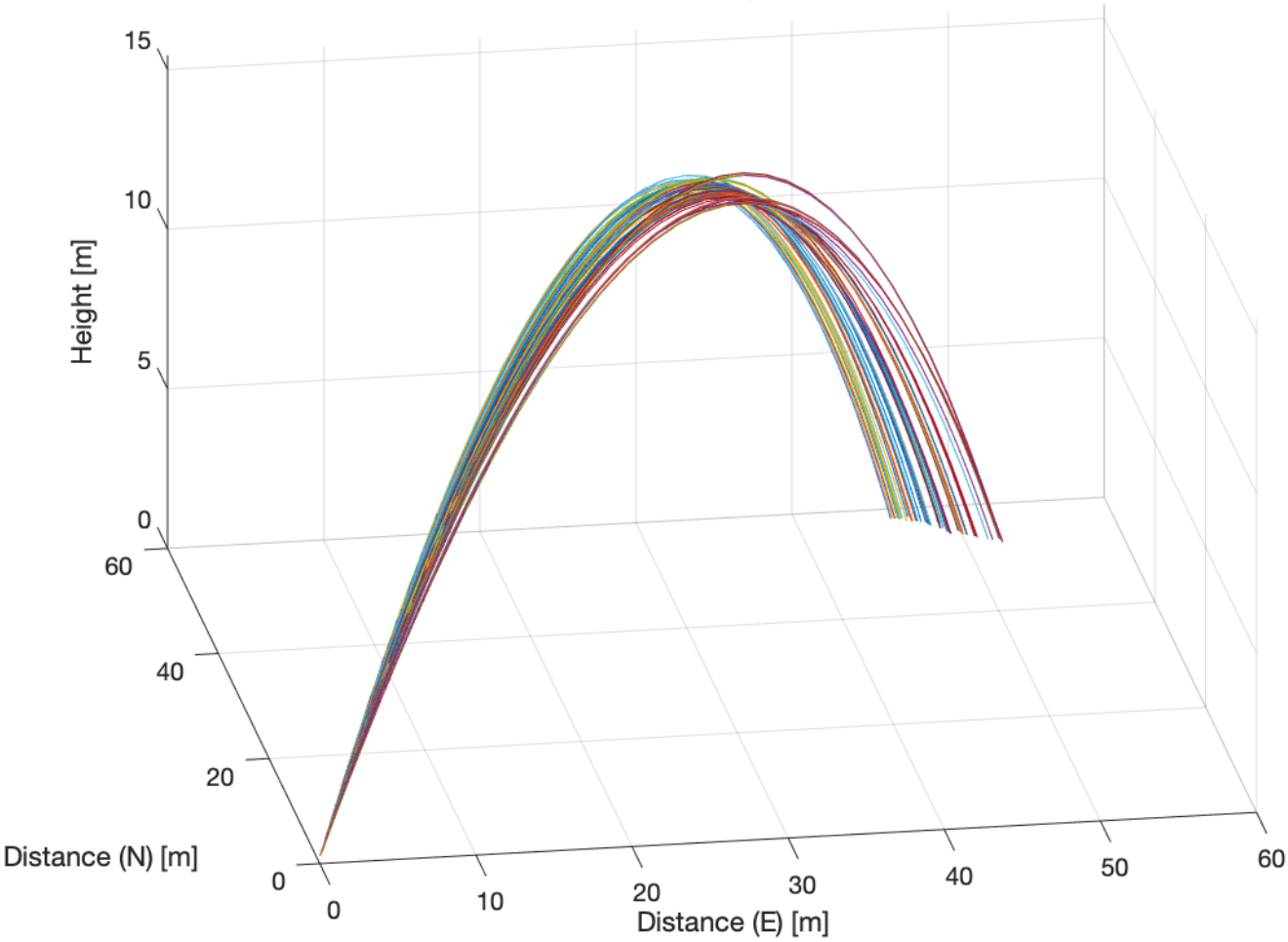


Monte Carlo Sim Height vs. Distance



# Developing a Thermodynamic Model for a Bottle Rocket with Varying Parameters and Uncertainties

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The purpose of this paper is to develop two bottle rocket launch models derived from aerodynamic and thermodynamic principles. The first model will be 2-dimensional and several parameters will be changed in order to analyze and discuss their implications on the rocket's trajectory and thrust. From there, it will be altered to become a 3-dimensional model in order to account for external forces acting on the rocket. Lastly, a Monte Carlo simulation will be done to reflect any uncertainties within the initial data. For each model, there will be verification data from past launches to ensure accuracy within the models. Instead of finding a specific solution for the optimized rocket, this paper serves as a discussion on the process and methods used to create the model.

## Nomenclature

$\vec{a}$	=	Rocket Acceleration
$A_B$	=	Cross-Sectional Area of the Front of the Bottle
$A_t$	=	Throat Area
$c_d$	=	Discharge Coefficient (<1)
$C_D$	=	Drag Coefficient (0.3 to 0.5)
$g$	=	Specific Heat Ratio (1.4)
$\vec{g}$	=	Gravity Vector ( $g_z = 9.8 \text{ m/s}^2$ )
$\vec{F}$	=	Rocket Thrust
$m_{air}$	=	Mass of Air in the Rocket
$m_B$	=	Mass of the Empty Bottle
$m_r$	=	Mass of the Rocket
$M_e$	=	Exit Mach Number
$p_{air}$	=	Air Pressure in the Rocket
$p_a$	=	Ambient Pressure
$p_e$	=	Exit Pressure
$p_*$	=	Critical Pressure
$q$	=	Dynamic Pressure
$R$	=	Ideal Gas Law Constant ( $287 \text{ J/kg}^{-1} \text{ K}^{-1}$ )
$T_{air}$	=	Temperature of Air in the Rocket
$v_{air}$	=	Volume of Air in the Rocket
$v_B$	=	Volume of Bottle
$V_e$	=	Exhaust Velocity
$\vec{V}$	=	Rocket Velocity
$\rho_{air}$	=	Density of Air in the Rocket
$\rho_w$	=	Density of Water in the Rocket

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## I. Introduction

Numerical, computational, or mathematical modeling is a common engineering tool that helps to understand or predict the behavior of a physical system, like a bottle rocket. Engineers can use the results of these numerical simulations to determine how to best design the system. The goal of this project is to practice using these tools to model the trajectory of the bottle rocket launch, using numerical integration of a system of ordinary differential equations.

A bottle rocket is a simple rocket consisting of a plastic bottle filled partially with a liquid and pressurized by air. When the launch begins, the stopper is removed allowing the water to be pushed out by the pressurized air creating a reactionary force that propels the bottle forward, according to Newton's laws of motion.

The goal is to develop a MATLAB code to determine the thrust as a function of time of this bottle rocket, and predict the resulting height and range of the rocket using the thermodynamics of water and air expansion. Then, this process will be repeated through numerical simulation to understand the functional dependence of bottle rocket performance on the design parameters. To better understand and explore the parameter space, a combination of variables will be changed to find what will allow the rocket to land within say, 1 meter of a 80 meter marker. From here, another model will be developed adding a 3rd dimension to the simulation in order to account for external factors in any direction.

Throughout the process of developing these models, they will be validated against actual launch data from a baseline rocket case. After developing a functional model, we will use it predict the performance of an optimized rocket, given parameter values previously determined. Lastly, the final model will undergo a Monte Carlo simulation with varying parameter values reflecting their respective uncertainties. This final model will be plotted and discussed.

## II. Phases of Launch

A bottle rocket is made up two forms of propulsion: the fluid expelled by the pressurized air trapped inside, along with the air itself which drives the rocket forward as the pressure balances with the that of the atmosphere. This creates three different phases throughout the launch of the rocket. The first is the water expulsion phase, followed by the gas expulsion phase, and finishing with the ballistic phase. Each of these have their respective conditions and equations which are explained in the *ASEN 2012 - Bottle Rocket Design 2020 - Equations of Motion* document, but are also summarized in the following subsections.

### A. Water Expulsion Phase

In the first phase of the launch, the water is being released propelling the rocket forward. The air is still trapped inside meaning the mass of the air,  $m_{air}$ , stays constant while the volume of the air,  $v_{air}$  increases, therefore decreasing air density,  $\rho_{air}$ . As we assume isentropic air expansion, an adiabatic process, and no friction loss, we arrive at the equation to approximate air pressure,  $p$ :

$$\frac{p}{p_{air}^i} = \left( \frac{v_{air}^i}{v} \right)^{\gamma} \quad (1)$$

Along with the water's mass flow rate and rocket's thrust ( $F$ ):

$$\dot{m} = c_d \rho_w A_t V_e \quad (2)$$

$$F = \dot{m} V_e + (p_e - p_a) A_t \quad (3)$$

From here, because the water is incompressible we can apply the Bernoulli equation for incompressible flows and derive the equation for exhaust velocity.

$$V_e = \sqrt{\frac{2(p - p_a)}{\rho_w}} \quad (4)$$

In this phase, the exit air pressure is equal to the ambient air pressure, greatly simplifying Eq. [3]. Now, by plugging in Eq. [2] and Eq. [4], we arrive at the following equation for thrust:

$$F = \dot{m} V_e = 2c_d A_t (p - p_a) \quad (5)$$

Also, by utilizing Eq. 1 and Eq. 4, we can find the rate of change of air volume.

$$\frac{dv}{dt} = c_d A_t V_e = c_d A_t \sqrt{\frac{2(p - p_a)}{\rho_w}} = c_d A_t \sqrt{\frac{2}{\rho_w} \left( p_{air}^i \left( \frac{v_{air}^i}{v} \right)^g - p_a \right)} \quad (6)$$

This needs to be solved using a 4th order Runge-Kutta or, as we will discuss later, the ODE45 function in MATLAB. Once the volume of the air in the bottle is equal to the volume of the bottle itself, we know we no longer need to iterate this function. Using the  $v$  just found, we can also solve for  $p$  using Eq. 1 once again.

