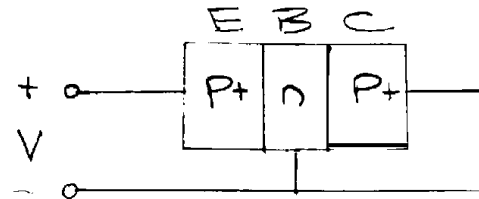


- Now we have I_E , I_C , and I_B in terms of materials parameters: W_b , ΔP_E and ΔP_C
 $\hookrightarrow D_p(\mu_p)$ and $L_p(T_p)$
- ΔP_E , ΔP_C relate to V_{BE} , V_{CB}
 so can get performance (α , β , δ) from I 's under different biasing.
- I_E , I_C , I_B equations are general
 - all biasing conditions *

Example



(hole current
since PNP)

$$V_{BC} = 0$$

$$\Delta P_C = 0$$

$$I_E = q \frac{AD_p}{L_p} \Delta P_E \coth\left(\frac{W_b}{L_p}\right)$$

$$I_C = q \frac{AD_p}{L_p} \Delta P_E \operatorname{csch}\left(\frac{W_b}{L_p}\right)$$

$$I_B = q \frac{AD_p}{L_p} \Delta P_E \tanh\left(\frac{W_b}{2L_p}\right)$$

Get ΔP_E from V

Or If V_{BE} shorted, then $\Delta P_E = 0$
etc.

For a *pnp* device with $I_{Ep} = 1 \text{ mA}$, $I_{En} = 0.01 \text{ mA}$, $I_{Cp} = 0.98 \text{ mA}$, and $I_{Cn} = 0.1 \text{ }\mu\text{A}$, calculate

- (a) Base transport factor \mathcal{B}
- (b) Emitter injection efficiency γ
- (c) α_{dc} and β_{dc} ; the value of I_B
- (e) If $I_{Cp} = 0.99 \text{ mA}$, calculate β_{dc} and I_B .
- (f) If $I_{Cp} = 0.99 \text{ mA}$ and $I_{En} = 0.005 \text{ mA}$, calculate β_{dc} and I_B .
- (g) How will β_{dc} change if I_{En} is increased?

Example

$$I_{Ep} = 1 \text{ mA} , \quad I_{En} = 0.01 \text{ mA} .$$

$$I_{Cp} = 0.98 \text{ mA} . \quad I_{Cn} = 0.1 \text{ }\mu\text{A}$$

(a) $\mathcal{B} = I_{Cp} / I_{Ep} =$

(b) $\gamma = \frac{I_{Ep}}{I_{En} + I_{Ep}} =$

(c)

$$\alpha_{dc} = \boxed{} = \boxed{}$$

$$\beta_{dc} = \boxed{} = \boxed{}$$

$$I_B = I_E - I_C = (\boxed{}) - (\boxed{}) \\ = \boxed{} \mu A$$

(e) $I_{Cp} = 0.99 \text{ mA}$

$$\beta = I_{Cp} / I_{Ep} = 0.99, \quad \alpha_{dc} = 0.9802$$

$$\beta_{dc} = \boxed{}$$

$$I_B = \boxed{}$$

(f) $I_{Cp} = 0.99 \text{ mA}, \quad I_{En} = 0.005 \text{ mA}$

$$\beta_{dc} = \boxed{}, \quad I_B = \boxed{}$$

(g) $I_{En} \uparrow \rightarrow P \downarrow \quad \therefore \alpha_{dc} \downarrow \rightarrow \beta_{dc} \downarrow \Rightarrow I_B \uparrow$

Approximations of the Terminal Currents

Can simplify general equations for I_E , I_C , and I_B for normal transistor biasing

Thus, for collector reverse-biased, $\Delta P_C = -P_n$
and for small P_n , can neglect ΔP_C .

