

# **ECE 3020**

# **Introduction to Electronics**

## **Section 5: Diodes**

**Spring 2024**

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**Dept. of Electrical & Computer Engineering**

**The Ohio State University**

# Acknowledgement

- ◆ The instructor would like to acknowledge and thank the following for kindly providing the lecture notes/handouts for this class. Some modifications and/or customizations to the original material is occasionally introduced by the instructor
  - Prof. Nima Ghalichechian
  - Prof. Asimina Kiourti
  - Prof. Ayman Fayed
  - Prof. George Valco



# Topics Covered in this Course

- ◆ Section 1: Basic Concepts
- ◆ Section 2: Operational Amplifiers (Op-Amps)
- ◆ Section 3: Introduction to Feedback
- ◆ Section 4: Filters
- ◆ **Section 5: Diodes and Applications**
- ◆ Section 6: Field Effect Transistors (FETs) and Applications
- ◆ Section 7: Bipolar Junction Transistors (BJTs) and Applications
- ◆ Section 8: Digital and Mixed-Signal Circuits
- ◆ Section 9: Circuit Simulation Software

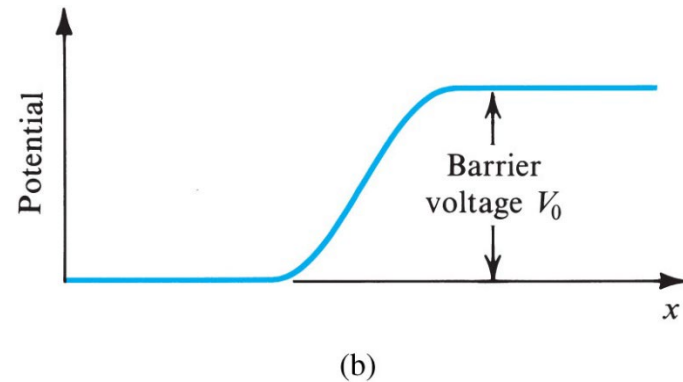
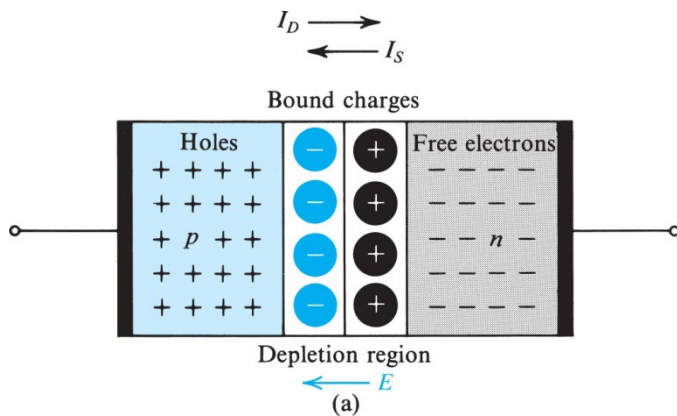
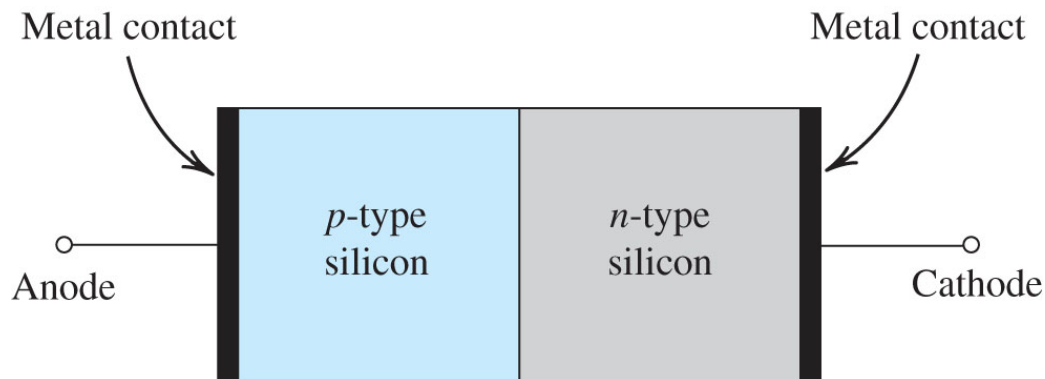


# Reading Assignment

- ◆ Text → pp 175-190 (Diode terminal characteristics and models)
- ◆ Text → pp 190-200 (Diode models)
- ◆ Text → pp 200-207 (Diode application for voltage regulation; Zener diodes)
- ◆ Text → pp 207-213 (Diodes & Rectifier Circuits)

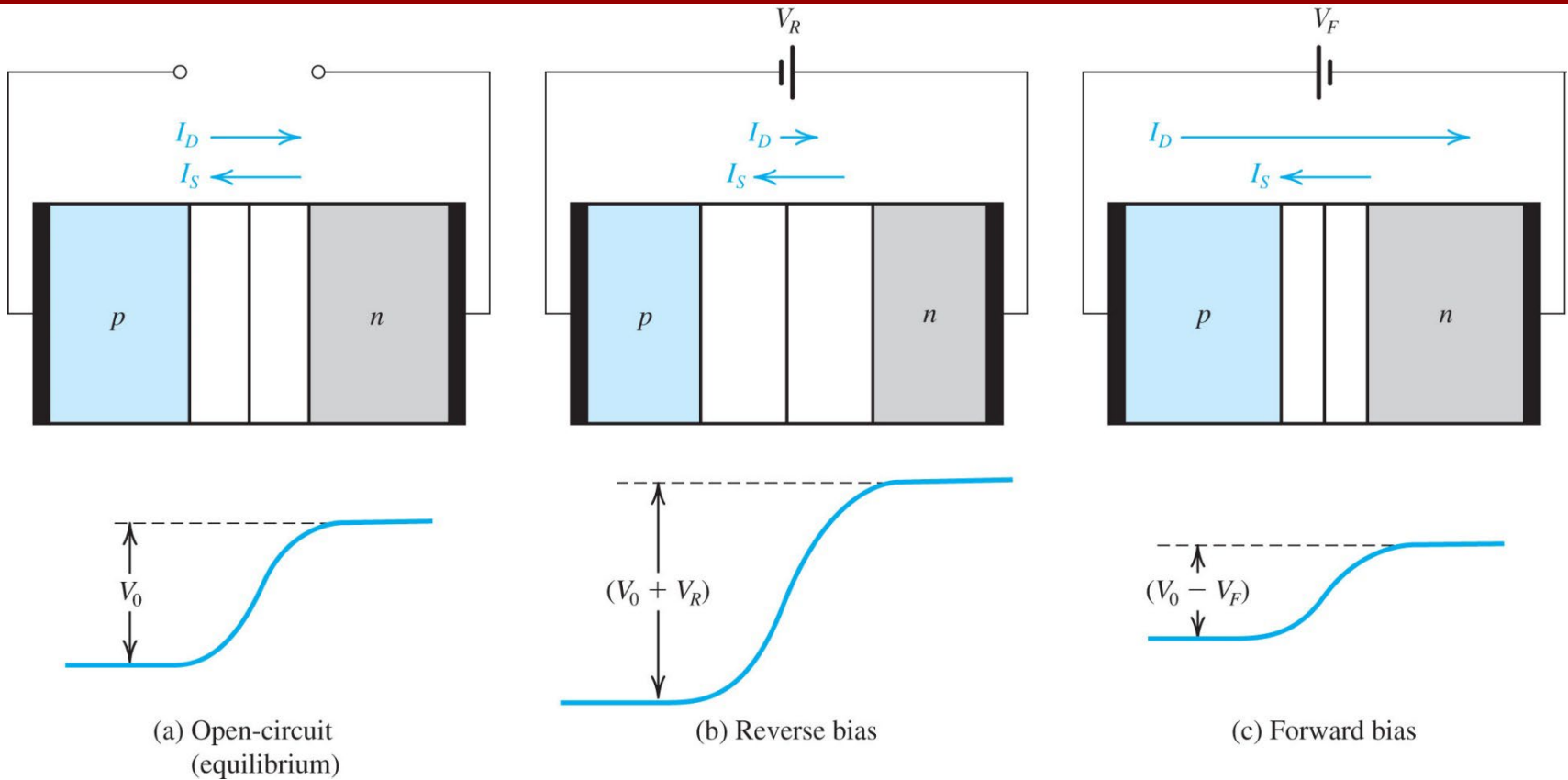


# PN Junction



The *pn* junction with no applied voltage (open-circuited terminals). **(b)** The potential distribution along an axis perpendicular to the junction.

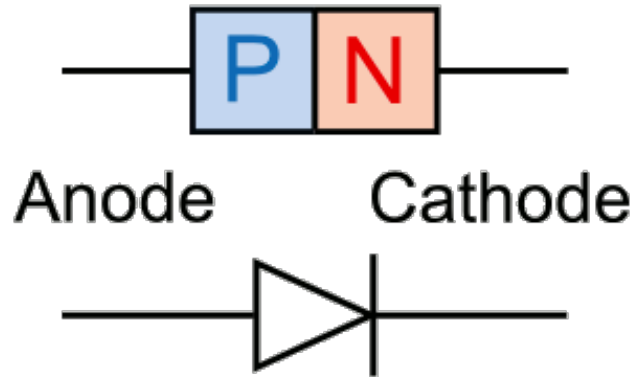
# PN Junction



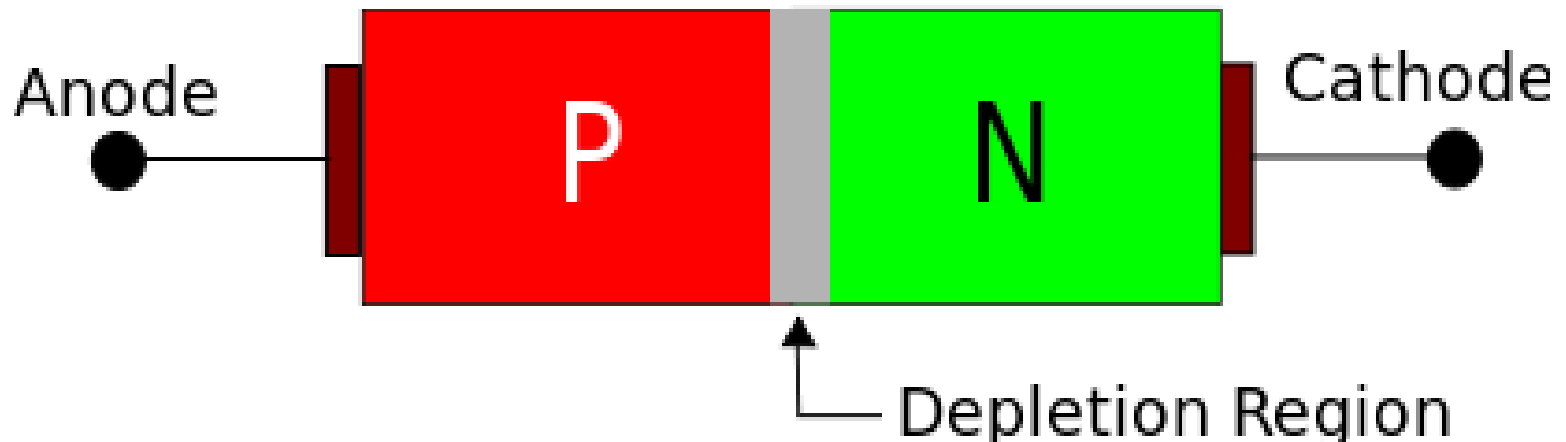
The *pn* junction in: **(a)** equilibrium; **(b)** reverse bias; **(c)** forward bias.



