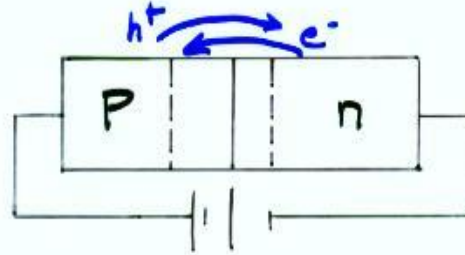
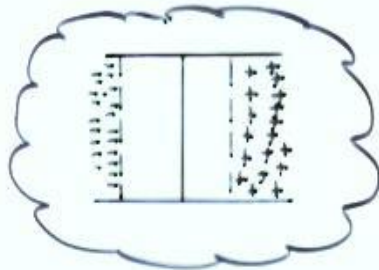


Excess  $h^+$   
injected into  
n-side.



Excess  $e^-$  injected  
into p-side!

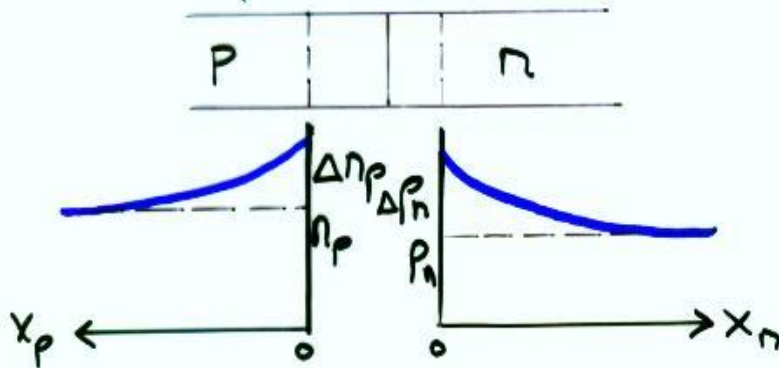


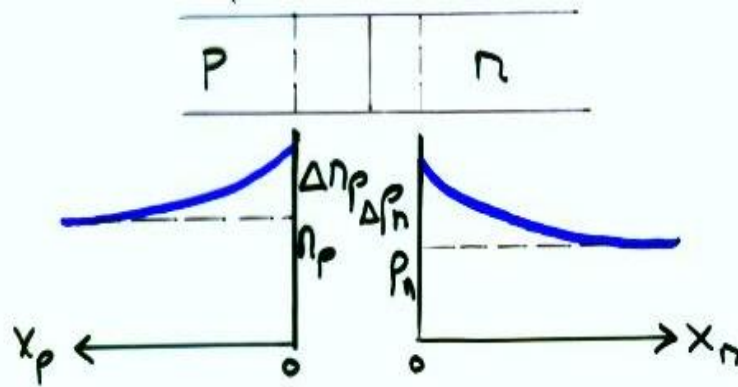
$$\Delta p_n = p_n (e^{qV/kT} - 1); \quad p_n =$$

$$\Delta n_p = n_p (e^{qV/kT} - 1); \quad n_p =$$

at the boundary only!

Plus diffusion / recombination:





To simplify solution of differential equation,  
new x-axis origins (neat trick)

Get exponential as in Lecture 17, page 1

$$\delta_n(x_p) = \boxed{\phantom{0}} = \boxed{\phantom{0}}$$

Since on p-side, use  $x_p$ . Since electrons diffusing, use  $L_n$ .

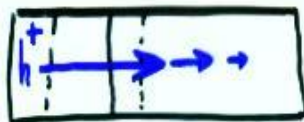
Likewise

$$\delta_p(x_n) = \boxed{\phantom{0}} = \boxed{\phantom{0}}$$

where  $L_p$  = minority carrier diffusion length <sup>(h<sup>+</sup> on n-side)</sup>  
 $L_n$  = " " " " <sup>e<sup>-</sup> on p-side</sup>

Again, this a big deal since now you know where all the charged particles are and

Can get currents at any point.