For $\gamma = 1$ (very efficient emitter injection),

$$I_E = I_{EP} \approx qA \frac{D_p}{L_p} \Delta P_E \coth h \frac{w_b}{L_p}$$

$$I_C = qA \frac{D_p}{L_p} \Delta P_E \operatorname{csch} \frac{w_b}{L_p}$$

$$I_B \approx qA \frac{D_p}{L_p} \Delta P_E \tanh \frac{w_b}{2L_p}$$

For small values of W_b/L_p , can expand Hyperbolic trig. functions and keep only lowest order:

$$\text{sech } (y) = 1 - y^2/2 + 5y^4/24 - \dots$$

$$\text{ctnh } (y) = 1/y + y/3 - y^3/45 + \dots$$

$$\text{csch } (y) = 1/y - y/6 + 7y^3/360 - \dots$$

$$\tanh (y) = y - y^3/3 + \dots$$

I_E only slightly larger than I_C .

$$q \frac{A D_E}{L_p} \left[\left(\frac{1}{2} + \frac{y}{3} \right) - \left(\frac{1}{2} - \frac{y}{6} \right) \right] \approx I_E - I_C$$

To lowest order, $\tanh y \approx y$, so

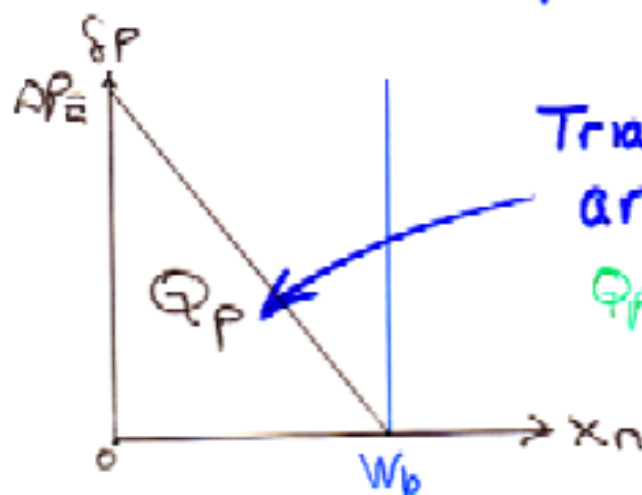
$$I_B \approx q \frac{A D_p}{L_p} \Delta P_E \frac{W_b}{2 L_p}$$

$$= q A \frac{\Delta P_E W_b}{2 \tau_p}$$

since $L_p^2 = D_p \tau_p$



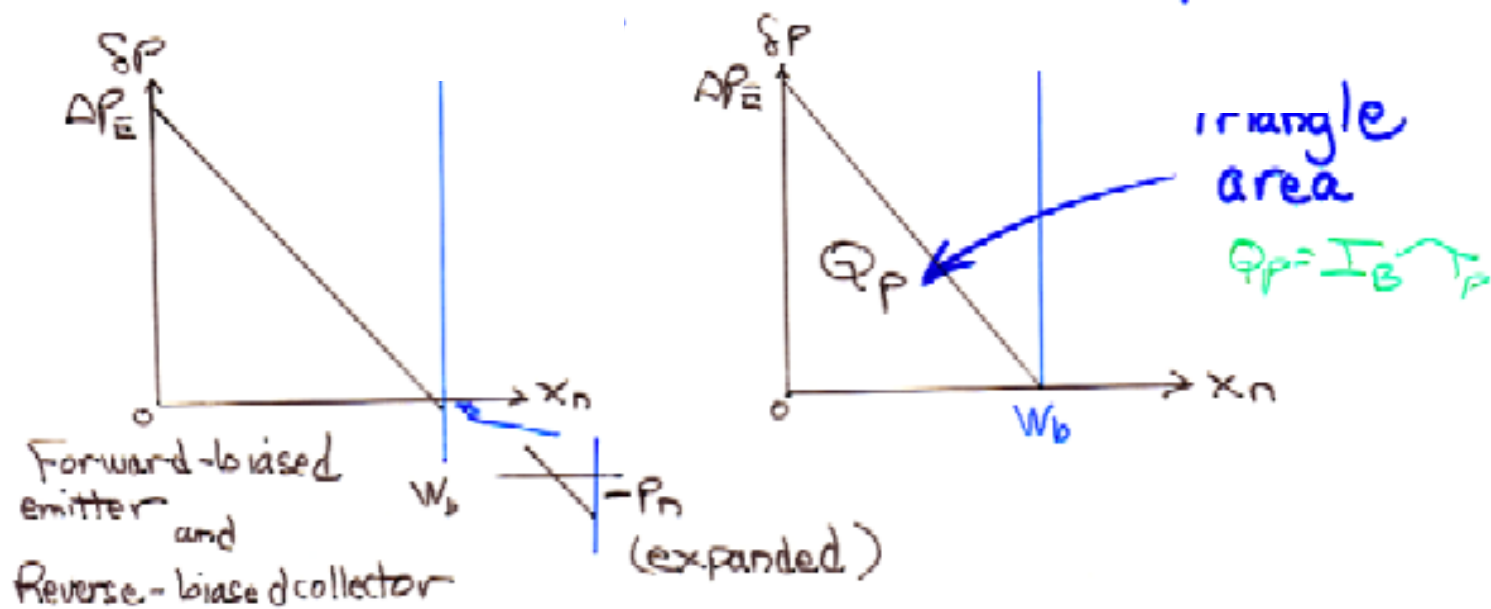
Forward-biased emitter and
Reverse-biased collector



