Lecture 3 Chemical Kinetics and Chemical Equilibrium

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 v_a, v_b, v_c , etc. are stoichiometric coefficients in a chemical balance equation where A, B, C, D are chemical formulae.

Then
$$\nu_a A + \nu_b B \leftrightarrow \nu_c C + \nu_d D$$

There are forward and reverse (backward) reaction rates here: Ω_{ab} and Ω_{cd}

 C_a , C_b , C_c , C_d are concentrations in (moles/volume)

$$\Omega_{ab} = -\frac{1}{\nu_a} \frac{dC_a}{dt} \Big|_{forward} = k_{ab} C_a^{\nu_a} C_b^{\nu_b} \qquad \qquad \Omega_{cd} = -\frac{1}{\nu_c} \frac{dC_c}{dt} \Big|_{reverse} = k_{cd} C_c^{\nu_c} C_d^{\nu_d} \\
= -\frac{1}{\nu_b} \frac{dC_b}{dt} \Big|_{forward} = -\frac{1}{\nu_a} \frac{dC_d}{dt} \Big|_{reverse} = +\frac{1}{\nu_a} \frac{dC_a}{dt} \Big|_{reverse}$$

 k_{ab} is a specific rate constant

$$\Omega_{cd} = -\frac{1}{\nu_c} \frac{dC_c}{dt} \bigg|_{reverse} = k_{cd} C_c^{\nu_c} C_d^{\nu_d}
= -\frac{1}{\nu_d} \frac{dC_d}{dt} \bigg|_{reverse} = +\frac{1}{\nu_a} \frac{dC_a}{dt} \bigg|_{reverse} = +\frac{1}{\nu_b} \frac{dC_b}{dt} \bigg|_{reverse}$$

 k_{cd} is a specific rate constant

Equilibrium Constant $K_p(T)$

At chemical equilibrium there is no net change so that: $\Omega_{ab} = \Omega_{cd}$ and $k_{ab}C_a^{\nu_a}C_b^{\nu_b} = k_{cd}C_c^{\nu_c}C_d^{\nu_d}$

$$\frac{k_{ab}}{k_{cd}} = \frac{C_c^{\nu_c} C_d^{\nu_d}}{C_a^{\nu_a} C_b^{\nu_b}}$$

Note that:

$$\frac{dC_a}{dt} = 0 = \frac{dC_a}{dt} \bigg|_{fwrd} + \frac{dC_a}{dt} \bigg|_{rev}$$

Partial pressure: $P_i = \frac{n_i}{V}RT$

For a perfect gas

So:
$$C_i = \frac{P_i}{RT}$$
 $P_i = C_i RT = C_i W_i \frac{R}{W_i} T = \rho_i R_i T$
$$\frac{k_{ab}}{k_{cd}} = \frac{P_c^{\nu_c} P_d^{\nu_d}}{P_a^{\nu_a} P_b^{\nu_b}} (RT)^{\nu_a + \nu_b - \nu_c - \nu_d}$$

$$K_{p}(T) = \frac{P_{c}^{\nu_{c}} P_{d}^{\nu_{d}}}{P_{a}^{\nu_{a}} P_{b}^{\nu_{b}}} = \frac{k_{ab}}{k_{cd}} (RT)^{\nu_{c} + \nu_{d} - \nu_{a} - \nu_{b}}$$

Where $K_p(T) = \exp\left[-\frac{\Delta G^{\circ}(T)}{RT}\right] = \exp\left[\frac{G^{\circ}ab - G^{\circ}cd}{RT}\right]$

G is Gibbs Free Energy G° is the value at one atmosphere

$$G = H - TS$$

Since K_p is a function of T, we expect k to be a function of T also. In fact, we find that:

$$k = aT^{\lambda} \exp\left[-\frac{(G^* - G)}{RT}\right]$$
 Note: $\ln K_p = \frac{\Delta G}{RT}$

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$$\ln K_p = \ln k_{ab} - \ln k_{cd} + [(\nu_c + \nu_d) - (\nu_a + \nu_b)] \ln RT$$

$$\ln K_p \approx \ln k_{ab} - \ln k_{cd}$$

The remaining dependence on temperature is not that strong!