Varies due to recombination

$$I_p(x_n) = J_p(x_n) \cdot \underset{\text{area}}{A} = -qAD_p \frac{d\delta p(x_n)}{dx_n}$$

Diffusion current for holes

$$= +qA \frac{D_p}{L_p} \Delta p_n e^{-x_n/L_p}$$

See, e.g., S&B Eq. 5-32

$$= qA \frac{D_p}{L_p} (e^{qV/kT} - 1) e^{-x_n/L_p}$$

$$= +qA \frac{D_p}{L_p} \Delta p_n e^{-x_n/L_p} = qA \frac{D_p}{L_p} (e^{qV/kT} - 1) e^{-x_n/L_p}$$

Likewise,  $I_n(x_p) = -qA \frac{D_n}{L_n} (e^{qV/kT} - 1) e^{-x_p/L_n}$

Diffusion current  
for electrons

{extra minus sign since  
 $x_p$  opposite to  $x$ -direction}

Add to get total current.

(assume  $\Delta p(x_p=0) = \Delta p(x_n=0)$  and  
 $\Delta n(x_n=0) = \Delta n(x_p=0)$ )

No recombination in transition region.

$$I = I_p(x_n=0) - I_n(x_p=0)$$

passing through transition region

$$= qA \frac{D_p}{L_p} \Delta p_n + qA \frac{D_n}{L_n} \Delta n_p$$

{relative to the  $x_n = x$   
direction }

$$\boxed{I = qA \left( \frac{D_p}{L_p} p_n + \frac{D_n}{L_n} n_p \right) (e^{qV/kT} - 1)}$$

$$= I_0 (e^{qV/kT} - 1)$$

Diode Equation!

(Ideal Case)



Since all current is in the same direction and everything is in series, total current must be constant throughout the device.

(Individual  $h^+$  and  $e^-$  currents can vary but add up to a constant)

Now check out reverse bias:  $V \rightarrow -V$

$(e^{qV/kT} - 1) \rightarrow -1$  for  $V \rightarrow -V$  large

$$I_R = -I_0 = -qA \left( \frac{D_p}{L_p} p_n + \frac{D_n}{L_n} n_p \right)$$

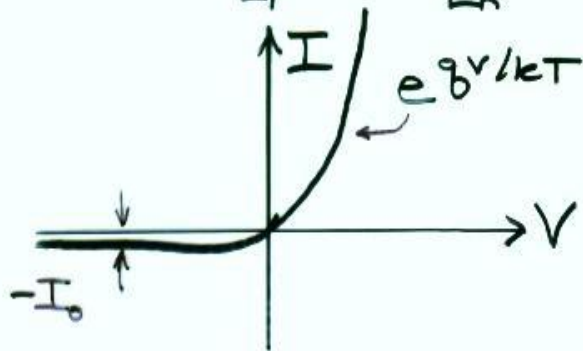
Reverse bias current

## Forward Bias Current


$$I_F \approx I_0 e^{qV/kT}$$

$$\approx \left( \frac{D_p}{L_p} p_n + \frac{D_n}{L_n} n_p \right) e^{qV/kT}$$

for  $V$  large  
such that  $e^{qV/kT} \gg 1$



*I-V in terms of  
fundamental physical  
parameters*

This shows the rectifier character we know  
and love. 

Can also calculate total current another way: Total stored charge  $Q_n$  divided by  $\tau_n$   
 $+ \quad " \quad " \quad " \quad " \quad Q_p \quad " \quad " \quad \tau_p$

"Charge Control Approximation"

$$Q_p = qA \int_0^{\infty} \delta p(x_n) dx_n \quad \text{and} \quad I_p = \frac{Q_p}{\tau_p} = qA \frac{L_p}{\tau_p} \Delta p_n$$



## Diode Equation for Asymmetric Junctions

(Very Common)

