

MAE 158 Fall 2024

Lecture 2

Announcements: Discussions start this week

Today's Objectives: Fluid Mechanics Review ^{shevell ch. 6}
Atmosphere ^{ch. 5}
Nature of Aerodynamic Forces ^{ch. 3}

Last time:

Conservation of Mass:
(continuity)

$$\rho_1 A_1 U_1 = \rho_2 A_2 U_2$$

if incompressible:

$$A_1 U_1 = A_2 U_2$$

Conservation
of momentum:

$$P_2 + \rho \frac{U_2^2}{2} = P_1 + \rho \frac{U_1^2}{2}$$

↳ Bernoulli's equation
for incompressible, inviscid,
& along a streamline

also

$$P + \frac{1}{2} \rho U^2 = \text{const}$$

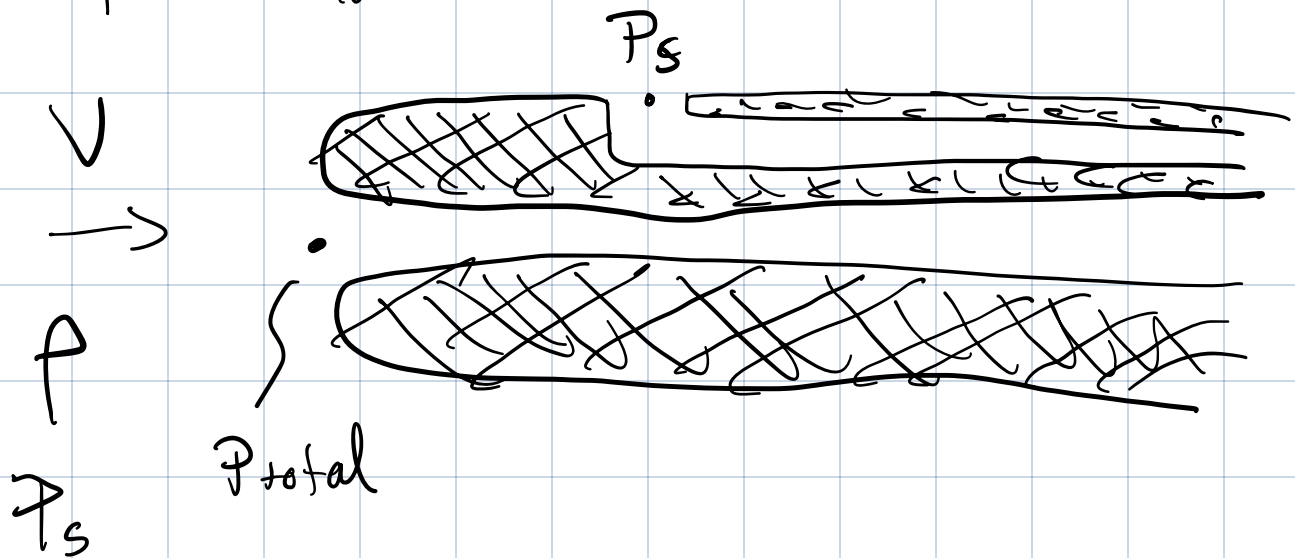
↳ Relation between P, U

Finally, equation of state,

$$P = \rho R T \quad @ \text{ some point}$$

Airspeed Indicators

Pitot Static tube



$$P_{total} = P_s + \frac{1}{2} \rho V^2$$

$$\frac{1}{2} \rho V^2 = P_{total} - P_s$$

$$\hookrightarrow V = \sqrt{\frac{2}{\rho} (P_{total} - P_s)}$$

$$L = \frac{1}{2} \rho V^2 S_{REF} C_L$$

$$\downarrow \frac{1}{2} \rho V^2 \rightsquigarrow \rho @ \text{altitude}$$

$\rightsquigarrow V_{\text{true airspeed}}$

true velocity of airplane wRT the air it is flying through

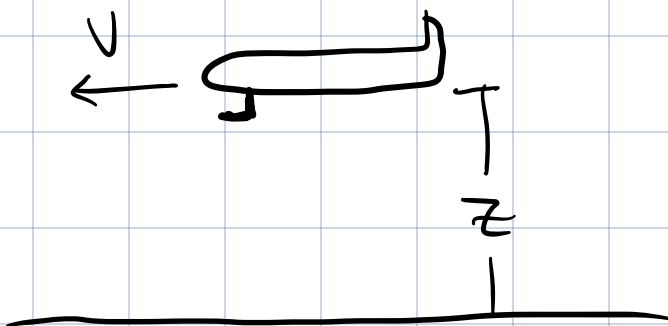
$$V_{\text{Reading}} \Rightarrow V_{\text{equivalent airspeed}} = V_{\text{indicated (incompressible flow)}}$$