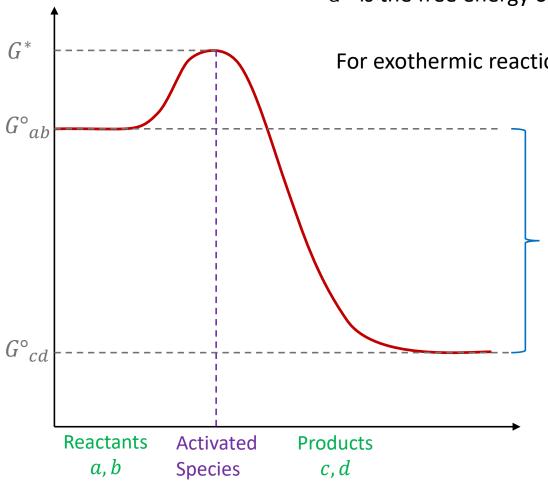
So:
$$\ln K_p \approx \ln k_{ab} - \ln k_{cd} = \frac{G^{\circ}_{ab} - G^{\circ}_{cd}}{RT}$$

$$\ln K_p = -\frac{G^* - G^{\circ}_{ab}}{RT} + \frac{G^* - G^{\circ}_{cd}}{RT}$$

Then we can consider:
$$k_{ab} =$$

Then we can consider:
$$k_{ab} = A \exp \left[-\frac{G^* - G^{\circ}_{ab}}{RT} \right]$$
; $k_{cd} = A \exp \left[-\frac{G^* - G^{\circ}_{cd}}{RT} \right]$

 G^* is the free energy of an activated species



For exothermic reaction:
$$\exp\left[-\frac{\Delta G}{RT}\right] = \exp\left[-\frac{\Delta H}{RT}\right] \exp\left[-\frac{\Delta S}{R}\right]$$

$$\exp\left[-\frac{\Delta G}{RT}\right] = \exp\left[-\frac{E}{RT}\right] \exp\left[-\frac{\Delta S}{R}\right]$$

Energy release in reaction (heat of reaction)

E is the activation energy

$$E \equiv \Delta H$$

Consider as an example:

$$OH + CO \rightarrow HOCO \rightarrow H + OCO$$

A barrier exists for the reaction to occur; only a fraction of those colliding will react!

$$\Omega_{ab} = k_{ab} C_a^{\nu_a} C_b^{\nu_b}$$

$$\Omega_{ab} = \left(A C_a^{\nu_a} C_b^{\nu_b} \right) \exp \left[-\frac{G^* - G^{\circ}_{ab}}{RT} \right]$$

$$\Omega_{ab} = A C_a^{\nu_a} C_b^{\nu_b} \exp \left[-\frac{E}{RT} \right]$$

The definition of A follows from above

The backward reaction above would be an example of an exothermic reaction!

Suppose we heat 1 mole of CO_2 from standard temperature to $4880^{\circ}R$ How much dissociation occurs?

$$CO_2 \leftrightarrow xCO + yCO_2 + zO_2$$

Initially: 1 CO₂

Finally:
$$(1-x)CO_2$$
, xCO , $\frac{x}{2}O_2$

$$CO + \frac{1}{2}O_2 \leftrightarrow CO_2$$

• Oxygen:
$$2 = x + 2y + 2z$$

• Carbon: $1 = x + y \to y = 1 - x$ $z = \frac{x}{2}$

$$n_{CO_2} = 1 - x, n_{CO} = x, n_{O_2} = \frac{x}{2}$$

 $n = n_{CO_2} + n_{CO} + n_{O_2} = 1 + \frac{x}{2}$

n would be greater if other species were present, i.e. N_2

$$P_{CO_2} = \frac{n_{CO_2}}{n}P = \frac{1-x}{1+\frac{x}{2}}P$$

$$P = P_{CO_2} + P_{CO} + P_{O_2}$$
 is measured in atm!

$$P_{CO} = \frac{n_{CO}}{n}P = \frac{x}{1 + \frac{x}{2}}P$$

$$P_{O_2} = \frac{n_{O_2}}{n}P = \frac{\frac{x}{2}}{1 + \frac{x}{2}}P = \frac{x}{x + 2}P$$

Note that partial pressure and K_p remain the same if the number of moles is multiplied. Also, the formula for P_i does not change if n_i and n are replaced by molar density, n/V

$$K_p = \frac{P_{CO_2}}{P_{CO}P_{O_2}^{1/2}} = \frac{n_{CO_2}}{n_{CO}n_{O_2}^{1/2}} \frac{n^{1/2}}{P^{1/2}} = \frac{1 - x}{x} \left(\frac{2 + x}{x}\right)^{1/2} P^{-1/2} = 10.0 \text{ (at 4880°R)}$$