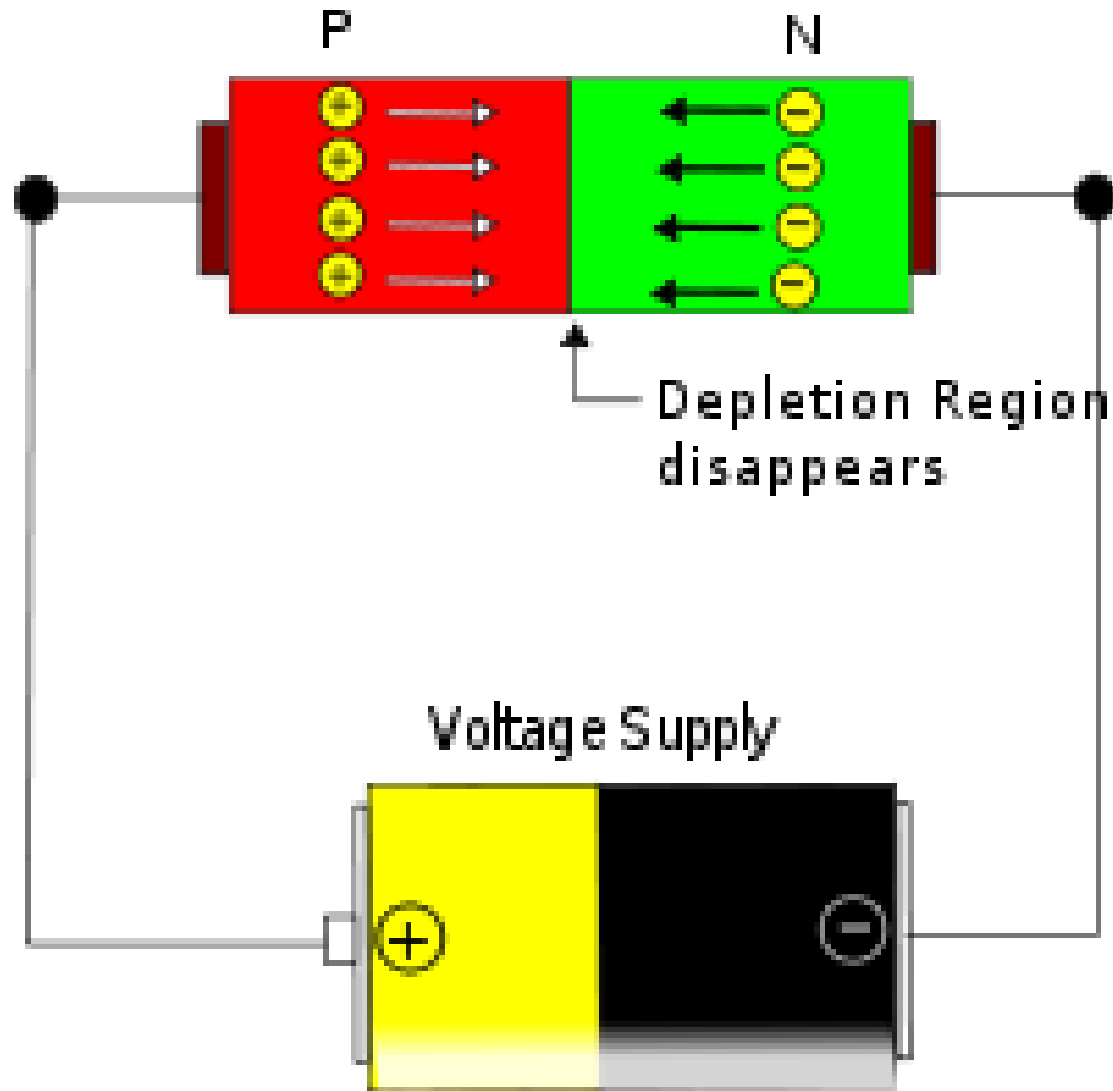
# The Semiconductor Diode



- **Forward-bias operation**
- **Reverse-bias operation**

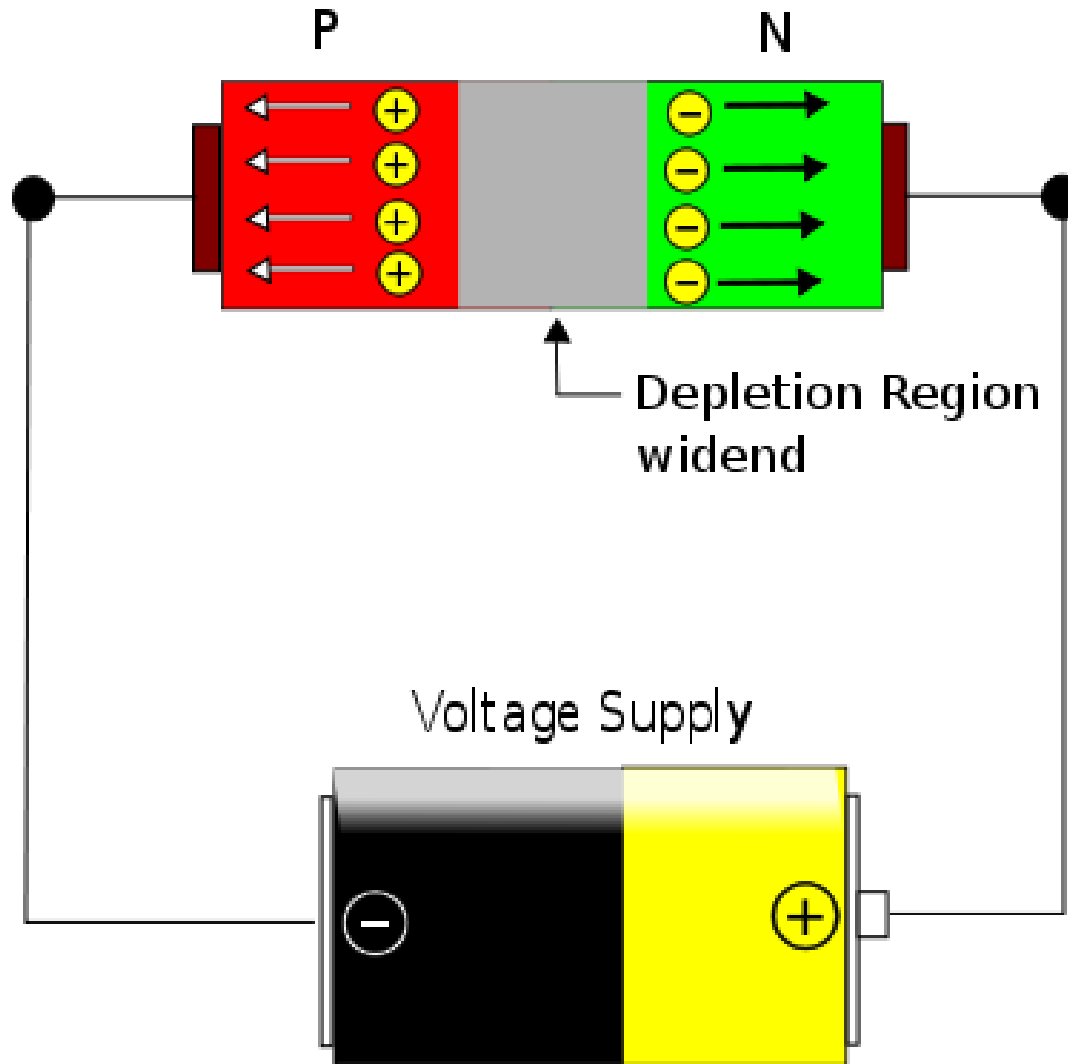


# Forward Bias Operation

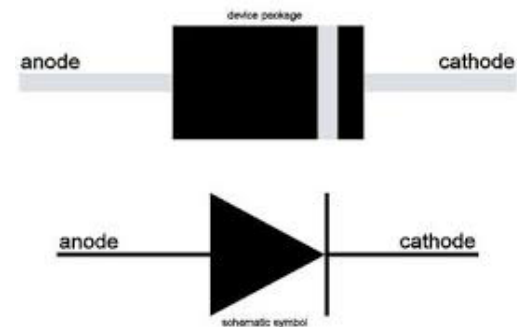
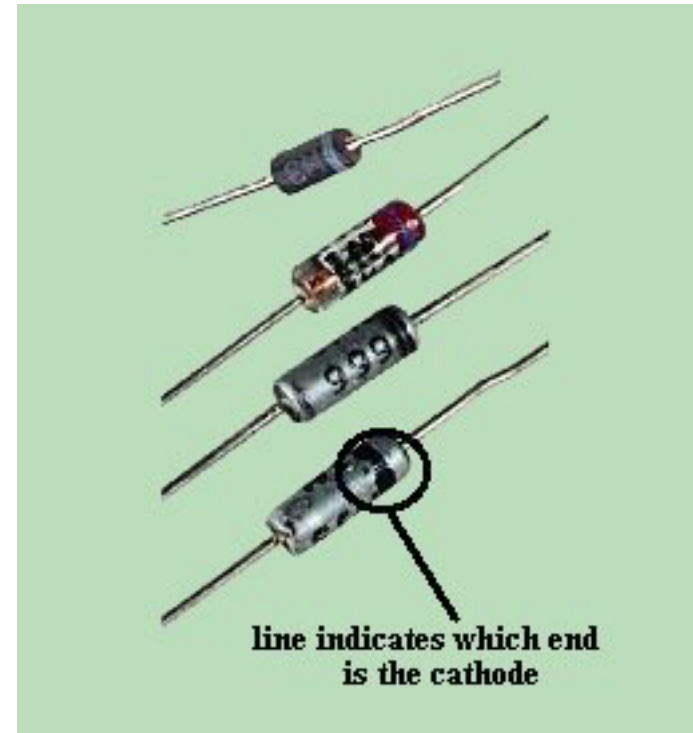
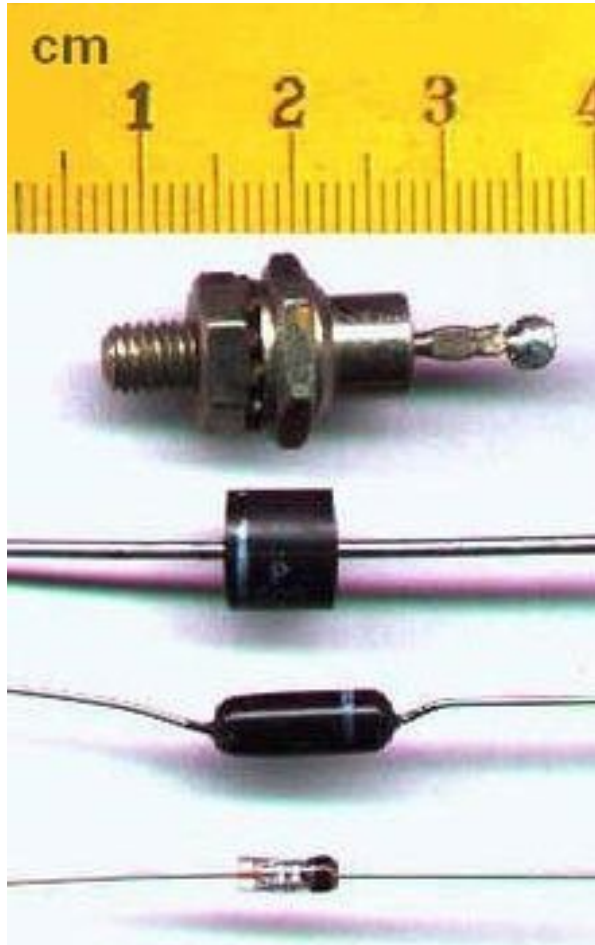




# Reverse Bias Operation



# Example Semiconductor Diodes

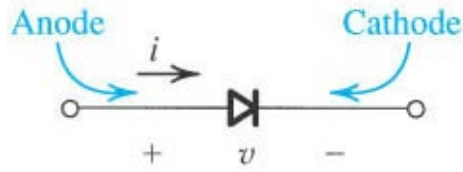


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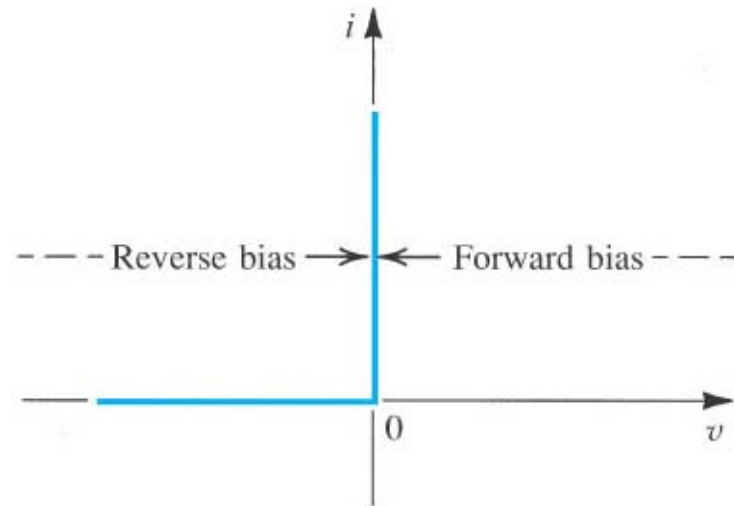
# **THE IDEAL DIODE**



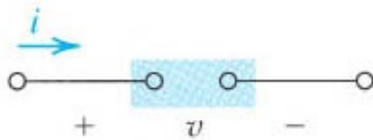
# The Ideal Diode Model



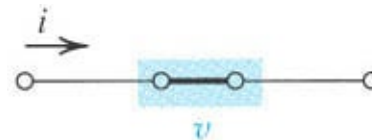
diode circuit symbol



$i$ - $v$  characteristic



equivalent circuit  
reverse bias (ideal)

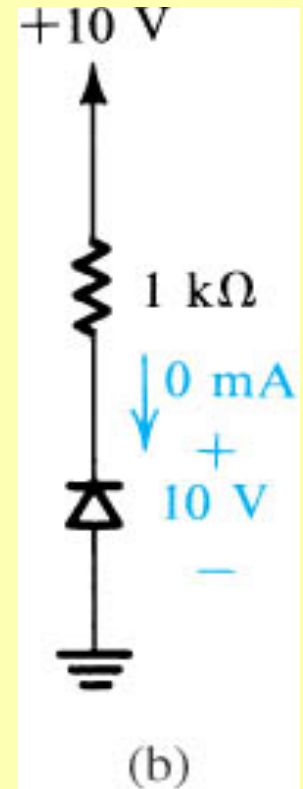
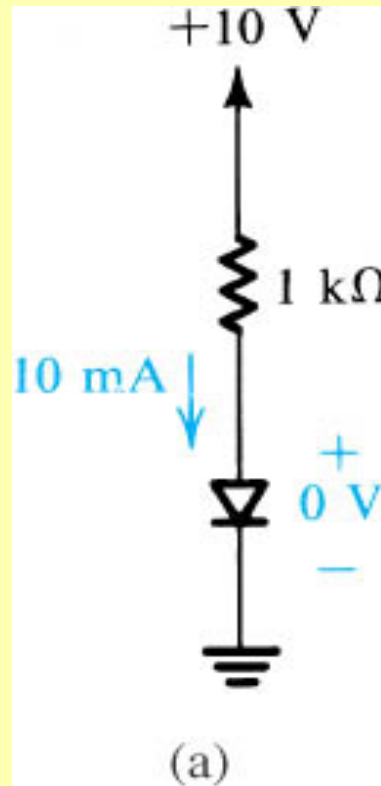


equivalent circuit  
forward bias (ideal)

# Exercise #1: Modes of Operation of Ideal Diodes

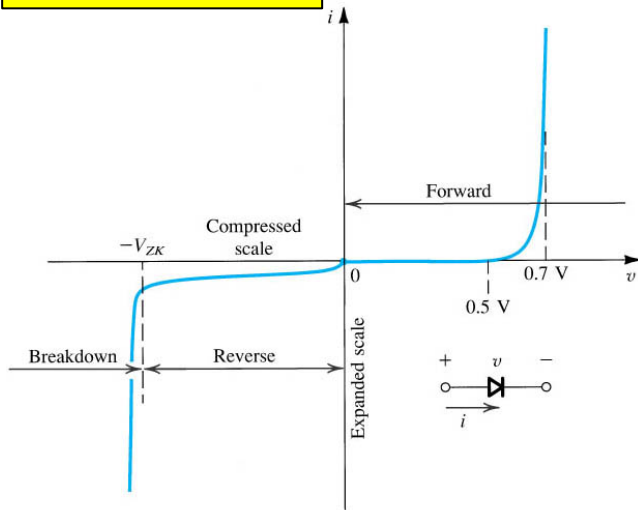
Assuming ideal diodes:

- 1) What is the voltage drop and current flowing through the diode in (a)?
- 2) What is the voltage drop and current flowing through the diode in (b)?

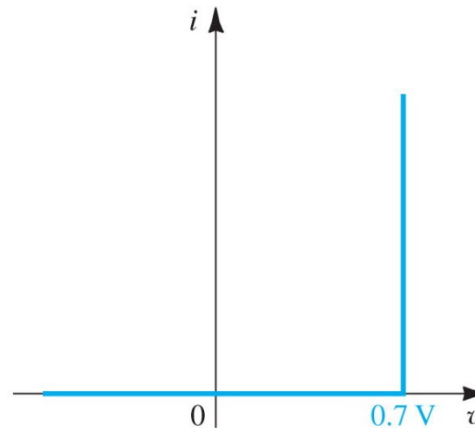


# Diode Models

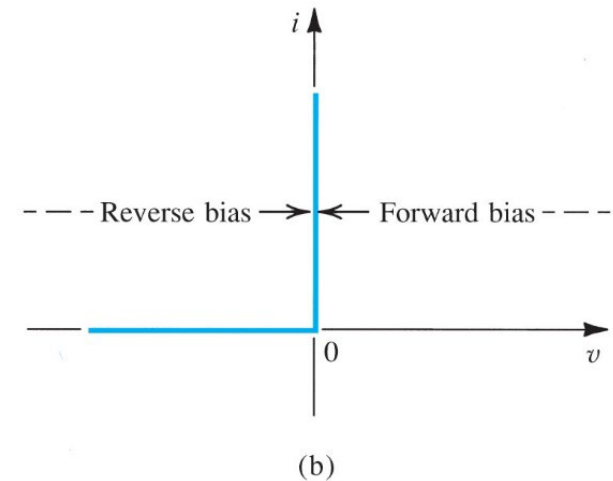
## 1) Real diode



## 2) constant-voltage-drop model



## 3) Ideal diode

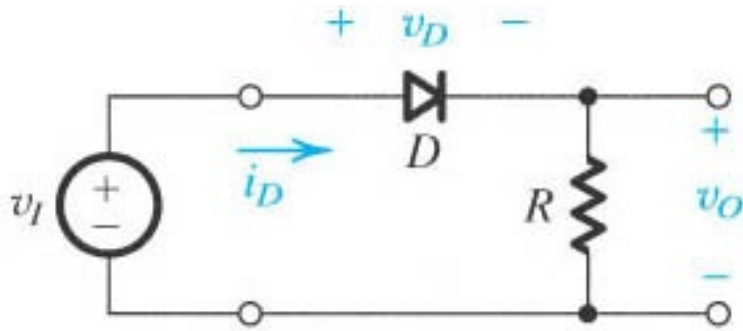


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# A SIMPLE APPLICATION: THE RECTIFIER



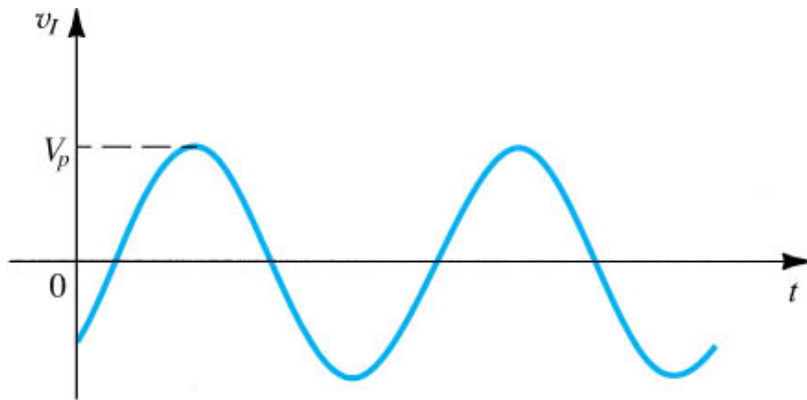
# A Simple Application: The Rectifier



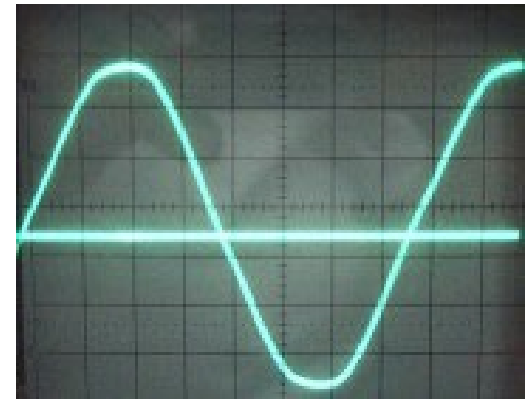
(a) Rectifier circuit

Diode connected in series with load resistor.

Model used for diode depends on sign of input.

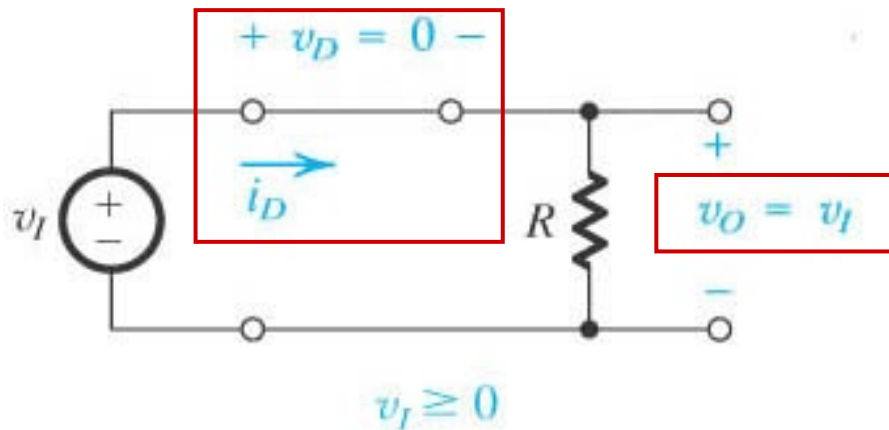


(b) Input waveform

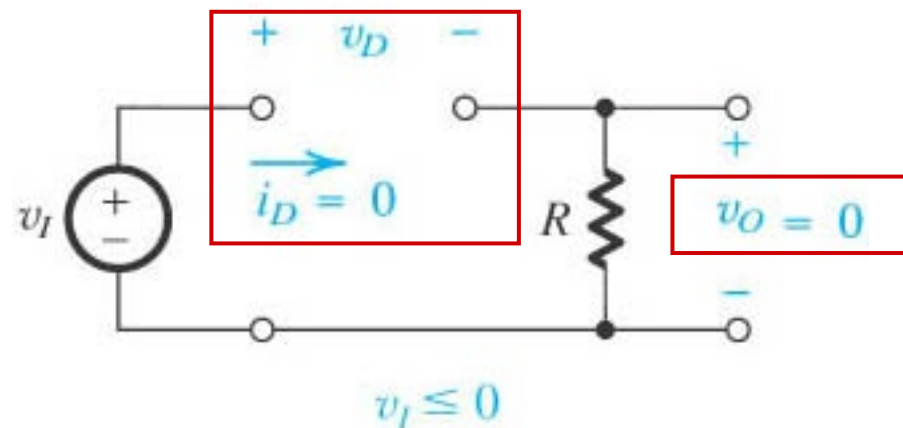




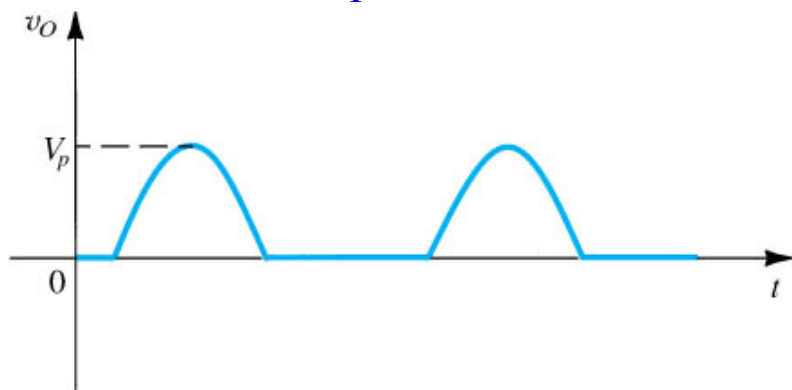
# A Simple Application: The Rectifier



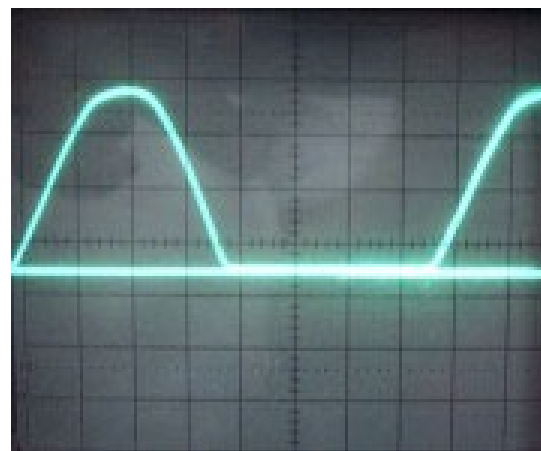
(c) Equivalent circuit when  $v_I \geq 0$ .



