

Name Solution

Wednesday, February 28th

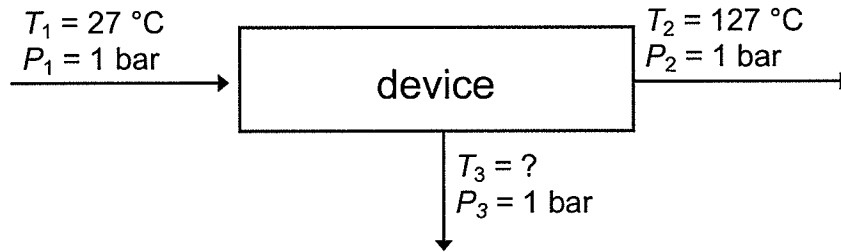
ECHE 363 – Thermodynamics of Chemical Systems
Midterm #1

Rules:

- 75 minutes total time. Once time is up, put aside answer sheets.
- Be sure to show all work to obtain maximum credit. This includes showing and simplifying any mass/mole, 1st Law, and 2nd Law balances that are needed to solve each problem.
- Closed book and no notes.
- Write your name on every page.
- Please only write on the front side of each page. Ask for additional paper if necessary.

Name _____

1. (25 points) Nitrogen gas at 27 °C in “stream 1” flows into a well-insulated device operating at steady state. There is no shaft work. Two-thirds of the nitrogen, by moles, exits at 127 °C and 1 bar in “stream 2”. The remainder of the nitrogen exit through “stream 3” at an unknown temperature and 1 bar. Find the temperature of the nitrogen in the “stream 3” outlet. Assume ideal gas behavior, where nitrogen has $c_{p,m} = 29.1 \text{ J/mol-K}$.



mass balance: $\frac{dn}{dt} = 0 = \dot{n}_1 - \dot{n}_2 - \dot{n}_3$

\downarrow steady state
 \uparrow system

$$\dot{n}_1 = \dot{n}_2 + \dot{n}_3$$

$$\dot{n}_2 = \frac{2}{3} \dot{n}_1, \quad \dot{n}_3 = \frac{1}{3} \dot{n}_1$$

1st Law: $\frac{d}{dt} (U + E_k + E_p) = 0 = \dot{n}_1 h_{m,1} - \dot{n}_2 h_{m,2} - \dot{n}_3 h_{m,3}$

\downarrow steady state
 \downarrow no shaft work
 \downarrow 0, insulated

$$0 = h_{m,1} - \frac{2}{3} h_{m,2} - \frac{1}{3} h_{m,3}$$

$$0 = 2 \underbrace{(h_{m,1} - h_{m,2})}_{= \int_{T_2}^{T_1} c_{p,m} dT} + \underbrace{(h_{m,1} - h_{m,3})}_{= \int_{T_3}^{T_1} c_{p,m} dT}$$

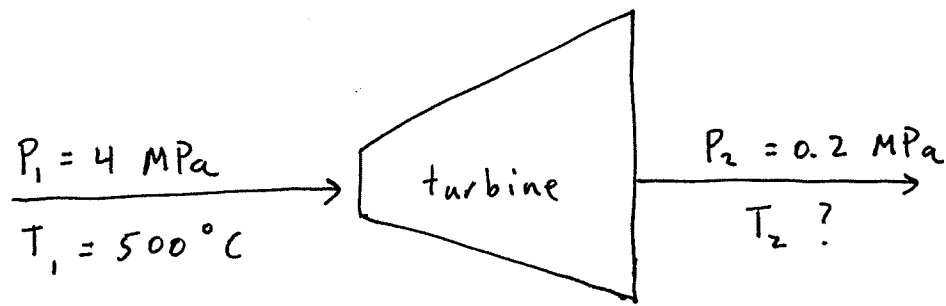
$$0 = 2 \overset{\substack{\text{constant} \\ \downarrow}}{C_{p/m}} (T_1 - T_2) + C_{p/m} (T_1 - T_3)$$

$$T_3 = 3T_1 - 2T_2 = 100 \text{ K} = -173^\circ \text{C}$$

Name _____

2. (40 points) Steam is fed to an adiabatic turbine at 4 MPa and 500 °C. It exits at 0.2 MPa. Assuming that the process occurs at steady state, what is the maximum possible work (per kg of steam) that can be extracted from the turbine?

