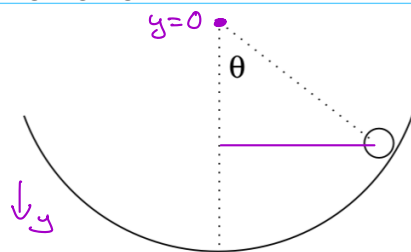


PHYS121 - Homework 7

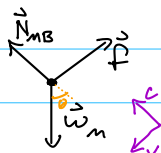
Problem 1)



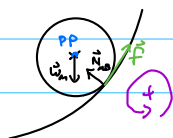
Given

- Marble of radius r and mass m
- Marble released @ rest w/ given angle θ_0
- Bowl has Radius of curvature R and $r \ll R$
- Friction, no slip no hole

a) FBD Marble



b) x FBD Marble



c) Determine Net Torque based on given

$$\begin{aligned} \tau_{\text{Net}} &= \tau_f + \tau_N + \tau_w \\ \tau_{\text{Net}} &= r f \sin 90^\circ + 0 + 0 \\ \tau_{\text{Net}} &= r f \end{aligned}$$

NZL $F_c = m a_c$
 $f - W \cos \theta = 0$ released @ rest
 $f = m g \sin \theta$
 $\tau_{\text{Net}} = m g r \sin \theta$
 $\tau_{\text{Net}} = \frac{2}{3} m R g \sin \theta$

d) NZL c-d.r

$$\begin{aligned} F_c &= m a_c \quad \text{UCM} \quad a_c = \frac{v_c^2}{r} \\ \vec{N}_{MB} - W_c &= m \frac{v_c^2}{R} \quad \text{@ rest} \\ \vec{N}_{MB} - W \cos \theta &= 0 \\ \vec{N}_{MB} &= m g \cos \theta \end{aligned}$$

NZL v-d.r

$$\begin{aligned} F_v &= m a_v \\ W_v - f &= m a_v \\ W \sin \theta - f &= m a_v \\ m g \sin \theta - f &= m a_v \end{aligned}$$

NZL Rot

$$\begin{aligned} \tau_{\text{Net}} &= I \alpha \\ \tau_N + \tau_w + \tau_f &= \frac{2}{3} m r^2 \alpha \\ 0 \cdot W + r N \sin 180^\circ + r f \sin 90^\circ &= \frac{2}{3} m r^2 \left(\frac{a_v}{r} \right) \\ r f &= \frac{2}{3} m r^2 \left(\frac{a_v}{r} \right) \\ f &= \frac{2}{3} m a_v \end{aligned}$$

Two Eqs, Two Unknowns

$$\begin{cases} m g \sin \theta - f = m a_v \\ f = \frac{2}{3} m a_v \end{cases}$$

$$\begin{aligned} m g \sin \theta - \frac{2}{3} m a_v &= m a_v \\ g \sin \theta &= \frac{5}{3} a_v \end{aligned}$$

$$\therefore a_v = \frac{3}{5} g \sin \theta$$

e) CoFME

Conditions: W_{ext} is conservative,

Normal Force $\perp \rightarrow$ no work & friction

does no work @ point of contact $m g y + \frac{1}{2} m v^2 + \frac{1}{2} I \omega^2 = m g y' + \frac{1}{2} m v'^2 + \frac{1}{2} I \omega'^2$

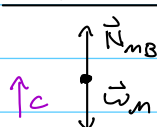
Rolling Constraint: $\omega = \frac{v}{r}$ $y = R \cos \theta, y' = R, v = 0, v' = ? \quad \omega = 0, \omega' = \frac{v'}{r}$

$$\begin{aligned} -m g R \cos \theta + 0 + 0 &= m g R + \frac{1}{2} m v_p^2 + \frac{1}{2} \left(\frac{2}{3} m r^2 \right) \left(\frac{v_p}{r} \right)^2 \\ -m g R \cos \theta &= m g R + \frac{1}{2} m v_p^2 + \frac{1}{3} m v_p^2 \\ g R - g R \cos \theta &= v_p^2 \left(\frac{1}{2} + \frac{1}{3} \right) \rightarrow g R (1 - \cos \theta) = \frac{5}{6} v_p^2 \end{aligned}$$