(d) Equivalent circuit when  $v_I \leq 0$ .



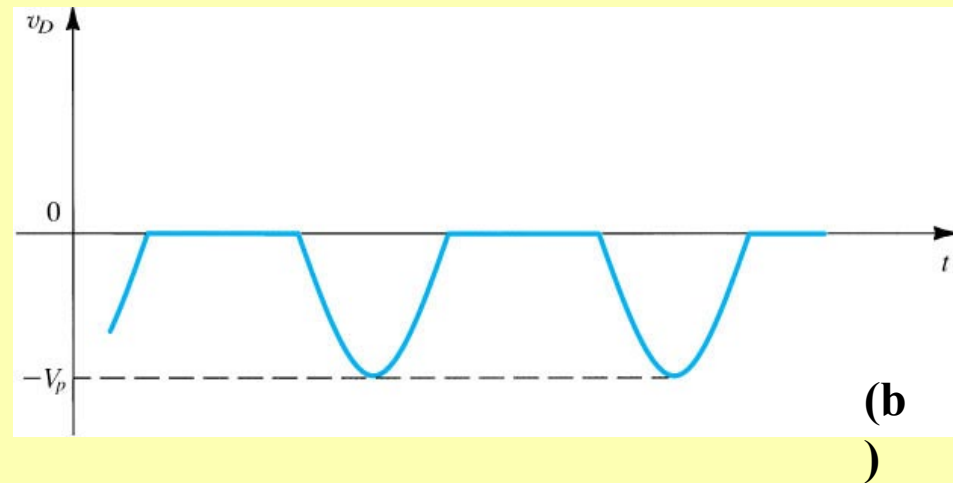
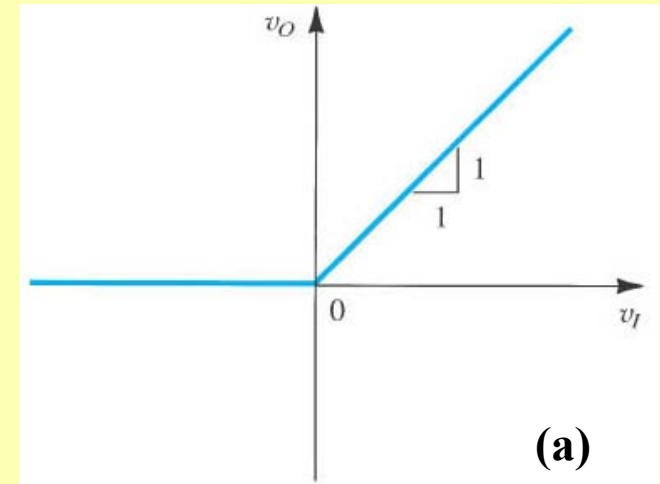
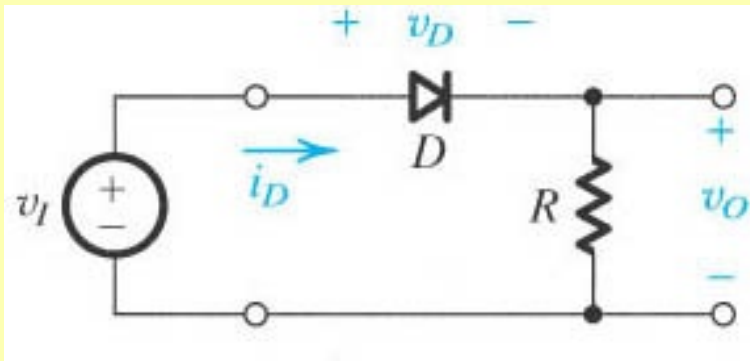
(e) Output waveform



# Exercise #2

For the single-diode rectifier circuit:

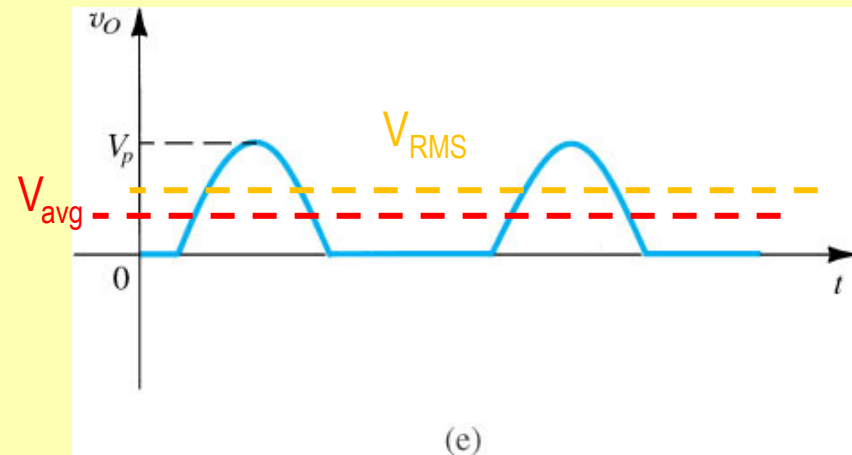
- Plot the transfer characteristic ( $v_o$  vs.  $v_I$ )
- Plot the waveform  $v_D$  as a function of time.



# Exercise #3

For half-wave rectified sine wave with peak voltage of  $V_P$ :

- 1) Find  $V_{\text{average}}$  or  $V_{\text{dc}}$ .
- 2) Find  $V_{\text{RMS}}$



**Ans:**

$$V_{\text{average}} = V_P / \pi$$

$$V_{\text{RMS}} = V_P / 2$$



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# **ANALYSIS OF DIODE CIRCUITS: EDUCATED GUESS APPROACH**



# Analysis of Diode Circuits

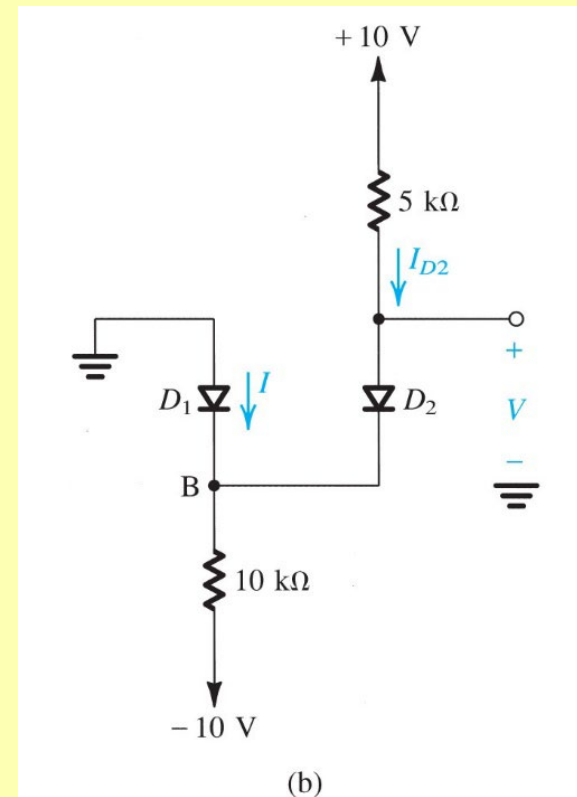
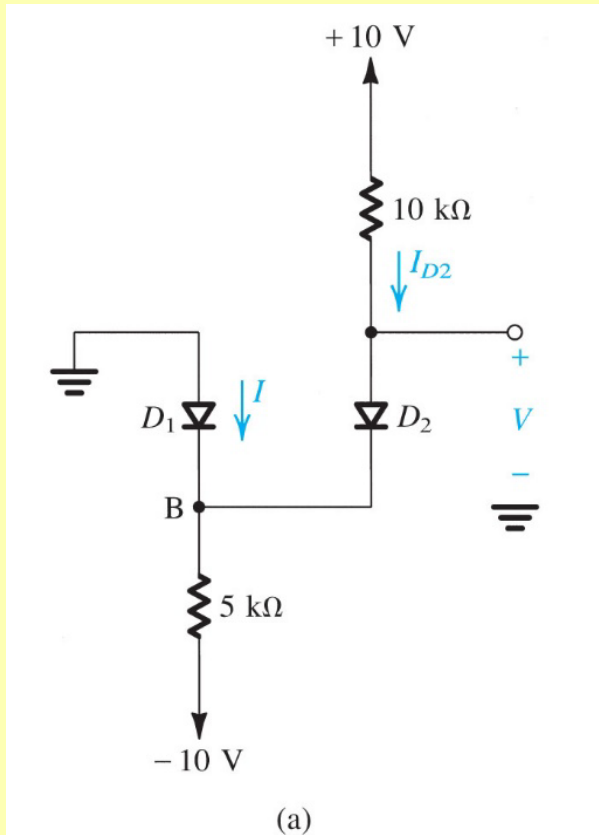
## Educated guess approach

- Relies on piecewise linear nature of our diode model
  - Overall  $i$ - $v$  characteristic of diode is extremely non-linear
  - But each section of our model is a straight line
  - If diode biased so that signal remains in one section  $\Rightarrow$  may use linear analysis
  - If signal crosses break-point linear analysis may not be used
- Make assumptions about “on” or “off” state of each diode
- Analyze circuit and verify assumptions by checking internal consistency
  - If consistent  $\Rightarrow$  done!
  - If inconsistent  $\Rightarrow$  learn from results and revise educated guess



# Exercise #4 (solutions provided)

Use the ideal diode model (for Exercise 4-8) to find the labeled unknown voltages and currents.



# Solutions: Exercise # 4 -7

## Exercise # 4

$$ID_2 = 1 \text{ mA}, I = 1 \text{ mA}, V = 0 \text{ V}$$

$$ID_2 = 1.3 \text{ mA}, I = 0 \text{ mA}, V = 3.3 \text{ V}$$

## Exercise #5

$$V = 3 \text{ V}, I_1 = 4 \text{ mA}, I_2 = -0.8 \text{ mA}$$

## Exercise #6

a) 2 mA and 0 V

b) 0 mA and 5 V

c) 0 mA and -5 V

d) 2 mA and 0 V

e) 3 mA and 3 V

f) 4 mA and 1 V

## Exercise #7

a) 0.6 mA and -3 V

b) 0 mA and 3 V

c) 0.6 mA and +3 V

d) 0 mA and -3 V

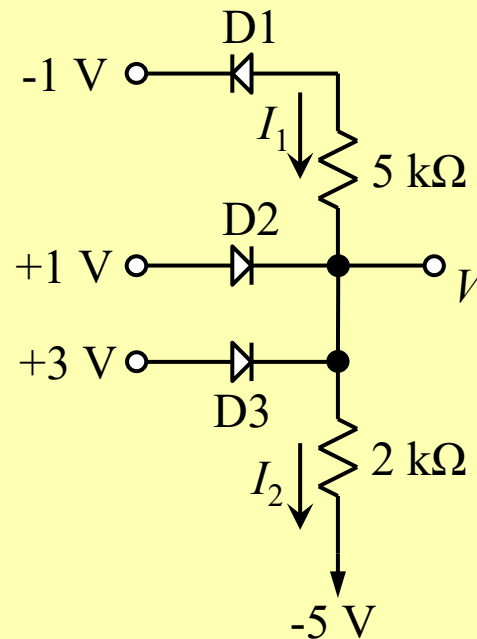
e) 2.5 mA and 2 V

f) 1 mA and 1 V



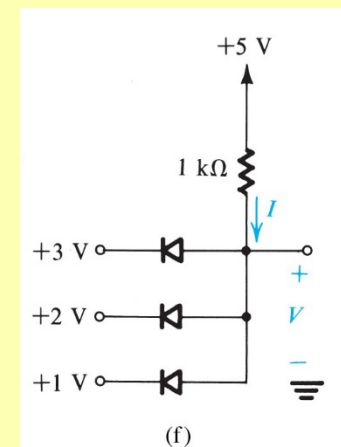
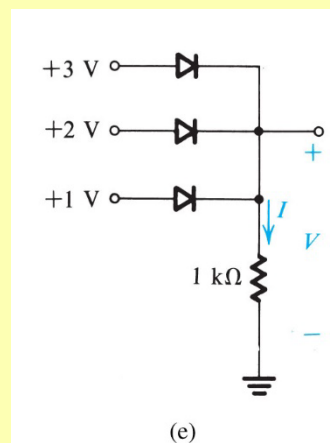
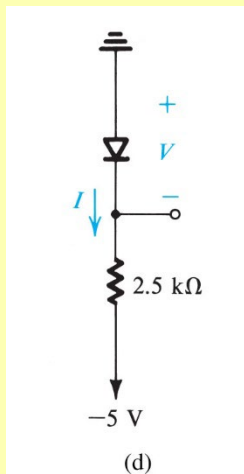
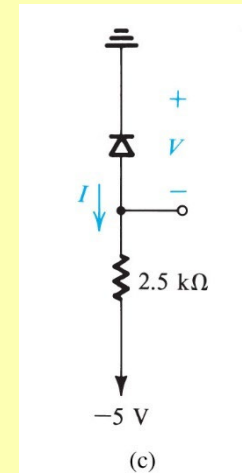
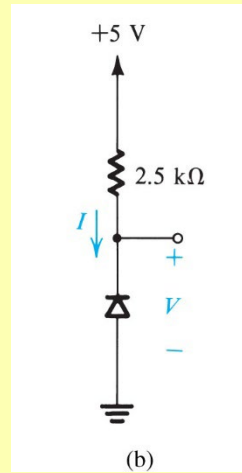
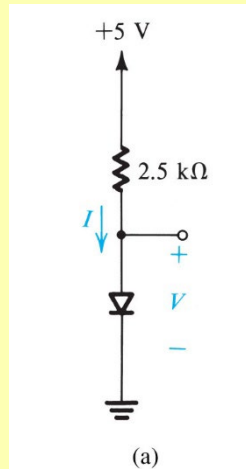
# Exercise #5

Use the ideal diode model (for Exercise 4-8) to find the labeled unknown voltages and currents.

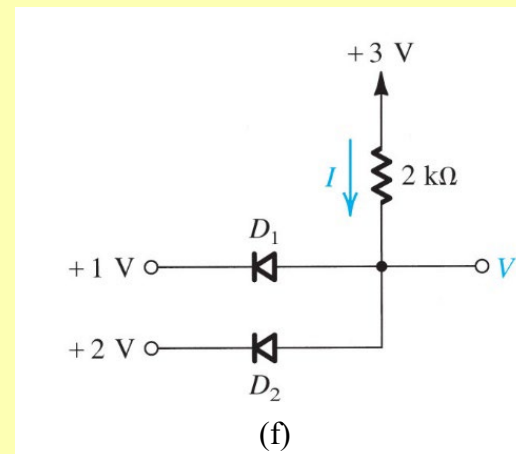
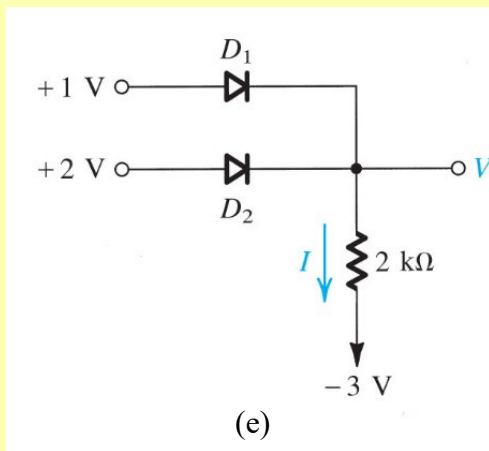
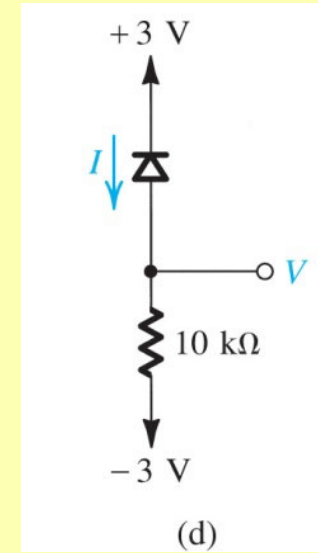
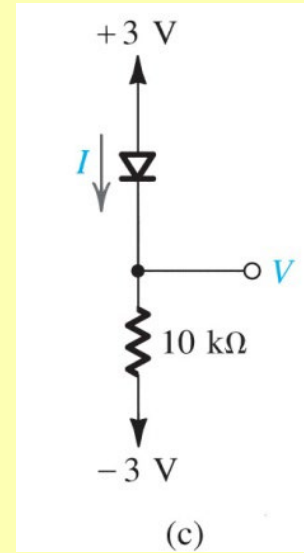
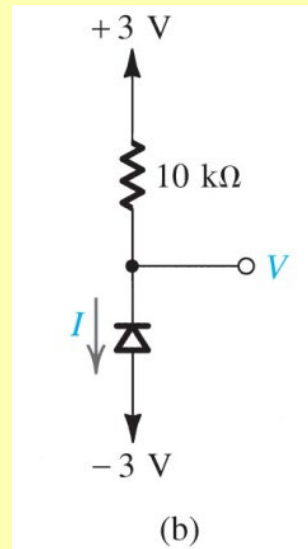
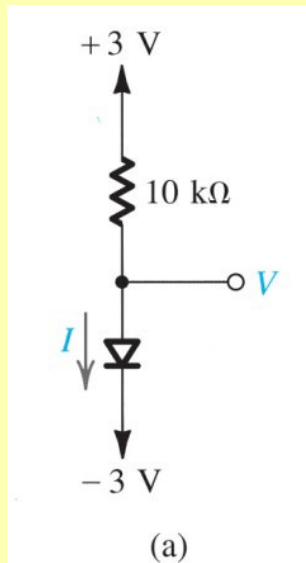




