

$$(1) \log_{10} P_{\text{bar}}^{\text{sat}} = A - \frac{B}{T_{\text{K}} + C}$$

Normal BP of menthol =  $63^{\circ}\text{C} = 336.15\text{K}$   
(M)

Menthol Antoine Constants

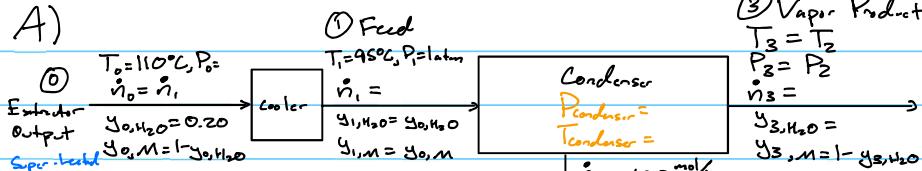
$$A = 5.38347$$

$$B = 2405.946$$

$$C = 111$$

Temp Range:  
329-485 K

A)



Add'l Eqs

$$(1) \log_{10} P_{H_2O}^{\text{sat}} = A - \frac{B}{T + C} \quad \text{X}$$

$$(2) \log_{10} P_m^{\text{sat}} = A - \frac{B}{T + C} \quad \text{X}$$

$$(3) P^{\text{tot}} = x_{2,H_2O} P_{H_2O}^{\text{sat}} + x_{2,m} P_m^{\text{sat}} \quad \text{X}$$

$$(4) 1 = \frac{y_{2,m} P_m^{\text{sat}} + y_{2,H_2O} P_{H_2O}^{\text{sat}}}{P_m^{\text{sat}} + P_{H_2O}^{\text{sat}}} \quad \text{X}$$

$$(5) y_{3,m} P = x_{2,m} P_m^{\text{sat}} \quad \text{X}$$

Gives & Want to Know

$$\text{B}) P_{\text{condenser}} = 1 \text{ atm}$$

$$\text{D}) \text{Want to know: } \dot{m}_3$$

Antoine Constants for H<sub>2</sub>O

$$0-60^{\circ}\text{C}: A = 6.10765; B = 1750.286; C = 235$$

$$60-150^{\circ}\text{C}: A = 7.96681; B = 1668.210; C = 228 \quad \text{On S. Use L1 More}$$

B) Condenser = 1 Pseudo How-to Solve

Plot should be  $x_{2,y}$  (mol fraction of menthol)

$$T_{\text{boil},H_2O}(1\text{ atm}) = 100.3^{\circ}\text{C} \quad \text{X} \text{ Wolfson}$$

$$T_{\text{boil},m}(\text{normal atm}) = 63^{\circ}\text{C} \quad \text{X} \text{ Given}$$

$$\text{Euler distribution: } \frac{100.3 - 63}{33 - 3}$$

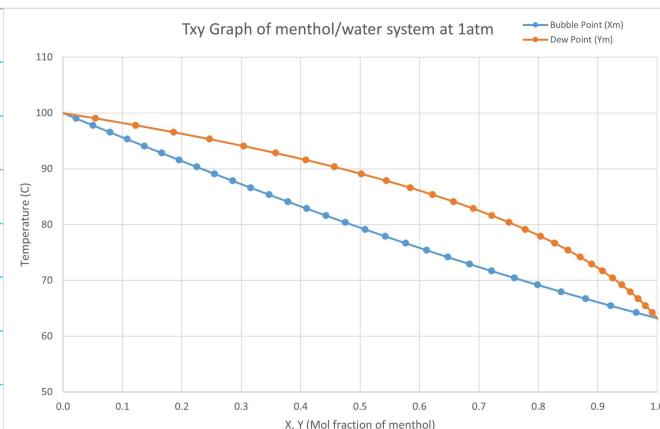
$$\text{X) } P_m^{\text{sat}}(1\text{ atm}) = 10^1 \left( A - \frac{B}{T + C} \right) \text{ D3}$$