Triangle area

$$Q_p = I_B \tau_p$$

(expanded)



Triangle area = charge in base = $\frac{\Delta P_E W_b}{2}$
 (assuming nearly straight line)

$$Q_P \equiv \frac{\Delta P_E W_b}{2} \cdot q A$$

Current = charge replaced per second

$$= q A \frac{\Delta P_E W_b}{2 \tau_F}$$

Charge Control Approximation

Comments

- Just an approximation : slope must differ between E and C. Otherwise,

$$I_B = 0$$

But for normal biasing, see basic relationships:

- $\frac{I_C}{I_B}$ = gain increases as I_B decreases.

$$\frac{I_C}{I_B} \sim \frac{\operatorname{csch} \frac{W_b}{L_p}}{\tanh \frac{W_b}{2L_p}} \approx \frac{\frac{1}{\gamma}}{\gamma/2} = \frac{1}{\gamma^2/2} = \frac{2L_p^2}{W_b^2}$$

as W_b gets smaller ("narrow base"), gain increases.

$$\frac{I_C}{I_B} \sim \frac{\cosh \frac{W_b}{L_p}}{\tanh \frac{W_b}{2L_p}} \approx \frac{\frac{1}{\gamma}}{\frac{\gamma}{2}} = \frac{1}{\gamma^2/2} = \frac{2L_p^2}{W_b^2}$$

as W_b gets smaller ("narrow base"), gain increases.

$$I_B = g_A \frac{D_E W_b}{2 \tau_p}$$

as τ_p gets larger, I_B decreases, gain
 can increase τ_p by light doping in base.
 (improves emitter efficiency too)

But tradeoff: longer $\tau_p \rightarrow$ lower bandwidth and frequency response

Current Transfer Ratio

▷ Emitter Injection Efficiency

can write in terms of emitter and base properties:

$$\gamma = \frac{I_{EP}}{I_{EP} + I_{EN}}$$

$$= \left[1 + \frac{L_p^n n_n \mu_n^p}{L_n^p p_p \mu_p^n} \tanh \frac{W_b}{L_p^n} \right]^{-1}$$

$$\approx \left[1 + \frac{W_b n_n \mu_n^p}{L_n^p p_p \mu_p^n} \right]^{-1}$$

Homework
problem:

$$\frac{I_{EP}}{I_{EP} + I_{EN}} = \left[1 + \frac{I_{EN}}{I_{EP}} \right]^{-1}$$