Hint: remember to determine the phase of both the input and output water streams.



mass balance: $\frac{dn}{dt} = 0 = \dot{n}_1 - \dot{n}_2 \leftrightarrow \dot{n}_1 = \dot{n}_2 = \dot{n}$

↑
steady state

$\dot{m}_1 = \dot{m}_2 = \dot{m}$

1st Law: $\frac{d}{dt}(U + E_k + E_p) = 0 = \underbrace{\dot{m}_1 \hat{h}_1 - \dot{m}_2 \hat{h}_2}_{\text{ignore KE, PE}} + \dot{W}_S + \underbrace{\dot{Q}}_{\substack{0 \\ \text{adiabatic}}}$

use MB $\longrightarrow 0 = \dot{m}(\hat{h}_1 - \hat{h}_2) + \dot{W}_S$

$\dot{W}_S = \dot{m}(\hat{h}_2 - \hat{h}_1)$

↑
unknown

↑
~~h₂~~

↑
h₁ can be looked up

Want $\dot{W}_{S, \max}$ (reversible case, $\frac{dS_{\text{univ}}}{dt} = 0$)

2nd Law: $\frac{dS_{univ}}{dt} = \overset{\text{rev}}{0} = \underbrace{\frac{dS}{dt}}_{0, \text{ steady state}} + \dot{m}_2 \hat{s}_2 - \dot{m}_1 \hat{s}_1 - \underbrace{\frac{\dot{Q}}{T_{burr}}}_{0, \text{ adiabatic}}$

use MB $\rightarrow 0 = \dot{m} (\hat{s}_2 - \hat{s}_1)$

$$\hat{s}_2 = \hat{s}_1$$

"1" is superheated, @ $T_1 = 500^\circ\text{C}$
 $P_1 = 4 \text{ MPa}$

$$\rightarrow \begin{aligned} \hat{s}_1 &= 7.09 \text{ kJ/kg-K} \\ \hat{h}_1 &= 3445.2 \text{ kJ/kg} \end{aligned}$$

Find where $\hat{s}_2 = \hat{s}_1 = 7.09 \text{ kJ/kg-K}$
 for $P_2 = 0.2 \text{ MPa}$

(a) $P_2 = 0.2 \text{ MPa}, T^{\text{sat}} = 120.23$

$$\hat{s}_L^{\text{sat}} = 1.53 \text{ kJ/kg-K}, \hat{h}_L^{\text{sat}} = 504.68 \text{ kJ/kg}$$

$$\hat{s}_V^{\text{sat}} = 7.1271 \text{ kJ/kg-K}, \hat{h}_V^{\text{sat}} = 2706.6 \text{ kJ/kg}$$

$$\hat{s}_L^{\text{sat}} < \hat{s}_2 < \hat{s}_V^{\text{sat}}$$

\therefore "2" is a saturated liq/vap mixture!

$$\hat{s}_2 = x \hat{s}_v^{sat} + (1-x) \hat{s}_L^{sat}$$

$$x = \frac{\hat{s}_2 - \hat{s}_L^{sat}}{\hat{s}_v^{sat} - \hat{s}_L^{sat}} = \frac{7.09 - 1.53}{7.1271 - 1.53} = 0.993$$

Back to 1st Law to find \dot{w}_s , max :