# Exercise #6

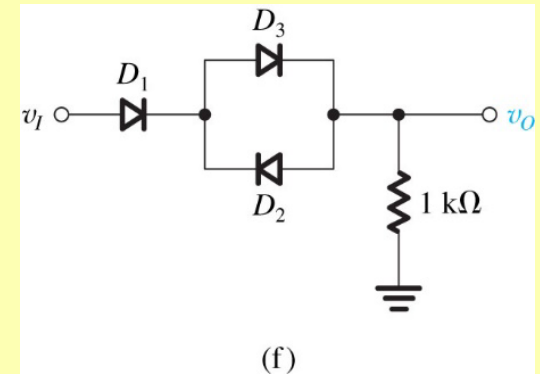
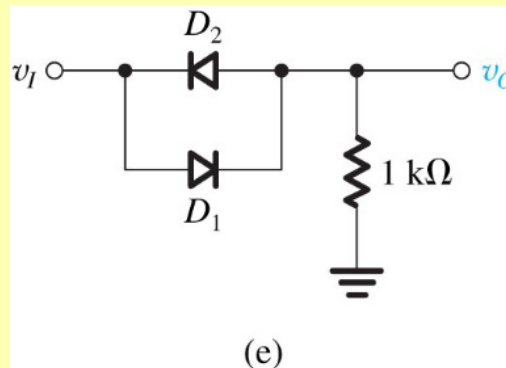
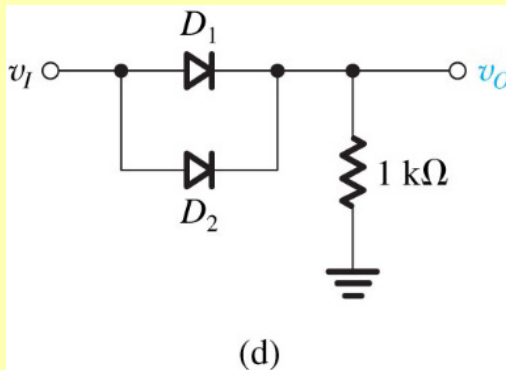
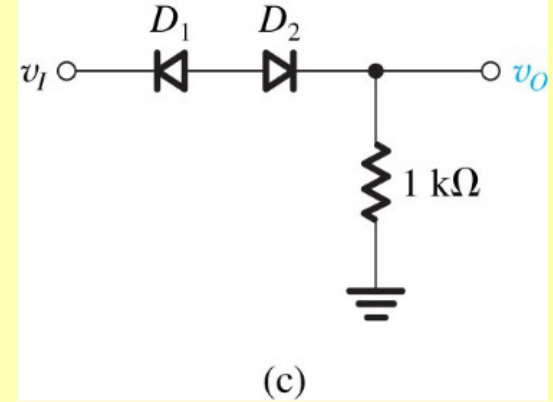
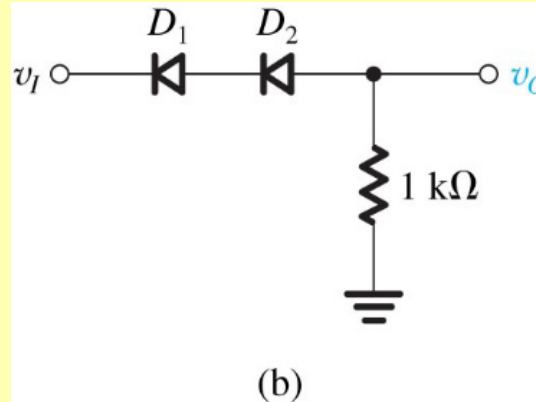
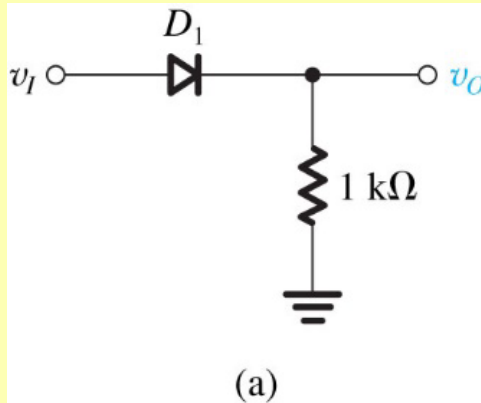


# Exercise #7

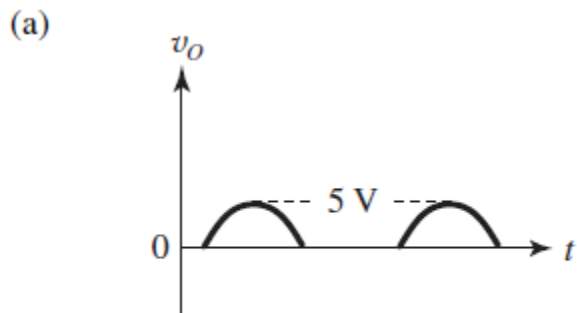


# Exercise #8

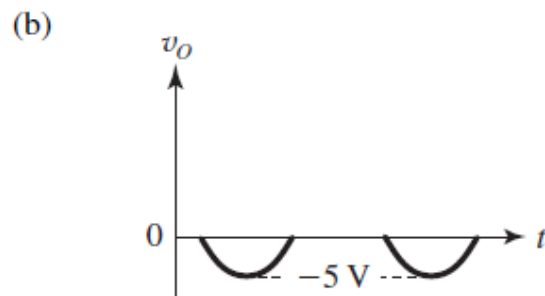
Assume:  $v_i$  is 1 kHz, 5V peak sine wave. Find  $v_o$ .



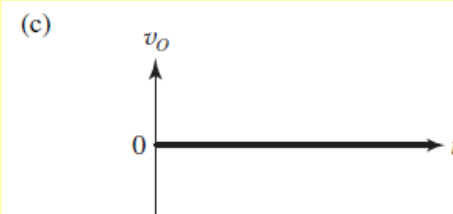
# Exercise #8: Solution



$$V_{p+} = 5 \text{ V} \quad V_{p-} = 0 \text{ V} \quad f = 1 \text{ kHz}$$

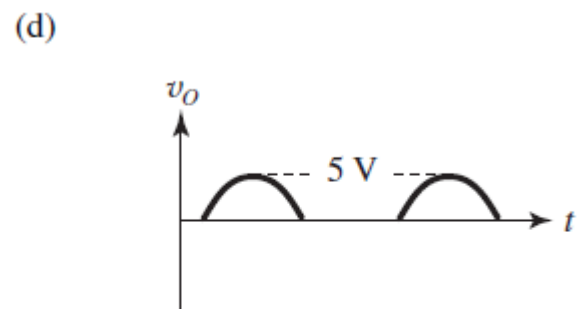


$$V_{p+} = 0 \text{ V} \quad V_{p-} = -5 \text{ V} \quad f = 1 \text{ kHz}$$



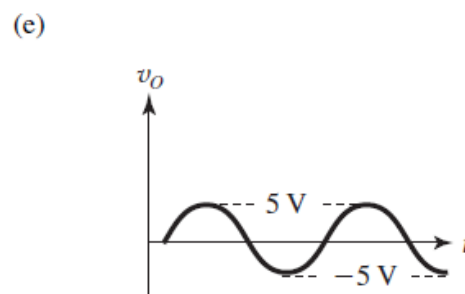
$$v_O = 0 \text{ V}$$

Neither  $D_1$  nor  $D_2$  conducts, so there is no output.



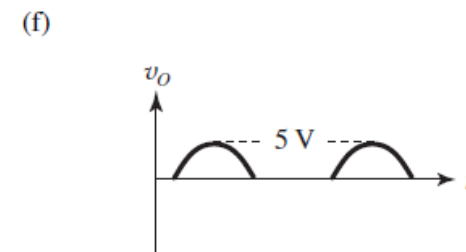
$$V_{p+} = 5 \text{ V}, \quad V_{p-} = 0 \text{ V}, \quad f = 1 \text{ kHz}$$

Both  $D_1$  and  $D_2$  conduct when  $v_I > 0$



$$V_{p+} = 5 \text{ V}, \quad V_{p-} = -5 \text{ V}, \quad f = 1 \text{ kHz}$$

$D_1$  conducts when  $v_I > 0$  and  $D_2$  conducts when  $v_I < 0$ . Thus the output follows the input.



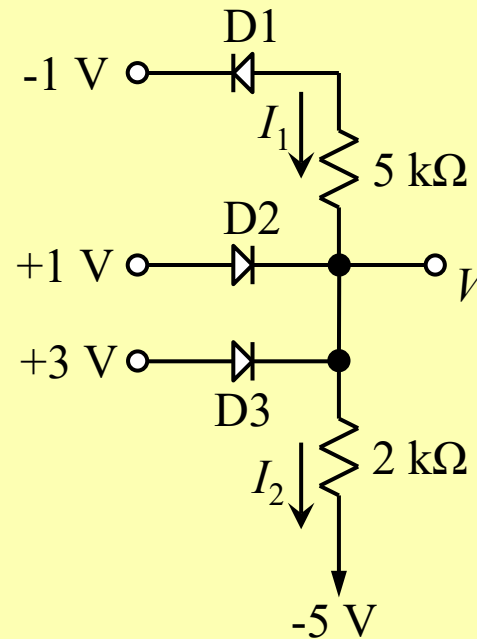
$$V_{p+} = 5 \text{ V}, \quad V_{p-} = 0 \text{ V}, \quad f = 1 \text{ kHz}$$



# Exercise #9: Non-ideal Diodes

Find  $V$ ,  $I_1$  and  $I_2$  (use: constant voltage model of 0.7 V)

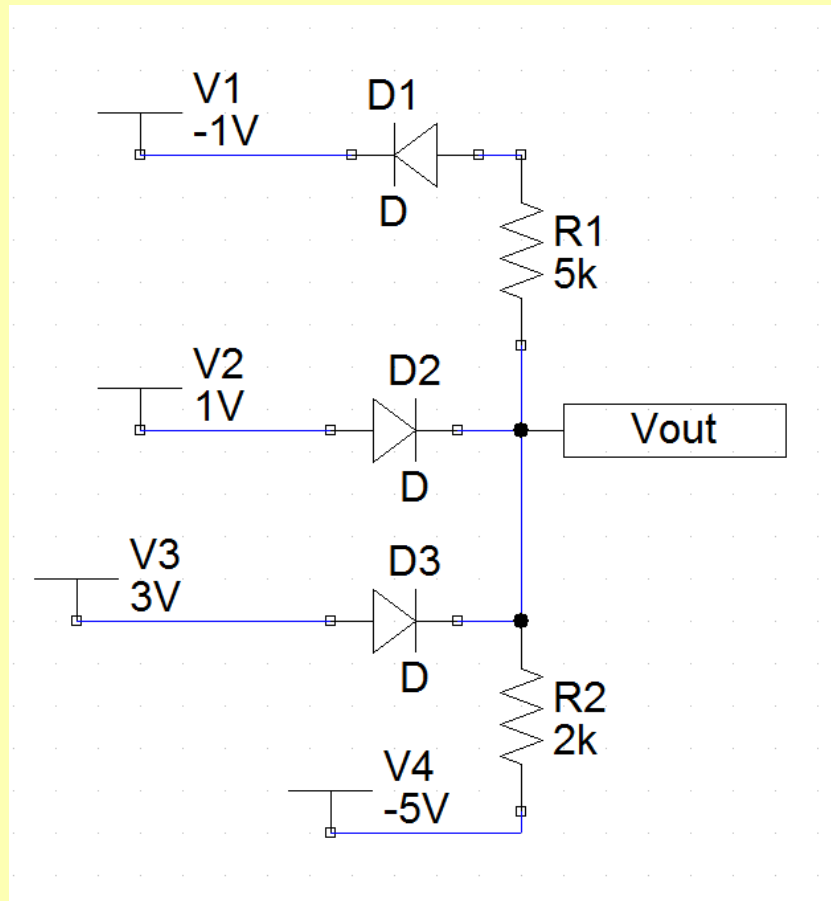
Compare your results to Exercise #5.



Ans:  $I_1 = -0.52\text{ mA}$ ,  $I_2 = 3.65\text{ mA}$ ,  $V = 2.3\text{ V}$



# Exercise #10: Spice Verification



SMALL SIGNAL BIAS SOLUTION		TEMPERATURE
*****		
NODE	VOLTAGE	
V (1)	-3.61136484E-01	
V (V1)	-1.00000000E+00	
V (V2)	1.00000000E+00	
V (VOUT)	2.30785900E+00	
V (V3)	3.00000000E+00	
V (V4)	-5.00000000E+00	
SOURCE	CURRENT	
I (V2)	1.31785889E-12	
I (V3)	-4.18772860E-03	
I (V4)	3.65392950E-03	
I (V1)	5.33799096E-04	
RESISTOR	CURRENT	
I (R1)	5.33799096E-04	
I (R2)	3.65392950E-03	

Compare your results to Exercise #9.

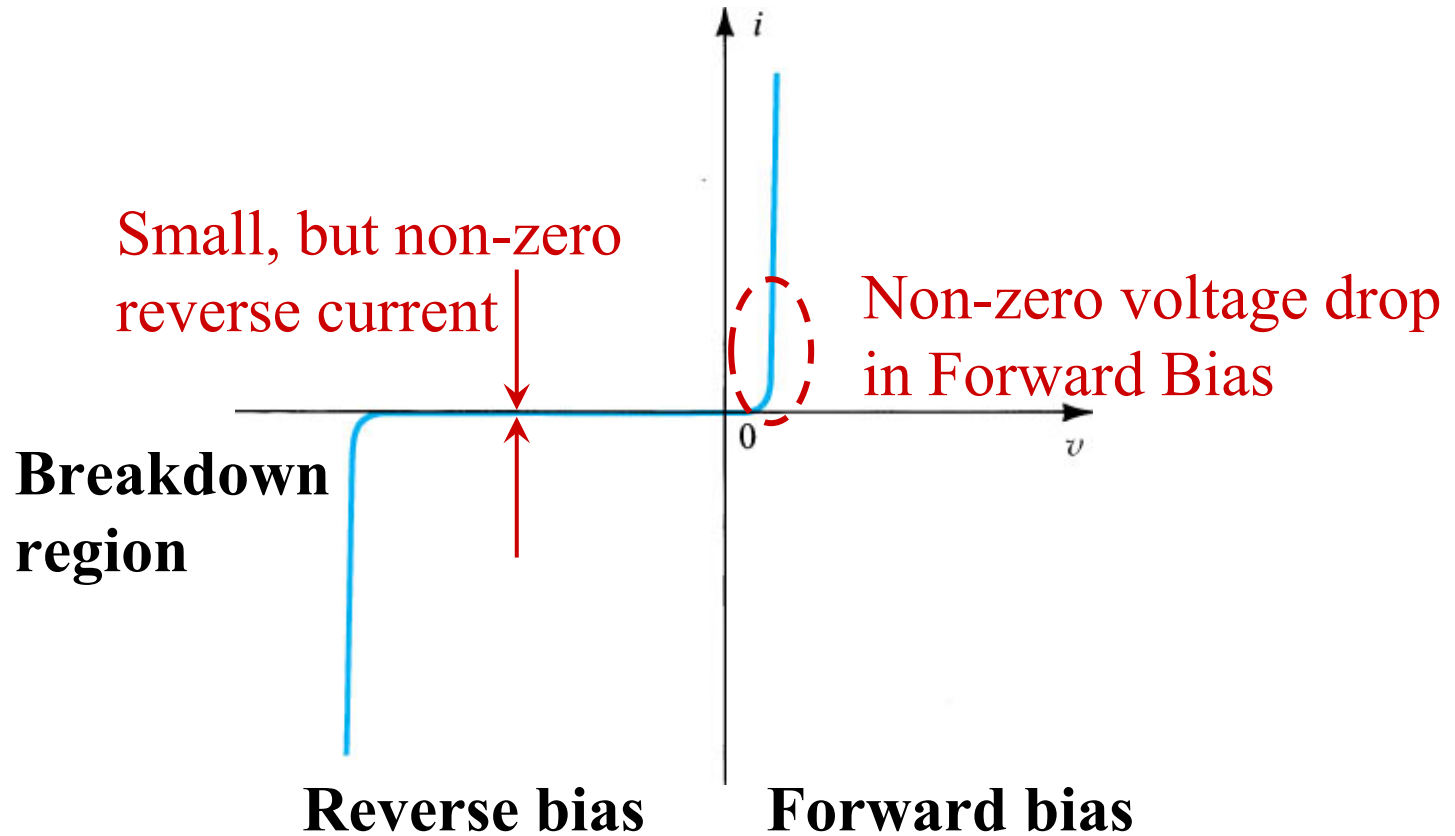


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# **REAL DIODES**



# Terminal Characteristics of Real Diodes





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# **REAL DIODES:** **THE FORWARD BIAS REGION**

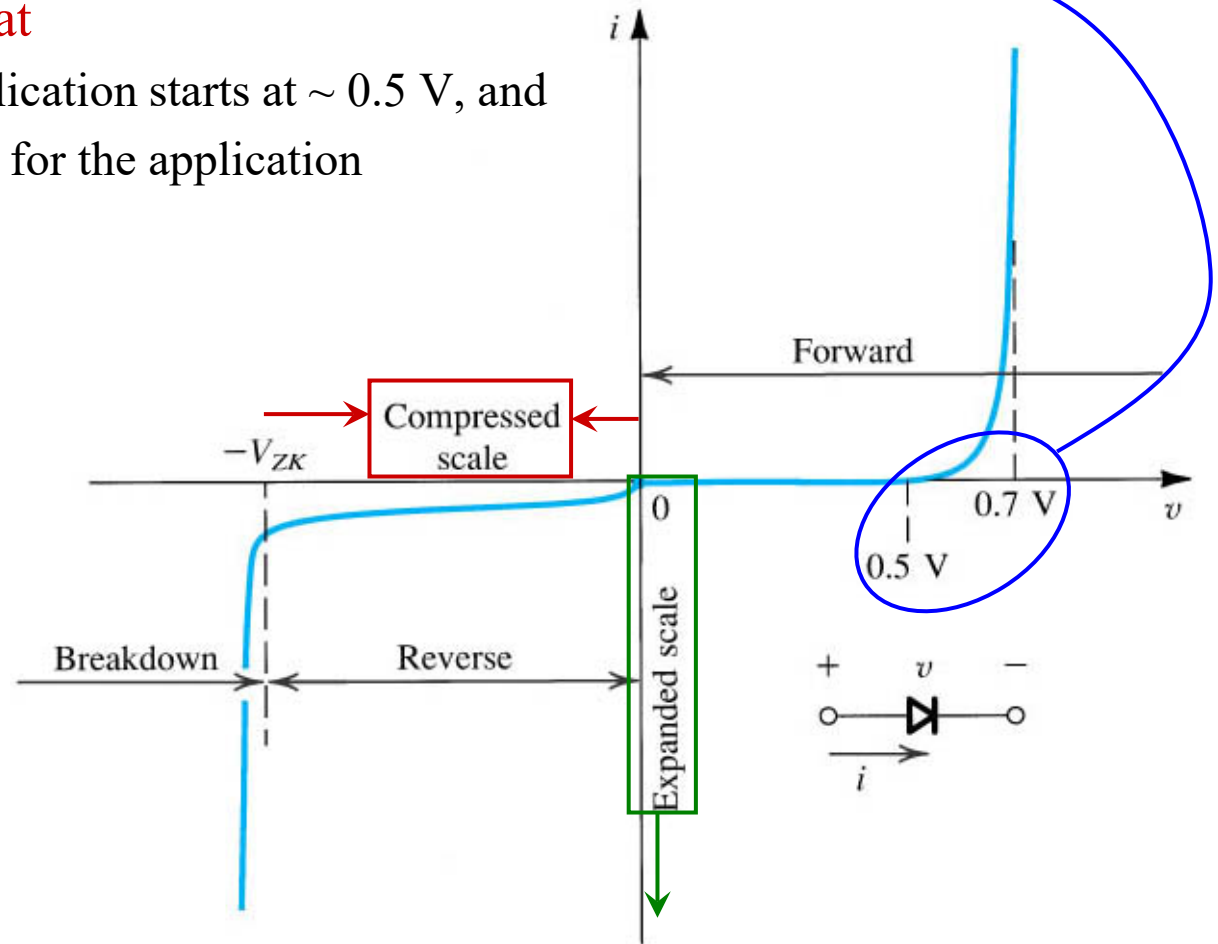


# Terminal Characteristics of Real Diodes

Forward current is actually  $\sim$ exponential, but

Diode typically sized so that

- Significant current for application starts at  $\sim 0.5$  V, and
- By  $\sim 0.7$  V, current is large for the application



