# Algorithms for Wireless Communications II

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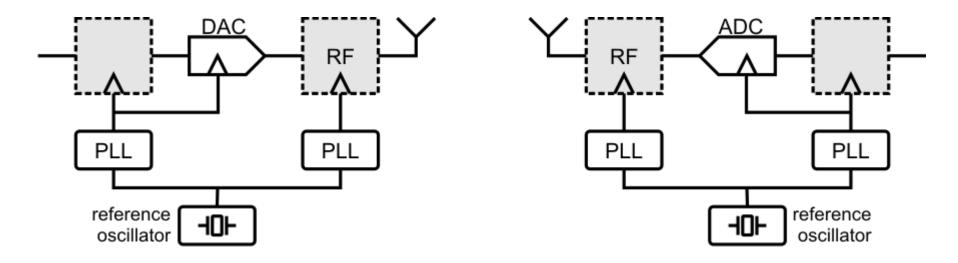
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## **OFDM Synchronization**



## The Need for Synchronization



- A reference oscillator provides a reference frequency
  - Typical references: 1 MHz, 10 MHz, or 20 MHz (good quartz oscillators available)
- All system frequencies (samling frequency and carrier frequency) are derived from this reference using Phase Locked Loops

#### Each device has ist own reference

- References are never 100% accurate
- Signal propagation causes an unknown delay (phase) between devices



## The Need for Synchronization

- Frequency reference oscillators are specified only by ist nominal value
- Individual parts can and do deviate from this nominal value
- Oscillator accuracy is espressed in *Parts per Million [ppm]* 
  - Frequency independent metric
  - PPM is typically specified on both directions
- Impact of oscillator accuracy on frequency offset/error

Reference: 
$$\Delta f_{\text{ref}} = \varphi \frac{f_{\text{ref}}}{10^6}$$

After PLL: 
$$\Delta f_0 = \varphi \frac{f_{\text{ref}} N}{10^6 K} = \varphi \frac{f_0}{10^6}$$

■ Typical reference accuracy: 8 – 20ppm



## **Synchronization Errors**

- Initial Timing Offset
- Carrier Frequency Offset
- Signal to Noise Ratio
- Carrier Phase Noise
- Sampling Frequency Offset



#### Example: IEEE 802.11n WLAN

- Carrier frequency: 2.4 GHz
- Bandwidth (sampling frequency): 40 Mhz (128 tones: 312.5 KHz carrier spacing)
- Reference oscillator: ±10 ppm

#### Carrier frequency

$$-24 \text{ kHz} < \Delta f_0^{Tx} < +24 \text{ kHz}$$
  $-24 \text{ kHz} < \Delta f_0^{Rx} < +24 \text{ kHz}$ 

$$-48 \text{ kHz} < \left| f_0^{Tx} - f_0^{Rx} \right| < +48 \text{ kHz}$$

- More than 10% of the carrier spacing
- 70deg per OFDM symbol

#### Sampling frequency

$$-400 \text{ Hz} < \Delta f_s^{Tx} < +400 \text{ Hz}$$
  $-400 \text{ Hz} < \Delta f_s^{Rx} < +400 \text{ Hz}$ 

$$-800 \text{ Hz} < |f_S^{Tx} - f_S^{Rx}| < +800 \text{ Hz}$$

1 sample per 300 OFDM symbols



## Synchronization (Tx Matched Filter)

y[t]

Preamble p[t]

Data

Data

Preamble  $p^*[t]$ 

#### Received signal with frequency offset (no noise) - Dirac channel

$$y[t] = e^{\frac{2\pi\Delta ft}{N}}p[t-t_0]$$
 normalized to the

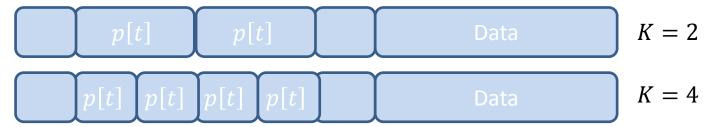
 $\Delta f$ : Frequency offset, normalized to the symbol duration. One period in  $\frac{1}{NT_S} \Rightarrow \Delta f = 1$ 

