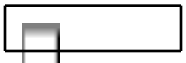




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Case Studies in Process Design II

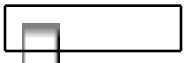
Clemens Isert, Selina Schlotterbeck, Tobias Seidler, Mithurshan Tharmalingam, Pauline Oeuvray





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Reactor flow sheet

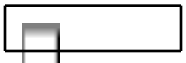


General Modelling Approach

- Four cases considered:

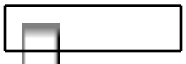
	Case 1	Case 2	Case 3	Case 4
Gas model	ideal gas law	ideal gas law	Peng-Robinson-EOS	Peng-Robinson-EOS
Heating mode	cross-current	cross-current	cross-current	co-current
Absorbers	shortcut model	shortcut model	non-ideal Eq.-model	non-ideal Eq.-model
Distillation	Fenske-Underwood-Gilliland	Fenske-Underwood-Gilliland	NRTL	NRTL
ΔP considered	no	yes	yes	yes

- Overall optimization with a “black box” approach



ODE-system governing the reactor

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Assumptions for Ammonia Absorber

General

- Isothermal column
- Instantaneous & irreversible reaction
- Heat of absorption neglected
- Outlet temperature for liquid and gas alike
- No HCN absorption in water
- No pressure drop
- 20 % excess of sulfuric acid

Ideal case

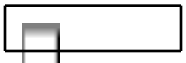
- Heat capacities are T independent

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Non ideal case

- Heat capacities are T dependent

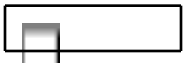
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Sensitivity Analysis of the Ammonia Absorber

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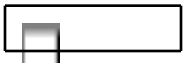
Made assumptions for the HCN absorber

Ideal case

- Isothermal column
- Heat of absorption neglected
- Outlet temperature same for gas and liquid
- Only HCN is absorbed
- Heat capacities not temperature dependent
- No HCN in liquid inlet stream
- Resistivity in the liquid phase neglected

Non-ideal case

- Isothermal column
- Heat of absorption neglected
- Outlet temperature same for gas and liquid
- Only HCN is absorbed



Sensitivity analysis of the HCN Absorber



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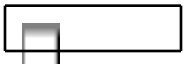
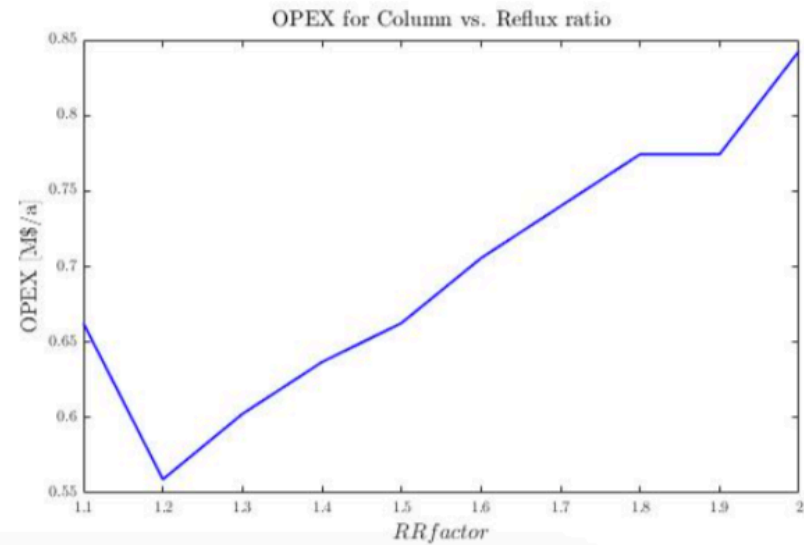
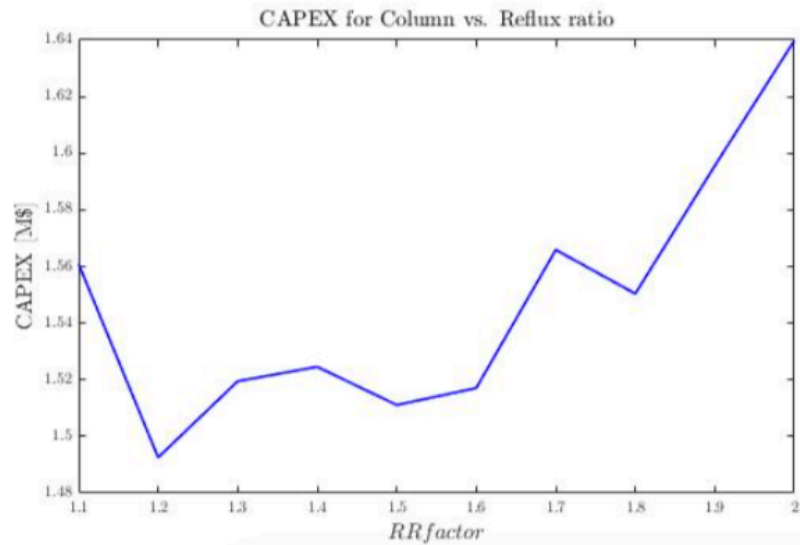
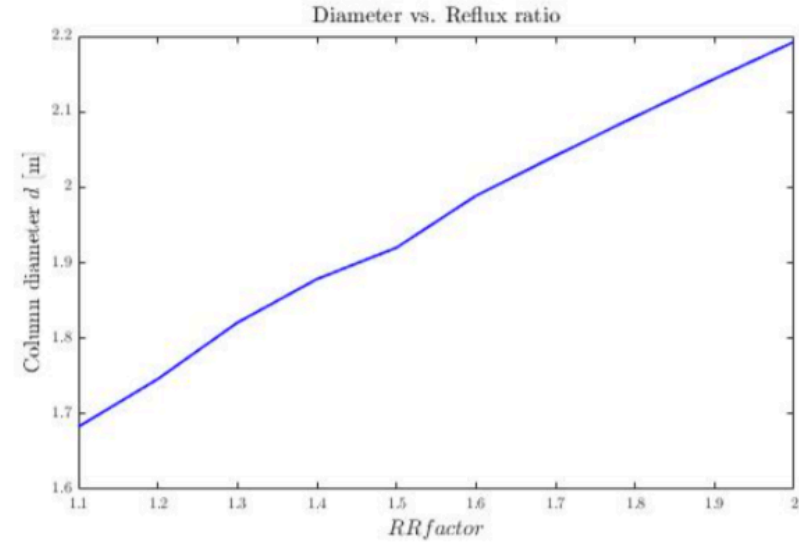
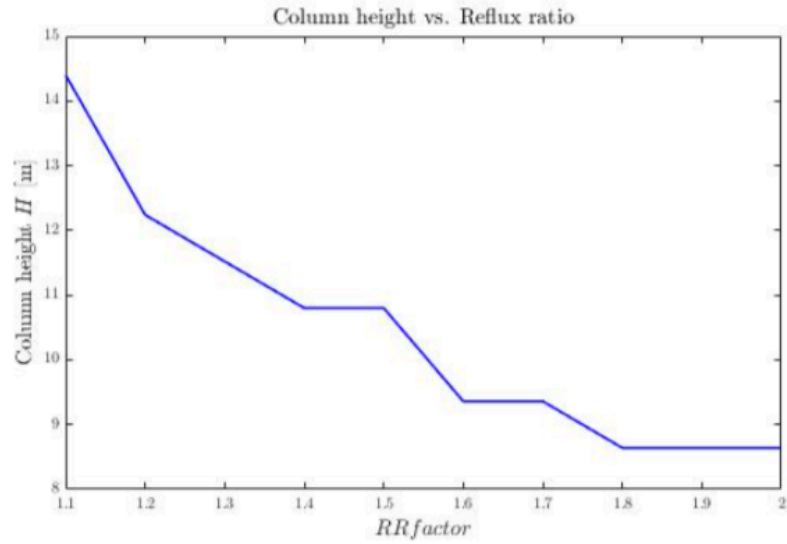
- Height of the column increases with decreasing inlet liquid flow
- Better absorption
- CAPEX decreases
- OPEX increases