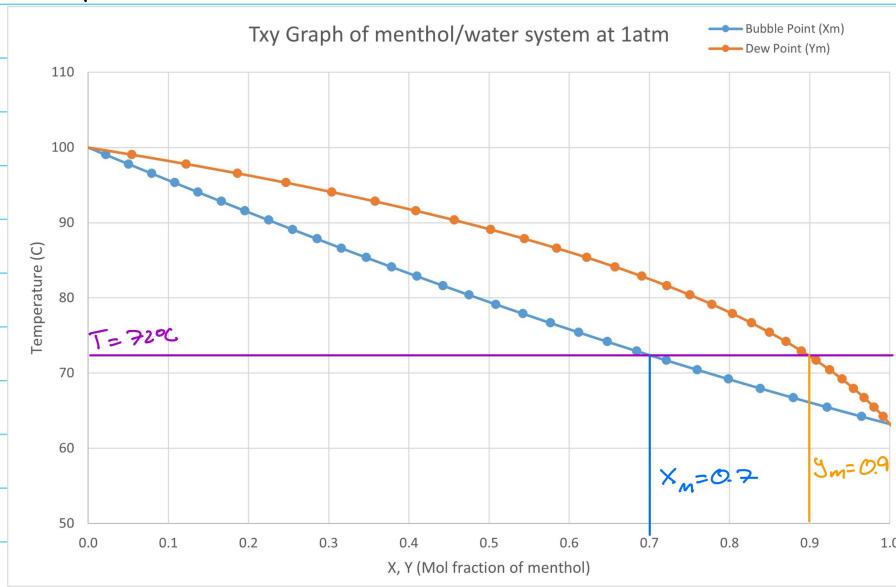
$$\text{X) } P_{H_2O}^{\text{sat}}(1\text{ atm}) = 10^1 \left( A - \frac{B}{T + C} \right) \text{ F3}$$

$$1 \text{ bar} \times \frac{750.06156 \text{ mmHg}}{1 \text{ bar}} \quad \text{E3}$$

$$\begin{aligned} P^{\text{tot}} &= x_m P_m^{\text{sat}} + (1-x_m) P_{H_2O}^{\text{sat}} \Rightarrow x_m = \frac{P^{\text{tot}} - P_{H_2O}^{\text{sat}}}{P_m^{\text{sat}} - P_{H_2O}^{\text{sat}}} \quad \text{G3} \\ &= x_m P_m^{\text{sat}} + P_{H_2O}^{\text{sat}} - x_m P_{H_2O}^{\text{sat}} \\ &= x_m (P_m^{\text{sat}} - P_{H_2O}^{\text{sat}}) + P_{H_2O}^{\text{sat}} \end{aligned}$$

$$y_m = \frac{x_m P_m^{\text{sat}}}{P^{\text{tot}}} \quad \text{H3}$$



Herbal Oil Production (Continued)C) Temperature =  $72^\circ\text{C}$ 

At  $72^\circ\text{C}$  Out

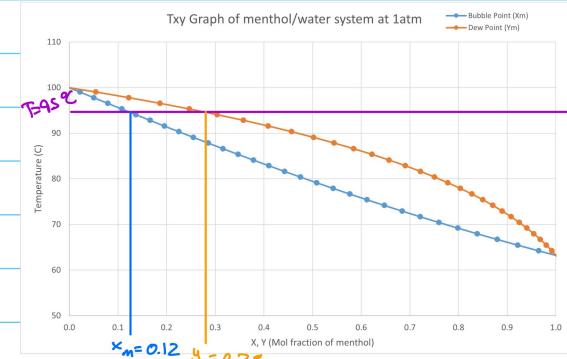
Liquid:  $x_{3,\text{H}_2\text{O}} = 0.7$   
 $x_{3,\text{H}_2\text{O}} = 0.3$

Vapor:  $y_{3,\text{H}_2\text{O}} = 0.9$   
 $y_{3,\text{H}_2\text{O}} = 0.1$

D) Horizontal line under part D indicates that we should continue to use the same process conditions from B and C. I will assume  $T_{\text{condenser}} = 72^\circ\text{C}$  and  $P_{\text{condenser}} = 1 \text{ atm}$  as the process conditions are only explicitly stated to change in part E.

D.o.F Condenser

- 2 Unknowns ( $\dot{n}_1, \dot{n}_3$ ) *All components can be read from Txy plot*
- + 0 Chemical Reactions
- 2 Material Balances ( $\text{H}_2\text{O}$  & Menthol)
- 0 Additional E.Qs

Soluble*Every stream is multiphase*Material Balances Condenser

$$\text{H}_2\text{O}: \dot{n}_1 y_{1,\text{H}_2\text{O}} + \dot{n}_1 x_{1,\text{H}_2\text{O}} = \dot{n}_2 x_{2,\text{H}_2\text{O}} + \dot{n}_3 y_{3,\text{H}_2\text{O}}$$

$$M: \dot{n}_1 y_{1,m} + \dot{n}_1 x_{1,m} = \dot{n}_2 x_{2,m} + \dot{n}_3 y_{3,m}$$

$$\text{Tot.1: } \dot{n}_1 = \dot{n}_2 + \dot{n}_3$$

From (c)

$$\begin{aligned} x_{3,m} &= 0.7 & y_{3,m} &= 0.9 \\ x_{3,\text{H}_2\text{O}} &= 0.3 & y_{3,\text{H}_2\text{O}} &= 0.1 \end{aligned}$$