Now, because we know the water mass is leaving the rocket, we can use Eq. 4 to set up the mass of the rocket as a function of discharge coefficient, throat area, water density, air pressure, and ambient air pressure; all values we've found at this point.

$$\dot{m}_r = -\dot{m} = -c_d \rho_w A_t V_e = -c_d A_t \sqrt{2\rho_w (p - p_a)} \quad (7)$$

Lastly, we can create an equation for the initial mass of the rocket knowing it is equal to the mass of the bottle plus the mass of the water and the mass of the air. The mass of the water can be found using its relationship with density and volume while the mass of the air can be found with the Ideal Gas Law yielding the following equation:

$$m_r^i = m_B + \rho_w (v_B - v_{air}^i) + \frac{p_{air}^i v_{air}^i}{RT_{air}^i} \quad (8)$$

## B. Gas Expulsion Phase

Before continuing into the next phase, we must first establish the final air pressure and temperature of the previous one.

$$p_{end} = p_{air}^i \left( \frac{v_{air}^i}{v_B} \right)^g; T_{end} = T_{air}^i \left( \frac{v_{air}^i}{v_B} \right)^{g-1} \quad (9)$$

Similar the idea of density changing in the water expulsion phase, in the gas expulsion phase air volume remains constant while its mass decreases, therefore decreasing the density. Now, because there is isentropic air expansion until air pressure drops to ambient air pressure, we can solve for the pressure at any time.

$$\frac{p}{p_{end}} = \left( \frac{m_{air}}{m_{air}^i} \right)^g \quad (10)$$

The density and temperature can also be found given by:

$$\rho = \frac{m_{air}}{v_B}; T = \frac{p}{\rho R} \quad (11)$$

Using these values, we now solve for critical pressure,  $p_*$ .

$$p_* = p \left( \frac{2}{g+1} \right)^{\frac{g}{g-1}} \quad (12)$$

From here, depending on whether or not the flow is choked determines which set of equations to use. If the flow is choked, meaning  $p_* > p_a$ , the following formulas are used:

$$M_e = 1 \quad (13)$$

$$V_e = \sqrt{gRT_e} \quad (14)$$

Where:

$$T_e = \left( \frac{2}{g+1} \right) T; \rho_e = \frac{p_e}{RT_e}; p_e = p_* \quad (15)$$

If the flow is not choked, meaning  $p_* < p_a$ , the following formulas are used:

$$\frac{p}{p_a} = \left( 1 + \frac{g-1}{2} M_e^2 \right)^{\frac{g}{g-1}} \quad (16)$$

$$\frac{T}{T_e} = \left( 1 + \frac{g-1}{2} M_e^2 \right); \rho_e = \frac{p_a}{RT_e}; p_e = p_a \quad (17)$$

$$V_e = M_e \sqrt{gRT_e} \quad (18)$$

From here, thrust is found for both cases by,

$$F = \dot{m}_{air} V_e + (p_a - p_e) A_t \quad (19)$$

Where

$$\dot{m}_{air} = c_d \rho_e A_t V_e \quad (20)$$

So, similar to Eq. 7, the mass of the rocket is given by:

$$\dot{m}_R = -\dot{m}_{air} = -c_d \rho_e A_t V_e \quad (21)$$

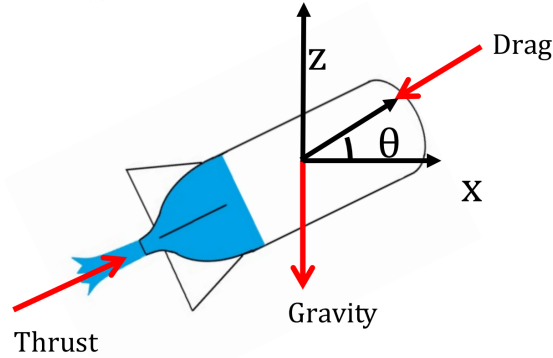
### C. Ballistic Phase

As mentioned earlier, thrust is generated by two forces: the water and the pressurized air. By the end of the water expulsion phase, no more thrust is generated by water and by the end of the gas expulsion phase, the pressure in the bottle is equal to the ambient pressure so no more thrust is generated by it either. Thrust at this point is equal to zero and the only effects acting on the rocket is gravity.

$$F = 0; m_R \sim m_B \quad (22)$$

### III. 2-D Propulsion Model

In order to take a look at the effects of varying certain parameters, we will begin by developing a 2-dimensional model in the horizontal ( $x$ ) and vertical ( $z$ ) directions using the equations discussed.



**Fig. 1 Free Body Diagram of Bottle Rocket<sup>†</sup>**

By examining the FBD in Fig. 1 above and applying Newton's laws of motion, the following equation can be derived for the sum of forces acting on the rocket:

$$\Sigma Forces = m_r \vec{a} = m_r \begin{bmatrix} a_x \\ a_z \end{bmatrix} = m_r \vec{V} = \vec{F} - \vec{D} + m_r \vec{g} \quad (23)$$

With a drag force equal to the product of the dynamic pressure, the drag coefficient, and the cross-sectional area of the front of the bottle.

$$D = q C_D A_B = \frac{1}{2} \rho V^2 C_D A_B \quad (24)$$

#### A. Model Outline

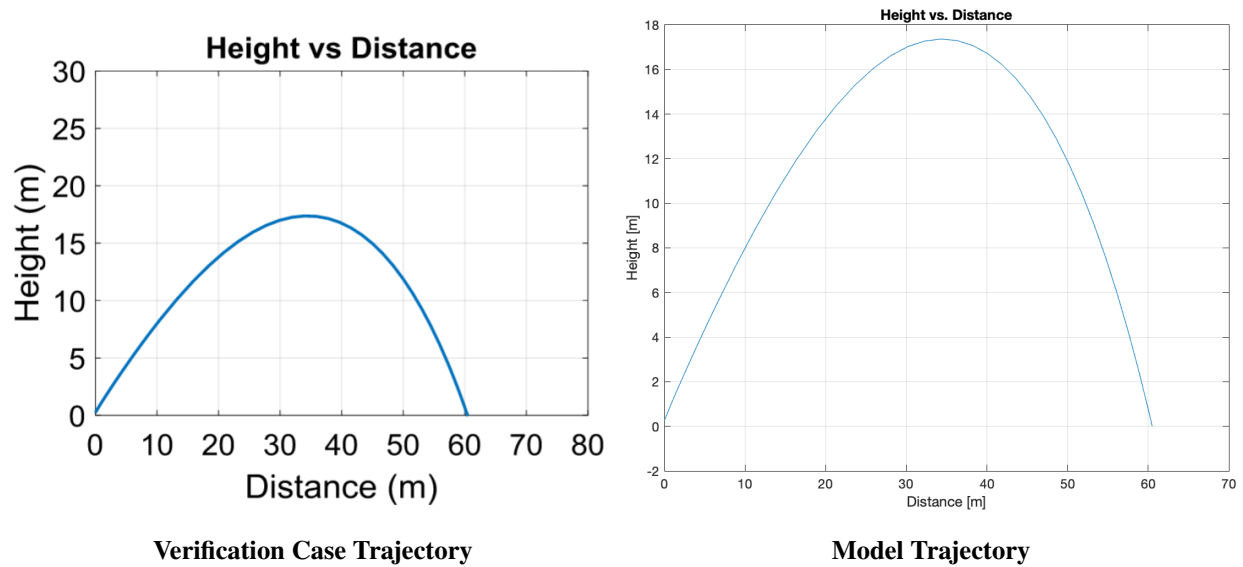
Now, we have everything we need to begin programming the model in MATLAB. For the full MATLAB Script of the 2-D Model, see Appendix A. However, it is outlined below:

- Establish constants
- Create initial state vector
- Create state function
  - Load in constants
  - Load in state vector (for the first iteration, this will be the initial state vector established earlier)
  - Convert heading vector in terms of theta (angle of flight) and overall velocity
  - Determine which phase of flight the rocket is in
    - \* Phase 1: Volume of Air < Volume of Bottle
    - \* Phase 2: Volume of Air = Volume of Bottle and Air Pressure in Bottle > Ambient Pressure
      - Determine if flow is choked
    - \* Phase 3: Volume of Air = Volume of Bottle and Air Pressure in Bottle = Ambient Pressure
  - Find final state values
    - \* Determine magnitude of drag force
    - \* Sum of forces in the x-direction and z-direction
    - \* Find accelerations in the x-direction and z-direction from their respective forces
  - Confirm rocket is above ground (if not, set all state vector values to zero)
  - Establish new state vector
- Run function through ODE45
- Plot resulting trajectory and thrust

<sup>†</sup>Image from ASEN 2012 - Bottle Rocket Design 2020 - Equations of Motion lab document

## B. Model Results

Once the script was completed, the resulting trajectory plot was compared to that of the provided verification case.



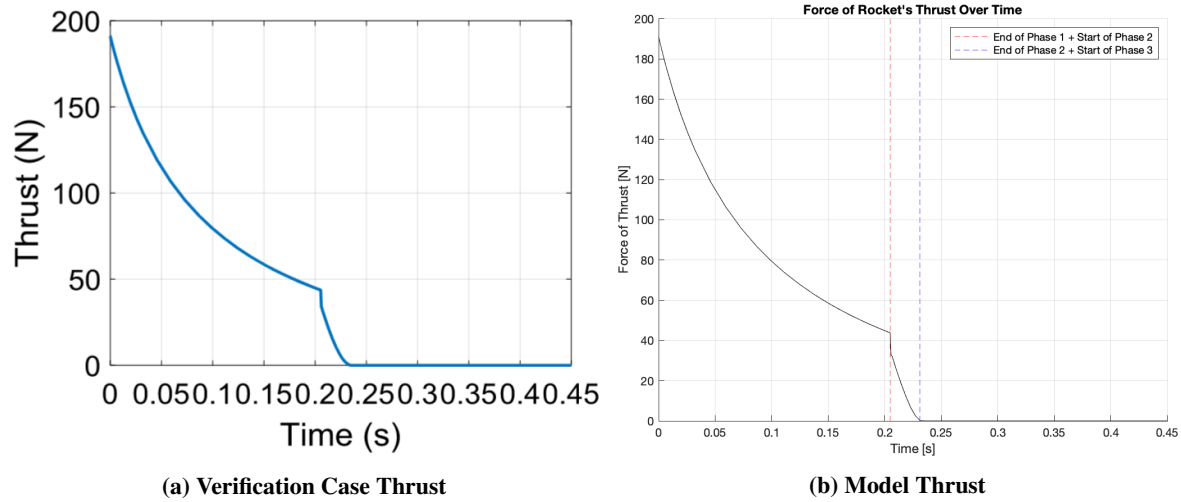
**Fig. 2 Verification and Model Trajectory Comparison**

Consideration	Verification Case	Model
Max Height [m]	17.37	17.36
Max Distance [m]	60.45	60.50

**Table 1 Trajectory Comparison**

After comparing the model with the verification case, it's apparent that the developed model is quite accurate. The maximum trajectory height is only off by 0.01 m, or 1 cm! Likewise, maximum trajectory distance is only 0.05 m, or 5 cm, greater than the verification case.

However, despite the incredible precision of the model's trajectory, it is also important to compare the thrust plots of the two cases to ensure model accuracy:



**Fig. 3 Verification and Model Thrust Comparison**

Phase Change	Verification Case	Model
Phase 1 → Phase 2 [s]	0.205	0.205
Phase 2 → Phase 3 [s]	0.230	0.230

**Table 2 Thrust Comparison**

Although the values in Table 2 are estimated based on visual inspection of the graphs in Figure 3, it seems that the phase change between 1 (Water Expulsion) and 2 (Gas Expulsion), as well as 2 (Gas Expulsion) and 3 (Ballistic), occur at similar times. Obviously there is uncertainty due to a simple visual inspection, however, the models seem similar enough to verify the accuracy of the model.