$$\rho_{\text{sealevel}} \rightarrow \Delta P = \frac{1}{2} \rho \underset{\uparrow}{V}^2$$

$$\rho_{\text{sealevel}} \cdot \frac{V_{\text{ind}}^2}{2} = \Delta P = \frac{\rho @ \text{altitude} \cdot V_{\text{true}}^2}{2}$$

$$\underline{V_{\text{true}}} = \underset{\approx}{V_{\text{ind}}} \cdot \left(\frac{\rho_{\text{sealevel}}}{\rho @ \text{altitude}} \right)^{1/2}$$

ex:



@ z,

$$\rho = 0.00175 \frac{\text{slugs}}{\text{ft}^3}$$

$$V = 180 \text{ KIAS}$$

$$\sim 1.69 \text{ ft/s} / \text{knot}$$

indicated Airspeed (knots)

$$= 300 \text{ ft/s}$$

True airspeed
in knots: KTAS

What is the Drag (lbs)

Assume $S_{REF} = 1000 \text{ ft}^2$
 $C_D = 0.01$

$$D = \frac{1}{2} \rho V^2 S_{REF} \cdot C_D$$

$$\rho_{SL} = 0.00238 \frac{\text{slugs}}{\text{ft}^3}$$

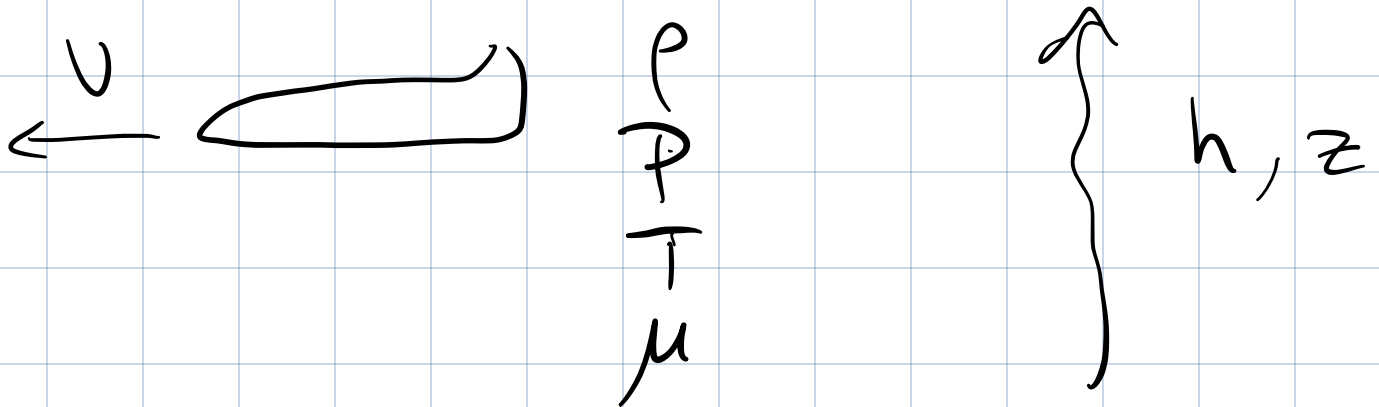
$$D = \frac{1}{2} \rho V^2 S_{REF} \cdot C_D = \frac{1}{2} \rho_{alt} \cdot V_{true}^2 S_{REF} \cdot C_D$$

$$= \frac{1}{2} \rho_{SL} \cdot V_{ind}^2 S_{REF} C_D$$

$$= \frac{1}{2} 0.00238 \frac{\text{slug}}{\text{ft}^3} \cdot (300 \text{ ft/s})^2 \cdot 1000 \text{ ft}^2 \cdot 0.01$$