Make γ large: ~ 1

For p-n-p transistor, make $p_p \square n_n$
and $L_n^p \square W_b$

Base Transport Factor

$$\beta = \frac{I_c}{I_{Ep}} = \frac{\cosh W_b/L_p}{\tanh W_b/L_p} = \operatorname{sech} \frac{W_b}{L_p}$$

for $\frac{W_b}{L_p}$ small, $\operatorname{sech} \frac{W_b}{L_p} \sim 1$

Current Transfer Ratio

$$\alpha = \beta \gamma \quad \text{efficiency} \times \text{transfer ratio}$$

Plug in for β and γ from above expressions

$$\begin{aligned} \alpha = \beta \gamma &= \operatorname{sech} \frac{W_b}{L_p} \cdot \left[1 + \frac{L_p^n n_n \mu_n^p}{L_n^p p_p \mu_p^n} \tanh \frac{W_b}{L_p} \right]^{-1} \\ &= \left[\cosh \frac{W_b}{L_p} + \frac{L_p^n n_n \mu_n^p}{L_n^p p_p \mu_p^n} \sinh \frac{W_b}{L_p} \right]^{-1} \end{aligned}$$

Example

p-n-p transistor

$$p_p = 10 n_n \quad \mu_n^p = \frac{1}{2} \mu_p^n \quad W_b = \frac{1}{10} L_p^n$$

carrier lifetimes $\tau_n = \tau_p$

Calculate α and β

$$L = \sqrt{D\tau}; \quad \frac{D}{\mu} = \frac{kT}{q}; \quad L = \sqrt{\mu kT \tau / q}$$

$$L_p^n / L_n^p = \sqrt{\mu_p^n / \mu_n^p} \quad \text{for equal lifetimes}$$

$$\alpha = [\cosh 0.1 + \sqrt{2} (0.1)(0.5) \sinh 0.1]^{-1}$$
$$= [1.005 + 0.0707 (0.1)]^{-1} = \boxed{}$$

$$\text{and } \beta = \frac{\alpha}{1-\alpha} = \boxed{}$$

Heterojunction Bipolar Transistors

Useful to improve device properties

Want high emitter efficiency $\gamma \rightarrow$ high α and β

$$\gamma \approx \left[1 + \frac{W_b}{L_p} \frac{n_n}{p_p} \frac{\mu_n^p}{\mu_p^n} \right]^{-1} \quad \text{for p-n-p}$$

so keep



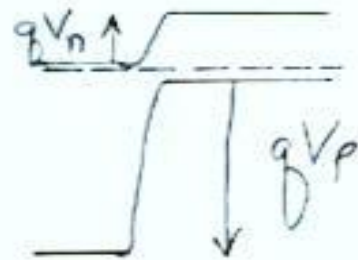
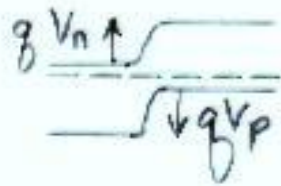
But also want low base resistance (lower voltage drop)
→ keep

And want low emitter junction capacitance (higher ω)
→ keep ($C \propto N^{1/2}$)

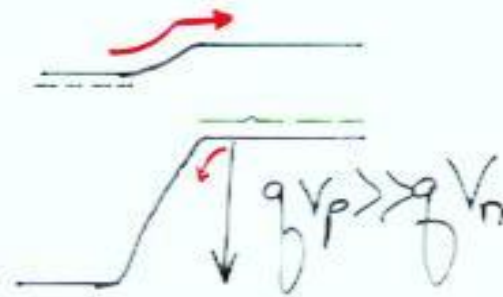
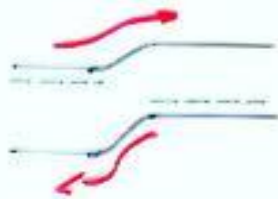
Need new mechanism to control relative injection across emitter junction

Solution:
→

Heterojunction Barrier Differences



Much bigger
hole barrier
so electron emitter
 α is high.



Exponential
Effect. So even
small ΔE_g has
huge effect.

Homojunction

Heterojunction

So could now choose heavily doped base & lightly doped emitter.

Example shows that:

Amplification depends on

- doping (P_p, n_n)
 - base width (W_b)
 - diffusion lengths (L_p^n, L_n^p)
 - mobility (μ_n^p, μ_p^n)
 - lifetime (τ_n, τ_p)
- Fundamental physical parameters
and design parameters