As mentioned, the bottle rocket flight consists of three distinct phases:

- 1) From the moment the stopper is removed until the water is exhausted
- 2) After the water is exhausted until the air pressure drops to the ambient value and the thrust phase ends
- 3) Ballistic phase

In the figure, we can see how the first two generate all of the thrust for the flight, however it is only a small fraction of the total flight time.



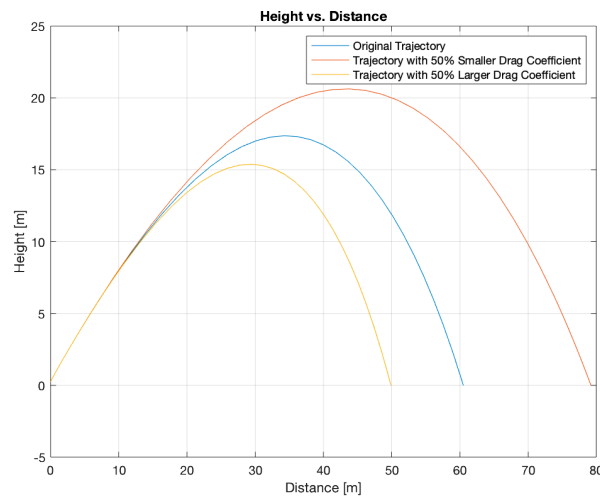
## IV. Analyzing Parameter Changes

After creating a model that accurately simulates that of the verification case, four parameters need to be changed in order to reach a new target distance, 80 m for example. Each parameter affects the rocket model in different ways. In this model, four possible flight parameters will be changed and their effects on the rocket will be analyzed. The four changeable flight parameters are as followed:

- Drag Coefficient
- Volume of Water
- Air Pressure
- Launch Angle

To analyze the effects of changes these parameters, each one will varied for the original model (originally mimicking the verification case).

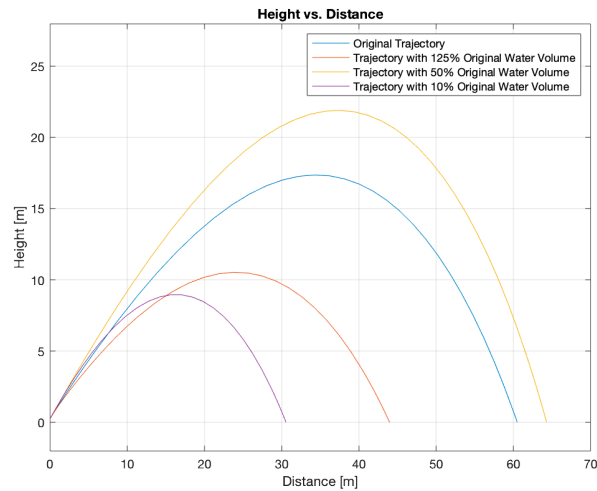
### A. Drag Coefficient



**Fig. 4 Rocket Trajectory with Varying Drag Coefficient**

The drag coefficient is essentially the friction caused by the air, so a smaller drag coefficient results in less “air friction,” and a larger distance traveled. Similarly, a larger drag coefficient results in more “air friction,” and a smaller distance traveled. Both of these effects can be seen in Figure 4. Unlike other parameters, there are not any drawbacks caused by a smaller drag coefficient making this an efficient parameter to change to optimize rocket performance.

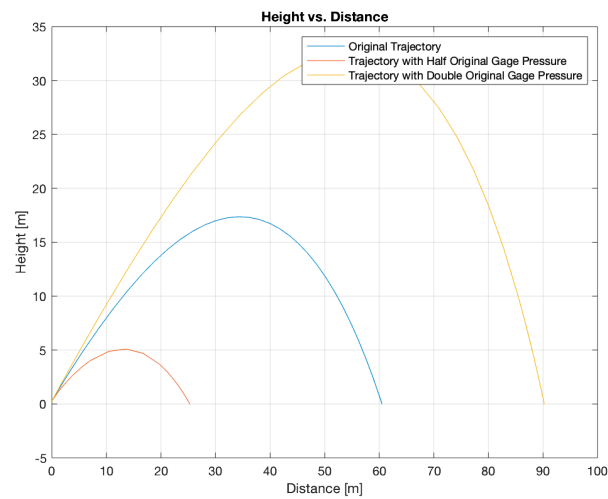
## B. Water Volume



**Fig. 5 Rocket Trajectory with Varying Water Volume**

The volume of water contributes to propulsion during Phase 1 (Water Expulsion) and overall mass of the rocket. Increasing or decreasing water volume will not directly increase or decrease distance traveled due to drawbacks between weight and propulsion. Figure 5 demonstrates how a decrease in water volume will increase distance, but too large of a water volume decrease will then decrease distance.

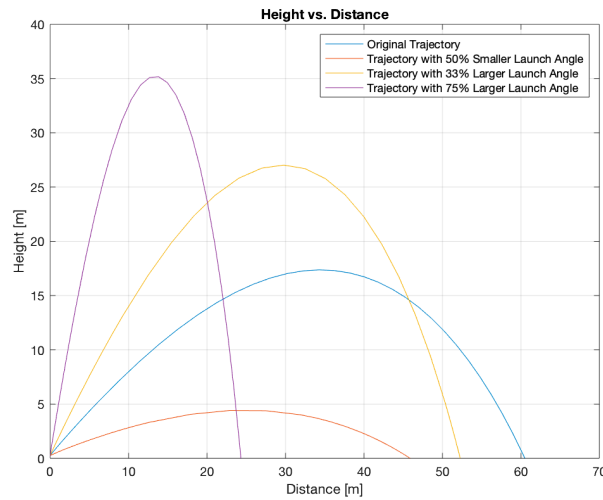
## C. Air Pressure



**Fig. 6 Rocket Trajectory with Varying Air Pressure**

As previously discussed, air pressure creates thrust during Phase 2, the Gas Expulsion Phase. Figure 7 demonstrates that increasing air pressure will increase propulsion potential of rocket, without any drawbacks. This means a decrease in air pressure results in less propulsion, and a smaller distance traveled while an increase in air pressure results in more propulsion, and a larger distance traveled.

## D. Launch Angle



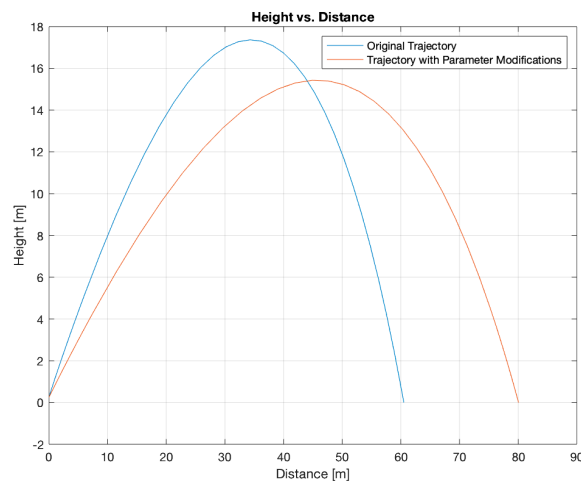
**Fig. 7 Rocket Trajectory with Varying Launch Angle**

After varying launch angles, it is apparent that  $45^\circ$  is actually the ideal launch angle. Launch angles smaller than  $45^\circ$  result in the rocket hitting the ground before utilizing all propulsion potential. On the other hand, launch angles larger than  $45^\circ$  result in the rocket using too much propulsion potential moving in the z-direction, and not enough in the x-direction. Ultimately, the optimized rocket's parameters will have a launch angle of  $45^\circ$  to ensure maximum downrange distance traveled.

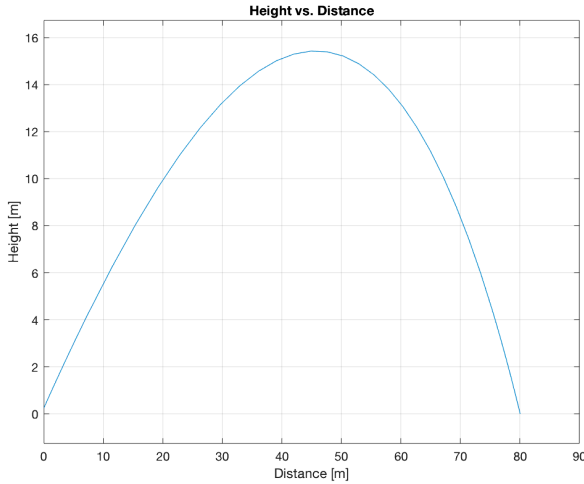
## E. Combining Parameter Changes

Hypothetically, the rocket can travel a specific distance with precision by combining multiple parameter changes. In this example, the goal is to travel  $80 \pm 0.1$  meters. There are an infinite number of combinations to do so, however the mix found in Figure 8 below yielding a distance of 80.05 meters is:

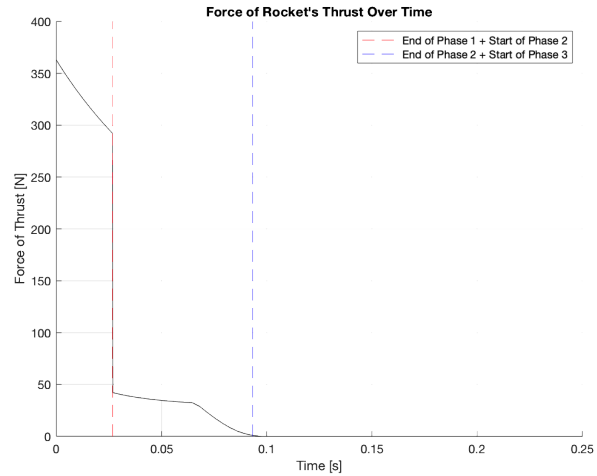
- A decrease in drag coefficient from 0.50 to 0.45 (increasing downrange distance)
- A decrease in water volume from  $1000 \text{ cm}^3$  to  $253 \text{ cm}^3$  (decreasing downrange distance)
- An increase in air pressure from 50 psi to 95 psi (increasing downrange distance)
- A decrease in launch angle from  $45^\circ$  to  $30^\circ$  (decreasing downrange distance)



**Fig. 8 Original Trajectory vs Trajectory with Parameter Modifications**



**Fig. 9 Modified Trajectory**



**Fig. 10 Modified Thrust**

Several factors affect the overall distance change and precision of the rocket. The first parameter discussed, drag coefficient, was decreased in this example, making the rocket more efficient during flight as there is less opposition. However, some parameters contributed to a decrease in downrange distance. For example, a smaller launch angle prevents the rocket from completing its full flight. Additionally, less water volume results in less fluid to be expelled. Probably most interesting though is the concept that a higher air pressure results in greater thrust increasing potential for maximizing distance but also results in exhaustion of water faster.