$$= 1100 \text{ lbs} \sim$$

Atmosphere



"Standard Atmosphere" \rightarrow to get
Representative conditions

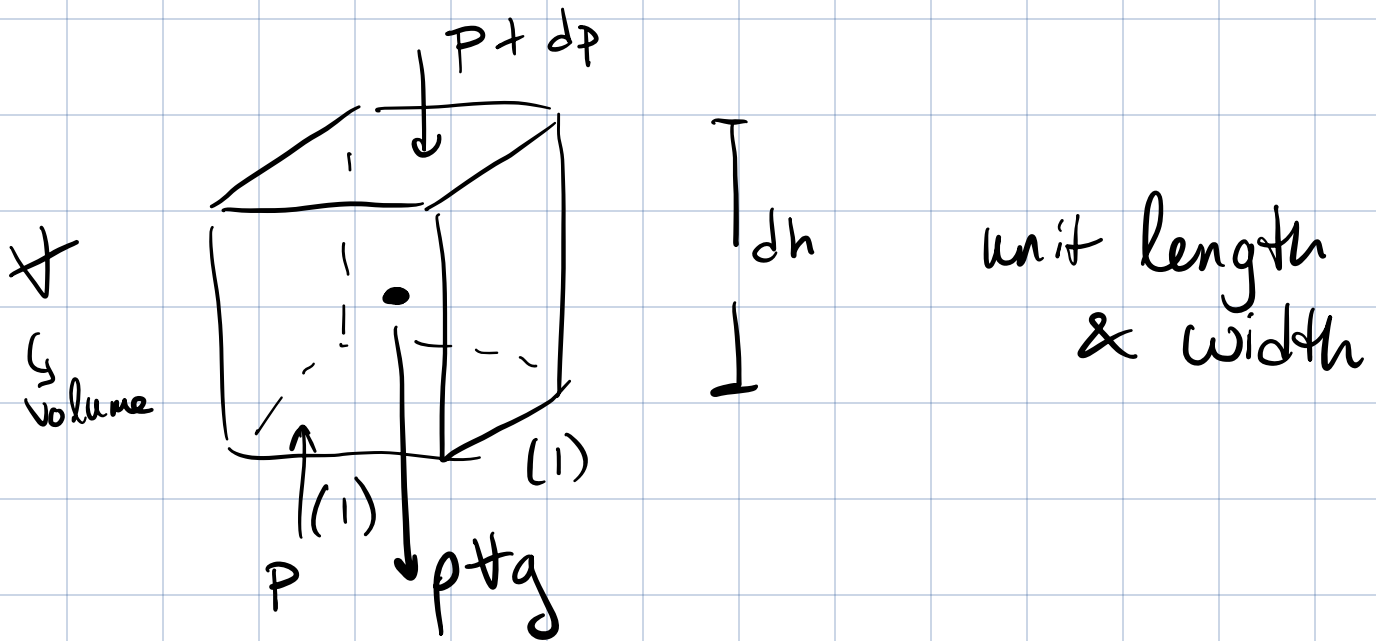
Sea level standard conditions

$$\begin{aligned} - \rho_{SL} &= 0.00238 \frac{\text{slug}}{\text{ft}^3} \\ &= 1.22 \text{ kg/m}^3 \end{aligned}$$

$$\begin{aligned} - P_{SL} &= 2116.2 \text{ lb/ft}^2 \\ &= 1.01325 \times 10^5 \text{ N/m}^2 \end{aligned}$$

$$\begin{aligned} - T &= 518.69 \text{ R} \\ &= 288.15 \text{ K} \end{aligned}$$

- hydrostatics (fluid element @ REST)



Forces acting:

