabla\cdot\left(\overset{4}{\mathbb{C}}{}^{f^{\mathbb{D}(\Omega)}_{(\lambda,\mu)}} : \nabla\boldsymbol{u}^{(s)}\right) + \rho\nabla V_e = \boldsymbol{0},$$

$$\text{s.t.} \quad a_{\text{Griffith}} := a^* = \arg\min_{a\in\mathbb{R}} \iiint_\Omega f(a, \boldsymbol{u}; \lambda, \mu, \boldsymbol{d}\otimes\boldsymbol{d})\, d\Omega - \iint_\Gamma f(a;\gamma)\, d\Gamma\Big|_{\boldsymbol{u}^{(s)}}$$

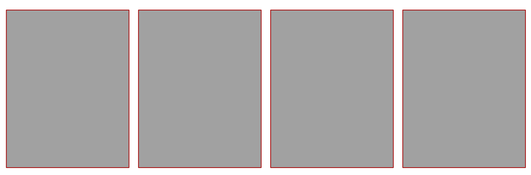
abc

Boundary condition settings

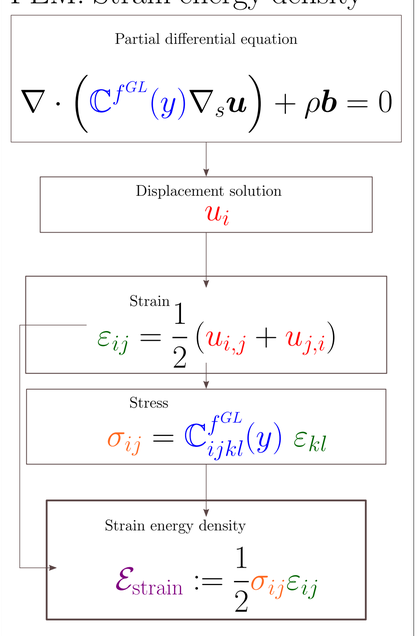




Comparison: Analytical vs. Numerical solutions



FEM: Strain energy density



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Airy-Westergaard function used for max. shear stress analysis

$${}^{\mathcal{M}}\mathcal{A} : \mathbb{C}\to\mathbb{C}, z\mapsto {}^{\mathcal{M}}\mathcal{A}(z) := \Re\Big(\oiint_\Gamma \mathcal{K}^{(\star)}\, dz\Big) + x_2\,\Im\Big(\oint_\Gamma \mathcal{K}^{(\star)}\, dz\Big), \mathcal{K}^c(z) := -p_h + p_h/\sqrt{1 - a^2/z^2},$$

where $\{p_h, a\}\in\mathbb{R}_+$ is the.

FEM implementation: element matrix $\boldsymbol{K}^e$ approx. by *Gauss quadrature*; indices imply $4+2=6$ *for-loop*:

$$K^{\alpha\beta}_{e\,ik} = \int_{\Omega^\xi}\left(\mathcal{L}^\alpha_1\ \mathbb{C}^{f^{GL}}_{i1k1}(y)\ \mathcal{R}^\beta_1 + \mathcal{L}^\alpha_1\ \mathbb{C}^{f^{GL}}_{i1k2}(y)\ \mathcal{R}^\beta_2 + \mathcal{L}^\alpha_2\ \mathbb{C}^{f^{GL}}_{i2k1}(y)\ \mathcal{R}^\beta_1 + \mathcal{L}^\alpha_2\ \mathbb{C}^{f^{GL}}_{i2k2}(y)\ \mathcal{R}^\beta_2\right)\det(\boldsymbol{J})\ d\Omega^\xi$$

where $\mathcal{L}^\alpha_j$ and $\mathcal{R}^\beta_l$ are gradients of basis functions at node α^{th} and β^{th}, respectively.

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