# The Forward Bias Region

$$i = I_S \left[ \exp\left(\frac{v}{nV_T}\right) - 1 \right]$$

- $I_S(T)$  “saturation” current (proportional to diode area)
- $V_T = kT/q$  is the thermal voltage
  - $k$  is Boltzmann’s constant
    - $= 1.38 \times 10^{-23} \text{ J/K}$
    - $= 8.617 \times 10^{-5} \text{ eV/K}$
  - $T$  is the diode temperature (Kelvin)
  - $q$  is the electron charge:  $1.6 \times 10^{-19} \text{ C} = 1 \text{ e}$
- $I_S(T)$  “rule of thumb”  $\Rightarrow$  doubles for each  $\sim +5^\circ \text{ C } \Delta T$
- $V_T = 25 \text{ mV}$  at  $17^\circ \text{C}$ ;  $25.2 \text{ mV}$  at  $20^\circ \text{C}$ ;  $25.9 \text{ mV}$  at  $300 \text{ K}$
- $n = 1$  to  $2$  (ideality factor) [assume 1 unless otherwise specified]



# The Forward Bias Region

$$i = I_S \exp\left(\frac{v}{nV_T}\right) \text{ for } i \gg I_S$$

Solving for  $v$ :

$$v = nV_T \ln\left(\frac{i}{I_S}\right) = 2.3 nV_T \log\left(\frac{i}{I_S}\right) \text{ using } \frac{1}{\log(e)} = 2.3$$

$2.3 nV_T = 60$  or  $120$  mV for  $n = 1$  or  $2$  respectively at  $20^\circ\text{C}$



# Logarithmic Rate of Change

Consider two different voltages;  $V_1$  and  $V_2$  (assume  $n=1$ )

$$I_1 = I_S \exp\left(\frac{V_1}{V_T}\right)$$

$$I_2 = I_S \exp\left(\frac{V_2}{V_T}\right)$$

We have:  $V_2 - V_1 = 2.3 V_T \log\left(\frac{I_2}{I_1}\right)$

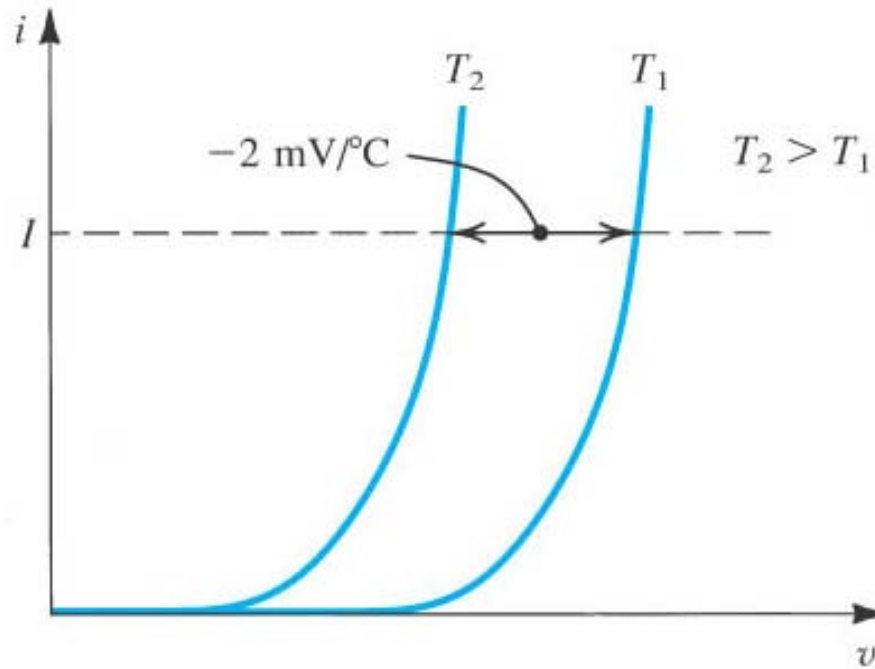
If diode is sized such that at 0.7 V  
the current is 1 mA

$V$	$I$
0.7 V	1 mA
0.758 V	10 mA

So for a decade change of current, we have  $2.3 V_T \approx 60 \text{ mV}$   
change in voltage



# Temperature Dependence of Diode Forward Characteristic



At a constant current, the voltage drop decreases by approximately 2 mV for every  $1^\circ\text{C}$  increase in temperature

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# **REAL DIODES:** **THE REVERSE BIAS REGION**



# Reverse-Bias Region

Starting from: 
$$i = I_S \left[ \exp\left(\frac{v}{nV_T}\right) - 1 \right]$$

If  $v$  is made negative and a few times larger than  $V_T$ :

$$i \approx -I_S$$

**Hence the name “saturation” current  
(a.k.a. *reverse* saturation current)**

$I_S$  is typically  $10^{-15}$  to  $10^{-14}$  A (1 to 10 fA)

Real diodes have larger “leakage” current: e.g. 1 nA

But depends on diode size

While  $I_S$  doubles every  $\sim 5^\circ\text{C}$  rise in  $T$

Leakage current doubles every  $\sim 10^\circ\text{C}$  rise in  $T$





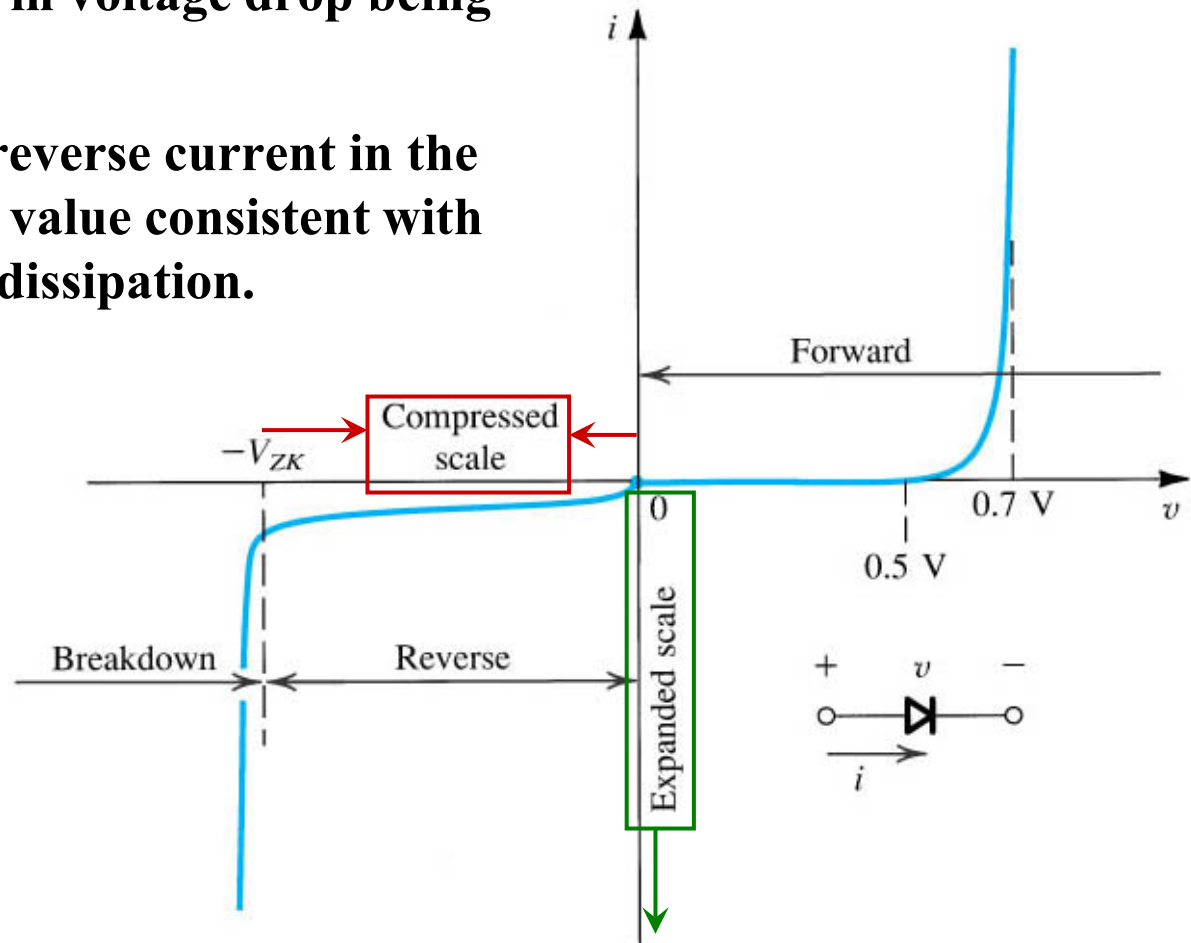
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# **REAL DIODES:** **THE BREAKDOWN REGION**



# The Breakdown Region

- The reverse current increases rapidly, with the associated increase in voltage drop being very small.
- Necessary to limit the reverse current in the breakdown region to a value consistent with the permissible power dissipation.



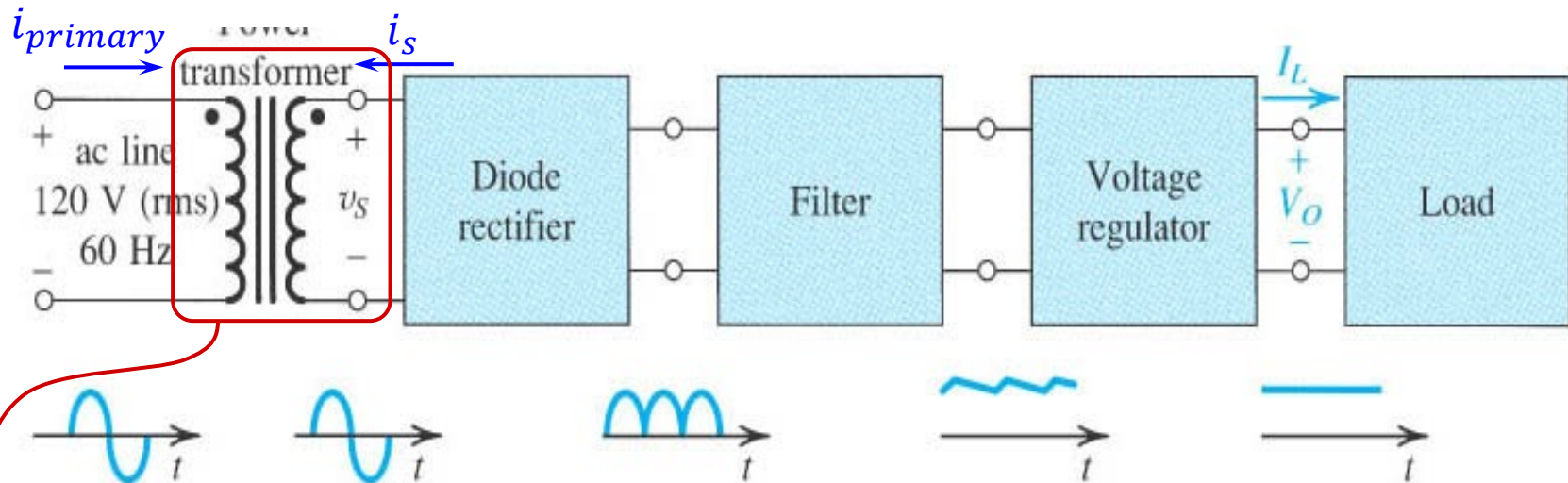
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# **RECTIFIER CIRCUITS**



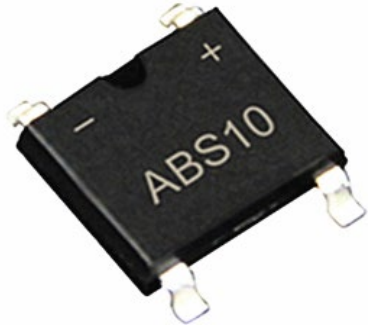
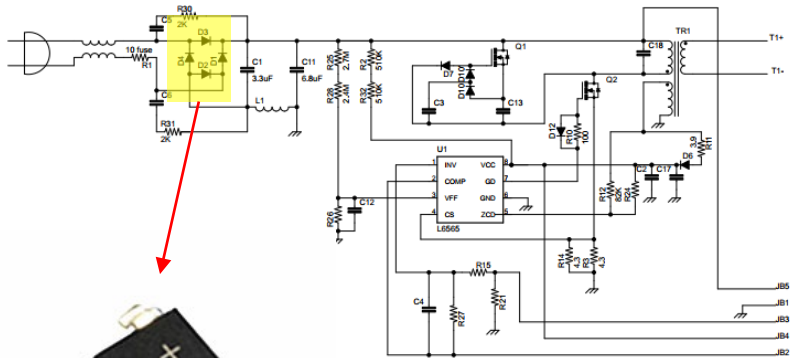
# Rectifier Circuits

## Block diagram of a dc power supply

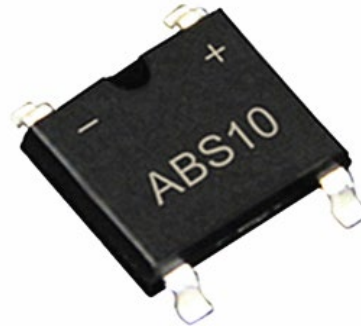


- Two separate coils wound on iron core that couples magnetic flux between coils
- Primary:  $N_1$  turns [e.g. 120 V(rms) line supply]
- Secondary:  $N_2$  turns
  - Ideally:  $v_s = \frac{N_2}{N_1} v_{primary}$  ;  $i_s = \pm \frac{N_1}{N_2} i_{primary}$  (+ for ref. direction into dots)
  - E.g.  $\frac{N_2}{N_1} = \frac{1}{6}$  turns ratio yields  $v_s = 20$  V(rms)

# Example: iPhone Charger



Example of bridge application



## Example of Commercial Bridge Diode

**Diotec**  
Semiconductor

ABS2 ... ABS10

**ABS2 ... ABS10**  
SMD Single Phase Bridge Rectifier  
SMD Einphasen-Brückengleichrichter

$I_{FAV1} = 1\text{ A}$   $V_{RRM} = 200 \dots 1000\text{ V}$   
 $V_F < 1.1\text{ V}$   $I_{FSM} = 27/30\text{ A}$   
 $T_{jmax} = 150^\circ\text{C}$   $t_r \sim 1500\text{ ns}$

Version 2016-03-21

**Typical Application**  
50/60 Hz Mains Rectification,  
Power Supplies  
Commercial grade <sup>1)</sup>

**Features**  
4mm pitch for high creepage  
and clearance  
Compliant to RoHS, REACH,  
Conflict Minerals <sup>1)</sup>

**Mechanical Data <sup>1)</sup>**

Taped and reeled  
Weight approx.  
Case material  
Solder & assembly conditions  
MSL = 1



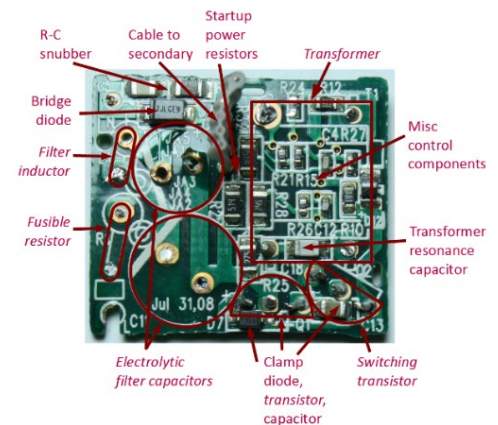
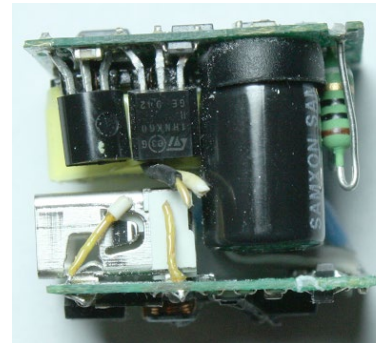
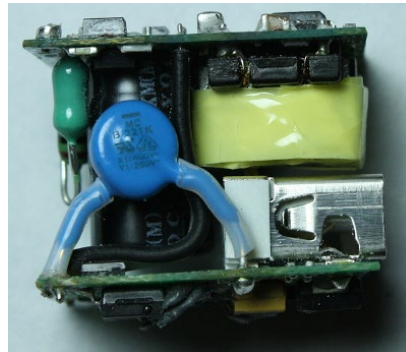
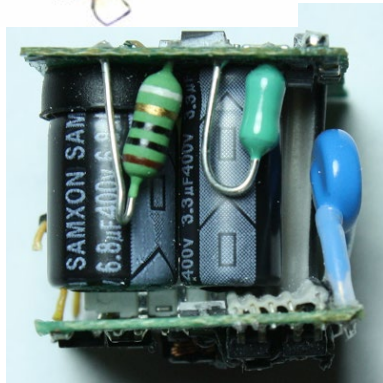
**Typische Anwendung**  
50/60 Hz Netzgleichrichtung,  
Stromversorgungen  
Standardausführung <sup>1)</sup>