**Correlation with transmitted sequence** 

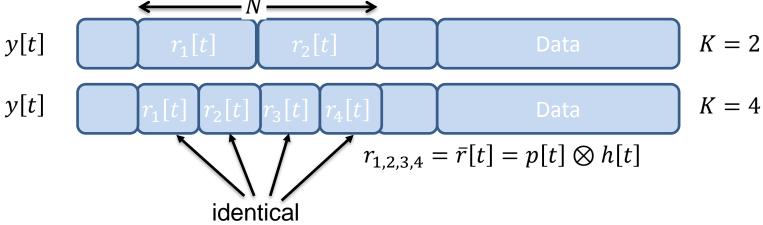
$$c_{\Delta t} = \sum_{t=0}^{N} y[t] p^*[t - \Delta t] = \sum_{t=0}^{N} e^{\frac{2\pi \Delta f t}{N}} p[t - t_0] p^*[t - \Delta t]$$

Assume  $\Delta t = t_0$ : what happens when the normalized frequency offset  $\Delta f = 1$ ?

#### New preamble design: OFDM symbol is periodic in itself

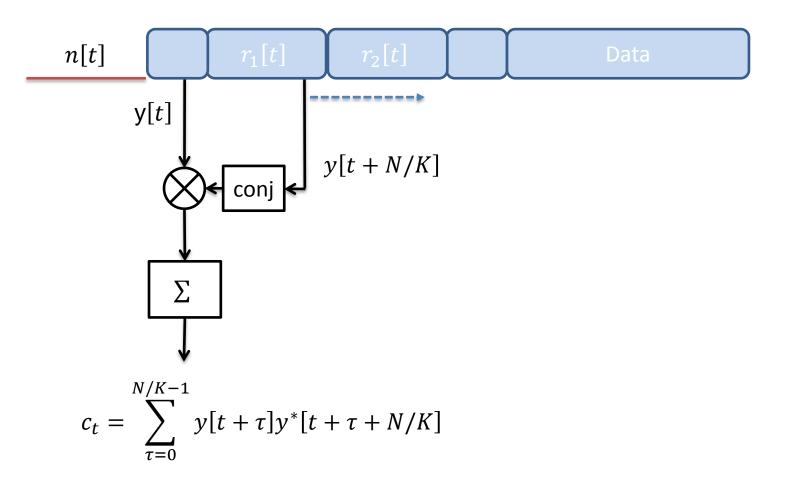


Received preamble after convolution with the channel (no freq. offset)

