

Charge Pump Derivation

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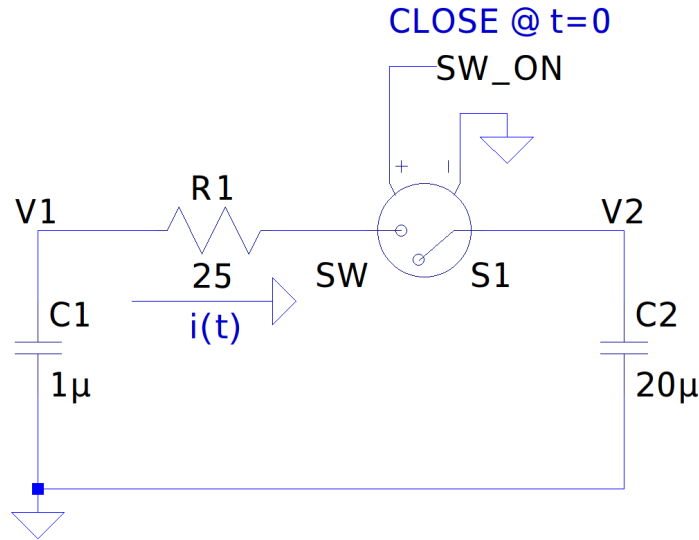


Figure 1: Charge Pump discharge cycle operation

0.1 Initial observations

Figure 1 depicts part of a charge pump circuit during the discharging cycle. C_1 is the flying capacitor that was charged to a voltage of V_1 . At time $t = 0$ the switch S_1 will close and C_1 will begin to discharge into C_2 .

The goal of this exercise is to determine how much energy is dissipated in $R1$ and determine the final voltage after the circuit has stabilized. A closed-form solution for $i(t)$ is determined, it can be used to quantify how much charge is transferred from C_1 to C_2 in this scenario. The final voltages, V_1 and V_2 , can be determined from the integral of i_t by subtracting this charge from C_1 or adding it to C_2 . In the final settled state it is apparent that $V_1 = V_2$.

0.2 Useful relationships

This section presents a set of fundamental relationships that may be used to determine the function for $i(t)$.

$$i(t) = -C_1 \frac{dV_1}{dt} \quad (1)$$

$$i(t) = C_2 \frac{dV_2}{dt} \quad (2)$$

$$i(t) = \frac{V_1(t) - V_2(t)}{R_1} \quad (3)$$

0.3 Derivation of $i(t)$

First find V_1 and V_2 from equations (1) and (2).

$$\begin{aligned} V_1(t) &= -\frac{1}{C_1} \int i(t) dt \text{ (Negative sign because current is going out of } C_1) \\ V_2(t) &= \frac{1}{C_2} \int i(t) dt \end{aligned} \quad (4)$$

Plug these into (3) and then solve the resulting differential equation for $i(t)$.

$$i(t) = -\frac{1}{R_1} \left(\frac{1}{C_1} \int i(t) dt - \frac{1}{C_2} \int i(t) dt \right) \quad (5)$$

Next differentiate and collect like terms.

$$\begin{aligned} \frac{di(t)}{dt} &= -\frac{\frac{1}{C_1} + \frac{1}{C_2}}{R_1} i(t) \\ R_1 \frac{C_1 C_2}{C_1 + C_2} \left(\frac{1}{i(t)} \right) \frac{di(t)}{dt} &= -1 \end{aligned} \quad (6)$$

Integrating both sides.

$$R_1 \frac{C_1 C_2}{C_1 + C_2} \int \frac{1}{i(t)} dt = \int -1 dt \quad (7)$$

$$R_1 \frac{C_1 C_2}{C_1 + C_2} \left(\ln(i(t)) + C \right) = -t \quad (8)$$

$$\ln(i(t)) + C = -t \frac{C_1 + C_2}{R_1 C_1 C_2} \quad (9)$$

Exponentiate to solve for $i(t)$,

$$\begin{aligned} e^{\ln(i(t))} e^C &= e^{-t \frac{C_1+C_2}{R_1 C_1 C_2}} \\ i(t) &= e^{-C} e^{-t \frac{C_1+C_2}{R_1 C_1 C_2}} \end{aligned} \quad (10)$$

Finally the integration constant can be determined by considering the initial conditions,

$$i(0) = \frac{V_1(0) - V_2(0)}{R_1} \quad (11)$$

The expression (10) is solved for the known initial conditions at $t = 0$ to determine the yet unknown constant of integration. In this case the constant C itself is a "don't care" quantity as we really want to know e^{-C} directly so the entire expression may be expressed in terms of initial voltages and the resistor value.

$$\begin{aligned} \frac{V_1(0) - V_2(0)}{R_1} &= e^{-C} e^{-0 \frac{C_1+C_2}{R_1 C_1 C_2}} \\ \frac{V_1(0) - V_2(0)}{R_1} &= e^{-C} \\ e^{-C} &= \frac{V_1(0) - V_2(0)}{R_1} \end{aligned} \quad (12)$$

Plugging (12) into (10), a closed-form expression for the resistor current, $i(t)$, is obtained.

$$i(t) = \frac{V_1(0) - V_2(0)}{R_1} e^{-t \frac{C_1+C_2}{R_1 C_1 C_2}} \quad (13)$$

Then to help tidy the appearance of things, let

$$V_1(0) = V_{i1} \quad (14)$$

$$V_2(0) = V_{i2} \quad (15)$$

$$\tau = \frac{1}{\frac{C_1+C_2}{R_1 C_1 C_2}} = R_1 \frac{C_1 C_2}{C_1 + C_2} \quad (16)$$

And then the final expression reveals a familiar time domain response. In fact, the circuit could be redrawn as a single capacitor and resistor network driven by a step response with amplitude $V_{i1} - V_{i2}$, and where the capacitor value is equivalent to the series combination of C_1 and C_2 .

$$i(t) = \frac{V_{i1} - V_{i2}}{R_1} e^{-\frac{t}{\tau}} \quad (17)$$