

# Charge Pump Derivation

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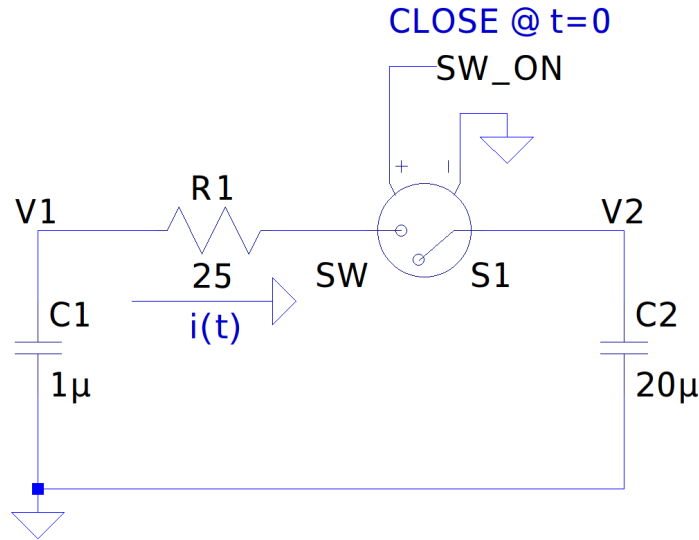


Figure 1: Charge Pump discharge cycle operation

## 0.1 Initial observations

Figure 1 depicts part of a charge pump circuit during the discharging cycle.  $C_1$  is the flying capacitor that was charged to a voltage of  $V_1$ . At time  $t = 0$  the switch  $S_1$  will close and  $C_1$  will begin to discharge into  $C_2$ .

The goal of this exercise is to determine how much energy is dissipated in  $R_1$  and determine the final voltage after the circuit has stabilized. A closed-form solution for  $i(t)$  is determined, it can be used to quantify how much charge is transferred from  $C_1$  to  $C_2$  in this scenario. The final voltages,  $V_1$  and  $V_2$ , can be determined from the integral of  $i(t)$  by subtracting this charge from  $C_1$  or adding it to  $C_2$ . In the final settled state it is apparent that  $V_1 = V_2$ .

## 0.2 Useful relationships

This section presents a set of fundamental relationships that may be used to determine the function for  $i(t)$ .

$$i(t) = -C_1 \frac{dV_1}{dt} \quad (1)$$

$$i(t) = C_2 \frac{dV_2}{dt} \quad (2)$$

$$i(t) = \frac{V_1(t) - V_2(t)}{R_1} \quad (3)$$

### 0.3 Derivation of $i(t)$

First find  $V_1$  and  $V_2$  from equations (1) and (2).

$$\begin{aligned} V_1(t) &= -\frac{1}{C_1} \int i(t) dt \text{ (Negative sign because current is going out of } C_1) \\ V_2(t) &= \frac{1}{C_2} \int i(t) dt \end{aligned} \quad (4)$$

Plug these into (3) and then solve the resulting differential equation for  $i(t)$ .

$$i(t) = -\frac{1}{R_1} \left( \frac{1}{C_1} \int i(t) dt - \frac{1}{C_2} \int i(t) dt \right) \quad (5)$$

Next differentiate and collect like terms.

$$\begin{aligned} \frac{di(t)}{dt} &= -\frac{\frac{1}{C_1} + \frac{1}{C_2}}{R_1} i(t) \\ R_1 \frac{C_1 C_2}{C_1 + C_2} \left( \frac{1}{i(t)} \right) \frac{di(t)}{dt} &= -1 \end{aligned} \quad (6)$$

Integrating both sides.

$$R_1 \frac{C_1 C_2}{C_1 + C_2} \int \frac{1}{i(t)} dt = \int -1 dt \quad (7)$$

$$R_1 \frac{C_1 C_2}{C_1 + C_2} \left( \ln(i(t)) + C \right) = -t \quad (8)$$

$$\ln(i(t)) + C = -t \frac{C_1 + C_2}{R_1 C_1 C_2} \quad (9)$$

Exponentiate to solve for  $i(t)$ ,

$$\begin{aligned} e^{\ln(i(t))} e^C &= e^{-t \frac{C_1+C_2}{R_1 C_1 C_2}} \\ i(t) &= e^{-C} e^{-t \frac{C_1+C_2}{R_1 C_1 C_2}} \end{aligned} \quad (10)$$

Finally the integration constant can be determined by considering the initial conditions,

$$i(0) = \frac{V_1(0) - V_2(0)}{R_1} \quad (11)$$

The expression (10) is solved for the known initial conditions at  $t = 0$  to determine the yet unknown constant of integration. In this case the constant  $C$  itself is a "don't care" quantity as we really want to know  $e^{-C}$  directly.

$$\begin{aligned} \frac{V_1(0) - V_2(0)}{R_1} &= e^{-C} e^{-0 \frac{C_1+C_2}{R_1 C_1 C_2}} \\ \frac{V_1(0) - V_2(0)}{R_1} &= e^{-C} 1 \\ e^{-C} &= \frac{V_1(0) - V_2(0)}{R_1} \end{aligned} \quad (12)$$

Plugging (12) into (10), a closed-form expression for the resistor current,  $i(t)$ , is obtained.

$$i(t) = \frac{V_1(0) - V_2(0)}{R_1} e^{-t \frac{C_1+C_2}{R_1 C_1 C_2}} \quad (13)$$