$$\therefore v_p = \sqrt{\frac{10}{7} g R (1 - \cos \theta)}$$

f) FBD Bottom

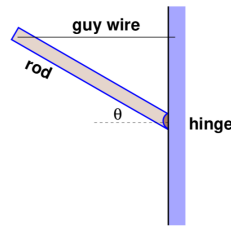
NZL c-d.r



$$\begin{aligned} F_c &= m a_c \quad \text{UCM} \quad a_c = \frac{v_c^2}{r} \\ N_{MB} - W_m &= m \frac{v_c^2}{R} \\ N_{MB} &= W_m + m \frac{v_c^2}{R} \\ &= m g + m \frac{\left(\sqrt{\frac{10}{7} g R (1 - \cos \theta)} \right)^2}{R} \end{aligned}$$

$$\begin{aligned} N_{MB} &= m g + \frac{10}{7} m g (1 - \cos \theta) \\ &= m g \left(1 + \frac{10}{7} - \frac{10}{7} \cos \theta \right) \\ \therefore N_{MB} &= m g \left(\frac{17}{7} - \frac{10}{7} \cos \theta \right) \\ N_{MB} &= \frac{1}{7} m g (17 - 10 \cos \theta) \end{aligned}$$

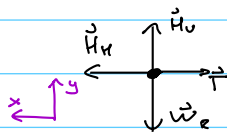
Problem 2)



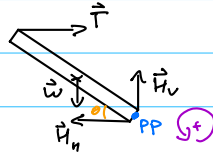
Given

- Rod of mass m and length l
- Rod has $I = \frac{1}{3}ml^2$
- Rod held in place @ θ
- Rod held by ideal string

a) FBD Rod



x FBD Rot



b) NZL Rod y-dir

$$F_y = m a_y$$

$$H_v - W_e = 0$$

$$H_v = mg$$

NZL Rod x-dir

$$F_x = m a_x$$

$$H_h - T = 0$$

$$H_h - \frac{1}{2}mg \tan \theta = 0$$

$$\therefore H_h = \frac{1}{2}mg \tan \theta$$

NZL Rot

$$\tau_{net} = I \alpha$$

$$\tau_H + \tau_v + \tau_T + \tau_w = 0$$

$$0 + 0 - l T \sin(40 - \theta) + \frac{l}{2} W \sin \theta = 0$$

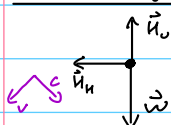
$$\frac{l}{2} mg \sin \theta - l T \cos \theta = 0$$

$$\frac{1}{2} mg \sin \theta = T \cos \theta$$

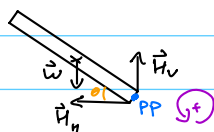
$$T = \frac{1}{2} mg \tan \theta$$

c) Rod starts @ rest!

FBD Rod



x FBD Rod



NZL Rot

$$\tau_{net} = I \alpha$$

R.C. $\alpha = \frac{a_v}{r} \Rightarrow \frac{l}{2} \text{ for Com}$

$$\tau_H + \tau_v + \tau_w = \frac{1}{3}ml^2 \left(\frac{a_v}{\frac{l}{2}} \right)$$

$$0 + 0 + \frac{l}{2} mg \sin \theta = \frac{1}{3}ml^2 \left(\frac{2a_v}{l} \right)$$

$$\frac{1}{2} mg \sin \theta = \frac{2}{3} m a_v$$

$$a_v = \frac{3}{4} g \sin \theta$$

d) CoFME

Conditions: $W_{e, \text{net}}$ is conservative

$$E_{\text{Tot}} = E'_{\text{Tot}}$$

Hinge does no work at contact.