**Besonderheit**  
4mm Raster für hohe  
Luft- und Kriechstrecken  
Konform zu RoHS, REACH,  
Konfliktmineralien <sup>1)</sup>

**Mechanische Daten <sup>1)</sup>**

5000 / 13"  
0.1 g  
UL 94V-0  
260°C/10s  
MSL = 1

**Grenzwerte <sup>2)</sup>**



<http://www.righto.com/2012/05/apple-iphone-charger-teardown-quality.html>

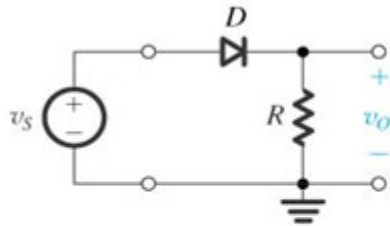


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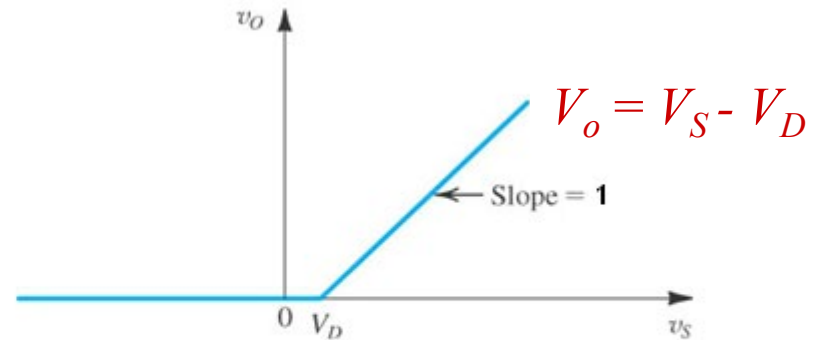
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45

# [1] The Half-Wave Rectifier

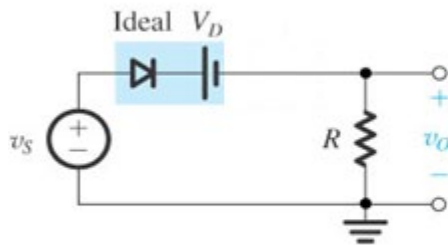


(a)

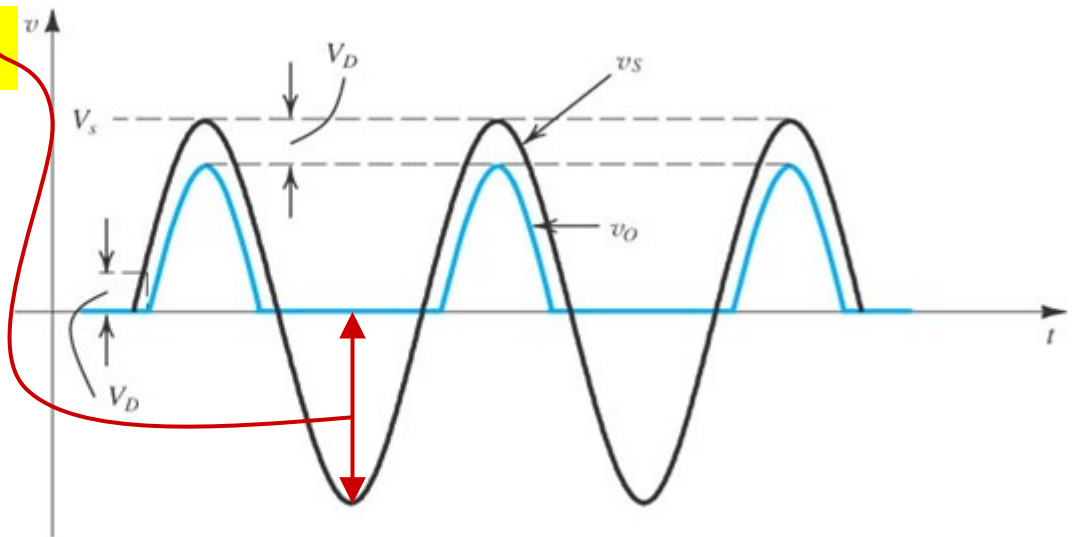


Transfer characteristic

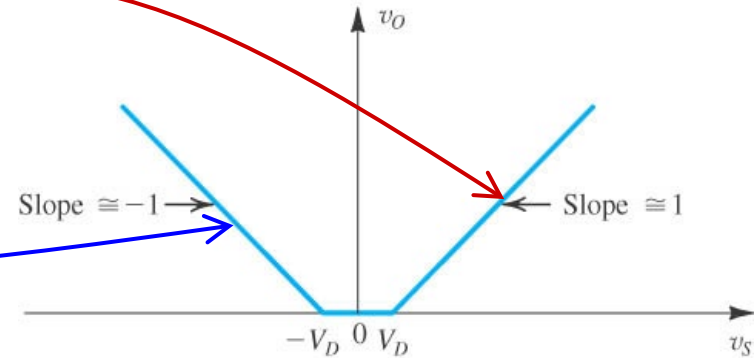
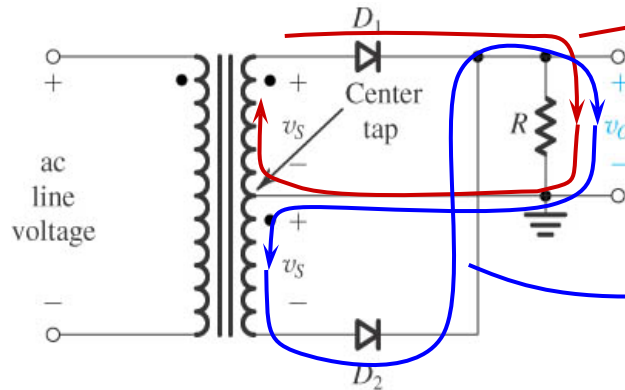
Peak Inverse Voltage:  $PIV = V_S$



Equivalent circuit



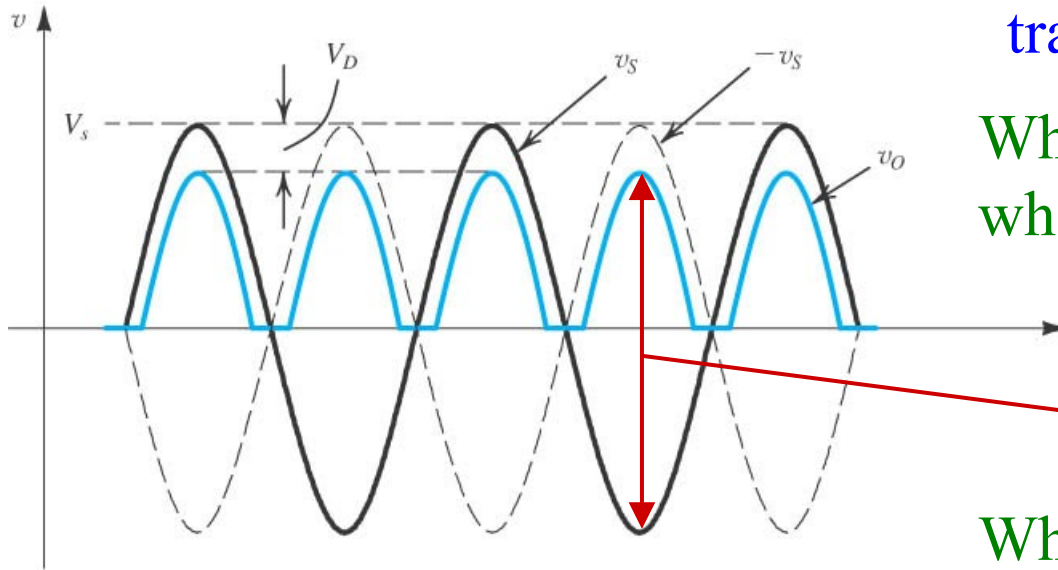
# [2] The Full-Wave Rectifier



transfer characteristic

What is path of current when  $v_S$  is positive?

What is path of current when  $v_S$  is negative?



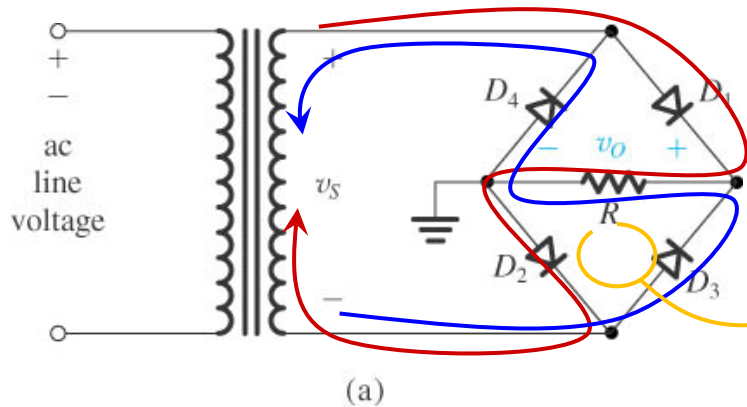
input and output waveforms

Peak Inverse Voltage:  
 $PIV = 2V_S - V_D$





# [3] The Bridge Rectifier



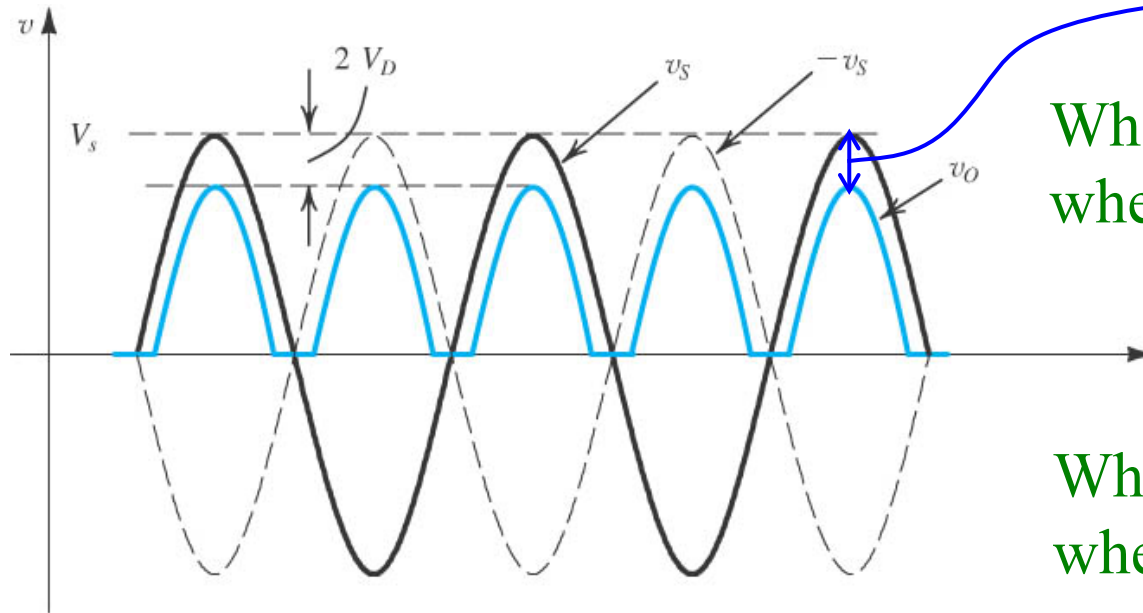
Peak Inverse Voltage:  
 $PIV = V_O + V_D = V_S - V_D$

mesh equation

$$V_O = V_S - 2V_D$$

What is path of current  
when  $v_s$  is positive?

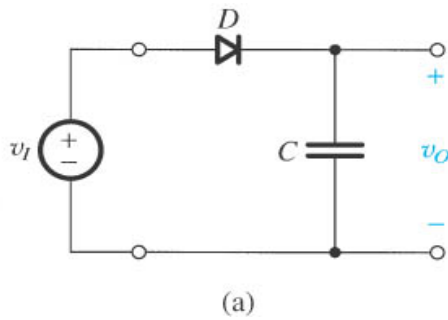
What is path of current  
when  $v_s$  is negative?



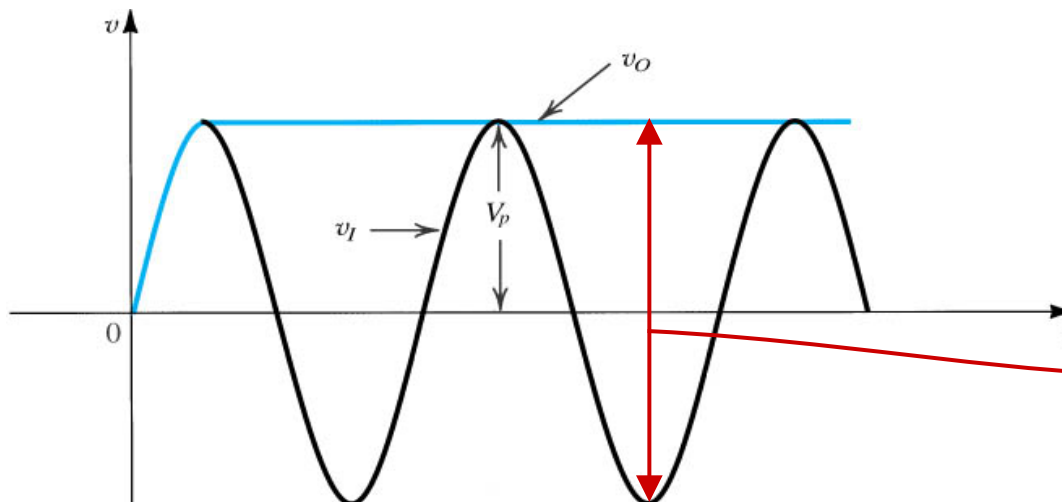
input and output waveforms



# Effect of a Filter Capacitor



Peak Inverse Voltage:  $PIV = V_I + V_O$



Input and output waveforms for no load current, and assuming an ideal diode

The circuit is known as a **peak detector**

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# MODELING THE DIODE FORWARD CHARACTERISTIC



# Modeling The Diode Forward Characteristic

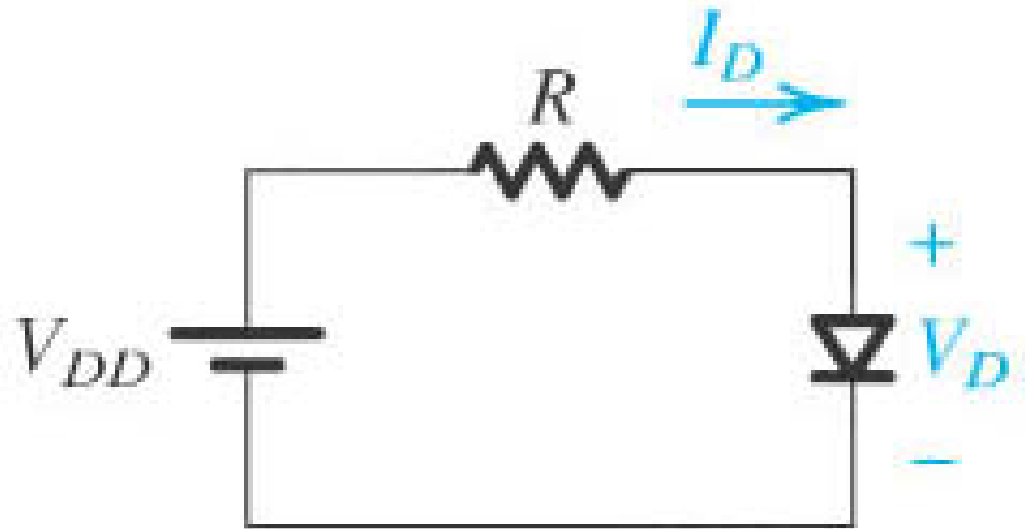
Two unknowns:  $V_D$  &  $I_D$

Need two equations:

$$I_D = I_S \left[ \exp\left(\frac{V_D}{V_T}\right) - 1 \right]$$

$$I_D = \frac{V_{DD} - V_D}{R}$$

Equate  $I_D$

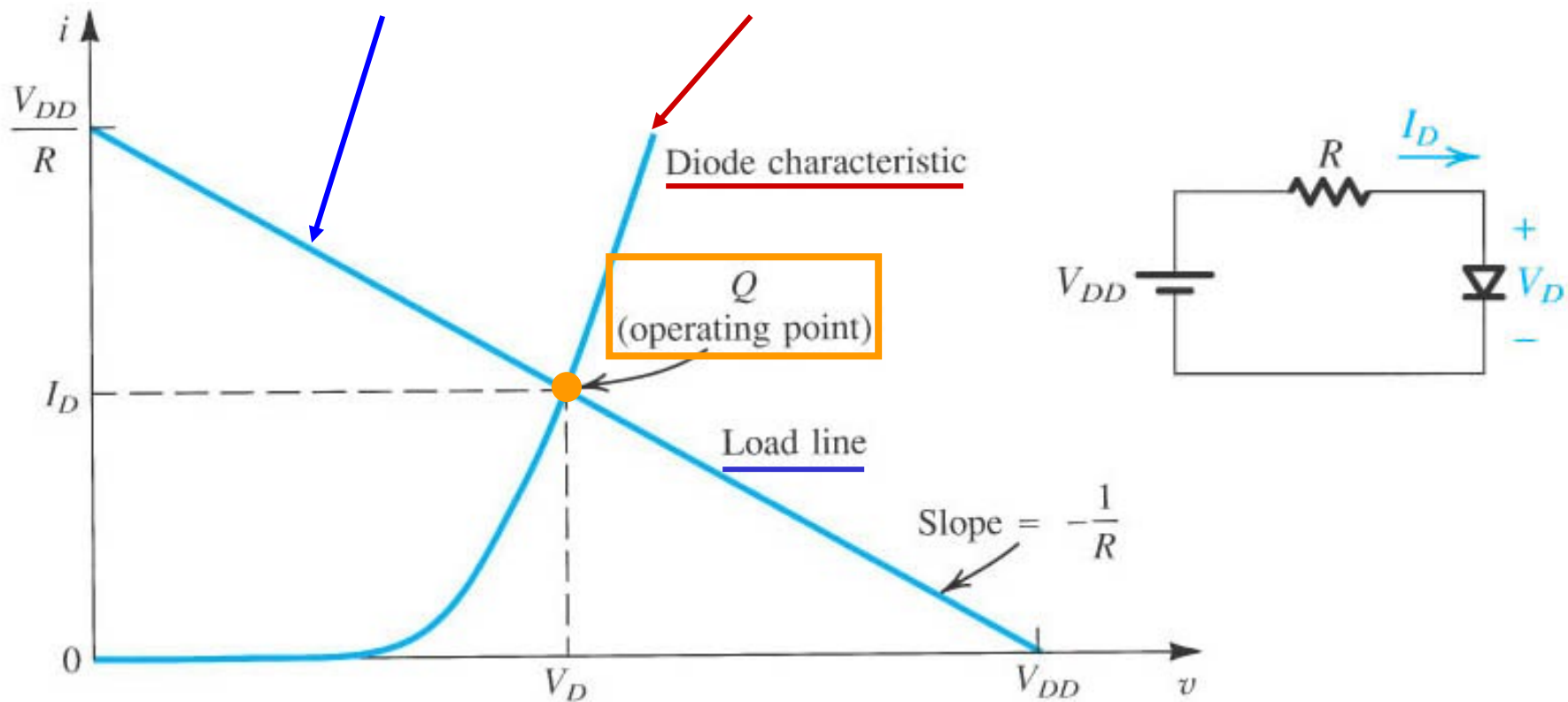


*A simple circuit used to illustrate the analysis in which the diode is forward conducting.*