To better understand this, by looking at the modified thrust plot, Figure 10, it's apparent that it is quite different from the original in Figure 3b.

During Phase 1, the initial thrust is much higher than that of the verification case. This is due to the greater air pressure expelling the water from the rocket at a faster rate, increasing  $\dot{m}$  and therefore  $F$ . However, it also seems that Phase 1 ends sooner than the original. This is due to a combination of higher air pressure causing water to release at a higher rate, as well as less initial water in the rocket meaning it will deplete quicker.

Now, taking a look at Phase 2, it seems that this one actually lasts longer. This is due to the higher air pressure which requires more time to balance with the surrounding air pressure.

Lastly, Phase 3 remains the same (0 N) for both cases because there are no other forces acting on the system other than gravity.

It's apparent that each parameter affects the downrange difference and overall performance of the rocket in different ways. In order to land at the desire distance, parameters differ to increase distance traveled (to avoid coming up short) and decrease distance traveled (to avoid exceeding target range).

Changes<sup>‡</sup> for *minimizing* distance:

- Decrease air pressure
- Inc/Dec water volume (significantly)
- Increase drag coefficient
- Changing launch angle from 45°

Changes<sup>‡</sup> for *maximizing* distance:

- Increase air pressure
- Decrease water volume (marginally)
- Decrease drag coefficient
- 45° launch angle

A balance between parameters using their respective trade-offs allow to narrow distance traveled to 80 meters, or whatever specified downrange distance for that matter.

<sup>‡</sup>In terms of changing original verification case parameters

## V. Modified 3-D Model

Now that there is an established understanding on the effects of varying modeling parameters, as well as an accurate 2-dimension rocket model, it's time to alter the model into one that is 3-dimension. This allows us to account for external forces, such as wind, and incorporate more aspects of uncertainty to make the model more realistic.

The main alteration that needs to be done is changing the heading vector to incorporate a third component, the y-direction. To do so, it would be the easiest to understand by changing the heading from theta and a magnitude to three components in an  $\hat{i}$ ,  $\hat{j}$ ,  $\hat{k}$  heading vector in the East, North, and up directions respectively. This also allows us to easily account for external forces,  $\vec{v}_w$ , since we can simple subtract their respective magnitudes from the current  $\vec{v}_g$  to give us  $\vec{v}_{rel}$ .

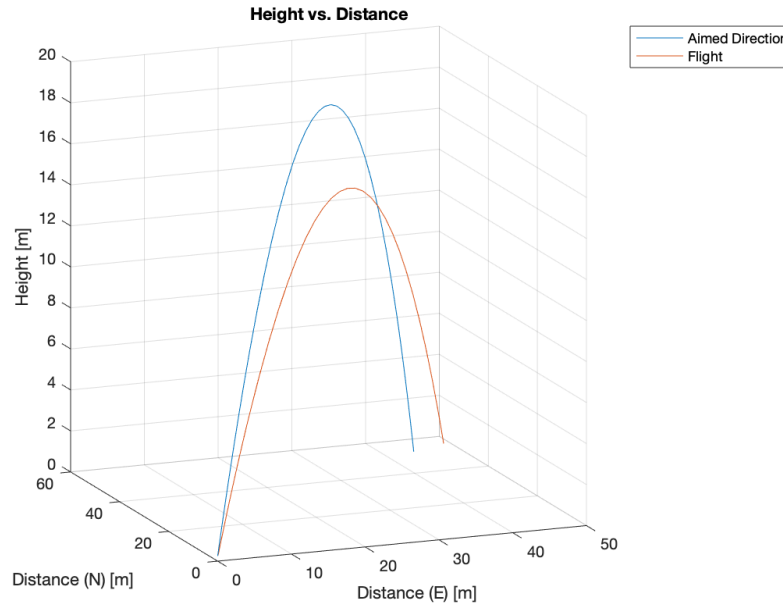
$$\vec{v}_{rel} = \begin{bmatrix} v_{gx} - v_{wx} \\ v_{gy} - v_{wy} \\ v_{gz} - v_{wz} \end{bmatrix} \quad (25)$$

From here, we can find the heading vector by:

$$\vec{h} = \frac{\vec{v}_{rel}}{\|\vec{v}_{rel}\|} \quad (26)$$

Next, it's quite simple to adjust the MATLAB script to account for the two extra values in the state vector,  $v_y$  and  $a_y$ . All that needs to be done is add the third direction wherever the x-direction and z-directions are used. For the most part, the main state function and ODE45 call remain the same. However, the updated script can be found in Appendix B.

In this example, we're examining a 3 mph wind pointing on a  $45^\circ$  heading from the North. The only thing that needs to be done to account for this is the code is adding it to the velocity vector in the respective direction(s) at the beginning of the state function. The force caused by the wind creates differences in velocities in all three direction. The resulting flight path (orange) can be compared to the original aimed path from the 2-dimensional model (blue) in Figure III.



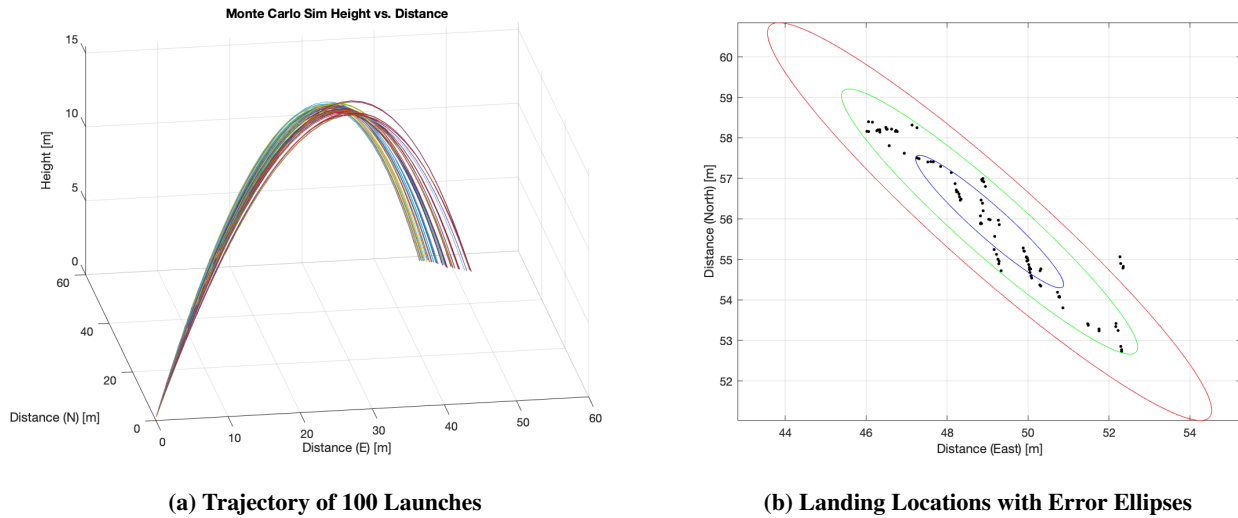
**Fig. 11 Original Trajectory with No External Forces vs Actual Expected Flight Path**

As you can see, the North-East wind will carry the rocket toward the right of the original path, with less height but a further downrange distance.

## VI. Monte Carlo Simulation

The last factor that needs to be taken into account is uncertainty within the parameters. From the direction of the wind heading vector to uncertainty in mass measurements to fluctuations in air temperature, most values will have some sort of uncertainty. To understand how these uncertainties affect the trajectory of the rocket, a Monte Carlo simulation was done.

First, the original parameters were changed to the ideal expected values of an optimized bottle rocket launch (0.30 drag coefficient, 8 mph wind, etc.). From here, the uncertainties were taken into account through random number generation based on their severity. For example, wind had a heading of  $45 \pm 11.25^\circ$  so a random angle between  $33.75^\circ$  and  $56.25^\circ$  was generated and ran through the constants or initial state vector of the following function. For the model here, wind uncertainty ( $45 \pm 11.25^\circ$ ) and initial water mass uncertainty ( $0.600 \pm 0.0005$  kg) were accounted for. These random values were generated and flight trajectories were plotted through a loop of 100 iterations. All 100 of these trajectories are shown below in Figure. [12a](#)



**Fig. 12 Resulting Plots from the Monte Carlo Simulation**

As you can see, the 100 Monte Carlo iterations have the trajectories modeled simulating the possible combinations of uncertainties in both wind direction and mass of water in the rocket.

The landing locations of each launch were also plotted from a vertical perspective (looking in the  $-\hat{k}$  direction) in Figure [12b](#). The downrange distance is predicted by taking the mean of all of these landing points, in this case 74.39m. Their error ellipses are also plotted to give a more general prediction of the landing zones.

## **VII. Conclusion and Recommendations**

### *Improvements to Be Made:*

Obviously, the current model has a few apparent flaws. For starters, in the 3-dimensional model only two parameter uncertainties were accounted for, those being wind heading and initial water mass. Although incorporating more parameter uncertainties will make the landing area less precise, they will make the error ellipses more accurate and we can better predict the general area where the rocket will land. Another improvement that can be made is improving the Monte Carlo simulation itself. Additional iterations will, theoretically, help condense the error ellipses as more values results in outliers or rare occurrences having a smaller impact on the rest of the data.

### *Conclusion:*

It's difficult to accurately model something like a bottle rocket launch due to all the factors and uncertainties involved. However, functions like MATLAB's ODE45 and computational algorithms like Monte Carlo simulations can effectively and efficiently improve your model. This modeling process has helped the user not only apply the aerodynamic and thermodynamic properties of a simple rocket launch to real application, but has also taught the user how essential programming software can be. An infinite number of simulations can be done and improvements can be made before the first real rocket launch is done. This helps minimize time and money for the engineers and the company. Overall, this was an exciting application and it was interesting to learn how to create and run the model.