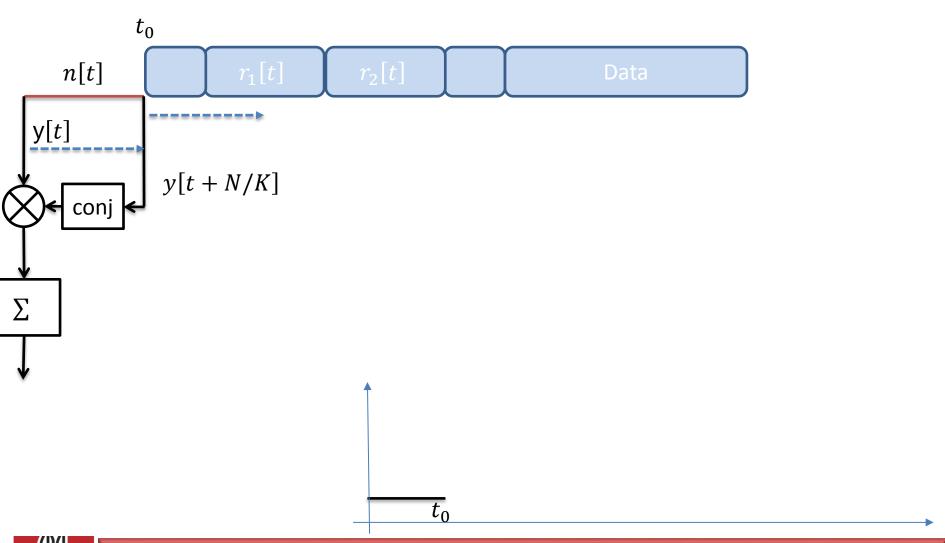


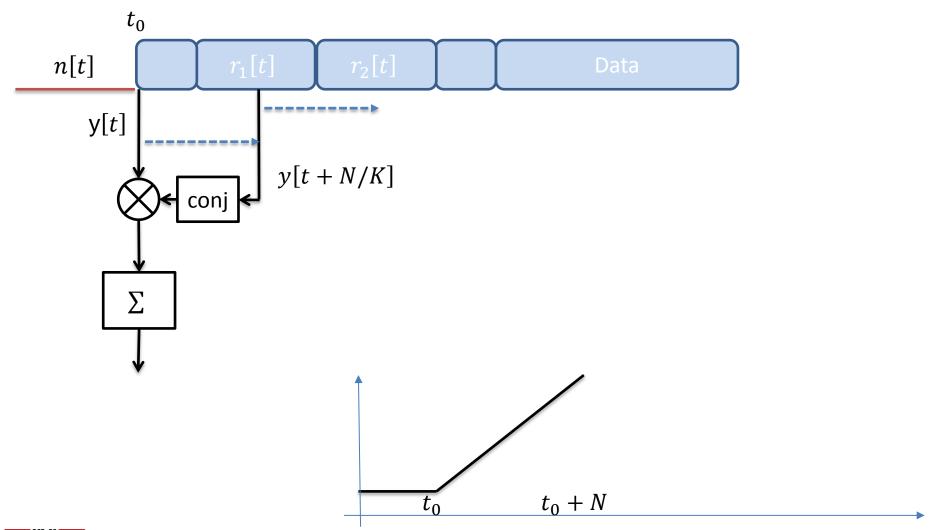
With frequency offset: 
$$r_k[t] = e^{\frac{2\pi\Delta ft}{N} + \frac{2\pi\Delta f(k-1)}{K}} \, \bar{r}[t]$$