Injection from more heavily doped side dominates total current



$$|p| \neq |n|$$

Equilibrium

$$|p| \gg |n|$$

p+ side

$$p_p = N_a$$

$$n_p = \frac{n_i^2}{N_a}$$

n-side

$$n_n = N_d$$

$$p_n = \frac{n_i^2}{N_d}$$

$N_a \gg N_d$  so  $p_n \gg n_p$ . So  $h^+$  injection dominates.

$$I = qA \left[ \frac{D_p}{L_p} p_n + \frac{D_n}{L_n} n_p \right] (e^{qV/kT} - 1)$$

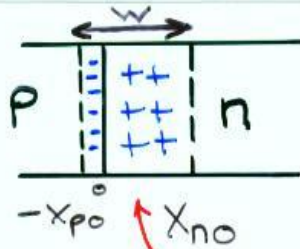
$$\approx qA \frac{D_p}{L_p} p_n (e^{qV/kT} - 1)$$

Example:  $N_d = 10^{16} \text{ cm}^{-3}$ ,  $N_a = 10^{18} \text{ cm}^{-3}$ .  $L_p \sim L_n$ ,  $D_p \sim D_n$ ,  
so  $p_n = 100 n_p$ . Only 1% correction.

Hole and electron distributions for asymmetric junction:

Different equilibrium minority concentrations  
" forward bias distributions  
" reverse bias "  
" widths

p-n  
junction

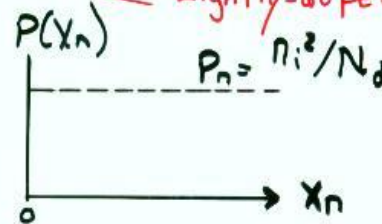
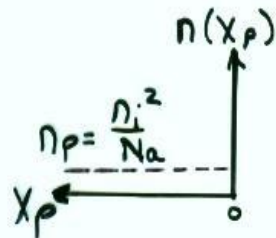


$$x_{p0} N_a = x_{n0} N_d$$

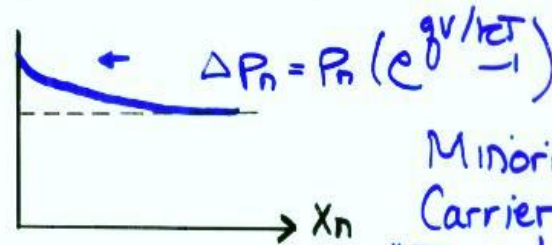
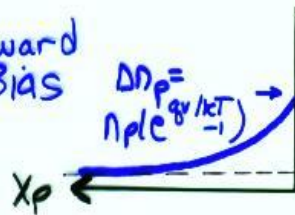
$$x_{p0} / x_{n0} = N_d / N_a \ll 1$$

Lightly-doped side is wider.

Zero  
Bias

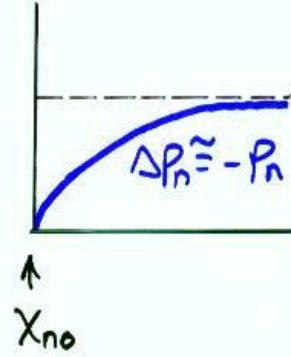
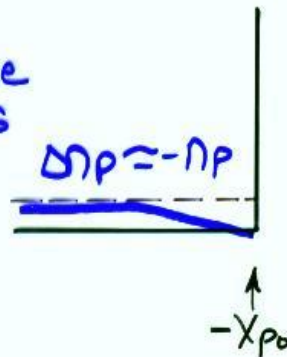


Forward  
Bias



Minority  
Carrier  
"Injection"

Reverse  
Bias



Minority  
Carrier  
"Extraction"

Important to understand all this.

Thermal generation supplies carriers to transition region from the bulk.  $\rightarrow$  reverse saturation current.

From within the diffusion length distance of the edge.

# Minority and Majority Carrier Currents

## I. Minority Carriers



A. Outside transition region  $W$

1. Drift Current  $\sim$  negligible,  $n_p(x) + p_n(x)$  low
2. Diffusion Current - depends on gradient

$$q D_p \frac{dp}{dx}, \quad q D_n \frac{dn}{dx} \text{ can be large}$$

even if concentrations are low, as long as the gradients are large.