## VIII. Appendix A

### ASEN 2012 MATLAB Script (2-Dimensional Trajectory and Parameter Analysis)

```
1
2 % ASEN 2012 Project 2
3 % Author: Travis Choy
4 % ID: 109181287
5
6 % Date Created: November 13, 2020
7 % Date Modified: December 1, 2020
8 % Due Date: December 4, 2020
9
10 % Purpose: To utilize ODE45 to numerically integrate an ordinary
11 % differential equation such as that of the flight of a bottle rocket. Plot
12 % and analyze the flight of the rocket and the effects of varying specific
13 % parameters.
14
15 %% Housekeeping
16
17 clear
18 close all
19 clc
20
21 %% Constants
22
23 g = 9.81; % Acceleration Due to Gravity [m/s^2]
24 C_d = 0.8; % Discharge Coefficient
25 p_amb = 0.961; % Ambient Air Density [kg/m^3]
26 V_bottle = 0.002; % Volume of Empty Bottle [m^3]
27 P_amb = 12.1; % Atmospheric Pressure [psi]
28 P_amb = P_amb * 6894.76; % Atmospheric Pressure [Pa]
29 cp_rat = 1.4; % Ratio of Specific Heats for Air
30 p_water = 1000; % Density of Water [kg/m^3]
31 D_throat = 2.1; % Diameter of Throat [cm]
32 D_throat = D_throat/100; % Diameter of Throat [m]
33 A_throat = pi * (D_throat/2)^2; % Area of Throat [m^2]
34 D_bottle = 10.5; % Diameter of Bottle [cm]
35 D_bottle = D_bottle/100; % Diameter of Bottle [m]
36 A_bottle = pi * (D_bottle/2)^2; % Cross-Sectional Area of Bottle [m^2]
37 R = 287; % Gas Constant of Air [J/kgK]
38 m_bottle = 0.15; % Mass of Empty 2-Liter Bottle with Cone
    and Fins [kg]
39 cd = 0.5; % Drag Coefficient
40 ls = 0.5; % Length of test stand [m]
41
42 %% Initial Value
43
44 P_gage_0 = 50; % Initial Gage Pressure of Air
    in Bottle [psi]
45 P_gage_0 = P_gage_0 * 6894.76; % Initial Gage Pressure of Air
    in Bottle [Pa]
46 P_bottle = P_amb + P_gage_0; % Initial Total Pressure of
    Air in Bottle [Pa]
```



```

47 V_water_0 = 0.001; % Initial Volume of Water
    Inside Bottle [m^3]
48 m_water_0 = p_water * V_water_0; % Initial Mass of Water [kg]
49 V_air_0 = V_bottle - V_water_0; % Initial Volume of Air Inside
    Bottle [m^3]
50 T_air_0 = 300; % Initial Temperature of Air [
    K]
51 m_air_0 = P_bottle * V_air_0 / ( R * T_air_0 ); % Initial Mass of Air [kg]
52 v_0 = 0.0; % Initial Velocity of Rocket [
    m/s]
53 v_x_0 = 0.0; % Initial Velocity of Rocket
    in X-Direction [m/s]
54 v_z_0 = 0.0; % Initial Velocity of Rocket
    in Z-Direction [m/s]
55 theta_0 = pi/4; % Initial Angle of Rocket (45
    ) [radians]
56 x_0 = 0.0; % Initial Horizontal Distance
    [m]
57 z_0 = 0.25; % Initial Vertical Height [m]
58 x_stand = ls * cos(theta_0) + x_0; % Initial X Distance of Rocket
    on Stand [m]
59 z_stand = ls * sin(theta_0) + z_0; % Initial Z Distance of Rocket
    on Stand [m]
60 R_stand = sqrt( x_stand ^ 2 + z_stand ^ 2 ); % Initial Distance of Rocket
    on Stand [m]
61
62 m_bottle_0 = m_water_0 + m_air_0 + m_bottle; % Initial Mass of Rocket [kg]
63 % Equation (11)
64
65 constants = [ V_bottle , V_air_0 , P_bottle , cp_rat , C_d , p_water , A_throat ,
    P_amb , p_amb , cd , A_bottle , T_air_0 , m_air_0 , R , g , R_stand , theta_0 ];
66
67 initial_state_vector = [x_0; z_0; v_x_0; v_z_0; m_bottle_0; m_air_0; V_air_0];
68
69 % Considering Part 2 Hypothetical:
70 hypothetical = false; % Change to True for
    Hypothetical conditions
71
72 if hypothetical
73     P_gage_0 = 95; % Initial Gage Pressure
        of Air in Bottle [psi]
74     P_gage_0 = P_gage_0 * 6894.76; % Initial Gage Pressure
        of Air in Bottle [Pa]
75     P_bottle = P_amb + P_gage_0; % Initial Total
        Pressure of Air in Bottle [Pa]
76     V_water_0 = 0.000253; % Initial Volume of
        Water Inside Bottle [m^3]
77     cd = 0.40; % Drag Coefficient
78     theta_0 = pi / 6; % Initial Angle of
        Rocket [radians]
79     m_water_0 = p_water * V_water_0; % Initial Mass of Water
        [kg]
80     V_air_0 = V_bottle - V_water_0; % Initial Volume of Air
        Inside Bottle [m^3]

```

```

81     m_air_0 = P_bottle * V_air_0 / ( R * T_air_0 ); % Initial Mass of Air [
           kg]
82     x_stand = ls * cos(theta_0) + x_0; % Initial X Distance of
           Rocket on Stand [m]
83     z_stand = ls * sin(theta_0) + z_0; % Initial Z Distance of
           Rocket on Stand [m]
84     R_stand = sqrt( x_stand ^ 2 + z_stand ^ 2 ); % Initial Distance of
           Rocket on Stand [m]
85     m_bottle_0 = m_water_0 + m_air_0 + m_bottle;
86
87     constants_par = [ V_bottle , V_air_0 , P_bottle , cp_rat , C_d , p_water ,
           A_throat , P_amb , p_amb , cd , A_bottle , T_air_0 , m_air_0 , R , g ,
           R_stand , theta_0 ];
88     initial_state_vector_par = [ x_0 ; z_0 ; v_x_0 ; v_z_0 ; m_bottle_0 ; m_air_0
           ; V_air_0 ];
89
90 end
91
92 %%% Calling ODE45
93
94 tspan = [0 5]; % [s]
95
96 [t , state_vector] = ode45(@(t,y) rocket_fun(t , y , constants) , tspan ,
           initial_state_vector);
97
98 if hypothetical
99     [t_par , state_vector_par] = ode45(@(t,y) rocket_fun(t , y , constants_par) ,
           tspan , initial_state_vector_par);
100 end
101
102 %%% Plot
103
104 % Plot Trajectory
105 figure(1)
106 plot( state_vector(:,1) , state_vector(:,2) )
107 hold on
108 xlabel(" Distance [m] ")
109 ylabel(" Height [m] ")
110 title(" Height vs. Distance ")
111 grid on
112 hold off
113
114 % Create Vector of Values for Thrust Graph
115 F_thrust = zeros(length(t),1);
116 P_air = zeros(length(t),1);
117 for i= 1: length(t)
118     [ F_thrust(i), P_air(i) ] = rocket_thrust_graph(t , state_vector(i,:) ,
           constants);
119     if state_vector(i,7) < V_bottle
120         t_phase_1(i) = t(i);
121     elseif state_vector(i,7) >= V_bottle && P_amb < P_air(i)
122         t_phase_2(i) = t(i);
123     end
124 end

```

```

125
126 % Plot Thrust
127 figure(2)
128 xline(t_phase_1(end),"--r");
129 hold on
130 xline(t_phase_2(end),"--b");
131 plot(t, F_thrust, "k")
132 xlim([0 0.45])
133 xlabel("Time [s]")
134 ylabel("Force of Thrust [N]")
135 title("Force of Rocket's Thrust Over Time")
136 legend("End of Phase 1 + Start of Phase 2", "End of Phase 2 + Start of Phase
137 3")
138 grid on
139 hold off
140
141 % Plot Hypothetical Trajectory
142 if hypothetical
143 figure(3)
144 plot(state_vector(:,1), state_vector(:,2))
145 hold on
146 plot(state_vector_par(:,1), state_vector_par(:,2))
147 legend("Original Trajectory", "Trajectory with Parameter Modifications")
148 xlabel("Distance [m]")
149 ylabel("Height [m]")
150 title("Height vs. Distance")
151 grid on
152 hold off
153
154 % Create Vector of Values for Thrust Graph
155 F_thrust_par = zeros(length(t_par),1);
156 P_air_par = zeros(length(t_par),1);
157 for i= 1: length(t_par)
158     [F_thrust_par(i), P_air_par(i)] = rocket_thrust_graph(t_par,
159         state_vector_par(i,:), constants_par);
160     if state_vector_par(i,7) < V_bottle
161         t_phase_1_par(i) = t_par(i);
162     elseif state_vector_par(i,7) >= V_bottle && P_amb < P_air_par(i)
163         t_phase_2_par(i) = t_par(i);
164     end
165 end
166
167 % Plot Thrust
168 figure(4)
169 xline(t_phase_1_par(end),"--r");
170 hold on
171 xline(t_phase_2_par(end),"--b");
172 plot(t_par, F_thrust_par, "k")
173 xlim([0 0.25])
174 xlabel("Time [s]")
175 ylabel("Force of Thrust [N]")
176 title("Force of Rocket's Thrust Over Time")
177 legend("End of Phase 1 + Start of Phase 2", "End of Phase 2 + Start of Phase
178 3")

```

```

176 grid on
177 hold off
178
179 end
180
181 %% Function Initial Conditions
182
183 function state_vector = rocket_fun(t, y, constants)
184
185     % Declare Constants
186     V_bottle = constants(1);
187     V_air_0 = constants(2);
188     P_bottle = constants(3);
189     cp_rat = constants(4);
190     C_d = constants(5);
191     p_water = constants(6);
192     A_throat = constants(7);
193     P_amb = constants(8);
194     p_amb = constants(9);
195     cd = constants(10);
196     A_bottle = constants(11);
197     T_air_0 = constants(12);
198     m_air_0 = constants(13);
199     R = constants(14);
200     g = constants(15);
201     R_stand = constants(16);
202     theta_0 = constants(17);
203
204     % State Values
205     x = y(1);
206     z = y(2);
207     v_x = y(3);
208     v_z = y(4);
209     m_bottle = y(5);
210     m_air = y(6);
211     V_air = y(7);
212
213     % Theta
214     rocket_pos = sqrt( x ^ 2 + z ^ 2 );
215     if ( rocket_pos > R_stand ) % determine if rocket has left stand
216         theta = atan( v_z / v_x );
217     else
218         theta = theta_0;
219     end
220
221     % Velocity
222     v = sqrt( v_x ^ 2 + v_z ^ 2 );
223
224     %% PHASE 1: Water Expulsion
225
226     if V_air < V_bottle
227
228         % Air Pressure
229         % Equation (3)

```

```

230     P_air = P_bottle * ( V_air_0 / V_air ) ^ cp_rat;
231
232     % Exhaust Velocity
233     % Equation (7)
234     v_exhaust = sqrt( 2 * ( P_air - P_amb ) / p_water );
235
236     % Mass Flow Rate of Water
237     % Equation (4)
238     m_dot_w = C_d * p_water * A_throat * v_exhaust;
239
240     % Mass Flow Rate of Rocket
241     % Equation (10)
242     m_dot_r = -m_dot_w;
243
244     % Mass Flow Rate of Air
245     m_dot_a = 0; % Air mass doesn't change in this phase
246
247     % Rate of Change of Volume of Air
248     % Equation (9)
249     V_dot = C_d * A_throat * v_exhaust;
250
251     % Force of Thrust
252     % Equation (8)
253     F_thrust = 2 * C_d * A_throat * ( P_air - P_amb );
254
255     else % set up Pressure and Temperatures for Phase 2 and 3
256
257         % Air Pressure and Temperature After Water Exhausted
258         % Equation (13)
259         P_end = P_bottle * ( V_air_0 / V_bottle ) ^ cp_rat;
260
261         % New Pressure Equation
262         % Equation (14)
263         P_air = P_end * (( m_air / m_air_0 )) ^ cp_rat;
264
265     end
266
267     %% PHASE 2: Gas Expulsion
268
269     if ( V_air >= V_bottle ) && ( P_air > P_amb )
270
271         % Change in Volume
272         V_dot = 0;
273
274         % Calculate Density and Temperature
275         % Equation (15)
276         rho = m_air / V_bottle;
277         T = P_air / ( rho * R );
278
279         % Critical Pressure
280         % Equation (16)
281         P_crit = P_air * ( 2 / ( cp_rat + 1 ) ) ^ ( cp_rat / ( cp_rat - 1 ) );
282
283         % If Choked Flow