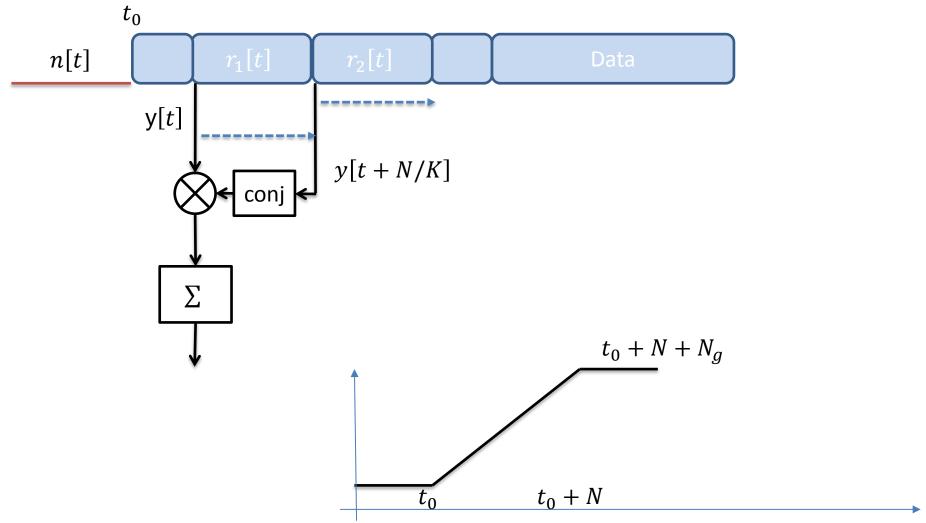




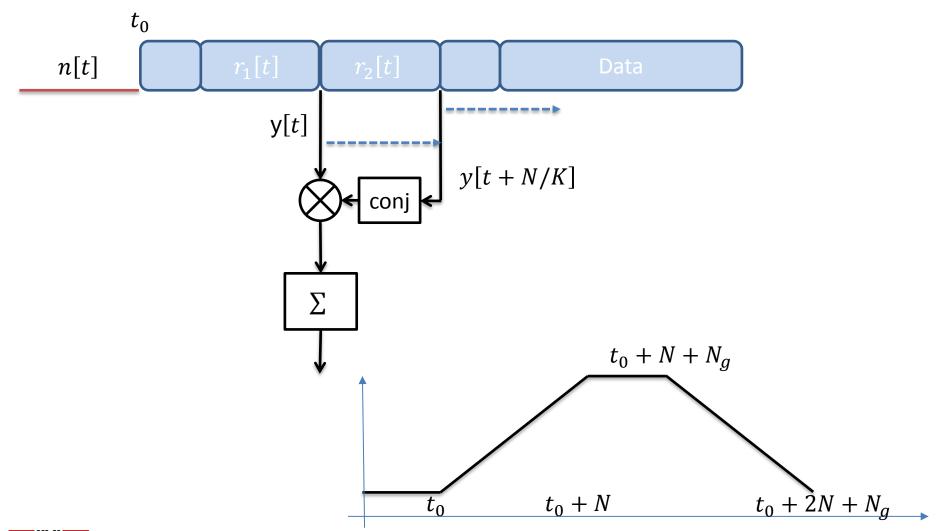




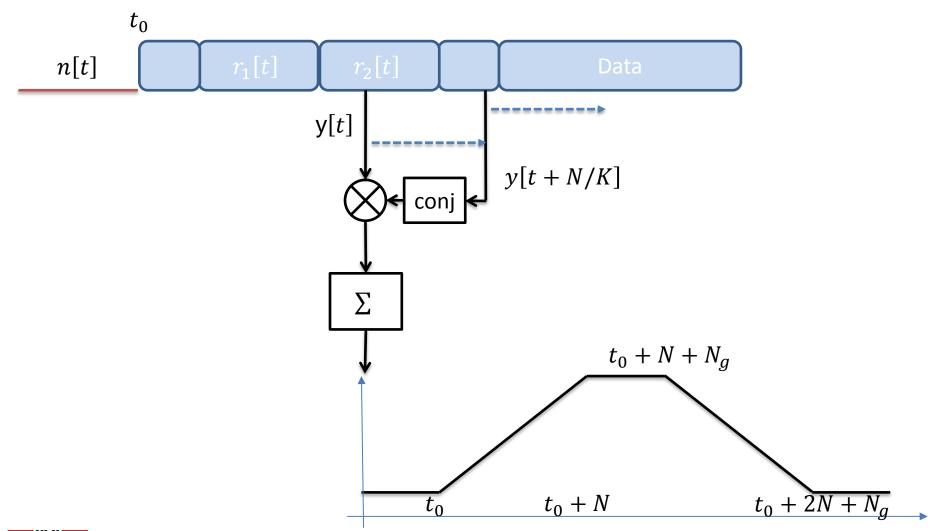




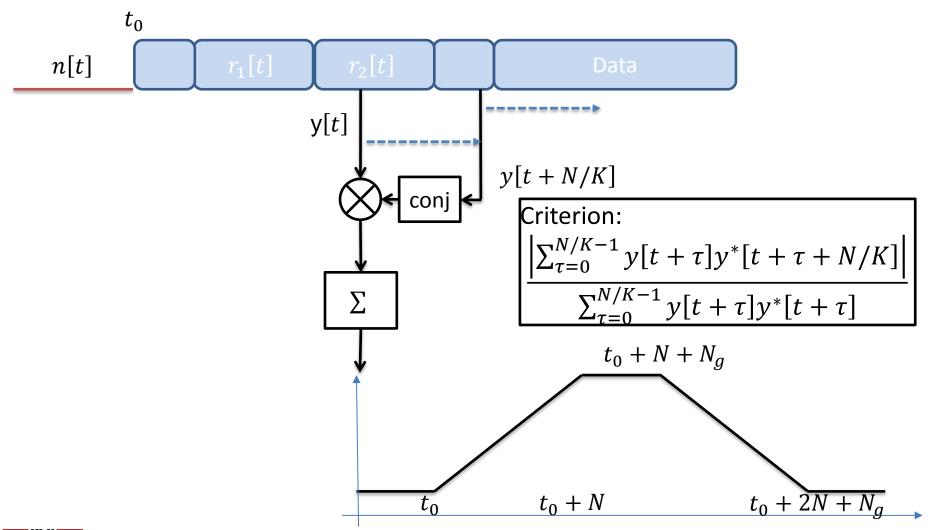






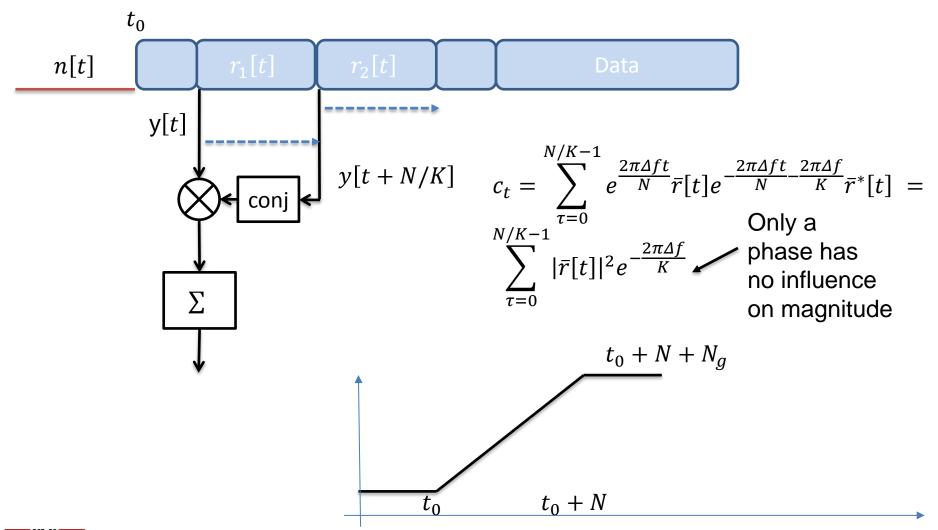








#### Robustness against frequency offset





## Freq. Offset Estimation with Periodic Preamble (OFDM)

Idea: use phase of the autocorrelation at  $t_0 + N + N_g$  for freq. offset estimation

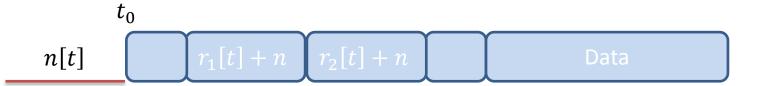


$$c_{t_0+N+N_g} = \sum_{\tau=0}^{N/K-1} |\bar{r}[t]|^2 e^{-\frac{2\pi\Delta f}{K}}$$
$$-2\pi\Delta f_0 K = \angle c_t$$
$$\Delta f_0 = -\frac{\angle c_t}{2\pi K}$$



## **SNR Estimation with Periodic Preamble (OFDM)**

#### Introduce a preamble consisting of two identical OFDM training symbols



$$y[t + kN/K] = \bar{r}[t] + n[t + kN/K]$$

$$A = \frac{1}{N} \sum_{\tau=0}^{N-1} y[t] y^*[t + kN/K] = \frac{1}{N} \sum_{\tau=0}^{N-1} \bar{r}[t] \bar{r}^*[t] + n[t] n^*[t + kN/K] \approx E\{|\bar{r}[t]|^2\} + \underbrace{E\{n[t]n^*[t + kN/K]\}}_{\to 0}$$

$$B = \frac{1}{N} \sum_{\tau=0}^{N-1} |y[t]|^2 \approx E\{|\bar{r}[t]|^2\} + E\{|n[t]|^2\} \qquad SNR = \frac{E\{|\bar{r}[t]|^2\}}{E\{|n[t]|^2\}} = \frac{A}{B-A}$$