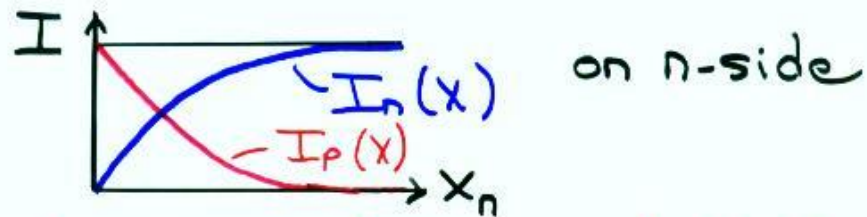


B. Inside transition region  $w$

1. Drift Current  $\sim$  zero, almost all carriers swept out.
2. Diffusion Current = constant (assume no recombination inside  $w$ ).

II. Majority Carriers

Calculate from minority current  
since  $I = I_n + I_p$  in all regions



Minority current outside  $W$

$$I_p(x_n) = q A \frac{D_p}{L_p} \Delta p e^{-x_n/L_p}$$

$$= q A \frac{D_p}{L_p} \left[ p_n (e^{qV/kT} - 1) \right] e^{-x_n/L_p}$$

decreases with  $x_n$  ←

so majority current outside  $W$  is:

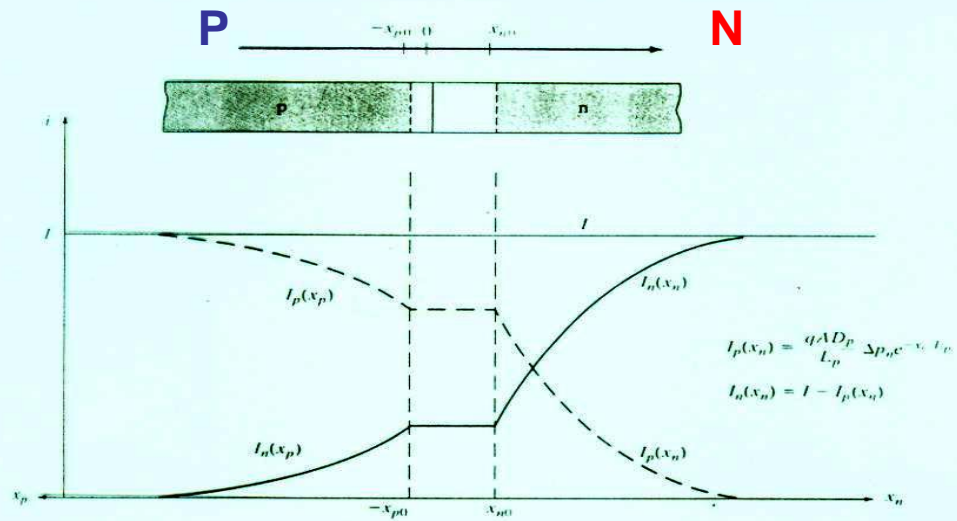
$$I_n(x_n) = I - I_p(x_n)$$

$$= q A \left[ \frac{D_p}{L_p} p_n + \frac{D_n}{L_n} n_p \right] (e^{qV/kT} - 1) - I_p(x_n)$$

$$= q A \left[ \frac{D_p}{L_p} (1 - e^{-x_n/L_p}) p_n + \frac{D_n}{L_n} n_p \right] (e^{qV/kT} - 1)$$

Increases with  $x_n$ . ←

- Electric field in neutral region not strictly zero. But carrier concentration so large that  $E$  can be very small and still feed current to transition region.
- Currents far from transition region supply charges needed for recombination as well as " " " injection.



$N_a$   $N_d$

$L_p$   $L_n$

$N_a$   $N_d$

$D_p$   $D_n$

$\tau_p$   $\tau_n$