Then to help tidy the appearance of things, let

$$V_{i1} = V_1(0) \quad (14)$$

$$V_{i2} = V_2(0) \quad (15)$$

$$\tau = \frac{1}{\frac{C_1+C_2}{R_1 C_1 C_2}} = R_1 \frac{C_1 C_2}{C_1 + C_2} \quad (16)$$

And then the final expression reveals a familiar time domain response. In fact, the circuit could be redrawn as a single capacitor and resistor network driven by a step response with amplitude  $V_{i1} - V_{i2}$ , and where the capacitor value is equivalent to the series combination of  $C_1$  and  $C_2$ .

$$i(t) = \frac{V_{i1} - V_{i2}}{R_1} e^{-\frac{t}{\tau}} \quad (17)$$

## 0.4 Determine final settled voltage

Either one of two approaches may be used to determine the final voltage measured at nodes  $V_1 = V_2$ . One approach integrates the current,  $i(t)$ , to determine the charge transferred and then using the formula  $Q = CV$  to solve for the final voltage.

A second approach looks directly to energy lost during the stabilization, or,

$$E_{R1} = R_1 \int_0^\infty i(t)^2 dt \quad (18)$$

### 0.4.1 Charge based approach

The total charge transfer is the following.

$$\begin{aligned} Q_{R1} &= \frac{V_{i1} - V_{i2}}{R_1} \int_0^\infty e^{-\frac{t}{\tau}} dt \\ &= \frac{V_{i1} - V_{i2}}{R_1} \left[ -\tau e^{-\frac{t}{\tau}} \right]_0^\infty \\ &= \frac{V_{i1} - V_{i2}}{R_1} \left[ 0 - \left( -\tau e^{-\frac{0}{\tau}} \right) \right] \\ &= \tau \frac{V_{i1} - V_{i2}}{R_1} \end{aligned} \quad (19)$$

Next it is observed that the same amount of charge leaves  $C_1$  and is added to  $C_2$ . The final charge,  $Q_f$ , can be expressed in terms of either  $V_1$  or  $V_2$  as follows.

$$\begin{aligned}
Q_{f1} &= C_1 V_{i1} - Q_{R1} = C_1 V_f \\
Q_{f2} &= C_2 V_{i2} + Q_{R1} = C_2 V_f
\end{aligned} \tag{20}$$

Picking one,

$$Q_{f2} = C_2 V_{i2} + \tau \frac{V_{i1} - V_{i2}}{R_1} \tag{21}$$

Since the quantity  $V_f$  is wanted, the expression (21) is solved.

$$\begin{aligned}
C_2 V_f &= C_2 V_{i2} + \tau \frac{V_{i1} - V_{i2}}{R_1} \\
V_f &= V_{i2} + \tau \frac{V_{i1} - V_{i2}}{R_1 C_2}
\end{aligned} \tag{22}$$

#### 0.4.2 Energy based approach

Combined with knowledge of energy stored in capacitors,

$$\begin{aligned}
E_{FINAL} &= E_{C1} + E_{C2} - E_{R1} \\
&= \frac{1}{2}(C_1 + C_2)V_{FINAL}^2
\end{aligned} \tag{23}$$

where,

$$\begin{aligned}
E_{C1} &= \frac{1}{2}C_1 V_1^2 \\
E_{C2} &= \frac{1}{2}C_2 V_2^2
\end{aligned} \tag{24}$$

And then the expression for  $E_{R1}$  is determined by the following,

$$\begin{aligned}
E_{R1} &= R_1 \int_0^\infty \left( \frac{V_{i1} - V_{i2}}{R_1} e^{-\frac{t}{\tau}} \right)^2 dt \\
&= R_1 \left( \frac{V_{i1} - V_{i2}}{R_1} \right)^2 \int_0^\infty e^{-\frac{2t}{\tau}} dt \\
&= \frac{(V_{i1} - V_{i2})^2}{R_1} \left[ \frac{\tau}{2} e^{-\frac{2t}{\tau}} \right]_0^\infty \\
&= \frac{(V_{i1} - V_{i2})^2}{R_1} \left[ \frac{\tau}{2} e^{-\frac{2(0)}{\tau}} - \frac{\tau}{2} e^{-\frac{2(\infty)}{\tau}} \right] \\
&= \frac{(V_{i1} - V_{i2})^2}{R_1} \left[ \frac{\tau}{2} - 0 \right] \\
&= \frac{\tau}{2R_1} (V_{i1} - V_{i2})^2
\end{aligned} \tag{25}$$

Then (23) is expanded.

$$\begin{aligned}
\frac{1}{2}(C_1 + C_2)V_{FINAL}^2 &= \frac{1}{2}C_1V_{i1}^2 + \frac{1}{2}C_2V_{i2}^2 - \frac{\tau}{2R_1}(V_{i1} - V_{i2})^2 \\
V_{FINAL}^2 &= \frac{C_1V_{i1}^2 + C_2V_{i2}^2 - \frac{\tau}{R_1}(V_{i1} - V_{i2})^2}{C_1 + C_2} \\
V_{FINAL} &= \sqrt{\frac{C_1V_{i1}^2 + C_2V_{i2}^2 - \frac{\tau}{R_1}(V_{i1} - V_{i2})^2}{C_1 + C_2}}
\end{aligned} \tag{26}$$

With sufficient substitution and algebraic manipulation of (26) the expression stated in (22) can be obtained even though equivalence is not immediately apparent. The expression for final voltage from the energy-based approach shows how the charge-based approach is less work.