$$U + K_T + K_R = U' + K'_T + K'_R$$

$$mg y + \frac{1}{2} m v^2 + \frac{1}{2} I \omega^2 = mg y' + \frac{1}{2} m v'^2 + \frac{1}{2} I \omega'^2$$

$$y = \frac{l}{2} \sin \theta, y' = -\frac{l}{2}, v = 0, v' = \omega r = \frac{\omega l}{2}, \omega = 0, \omega' = \omega'$$

$$mg \left(\frac{l}{2} \sin \theta \right) + 0 + 0 = mg \left(-\frac{l}{2} \right) + \frac{1}{2} m \left(\frac{\omega l}{2} \right)^2 + \frac{1}{2} \left(\frac{1}{3} m l^2 \right) \omega^2$$

$$\frac{1}{2} m g l \sin \theta = -\frac{1}{2} m g l + \frac{1}{8} m l^2 \omega^2 + \frac{1}{6} m l^2 \omega^2$$

$$\frac{1}{2} g \sin \theta = -\frac{1}{2} g + \frac{1}{8} l \omega^2 + \frac{1}{6} l \omega^2$$

$$\frac{1}{2} g (\sin \theta + 1) = \omega^2 \left(\frac{1}{8} l + \frac{1}{6} l \right)$$

$$\frac{1}{2} g (\sin \theta + 1) = \omega^2 \left(\frac{7}{24} l \right)$$

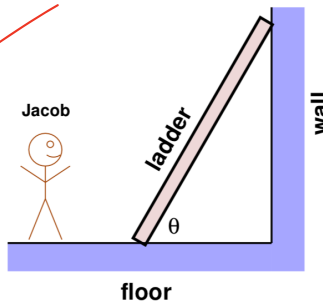
$$\omega^2 = \frac{12}{7} g (\sin \theta + 1)$$

$$\omega_{\text{net}} = \sqrt{\frac{12g}{7l} (\sin \theta + 1)}$$

$$= \sqrt{\frac{8g}{7} (\sin \theta + 1)}$$

Problem 3)

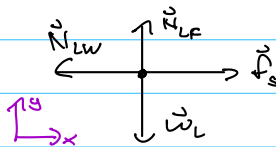
gravity



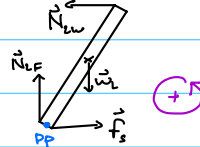
Given

- Ladder with length L , mass M
- Ladder @ rest \leftarrow statics
- Given angle θ with wall
- No friction with wall
- Friction with floor

a) FBD Ladder



x FBD Ladder



4 forces total

b) NZL y-dir

$$F_y = m a_y$$

$$N_{LF} - W_L = 0$$

$$\textcircled{1} W_L = M g$$

$$\textcircled{2} N_{LF} = M g$$

NZL x-dir

$$F_x = m a_x$$

$$f_s - N_{LW} = 0$$

Stop!

NZL Rot

$$\tau_{Net} = I \alpha$$

$$\tau_{N_L} + \tau_{f_s} + \tau_W + \tau_{N_W} = 0$$

$$0 + 0 - \frac{1}{2} W_L \sin \theta + L N_{LW} \sin(90 - \theta) = 0$$

$$N_{LW} \cos \theta - \frac{1}{2} M g \sin \theta = 0$$

$$N_{LW} \cos \theta = \frac{1}{2} M g \sin \theta$$

$$\therefore N_{LW} = \frac{1}{2} M g \tan \theta \quad \textcircled{3}$$

$$\begin{cases} f_s - N_{LW} = 0 \end{cases} \rightarrow f_s = N_{LW}$$

$$\begin{cases} N_{LW} = \frac{1}{2} M g \tan \theta \end{cases} \therefore f_s = \frac{1}{2} M g \tan \theta \quad \textcircled{4}$$

c) Given μ_s and μ_k for static and kinetic friction, respectively

Constraint $f_s \leq \mu_s N_{LF}$ Plug $\textcircled{2}$ and $\textcircled{4}$ from (b)

$$\frac{1}{2} M g \tan \theta \leq \mu_s (M g)$$

$$\mu_s \geq \frac{1}{2} \tan \theta$$

$$\therefore \theta \leq \arctan(2\mu_s)$$