At 1 atmosphere, P = 1

$$\frac{1-x}{x} \left(\frac{2+x}{x}\right)^{1/2} P^{-1/2} = 10.0$$

$$(1-x)^2 (2+x) = 100x^3 \to 2 - 3x + 2x^2 + x^3 = 100x^3$$

$$2 - 3x + 2x^2 - 99x^3 = 0$$

Iterations: x = .272, x = .221, x = .232

So: x = 23%

This assumes only CO_2 , CO, and O_2 are present. In a practical case, exhaust would include other species and n would be modified!

Consider now: P = 10.0 atm

Then:

$$K_p = \frac{1 - x}{x} \left(\frac{2 + x}{x}\right)^{1/2} (10.0)^{-1/2} = 10.0$$

$$\frac{1 - x}{x} \left(\frac{2 + x}{x}\right)^{1/2} = 10.0\sqrt{10}$$

$$(1 - x)^2 (2 + x) = 1000x^3$$

$$2 - 3x - 999x^3 = 0$$

Iterations:
$$x = .1260$$
, $x = .1168$, $x = .1181$
So: $x \approx 11\% - 12\%$

The higher the pressure, the less dissociation since a smaller volume (fewer moles) is preferred!

Suppose we burn carbon in oxygen (no nitrogen)

y is given.

y = 1 is stoichiometric

y > 1 is excess air

$$C + yO_2 \leftrightarrow xCO + (1 - x)CO_2 + (y + \frac{x}{2} - 1)O_2$$

The products CO, CO_2 , and O_2 are in equilibrium

$$CO + \frac{1}{2}O_2 \leftrightarrow CO_2$$

$$K_p = \frac{P_{CO_2}}{P_{CO}P_{O_2}^{1/2}} = \frac{n_{CO_2}}{n_{CO}n_{O_2}^{1/2}} \frac{n^{1/2}}{P^{1/2}}$$

Now:

$$n = x + 1 - x + y + \frac{x}{2} - 1 = y + \frac{x}{2}$$

$$K_p = \frac{1 - x}{x \left(y + \frac{x}{2} - 1 \right)^{1/2}} \frac{\left(y + \frac{x}{2} \right)^{1/2}}{P^{1/2}}$$

Consider: P = 10.0 atm and T = 4880°R

$$K_p(T) = 10.0$$

$$K_p \sqrt{10} = \frac{1-x}{x\left(y+\frac{x}{2}-1\right)^{1/2}} \left(y+\frac{x}{2}\right)^{1/2} = 10.0\sqrt{10}$$

Consider y = 1

Then:

$$K_p \sqrt{10} = \frac{1-x}{x\left(\frac{x}{2}\right)^{1/2}} \left(1 + \frac{x}{2}\right)^{1/2} = 10.0\sqrt{10}$$

This is same as before: x = .118

Consider now excess oxygen, y = 2

Then:
$$K_p \sqrt{10} = \frac{1-x}{x\left(1+\frac{x}{2}\right)^{1/2}} \left(2+\frac{x}{2}\right)^{1/2} = 10.0\sqrt{10}$$

$$(1-x)^2 \left(2 + \frac{x}{2}\right) = 1000x^2 \left(1 + \frac{x}{2}\right)$$

$$499.5x^3 + 999x^2 + \frac{7}{2}x - 2 = 0$$

Iterations lead to x = 0.0426

So: $x \approx 4\% - 5\%$

Excess oxygen drives reaction toward completion!

If y < 1 by a slight amount, the same formula holds, but for y too small, no solution may exist! This indicates that carbon may exist in the products and we should consider:

$$C + CO_2 \leftrightarrow 2CO$$
 As the equilibrium condition

Note that if other species are present, their pressure must be considered in calculating the total number of moles, n.

Example: 1 mole of CO_2 , 3.76 moles of N_2

$$K_p = \frac{P_{CO_2}}{P_{CO}P_{O_2}^{1/2}}$$

$$\bullet \quad n_{CO_2} = 1 - x$$

•
$$n_{CO} = x$$

$$\bullet \quad n_{O_2} = \frac{x}{2}$$

$$n = 3.76 + 1 - x + x + \frac{x}{2} = 4.76 + \frac{x}{2}$$