Inlet Conditions

$$\begin{aligned} x_m &= 0.12 & y_m &= 0.28 \end{aligned}$$

How to Solve

- Use Txy diagram to get  $x_m, y_m$  at  $95^\circ\text{C}$  and 1 atm (inlet conditions), and use PFD to get  $x_{1,\text{H}_2\text{O}}$  and  $y_{1,\text{H}_2\text{O}}$
- Substitute  $\dot{n}_1 = \dot{n}_2 + \dot{n}_3$  into M balance to solve for  $\dot{n}_3$   
*bc can do this bc 3 eqns 2 unknowns*

Done, we have  $\dot{n}_3$ , production rate of vapor phase

Herbal Oil Production (Continued)

E. Boyer requests  $y_{3, \text{H}_2\text{O}} \leq 0.05$ .  $P_{\text{condenser}} = 1 \text{ atm}$  still; find  $T_{\text{condenser}}$  for  $y_{3, \text{H}_2\text{O}} = 0.05$  maximum allowable temp

$$\text{Dew Point Eq: } 1 = \frac{P_{y_{3,m}}}{P_m} + \frac{P_{y_{3,\text{H}_2\text{O}}}}{P_{\text{H}_2\text{O}}} \quad \text{Tip: P_bar} \rightarrow P_m \quad \text{Tip: C, D in mmHg} \quad \star$$

Pseudo "How to Solve"

(1) Find  $y_{3,m}$  using PFD:  $y_{3,m} = 1 - y_{3,\text{H}_2\text{O}} = 1 - 0.05 = 0.95$

(2) Convert  $P_{\text{condenser}}$  to bar and mmHg for dimensional homogeneity

$$1 \text{ atm} \times \frac{1.013 \text{ bar}}{1 \text{ atm}} \quad \text{and} \quad 1 \text{ atm} \times \frac{760 \text{ mmHg}}{1 \text{ atm}} \quad \text{Conversions done in excel}$$

(3) Substitute Antoine Equation into Dew Point Equations

$$1 = \frac{y_{3,m} P}{10^A (A - \frac{B}{T_{\text{FC}}})} + \frac{y_{3,\text{H}_2\text{O}} P}{10^A (A - \frac{B}{T_{\text{FC}}})}$$

Final Answer is in  $^{\circ}\text{C}$ , so guesses will be performed in  $^{\circ}\text{C}$

$\Rightarrow P_m^{\text{sat}}$  is in terms of  $K$ , so shift left  $273.15K$

$$\Rightarrow 1 = \frac{y_{3,m} P^{\text{bar}}}{10^A (A - \frac{B}{(T+273.15)+C})} + \frac{y_{3,\text{H}_2\text{O}} P^{\text{mmHg}}}{10^A (A - \frac{B}{T_{\text{FC}}})} \quad \star$$

$P^*1 \leftarrow \text{excel} \rightarrow P^*2$

(4) Guess a temperature of  $80^{\circ}\text{C} = T_{\text{guess}}$

(5) Calculate Cells for  $P^*1$  and  $P^*2$  with  $T_{\text{guess}}$

(6) Use Goal seek to find when  $T_{\text{guess}}$  is  $\boxed{=}$  yield  $\approx 0.05$

LHS Dew Point = 6.999937 when  $T_{\text{guess}} = 68.3667^{\circ}\text{C}$

Maximum allowed temperature:  $68.37^{\circ}\text{C}$

- F) **Reflection:** Discuss the pros and cons of using Solver in excel vs. an already generated Txy diagram.

Solver is an extremely powerful tool that allows for determining accurate solutions via guessing. This is particularly useful for solving for Temperature from the Dew Point or Bubble Point equations. These questions can be hard or impossible to solve as they involve the unknown being in a fractional exponent. Excel's ability to do this is great for these applications, but when I played around with it, it looks like Excel will give up after too many failed attempts. This seems like a small issue as you need to have a general idea of the range your goal is in, or else Excel may just fail. This might be difficult in real-world applications where behavior is more unpredictable. Also it is a little hard to set up sometimes as you need to keep track of the different references in complex equations and make sure all of your units are homogenous. That being said, it is great for more predictable systems like ones where a Txy plot is already generated and you know a standard operating range. Also the immense speed of the checks is great from a time-saving point of view, and the UI is simple. For Txy plots, they can be very useful for quickly reading compositions based off provided temperature, or the other way around. This makes them very useful for the system they were designed for, but as soon as the operating pressure changes, the Txy plot doesn't work anymore. Despite the readability and ease of understanding, the Txy plot is much weaker than the Solver function in Excel which can react to changes in input data easily as you just have to rerun the command. You need to remake a full plot if you change the input parameters of a Txy plot, which can definitely be a downside. Overall, Txy and Solver plots in Excel aren't necessarily better than each other, and can be used well given that you understand the software and your situation lends itself to the strength of either method.