```

```

284     if ( P_crit > P_amb )
285
286         % Exit Temperature
287         % Equation (18)
288         T_exit = ( 2 / ( cp_rat + 1 )) * T;
289
290         % Exit Velocity
291         % Equation (17)
292         V_exit = sqrt( cp_rat * R * T_exit );
293
294         % Exit Pressure
295         % Equation (18)
296         P_exit = P_crit;
297
298     % If Not Choked Flow
299     else
300
301         % Exit Mach Number
302         % Equation (19)
303         Mach_exit = sqrt(abs((( P_air / P_amb ) ^ (( cp_rat - 1) / cp_rat)
304             - 1 ) / (( cp_rat - 1 ) / 2))));
305
306         % Exit Temperature
307         % Equation (20)
308         T_exit = T / ( 1 + ( ( cp_rat - 1) / 2 ) * Mach_exit ^ 2);
309
310         % Exit Pressure
311         % Equation (20)
312         P_exit = P_amb;
313
314         % Exit Velocity
315         % Equation (21)
316         V_exit = Mach_exit * sqrt(abs( cp_rat * R * T_exit ));
317
318     end
319
320     % Exit Density
321     % Equation (18) and (20)
322     rho_exit = P_exit / ( R * T_exit);
323
324     % Change in Air Mass
325     % Equation (23)
326     m_dot_a = -C_d * rho_exit * A_throat * V_exit;
327
328     % Force of Thrust
329     % Equation (22)
330     F_thrust = (-m_dot_a * V_exit) + (( P_amb - P_exit ) * A_throat);
331
332     % Change in Rocket Mass
333     % Equation (24)
334     m_dot_r = m_dot_a;
335
336 end

```

```

337 %% PHASE 3: Ballistic Phase
338
339     if (V_air >= V_bottle) && (P_air <= P_amb)
340
341         % No more water or gas so theres no change in mass, volume, or thrust
342         % Equation (25)
343         F_thrust = 0;
344         m_dot_r = 0;
345         m_dot_a = 0;
346         V_dot = 0;
347
348     end
349
350 %% Final State Function Calculations
351
352     % Force of Drag
353     % Equation (2)
354     F_drag = (1/2) * p_amb * (v ^ 2) * cd * A_bottle;
355
356     % Sum of Forces
357     % Equation (1)
358     sum_F_x = F_thrust * cos(theta) - F_drag * cos(theta);
359     sum_F_z = F_thrust * sin(theta) - F_drag * sin(theta) - m_bottle * g;
360
361     % Acceleration
362     % Equation (1)
363     acc_x = sum_F_x / m_bottle;
364     acc_z = sum_F_z / m_bottle;
365
366     % Keep Above x-axis
367     if z <= 0
368         v_x = 0;
369         v_z = 0;
370         acc_x = 0;
371         acc_z = 0;
372         m_dot_r = 0;
373         m_dot_a = 0;
374         V_dot = 0;
375     end
376
377     % Resulting State Values
378     state_vector(1,1) = v_x;
379     state_vector(2,1) = v_z;
380     state_vector(3,1) = acc_x;
381     state_vector(4,1) = acc_z;
382     state_vector(5,1) = m_dot_r;
383     state_vector(6,1) = m_dot_a;
384     state_vector(7,1) = V_dot;
385
386
387 end
388
389 %% Function for Thrust Plot
390

```

```

391 function [F_thrust, P_air] = rocket_thrust_graph(t, y, constants)
392
393 % Declare Constants
394 V_bottle = constants(1);
395 V_air_0 = constants(2);
396 P_bottle = constants(3);
397 cp_rat = constants(4);
398 C_d = constants(5);
399 A_throat = constants(7);
400 P_amb = constants(8);
401 m_air_0 = constants(13);
402 R = constants(14);
403
404 % State Values
405 v_x = y(3);
406 v_z = y(4);
407 m_air = y(6);
408 V_air = y(7);
409
410 % Velocity
411 v = sqrt( v_x ^ 2 + v_z ^ 2 );
412
413 %%% PHASE 1: Water Expulsion
414
415 if V_air < V_bottle
416
417     % Air Pressure
418     % Equation (3)
419     P_air = P_bottle * (V_air_0 / V_air) ^ cp_rat;
420
421     % Force of Thrust
422     % Equation (8)
423     %F_thrust = m_dot_r * v_exhaust;
424     F_thrust = 2 * C_d * A_throat * (P_air - P_amb);
425
426 else % set up Pressure and Temperatures for Phase 2 and 3
427
428     % Air Pressure and Temperature After Water Exhausted
429     % Equation (13)
430     P_end = P_bottle * ( V_air_0 / V_bottle ) ^ cp_rat;
431
432     % New Pressure Equation
433     % Equation (14)
434     P_air = P_end * (( m_air / m_air_0)) ^ cp_rat;
435
436 end
437
438 %%% PHASE 2: Gas Expulsion
439
440 if (V_air >= V_bottle) && (P_air > P_amb)
441
442     % Calculate Density and Temperature
443     % Equation (15)
444     rho = m_air / V_bottle;

```



```

445     T = P_air / ( rho * R );
446
447     % Critical Pressure
448     % Equation (16)
449     P_crit = P_air * ( 2 / ( cp_rat + 1 )) ^ ( cp_rat / ( cp_rat - 1 ));
450
451     % If Choked Flow
452     if ( P_crit > P_amb )
453
454         % Exit Temperature
455         % Equation (18)
456         T_exit = ( 2 / ( cp_rat + 1 )) * T;
457
458         % Exit Velocity
459         % Equation (17)
460         V_exit = sqrt( cp_rat * R * T_exit );
461
462         % Exit Pressure
463         % Equation (18)
464         P_exit = P_crit;
465
466     % If Not Choked Flow
467     else
468
469         % Exit Mach Number
470         % Equation (19)
471         Mach_exit = sqrt(abs((( P_air / P_amb ) ^ (( cp_rat - 1) / cp_rat)
472             - 1 ) / (( cp_rat - 1 ) / 2))));
473
474         % Exit Temperature
475         % Equation (20)
476         T_exit = T / ( 1 + ( ( cp_rat - 1) / 2 ) * Mach_exit ^ 2);
477
478         % Exit Pressure
479         % Equation (20)
480         P_exit = P_amb;
481
482         % Exit Velocity
483         % Equation (21)
484         V_exit = Mach_exit * sqrt(abs( cp_rat * R * T_exit ));
485
486     end
487
488     % Exit Density
489     % Equation (18) and (20)
490     rho_exit = P_exit / ( R * T_exit);
491
492     % Change in Air Mass
493     % Equation (23)
494     m_dot_a = -C_d * rho_exit * A_throat * V_exit;
495
496     % Force of Thrust
497     % Equation (22)
498     F_thrust = (-m_dot_a * V_exit) + (( P_amb - P_exit ) * A_throat);

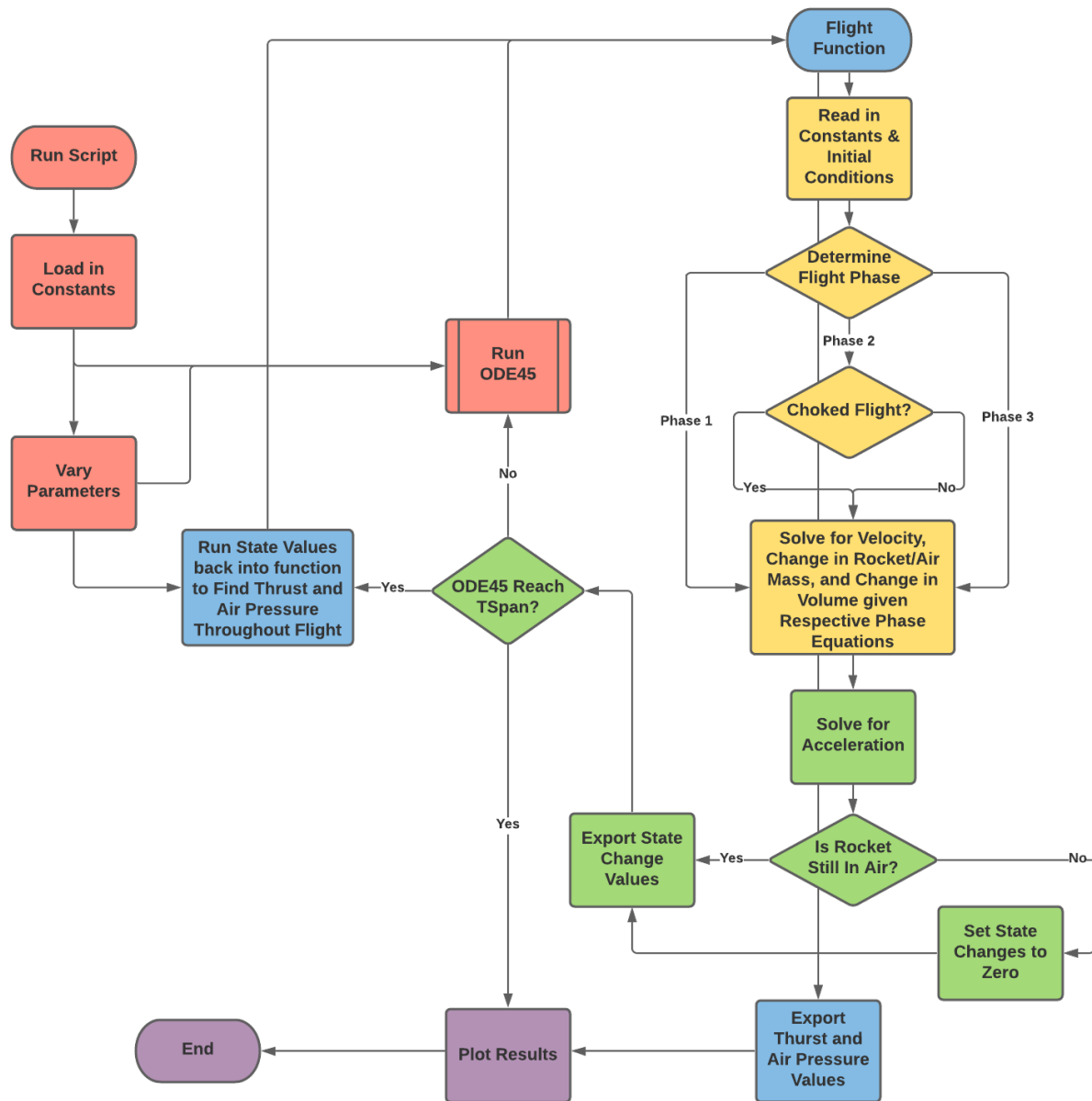
```

```

498
499     end
500
501 %% PHASE 3: Ballistic Phase
502
503     if (V_air >= V_bottle) && (P_air <= P_amb)
504
505         % No more water or gas so theres no change in mass, volume, or thrust
506         % Equation (25)
507         F_thrust = 0;
508
509     end
510
511 end