$$\dot{w}_s = \dot{m} (\hat{h}_2 - \hat{h}_1)$$

$$\frac{\dot{w}_s}{\dot{m}} = \hat{w}_s = \hat{h}_2 - \hat{h}_1$$

$$\hat{h}_2 = x \hat{h}_v^{sat} + (1-x) \hat{h}_L^{sat}$$

$$\hat{h}_2 = 2692.00 \text{ kJ/kg}$$

$$\hat{w}_s = 2692 - 3445.2$$

$$\boxed{\hat{w}_s = -753 \text{ kJ/kg}}$$

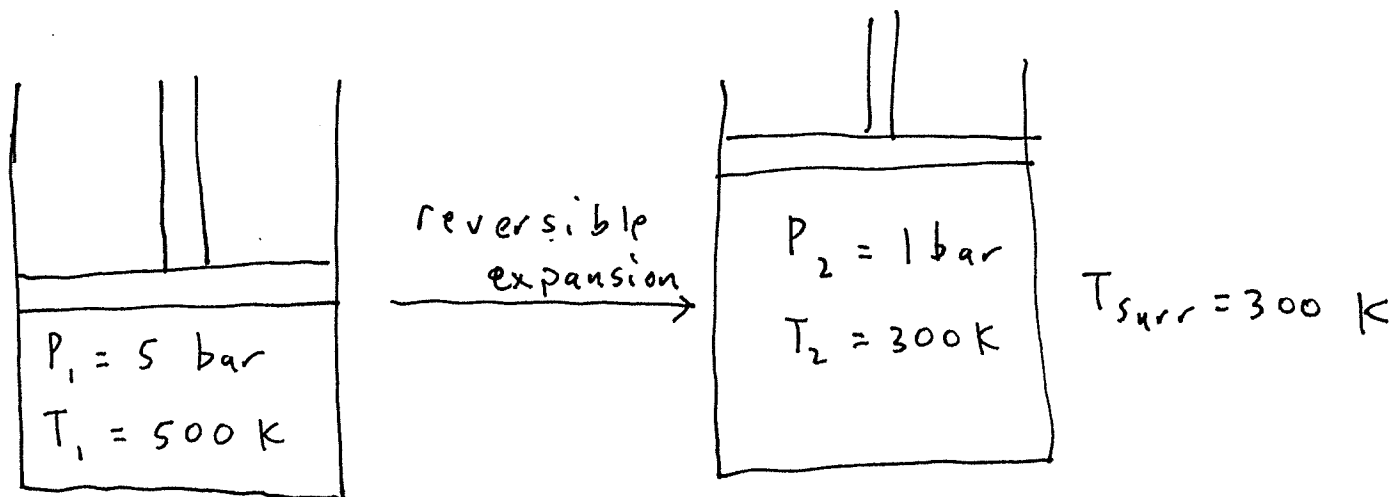
work extracted from turbine
per mass of steam.

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3. (35 points) One mole of an ideal gas contained within a piston–cylinder assembly has an initial pressure of $P_1 = 5$ bar and initial temperature of $T_1 = 500$ K. It undergoes a reversible expansion until it reaches a final pressure of $P_2 = 1$ bar and final temperature of $T_2 = 300$ K. The expansion is not adiabatic and thus heat transfer cannot be neglected. The surroundings have a temperature of $T_{\text{surr}} = 300$ K. The fluid has a constant-pressure heat capacity of:

$$c_{p,m}/R = A + BT, \text{ where } A = 3.5 \text{ and } B = 0.02 \text{ K}^{-1}$$

For the process described above, calculate: W , Q , ΔS_{sys} , ΔS_{surr} , ΔS_{univ} .



closed system, $n_1 = n_2 = n$

1st Law: $\Delta U = Q + W \leftarrow = - \int_{V_1}^{V_2} P_E dV$

\uparrow
 $= \int_{T_1}^{T_2} C_{v,m} dT$ can't neglect Q !

$\int_{T_1}^{T_2} C_{v,m} dT = Q - \int_{V_1}^{V_2} P_E dV$
 \uparrow
 reversible, $P_E = P$

$\int_{T_1}^{T_2} C_{v,m} dT = Q - \int_{V_1}^{V_2} P dV$
 \uparrow

P, V, T all changing
 cannot evaluate this
 integral!

use 2nd Law:

$$\Delta S_{\text{univ}} = \Delta S + \Delta S_{\text{surr}}$$

$$\boxed{\Delta S_{\text{univ}} = 0} \quad \text{reversible}$$

$$\Delta S = n \Delta S_m = n \int_{\text{"1"}}^{\text{"2"}} dS_m$$

↑
closed
sys

$$\Delta S = n \left[\int_{T_1}^{T_2} \frac{C_{P,m}}{T} dT - \int_{P_1}^{P_2} \frac{R}{P} dP \right]$$

$$\Delta S = nR \left[\int_{T_1}^{T_2} \left(\frac{A}{T} + B \right) dT - \int_{P_1}^{P_2} \frac{1}{P} dP \right]$$

$$\Delta S = nR \left[A \ln\left(\frac{T_2}{T_1}\right) - B(T_2 - T_1) - R \ln\left(\frac{P_2}{P_1}\right) \right]$$

$$\boxed{\Delta S = -34.74 \text{ J/K}}$$

$$\boxed{\Delta S_{\text{surr}} = -\Delta S = 34.74 \text{ J/K}}$$

$$\Delta S_{\text{surr}} = - \frac{Q}{T_{\text{surr}}}$$

$$Q = - T_{\text{surr}} \Delta S_{\text{surr}}$$

$$Q = -10421 \text{ J}$$

1st Law: $W = \Delta U - Q$

$$W = n \int_{T_1}^{T_2} C_{v,m} dT - Q$$

$$W = nR \int_{T_1}^{T_2} (A + BT - 1) dT - Q$$

$$W = nR \left[(A-1)(T_2 - T_1) + \frac{B}{2}(T_2^2 - T_1^2) \right] - Q$$

$$W = -7037.5 \text{ J}$$