Two methods of solutions possible: graphical & iterative

# Graphical Solution

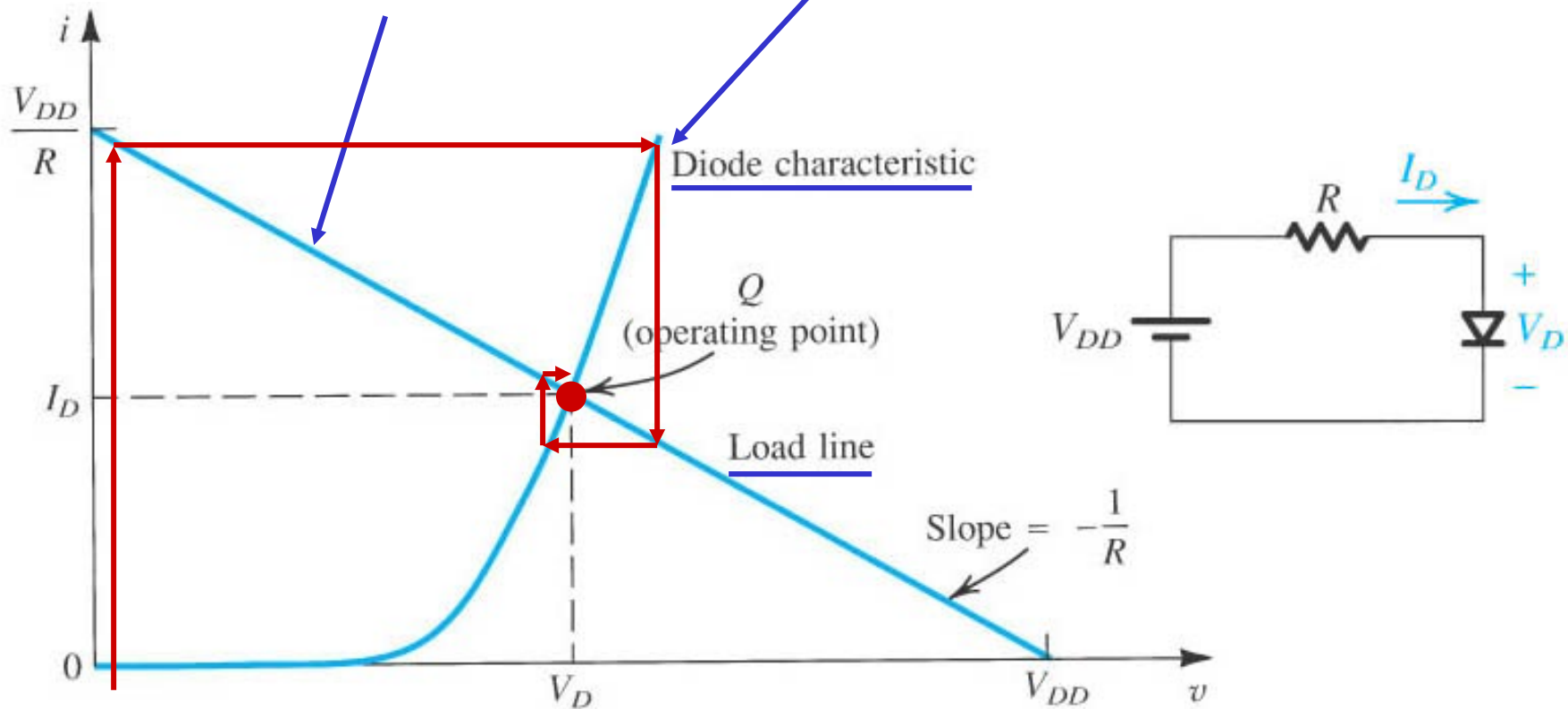
$$I_D = \frac{V_{DD} - V_D}{R} \qquad I_D = I_S \left[ \exp\left(\frac{V_D}{V_T}\right) - 1 \right]$$



# Iterative Analysis

$$I_D = \frac{V_{DD} - V_D}{R}$$

$$I_D = I_S \exp\left(\frac{V_D}{V_T}\right)$$



# Iterative Analysis --- Example

Circuit data:  $V_{DD} = 5\text{ V}$  and  $R = 1\text{ k}\Omega$

Diode has  $I_D = 1\text{ mA}$  for  $V_D = 0.7\text{ V}$

Start with  $V_1 = 0.7\text{ V}$  and calculate  $I_D$

$$I_D = \frac{V_{DD} - V_D}{R} = \frac{5 - 0.7}{1} = 4.3\text{ mA}$$

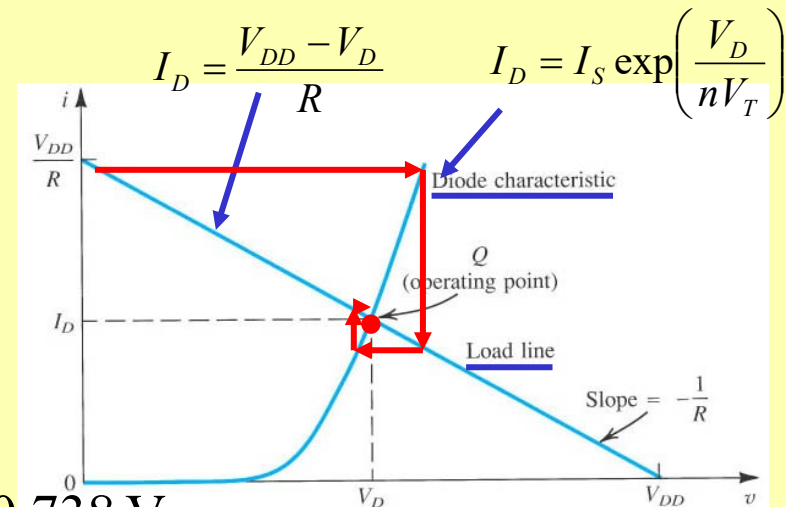
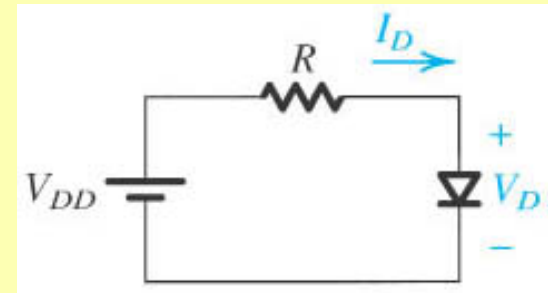
Calculate  $V_D$ :

$$V_2 - V_1 = 2.3 V_T \log\left(\frac{I_2}{I_1}\right)$$

$$V_2 = V_1 + 0.06 \times \log\left(\frac{I_2}{I_1}\right) = .7 + 0.06 \times \log\left(\frac{4.3}{1}\right) = 0.738\text{ V}$$

Next iteration we get

$$I_D = \frac{5 - 0.738}{1} = 4.262\text{ mA} \quad \text{and} \quad V_3 = .738 + 0.06 \times \log\left(\frac{4.262}{4.3}\right) = 0.738\text{ V}$$

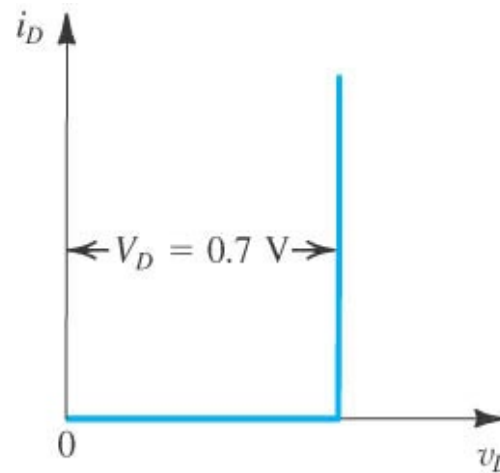
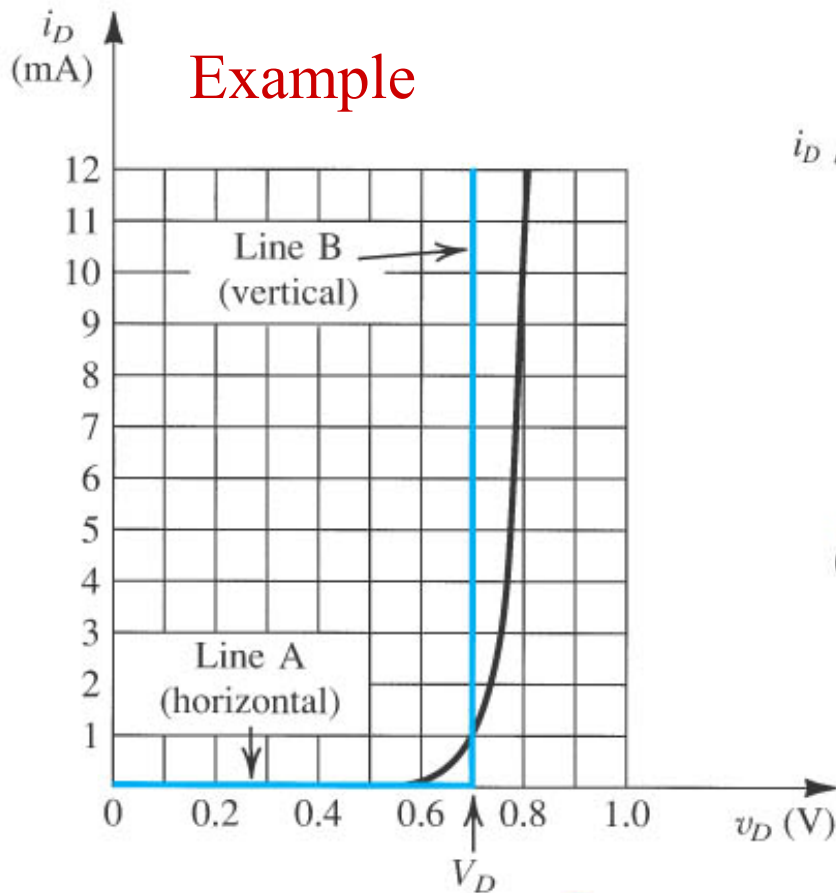


# Need For Rapid Analysis

- ◆ **The graphical and iterative analysis is too time consuming for complex circuits**
- ◆ **A simpler model is desired for a rapid analysis permitting to develop a first cut design**
- ◆ **More accurate analysis can then be performed using circuit simulation CAD tools such as TopSPICE to fine tune the circuit**

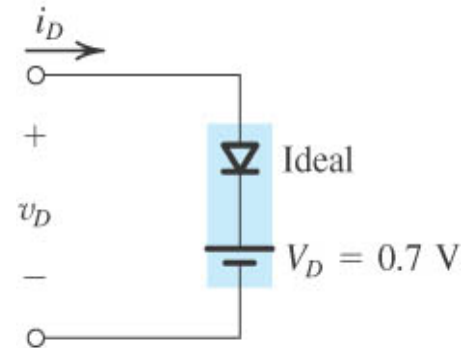


# Constant-Voltage-Drop Model



(a)

equivalent-circuit  
representation



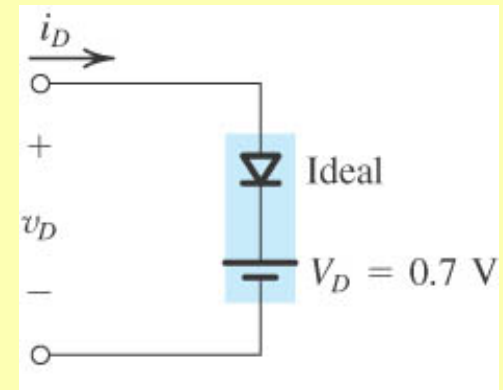
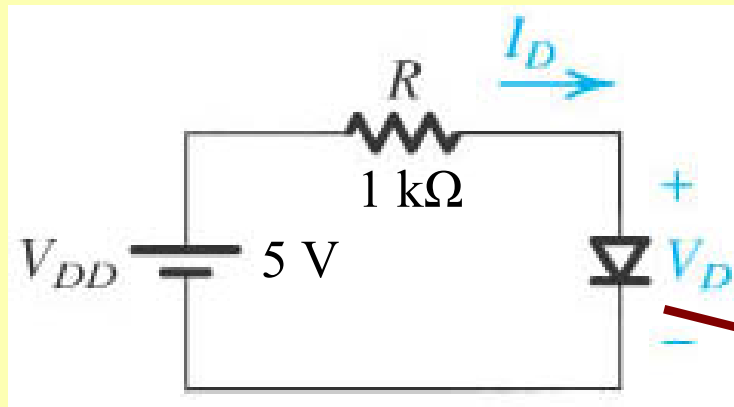
(b)

This simple model predicts  $V_D$  to within  $\pm 0.1$  V over the current range of 0.1 mA to 10 mA (**for this example**)



# Exercise #10

What is the current flowing through the diode?



Assuming  $V_D = 0.7\text{ V}$ . Therefore

$$I_D = \frac{V_{DD} - V_D}{R} = \frac{5 - 0.7}{1} = 4.3\text{ mA}$$

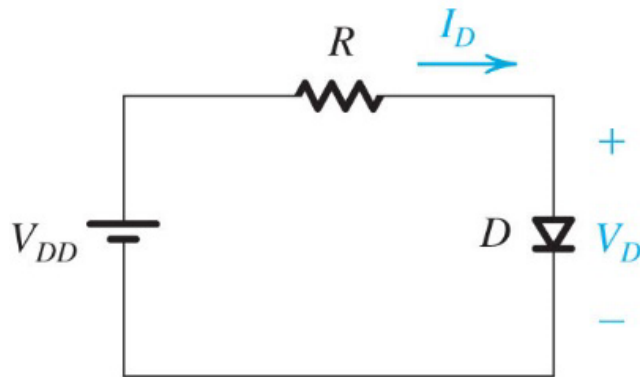
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# **SMALL SIGNAL MODEL**

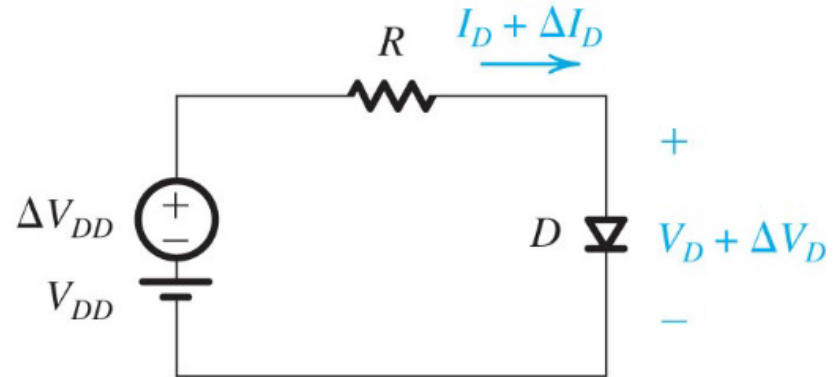


# Small Signal Model

When  $V_{DD}$  undergoes a small change  $\Delta V_{DD}$ , the current  $I_D$  changes by an increment  $\Delta I_D$ , and the diode voltage  $V_D$  changes by an increment  $\Delta V_D$ . We wish to find a **quick way to determine the values of these incremental changes**.