```

## ASEN 2012 MATLAB Script Flow Chart



## IX. Appendix B

### ASEN 2004 MATLAB Script (3-Dimensional Trajectory and Monte Carlo Simulation)

```
1
2 % ASEN 2004 Lab 2: Individual Modeling
3 % Author: Travis Choy
4 % ID: 109181287
5
6 % Date Created: November 13, 2020
7 % Date Modified: April 12, 2021
8 % Due Date: April 13, 2021
9
10 % Purpose: To plot and analyze the flight of the rocket and the effects of
11 % varying specific parameters. Verify and determine the predicted distance
12 % and error ellipses of the optimize rocket provided.
13
14 %% Housekeeping
15
16 clear
17 close all
18 clc
19
20 %% Constants
21
22 g = 9.81; % Acceleration Due to Gravity [m/s^2]
23 C_d = 0.8; % Discharge Coefficient
24 p_amb = 0.961; % Ambient Air Density [kg/m^3]
25 V_bottle = 0.002; % Volume of Empty Bottle [m^3]
26 P_amb = 12.1; % Atmospheric Pressure [psi]
27 P_amb = P_amb * 6894.76; % Atmospheric Pressure [Pa]
28 cp_rat = 1.4; % Ratio of Specific Heats for Air
29 p_water = 1000; % Density of Water [kg/m^3]
30 D_throat = 2.1; % Diameter of Throat [cm]
31 D_throat = D_throat/100; % Diameter of Throat [m]
32 A_throat = pi * (D_throat/2)^2; % Area of Throat [m^2]
33 D_bottle = 10.5; % Diameter of Bottle [cm]
34 D_bottle = D_bottle/100; % Diameter of Bottle [m]
35 A_bottle = pi * (D_bottle/2)^2; % Cross-Sectional Area of Bottle [m^2]
36 R = 287; % Gas Constant of Air [J/kgK]
37 %m_bottle = 0.128; % Mass of Empty 2-Liter Bottle with Cone
38 % and Fins [kg] (Baseline)
39 %m_bottle = 0.160; % Mass of Empty 2-Liter Bottle with Cone
40 % and Fins [kg] (Optimized)
41 %cd = 0.38; % Drag Coefficient (Baseline)
42 %cd = 0.30; % Drag Coefficient (Optimized)
43 %ls = 0.5; % Length of test stand [m]
44 %wind = 3; % Wind Speed [mph] (Baselined)
45 %wind = 8; % Wind Speed [mph] (Optimized)
46 %wind = wind * 1609.34 / 3600; % Wind Speed [m/s]
47 %wind_angle = 45; % Wind Angle from North [deg]
48 %wind_angle = 90 - wind_angle; % Wind Angle from East [deg]
49 %wind_y = wind * sind(wind_angle); % Wind Speed from South Direction [m/s]
50 %wind_x = wind * cosd(wind_angle); % Wind Speed from West Direction [m/s]
```

```

49  wind_uncertainty = 11.25;           % Wind Angle Uncertainty [deg]
50  l_heading = 40;                     % Launch Heading is 40 deg from North, -50
    from East
51  l_heading = 90 - l_heading;         % Launch Heading from x-axis (East) [deg]
52  l_heading = l_heading * (pi/180);   % Launch Heading [rad]
53
54  %% Initial Value
55
56  P_gage_0 = 40;                       % Initial Gage Pressure of Air
    in Bottle [psi]
57  P_gage_0 = P_gage_0 * 6894.76;      % Initial Gage Pressure of Air
    in Bottle [Pa]
58  P_bottle = P_amb + P_gage_0;        % Initial Total Pressure of
    Air in Bottle [Pa]
59  m_water_uncertainty = 0.0005;      % Initial Mass of Water
    Uncertainty [kg]
60  %m_water_0 = 1.001;                % Initial Mass of Water [kg]
    (Baseline)
61  m_water_0 = 0.600;                % Initial Mass of Water [kg] (
    Optimized)
62  V_water_0 = m_water_0 / p_water;    % Initial Volume of Water
    Inside Bottle [m^3]
63  V_air_0 = V_bottle - V_water_0;     % Initial Volume of Air Inside
    Bottle [m^3]
64  %T_air_0 = 62;                     % Initial Temperature of Air
    [F] (Baseline)
65  T_air_0 = 63;                      % Initial Temperature of Air [
    F] (Optimized)
66  T_air_0 = (T_air_0 - 32) * (5 / 9) + 273.15; % Initial Temperature of Air [
    K]
67  m_air_0 = P_bottle * V_air_0 / ( R * T_air_0 ); % Initial Mass of Air [kg]
68  v_0 = 0.0;                         % Initial Velocity of Rocket [
    m/s ]
69  v_x_0 = 0.0;                       % Initial Velocity of Rocket
    in X-Direction [m/s ]
70  v_y_0 = 0.0;                       % Initial Velocity of Rocket
    in Y-Direction [m/s ]
71  v_z_0 = 0.0;                       % Initial Velocity of Rocket
    in Z-Direction [m/s ]
72  theta_0 = pi/4;                    % Initial Angle of Rocket (45
    ) [radians]
73  x_0 = 0.0;                         % Initial Horizontal (X)
    Distance [m]
74  y_0 = 0.0;                         % Initial Horizontal (Y)
    Distance [m]
75  z_0 = 0.25;                        % Initial Vertical Height [m]
76  h_stand = ls * cos(theta_0) + x_0; % Initial Horizontal Distance
    of Rocket on Stand [m]
77  v_stand = ls * sin(theta_0) + z_0; % Initial Vertical Distance of
    Rocket on Stand [m]
78  R_stand = sqrt( h_stand ^ 2 + v_stand ^ 2 ); % Initial Length of Rocket on
    Stand [m]
79
80  m_bottle_0 = m_water_0 + m_air_0 + m_bottle; % Initial Mass of Rocket [kg]

```

```

81                                     % Equation (11)
82
83 constants_wind = [ V_bottle , V_air_0 , P_bottle , cp_rat , C_d , p_water , A_throat ,
      P_amb , p_amb , cd , A_bottle , T_air_0 , m_air_0 , R , g , R_stand , theta_0 ,
      wind_x , wind_y , l_heading ];
84 constants = [ V_bottle , V_air_0 , P_bottle , cp_rat , C_d , p_water , A_throat ,
      P_amb , p_amb , cd , A_bottle , T_air_0 , m_air_0 , R , g , R_stand , theta_0 , 0 ,
      0 , l_heading ];
85
86 initial_state_vector = [x_0; z_0; v_x_0; v_z_0; m_bottle_0; m_air_0; V_air_0;
      y_0; v_y_0];
87
88 %%% Calling ODE45
89
90 tspan = [0 5]; % [s]
91
92 [t, state_vector] = ode45(@(t,y) rocket_fun(t, y, constants), tspan ,
      initial_state_vector);
93 [t, state_vector_wind] = ode45(@(t,y) rocket_fun(t, y, constants_wind), tspan ,
      initial_state_vector);
94
95 %%% Plot
96
97 % Plot Trajectory
98 figure(1)
99 plot3(state_vector(:,1),state_vector(:,8),state_vector(:,2)) % Aimed Direction
100 hold on
101 plot3(state_vector_wind(:,1),state_vector_wind(:,8),state_vector_wind(:,2)) %
      Flight
102 xlabel("Distance (E) [m]")
103 %xlim([-5 60])
104 ylabel("Distance (N) [m]")
105 %ylim([-10 10])
106 zlabel("Height [m]")
107 title("Height vs. Distance")
108 legend("Aimed Direction", "Flight")
109 grid on
110 hold off
111
112 dist = sqrt( max(state_vector(:,1))^2 + max(state_vector(:,8))^2 );
113 dist_wind = sqrt( max(state_vector_wind(:,1))^2 + max(state_vector_wind(:,8))
      ^2 );
114
115 %%% Monte Python Simulation
116
117 Number_of_Iterations = 100;
118 monte_max_values = zeros(Number_of_Iterations,3);
119
120 for i = 1: Number_of_Iterations
121
122     % Change Wind Parameter
123     wind_change = wind_uncertainty * (rand(1)*2-1); % Rand(1) finds random #
      between 0 and 1, multiply by 2 and subtract 1 to find # between -1 and
      1

```

```

124     wind_angle_monte = 45 + wind_change;           % Wind Angle from North [
        deg]
125     wind_angle_monte = 90 - wind_angle_monte;       % Wind Angle from East [
        deg]
126     wind_y_monte = wind * sind(wind_angle_monte);   % Wind Speed from South
        Direction [m/s]
127     wind_x_monte = wind * cosd(wind_angle_monte);   % Wind Speed from West
        Direction [m/s]
128
129     % Change Mass of Water Parameter
130     m_water_change = m_water_uncertainty * (rand(1)*2-1); % Rand(1)
        finds random # between 0 and 1, multiply by 2 and subtract 1 to find #
        between -1 and 1
131     m_water_0_monte = m_water_0 + m_water_change;    %
        Initial Mass of Water [kg]
132     V_water_0_monte = m_water_0_monte / p_water;      % Initial
        Volume of Water Inside Bottle [m^3]
133     V_air_0_monte = V_bottle - V_water_0_monte;       % Initial
        Volume of Air Inside Bottle [m^3]
134     m_air_0_monte = P_bottle * V_air_0_monte / ( R * T_air_0 ); % Initial
        Mass of Air [kg]
135     m_bottle_0_monte = m_water_0_monte + m_air_0_monte + m_bottle; % Initial
        Mass of Rocket [kg]
136
137     % Redefine Constants and Initial State Vector
138     constants_wind = [ V_bottle , V_air_0_monte , P_bottle , cp_rat , C_d , p_water ,
        A_throat , P_amb , p_amb , cd , A_bottle , T_air_0 , m_air_0_monte , R , g ,
        R_stand , theta_0 , wind_x_monte , wind_y_monte , l_heading ];
139     initial_state_vector_monte = [ x_0 ; z_0 ; v_x_0 ; v_z_0 ; m_bottle_0_monte ;
        m_air_0_monte ; V_air_0_monte ; y_0 ; v_y_0 ];
140
141     % Call ODE45
142     [t , state_vector_monte] = ode45(@(t,y) rocket_fun(t , y , constants_wind) ,
        tspan , initial_state_vector);
143
144     % Assign Values to Table
145     monte_max_values(i ,1) = max(state_vector_monte(:,1)); % Assign Max X-Value
146     monte_max_values(i ,2) = max(state_vector_monte(:,8)); % Assign Max Y-Value
147     monte_max_values(i ,3) = max(state_vector_monte(:,2)); % Assign Max Z-Value
148
149     % Plot Trajectory
150     figure(2)
151     hold on
152     plot3(state_vector_monte(:,1) ,state_vector_monte(:,8) ,state_vector_monte
        (:,2))
153     xlabel(" Distance (E) [m]")
154     ylabel(" Distance (N) [m]")
155     zlabel(" Height [m]")
156     title("Monte Carlo Sim Height vs. Distance")
157     grid on
158     hold off
159
160 end
161