HCN Distillation

- Ideal or non-ideal (NRTL for liquid phase)
- No ΔP / ΔP
- Fenske-Underwood-Gilliland method (justified since relative volatilities were pretty similar)
- $x_{HCN}^D = 0.995, x_{HCN}^B = 10 \text{ ppm}$ (going below these limits only makes the separation more difficult \rightarrow higher CAPEX/OPEX)
- total condenser, $q = 1$ (requires another heat exchanger before the distillation column)

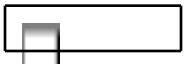
HCN Distillation



Results

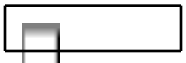
Reactor:

- Ideal vs. real (case 1/case 3)
 - Length: 12 m / 28 m
 - Number of tubes: 1'342 / 17'149
- Cross- vs. co-current (case 3/case 4)
 - Number of tubes: 17'149 / 40'642
 - Heating medium flow: 0.10 / 0.05
 - Conversion CH_4 : 0.82 / 0.59



Reactor profile case 3

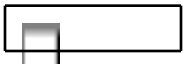
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Results

NH₃ absorber:

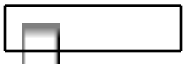
- Ideal vs. real (case 1/case 3)
 - Column height: 2.44 m / 4.39 m
 - Diameter: 0.79 m / 0.79 m
 - Flow rate ratio 0.80 / 1.64
 - Temperature in the column
 - Volumetric fraction H₂SO₄ : 0.37 / 2.01



Results

HCN absorber:

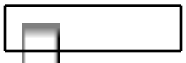
- Ideal vs. real (case 1/case 3)
 - Column height: 9.73 m / 10.31 m
 - Diameter: 1.11 m / 1.10 m
 - Outlet temperature: 294.72 K / 293.57 K
 - Water



Results

HCN distillation:

- Ideal vs. real (case 1/case 3)
 - Column height: 9.36 m / 10.08 m
 - Diameter: 1.73 m / 1.92 m
 - Heat exchanger area: 0.057 m² / 0.056 m²



Results

Costs

- Ideal vs. real (case 1/case 3)
 - Break-even price: 0.62 \$/kg / 0.76 \$/kg



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Thank you for your attention