(a)



(b)

# Small Signal Model

Consider the forward bias approximation:

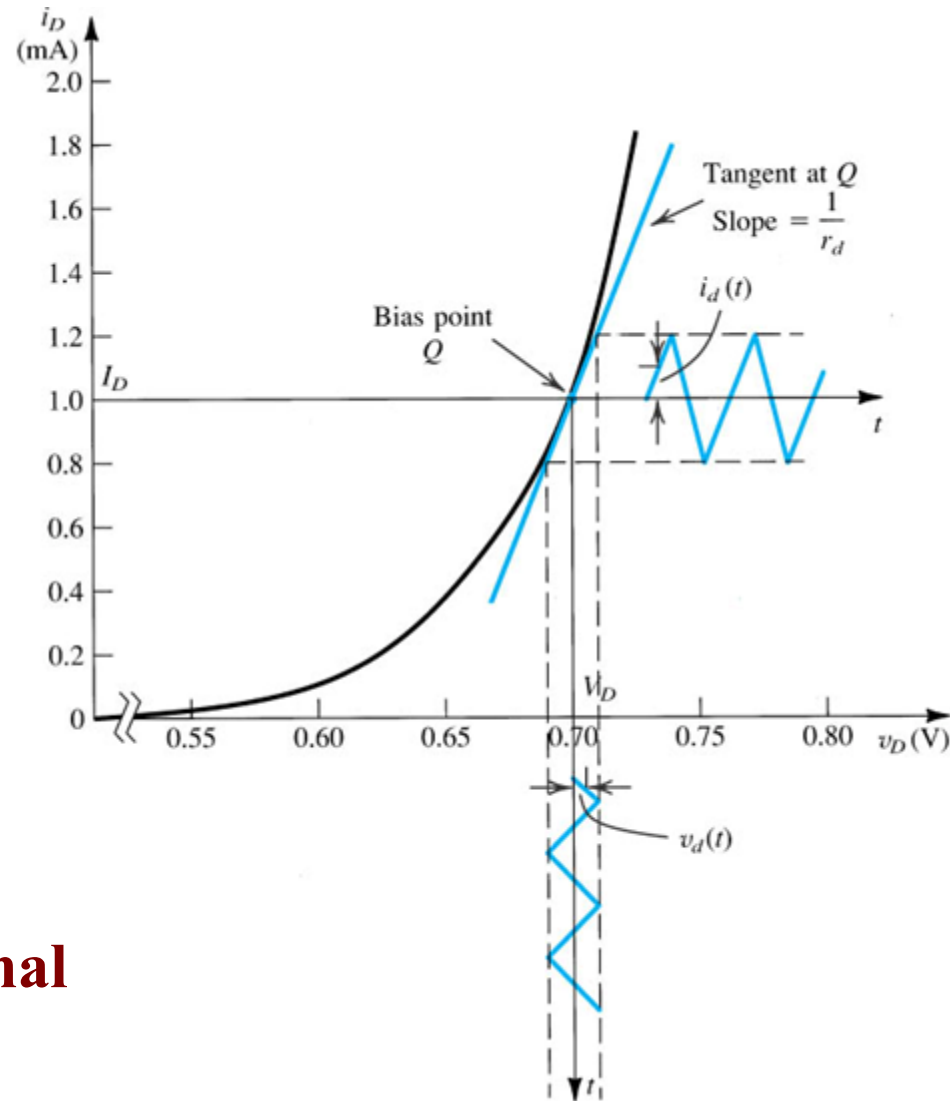
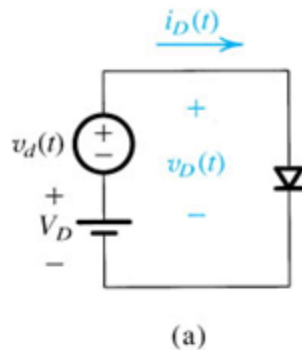
$$i_D = I_S \exp\left(\frac{v_D}{V_T}\right) = \underbrace{I_S \exp\left(\frac{V_D}{V_T}\right)}_{I_D} \times \exp\left(\frac{v_d}{V_T}\right) \approx I_D \left(1 + \frac{v_d}{V_T}\right)$$

using  $v_D = V_D + v_d$  and  $\exp(x) \approx 1 + x$  for  $x \ll 1$

$$i_D = I_D + i_d \Rightarrow i_d = \frac{I_D v_d}{V_T} = \frac{v_d}{r_d} \text{ with } r_d = \frac{V_T}{I_D} = \left[ \left| \frac{\partial i_D}{\partial v_D} \right|_{i_D = I_D} \right]^{-1}$$



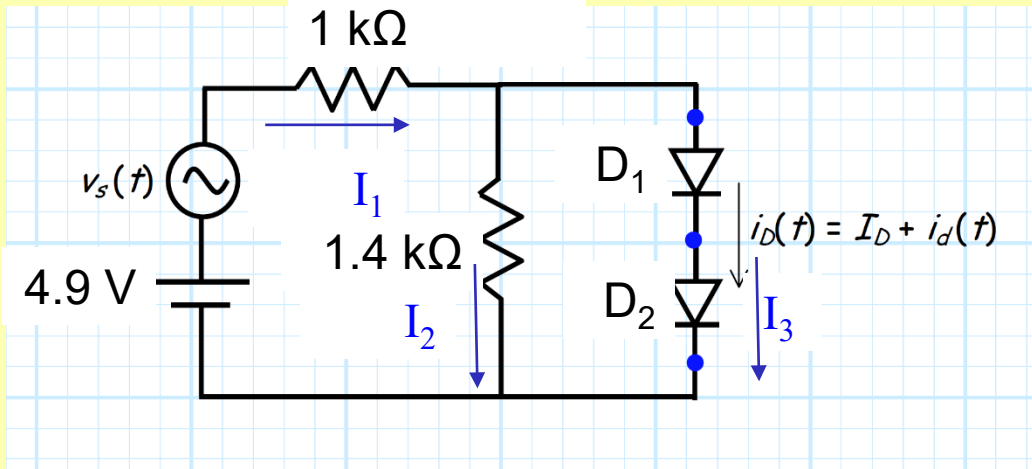
# Development of Diode Small-Signal Model



**Diode behaves as a resistor for a small signal perturbation!**

# Exercise #11: Small Signal Model

$$v_s(t) = 0.100 \sin \omega_0 t \text{ V}$$



Assume constant-voltage-drop model ( $V_D = 0.7 \text{ V}$ ) and  $V_T = 25 \text{ mV}$  for both diodes,

- 1) Determine  $r_d$  for  $D_1$  and  $D_2$ .
- 2) Build a small signal model for the circuit
- 3) Find  $i_d(t)$  and  $v_d(t)$  [note the subscript!]

**Ans:**

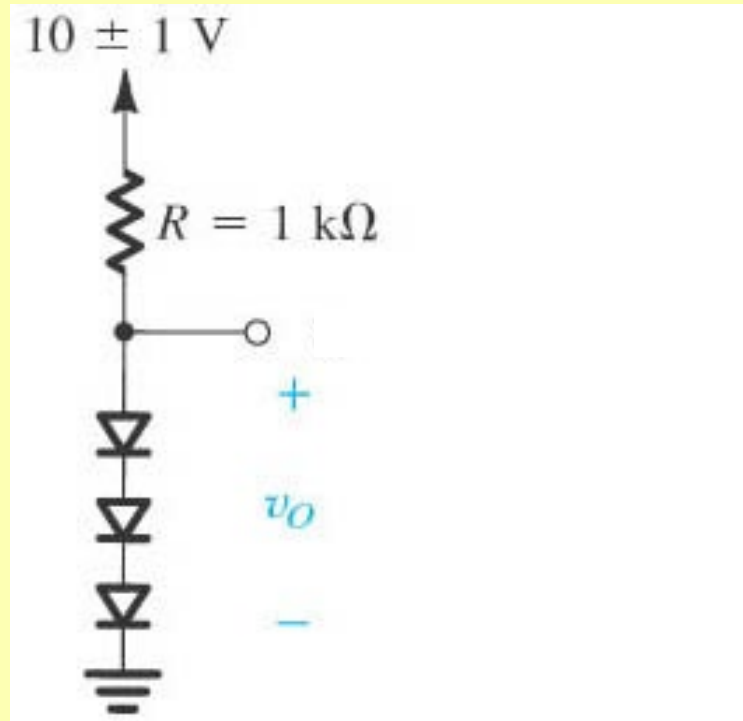
1)  $r_d = 10 \Omega$

3)  $v_d(t) = 0.97 \sin \omega_0 t \text{ mV}$  and  $i_d(t) = v_d(t) / r_d = 0.097 \sin \omega_0 t \text{ mA}$

Or  $v_d(t) \simeq \sin \omega_0 t \text{ mV}$  and  $i_d(t) \simeq 0.1 \sin \omega_0 t \text{ mA}$



# Exercise #12



**What is the output voltage fluctuation for 2 volt peak to peak fluctuation of the supply voltage?**

*(assume real diodes and use the constant voltage drop model of 0.7 V per diode)*

*Ans:  $v_o = 2.1 \text{ V} \pm 9.5 \text{ mV}$*

# Exercise #13

1) Find  $v_o/v_s$  ?

Assume that

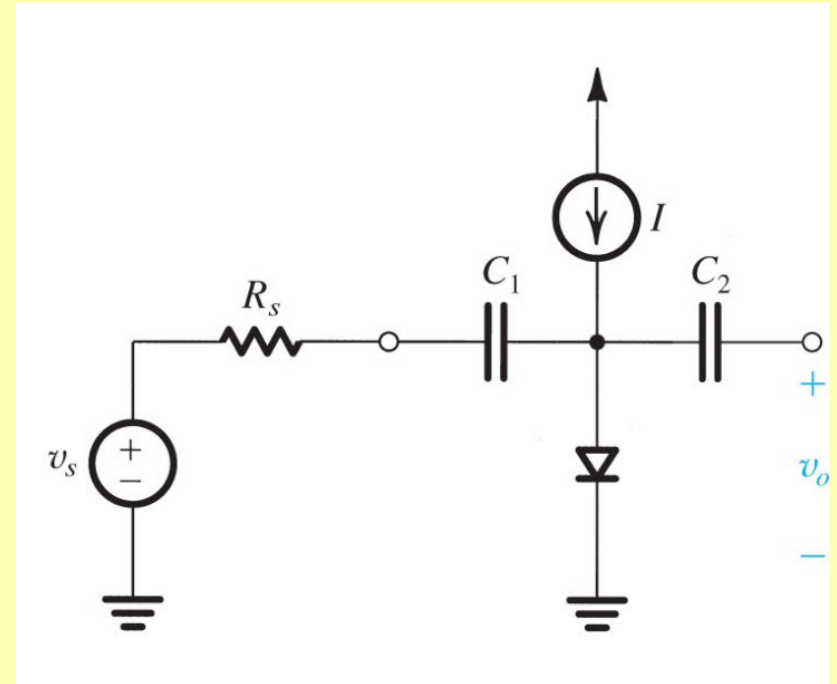
- $C_1$  and  $C_2$  are very large
- $I$  is DC

*Ans:*  $v_o = v_s \frac{V_T}{V_T + IR_S}$

2) Convince yourself that the circuit is the small-signal attenuator.

3) How can this circuit act as a variable attenuator?

*Ans: By changing dc bias  $I$ .*



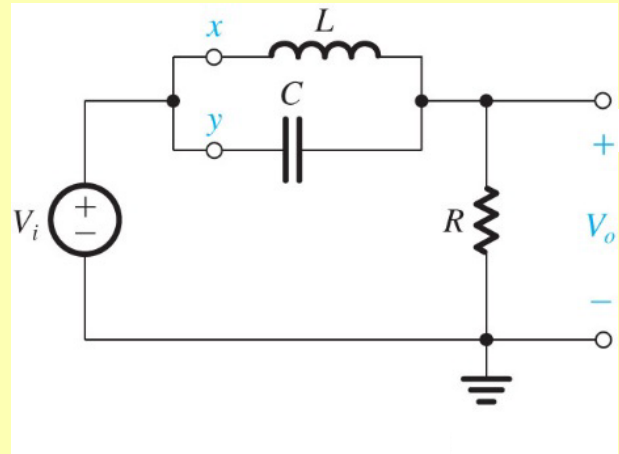
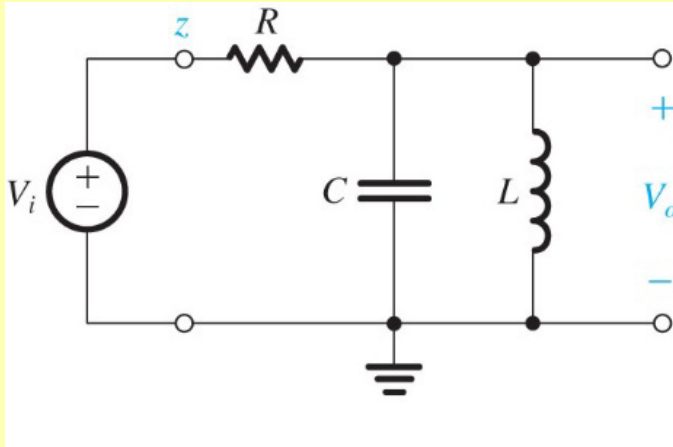
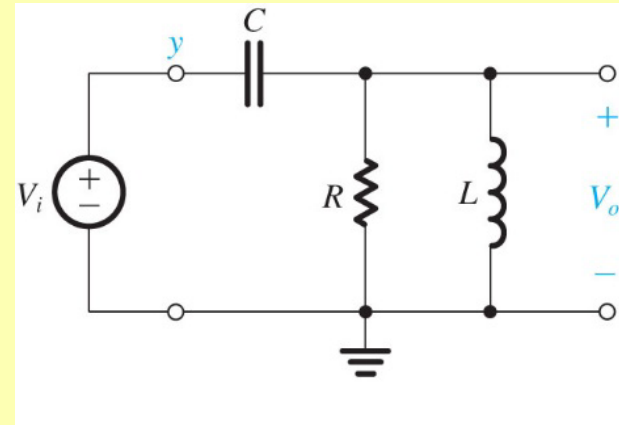
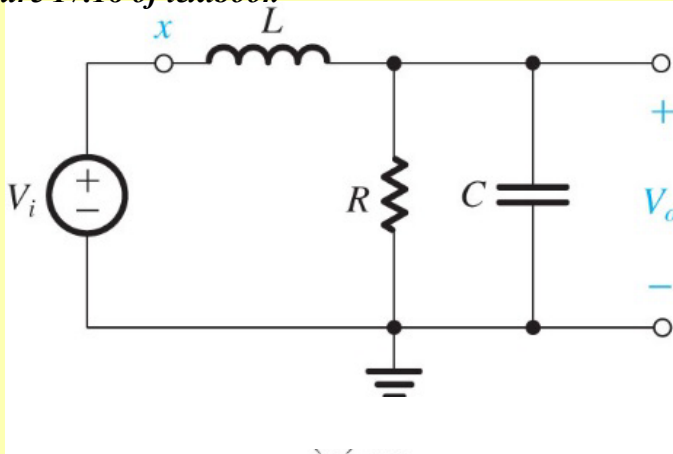
*Based on Problem 4.48*



# Filter Review - Intuitive Analysis

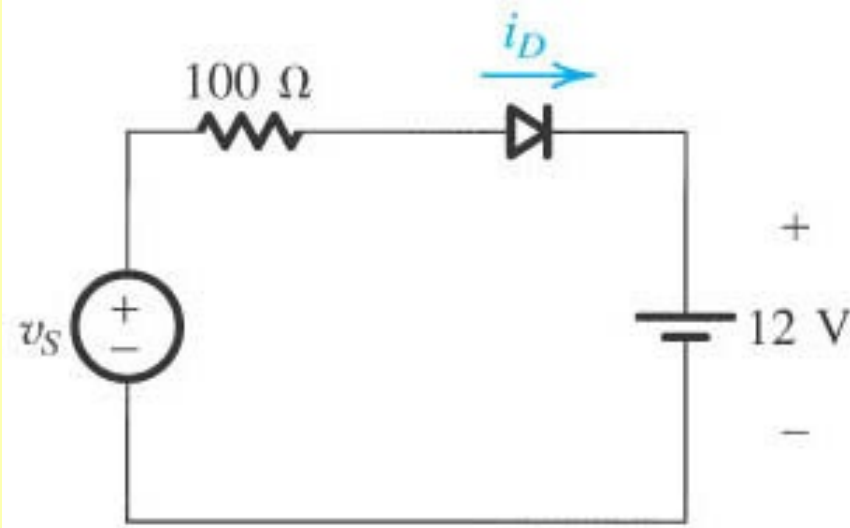
For each circuit: 1) find  $T(0)$ , 2)  $T(\infty)$ , 3) identify the filter type, and 4) draw bode plot for  $T(\omega)$ .

Based on Figure 17.18 of textbook



# Exercise #14: 12 V Battery Charger

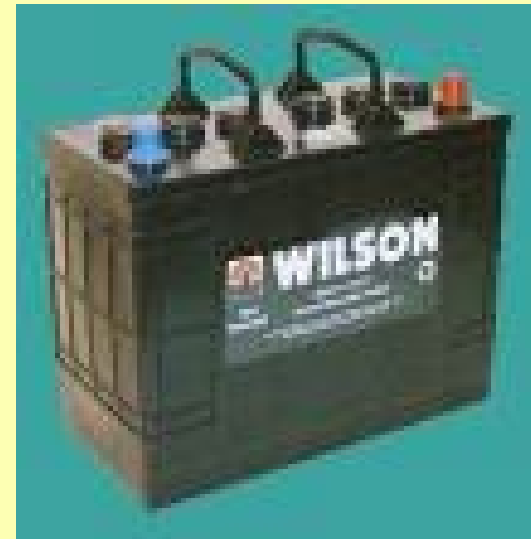
*Based on Example 4.1 of textbook*



$v_S = 24\text{ V}$  peak sinusoid

**Find**

- a) Fraction of each cycle diode conducts
- b) Peak diode current
- c) Max reverse voltage across diode



# Exercise #14: 12 V Battery Charger

**Ans.**

**a)  $\frac{\frac{2\pi}{3}}{2\pi} = \frac{1}{3}$  or 33%**

**b) 0.12 A**

**c) PIV=36 V**

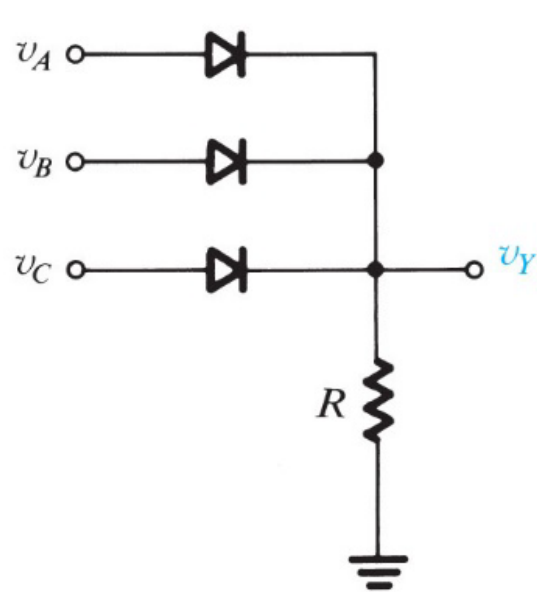


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# **ANOTHER APPLICATION: DIODE LOGIC GATES**

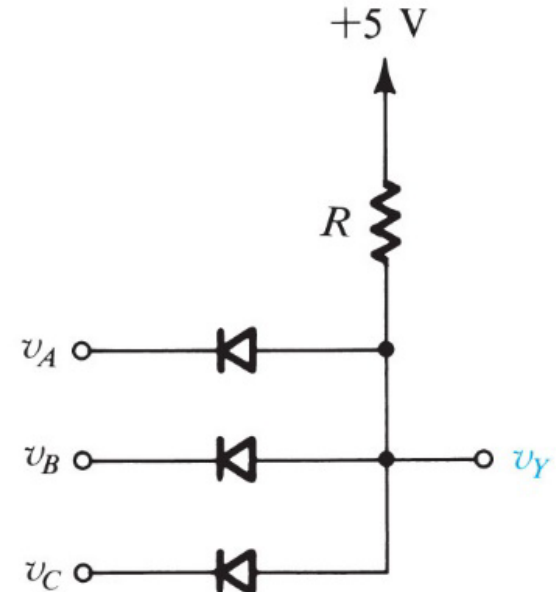


# Diode Logic Gates



**OR gate:**

$$Y = A + B + C$$



**AND gate:**

$$Y = A \cdot B \cdot C$$