```

```

162 [x_sim_mean, y_sim_mean] = error_ellipses(monte_max_values);
163 mean_dist = sqrt( x_sim_mean^2 + y_sim_mean^2 );
164
165 %% State Results
166
167 fprintf("The model predicts a total horizontal distance of %.2f m without wind
168         .\n",dist)
169 fprintf("The model predicts a total horizontal distance of %.2f m with wind.\n
170         ",dist_wind)
171 fprintf("The Monte Carlo Simulation predicts an average total horizontal
172         distance of %.2f m with wind.\n",mean_dist)
173
174 %% Function Initial Conditions
175
176 function state_vector = rocket_fun(t, y, constants)
177
178     %% Declare Constants
179     V_bottle = constants(1);
180     V_air_0 = constants(2);
181     P_bottle = constants(3);
182     cp_rat = constants(4);
183     C_d = constants(5);
184     p_water = constants(6);
185     A_throat = constants(7);
186     P_amb = constants(8);
187     p_amb = constants(9);
188     cd = constants(10);
189     A_bottle = constants(11);
190     T_air_0 = constants(12);
191     m_air_0 = constants(13);
192     R = constants(14);
193     g = constants(15);
194     R_stand = constants(16);
195     theta_0 = constants(17);
196     wind_x = constants(18);
197     wind_y = constants(19);
198     l_heading = constants(20);
199
200     horiz_0 = cos(theta_0); % Because theta was used in 2012 code, let's just
201     keep it and convert it to vector direction
202     z_dir_0 = sin(theta_0);
203     x_dir_0 = cos(l_heading) * horiz_0;
204     y_dir_0 = sin(l_heading) * horiz_0;
205     dir_0_mag = sqrt( x_dir_0^2 + y_dir_0^2 + z_dir_0^2);
206
207 %% State Values
208     p_x = y(1);
209     p_z = y(2);
210     v_x = y(3) + wind_x;
211     v_z = y(4);
212     m_bottle = y(5);
213     m_air = y(6);
214     V_air = y(7);
215     p_y = y(8);

```



```

212     v_y = y(9) + wind_y;
213
214 % Theta
215 rocket_pos = sqrt( p_x ^ 2 + p_y ^ 2 + p_z ^ 2 );
216 if ( rocket_pos > R_stand ) % determine if rocket has left stand
217     v_mag = sqrt( v_x^2 + v_y^2 + v_z^2);
218     z_dir = v_z / v_mag;
219     y_dir = v_y / v_mag;
220     x_dir = v_x / v_mag;
221 else
222     x_dir = x_dir_0 / dir_0_mag;
223     y_dir = y_dir_0 / dir_0_mag;
224     z_dir = z_dir_0 / dir_0_mag;
225 end
226
227 % Velocity
228 v = sqrt( v_x ^ 2 + v_y ^ 2 + v_z ^ 2 );
229
230 %% PHASE 1: Water Expulsion
231
232 if V_air < V_bottle
233
234     % Air Pressure
235     % Equation (3)
236     P_air = P_bottle * ( V_air_0 / V_air ) ^ cp_rat;
237
238     % Exhaust Velocity
239     % Equation (7)
240     v_exhaust = sqrt( 2 * ( P_air - P_amb ) / p_water );
241
242     % Mass Flow Rate of Water
243     % Equation (4)
244     m_dot_w = C_d * p_water * A_throat * v_exhaust;
245
246     % Mass Flow Rate of Rocket
247     % Equation (10)
248     m_dot_r = -m_dot_w;
249
250     % Mass Flow Rate of Air
251     m_dot_a = 0; % Air mass doesn't change in this phase
252
253     % Rate of Change of Volume of Air
254     % Equation (9)
255     V_dot = C_d * A_throat * v_exhaust;
256
257     % Force of Thrust
258     % Equation (8)
259     F_thrust = 2 * C_d * A_throat * ( P_air - P_amb );
260
261 else % set up Pressure and Temperatures for Phase 2 and 3
262
263     % Air Pressure and Temperature After Water Exhausted
264     % Equation (13)
265     P_end = P_bottle * ( V_air_0 / V_bottle ) ^ cp_rat;

```

```

266
267     % New Pressure Equation
268     % Equation (14)
269     P_air = P_end * (( m_air / m_air_0)) ^ cp_rat;
270
271     end
272
273     %% PHASE 2: Gas Expulsion
274
275     if ( V_air >= V_bottle ) && ( P_air > P_amb )
276
277         % Change in Volume
278         V_dot = 0;
279
280         % Calculate Density and Temperature
281         % Equation (15)
282         rho = m_air / V_bottle;
283         T = P_air / ( rho * R );
284
285         % Critical Pressure
286         % Equation (16)
287         P_crit = P_air * ( 2 / ( cp_rat + 1 )) ^ ( cp_rat / ( cp_rat - 1));
288
289         % If Choked Flow
290         if ( P_crit > P_amb )
291
292             % Exit Temperature
293             % Equation (18)
294             T_exit = ( 2 / ( cp_rat + 1 )) * T;
295
296             % Exit Velocity
297             % Equation (17)
298             V_exit = sqrt( cp_rat * R * T_exit );
299
300             % Exit Pressure
301             % Equation (18)
302             P_exit = P_crit;
303
304             % If Not Choked Flow
305             else
306
307                 % Exit Mach Number
308                 % Equation (19)
309                 Mach_exit = sqrt(abs((( P_air / P_amb ) ^ (( cp_rat - 1) / cp_rat)
310                     - 1 ) / (( cp_rat - 1 ) / 2))));
311
312                 % Exit Temperature
313                 % Equation (20)
314                 T_exit = T / ( 1 + ( ( cp_rat - 1) / 2 ) * Mach_exit ^ 2);
315
316                 % Exit Pressure
317                 % Equation (20)
318                 P_exit = P_amb;

```

```

319         % Exit Velocity
320         % Equation (21)
321         V_exit = Mach_exit * sqrt(abs( cp_rat * R * T_exit ));
322
323     end
324
325     % Exit Density
326     % Equation (18) and (20)
327     rho_exit = P_exit / ( R * T_exit);
328
329     % Change in Air Mass
330     % Equation (23)
331     m_dot_a = -C_d * rho_exit * A_throat * V_exit;
332
333     % Force of Thrust
334     % Equation (22)
335     F_thrust = (-m_dot_a * V_exit) + (( P_amb - P_exit ) * A_throat);
336
337     % Change in Rocket Mass
338     % Equation (24)
339     m_dot_r = m_dot_a;
340
341 end
342
343 %%% PHASE 3: Ballistic Phase
344
345 if (V_air >= V_bottle) && (P_air <= P_amb)
346
347     % No more water or gas so theres no change in mass, volume, or thrust
348     % Equation (25)
349     F_thrust = 0;
350     m_dot_r = 0;
351     m_dot_a = 0;
352     V_dot = 0;
353
354 end
355
356 %%% Final State Function Calculations
357
358 % Force of Drag
359 % Equation (2)
360 F_drag = (1/2) * p_amb * (v ^ 2) * cd * A_bottle;
361
362 % Sum of Forces
363 % Equation (1)
364 sum_F_x = F_thrust * x_dir - F_drag * x_dir;
365 sum_F_y = F_thrust * y_dir - F_drag * y_dir;
366 sum_F_z = F_thrust * z_dir - F_drag * z_dir - m_bottle * g;
367
368 % Acceleration
369 % Equation (1)
370 acc_x = sum_F_x / m_bottle;
371 acc_y = sum_F_y / m_bottle;
372 acc_z = sum_F_z / m_bottle;

```

```

373
374     % Keep Above x-axis
375     if p_z <= 0
376         v_x = 0;
377         v_z = 0;
378         acc_x = 0;
379         acc_z = 0;
380         m_dot_r = 0;
381         m_dot_a = 0;
382         V_dot = 0;
383         v_y = 0;
384         acc_y = 0;
385     end
386
387     % Resulting State Values
388     state_vector(1,1) = v_x;
389     state_vector(2,1) = v_z;
390     state_vector(3,1) = acc_x;
391     state_vector(4,1) = acc_z;
392     state_vector(5,1) = m_dot_r;
393     state_vector(6,1) = m_dot_a;
394     state_vector(7,1) = V_dot;
395     state_vector(8,1) = v_y;
396     state_vector(9,1) = acc_y;
397
398 end
399
400 %%% Error Ellipses Function
401
402 function [mean_x, mean_y] = error_ellipses(xyz_data)
403
404 N = length(xyz_data);
405 x = xyz_data(:,1);
406 y = xyz_data(:,2);
407
408 figure(3)
409 plot(x,y,'k.','markersize',6)
410 axis equal
411 grid on
412 xlabel('Distance (East) [m]')
413 ylabel('Distance (North) [m]')
414 hold on
415
416 % Calculate Covariance Matrix
417 P = cov(x,y);
418 mean_x = mean(x);
419 mean_y = mean(y);
420
421 % Calculate the define the error ellipses
422 n=100; % Number of points around ellipse
423 p=0:pi/n:2*pi; % angles around a circle
424
425 [eigvec,eigval] = eig(P); % Compute eigen-stuff
426 xy_vect = [cos(p'),sin(p')] * sqrt(eigval) * eigvec'; % Transformation

```

```

427 x_vect = xy_vect(:,1);
428 y_vect = xy_vect(:,2);
429
430 % Plot the error ellipses overlaid on the same figure
431 plot(1*x_vect+mean_x, 1*y_vect+mean_y, 'b')
432 plot(2*x_vect+mean_x, 2*y_vect+mean_y, 'g')
433 plot(3*x_vect+mean_x, 3*y_vect+mean_y, 'r')
434
435 end

```

## **X. References and Acknowledgements**

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### **B. Acknowledgements**

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