#### Residual carrier offset and phase noise

#### Signal after CFO compensation in time domain

- Assume phase  $\Theta(t)$  changes only very slowly => constant within an OFDM symbol
- Does not cause inter carrier interference, but

$$y[t] = e^{j\Theta(t)} \sum_{k=0}^{\infty} s[t - k(N + N_g)] \approx \sum_{k=0}^{\infty} e^{j\Theta(k(N + N_g))} s_k[t - k(N + N_g)]$$

#### Signal still rotates over time

#### Consider the freq. domain representation of the kth OFDM symbol

$$DFT\left\{e^{j\Theta\left(k(N+N_g)\right)}s_k[t]\right\} = e^{j\Theta\left(k(N+N_g)\right)}s[f]h[f]$$

- All tones are affected equally by the frequency offset
- Solution: insert known Pilot tones at carrier  $f_p$  to estimate  $\Theta\left(k(N+N_g)\right)$  as  $\Theta\left(k(N+N_g)\right) = \angle \psi_k[f_p] p^*[f] h^*[f]$



## Timing offset in frequency domain

#### Sampling offset leads to a drift in the start of OFDM symbols over time



$$DFT\{y_1[t]\} = p[f]h[f]$$

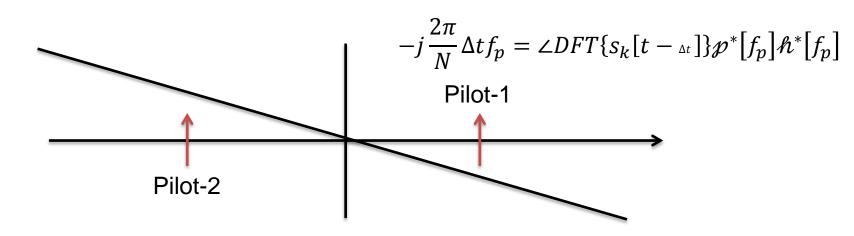


$$DFT\{y_k[t]\} = DFT\{s_k[t - \Delta t]\} = s[f] h[f] e^{-j\frac{2\pi}{N}\Delta tf}$$

Timing offset leads to a linear phase change over tones

Pilot tones @ 
$$f_p$$

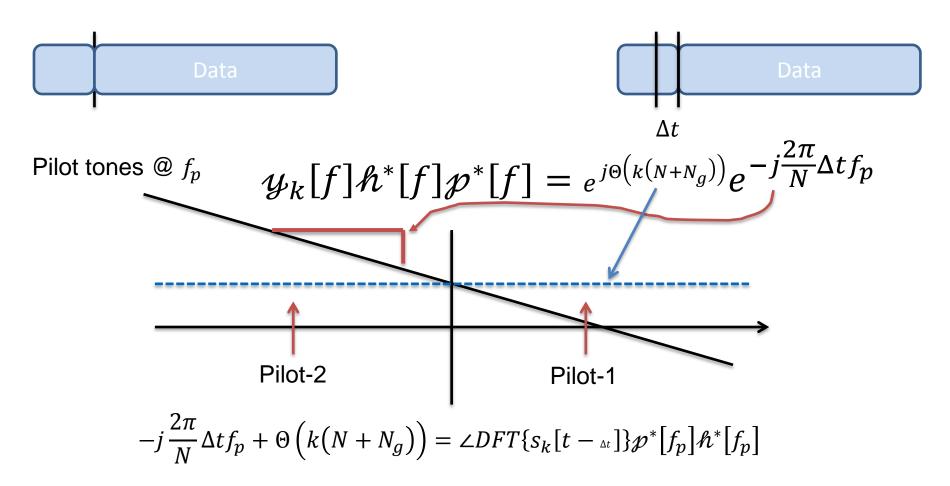
Pilot tones @ 
$$f_p$$
  $\psi_k[f] h^*[f] p^*[f] = e^{-j\frac{2\pi}{N}\Delta t f_p}$ 





#### Timing offset and phase noise in frequency domain

Sampling offset leads to a drift in the start of OFDM symbols over time



Slope (across tones): timing offset; mean (across tones): phase noise