Bottom: $P(1)(1)$

top: $(P + dp)(1)(1)$

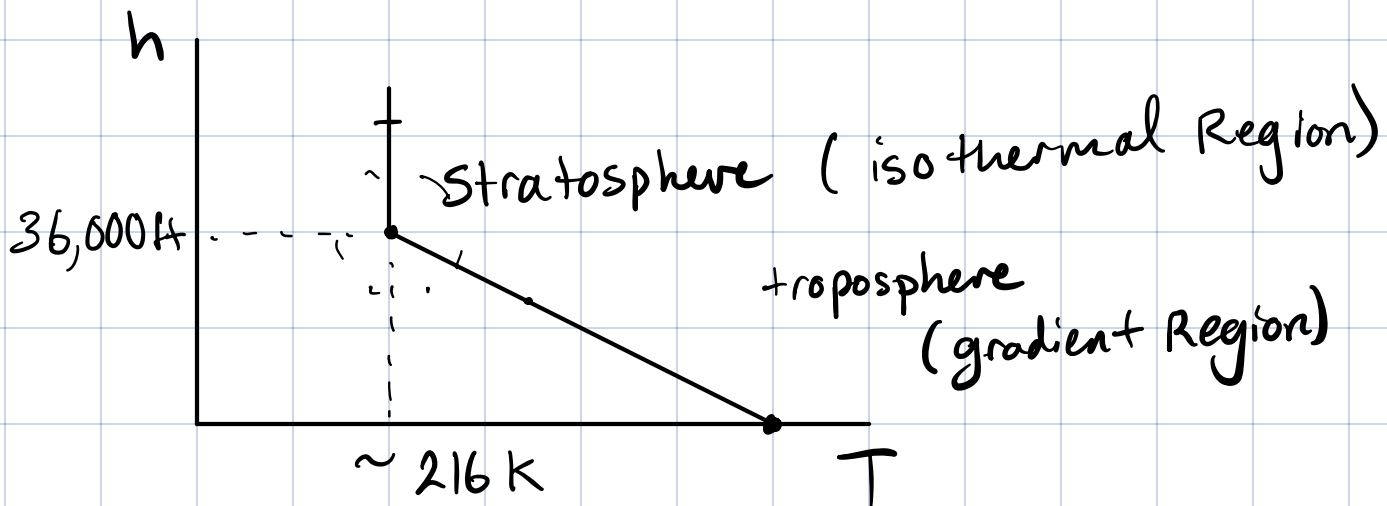
weight: $\rho \Delta g = \rho g (1)(1)(dh)$

$$P(1)(1) - (P + dp)(1)(1) - \rho g (1)(1)dh = 0$$

$$\rightarrow dp = -\rho g dh$$

↳ hydrostatics equation

$$\hookrightarrow g \approx \phi = 32.2 \text{ ft/s}^2, 9.8 \frac{\text{m}}{\text{s}^2}$$



divide the
hydrostatics
equation
by equation
of state

$$\frac{dp}{p} = \frac{-\cancel{p}g dh}{\cancel{p}RT} = \frac{-g}{RT} dh$$

Iso thermal Region $T = \phi$

$$\int \frac{dp}{p} = \frac{-g}{RT} \int dh$$

$$\rightarrow \ln\left(\frac{p}{p_1}\right) = \frac{-g}{RT} (h - h_1)$$

$$\hookrightarrow \frac{p}{p_1} = e^{-g/RT (h - h_1)}$$

$$\frac{P}{P_1} = \frac{\cancel{P} \cancel{RT}}{\cancel{P_1} \cancel{RT_1}} \rightarrow \frac{P}{P_1} = \frac{P}{P_1}$$

iso thermal
Region

$$\frac{P}{P_1} = e^{-g/RT(h-h_1)} = \frac{P}{P_1}$$

gradient Region \rightarrow T is linear

$$T = T_1 + a(h-h_1)$$

\uparrow lapse Rate

$$= \frac{dT}{dh} \rightarrow dh = \frac{1}{a} dT$$

$$a \approx -0.00356 \text{ R/ft}$$

$$= -0.0065 \text{ K/m}$$

plug in

hydrostatics equation, divide by
equation of state

$$\frac{dP}{P} = \frac{-g}{R \cdot a} \frac{1}{T} dT$$

$$\text{thus } \int \frac{dP}{P} = -\frac{g}{Ra} \int \frac{dT}{T}$$

$$\hookrightarrow \boxed{\frac{P}{P_1} = \left(\frac{T}{T_1}\right)^{-\gamma/\alpha R}}$$

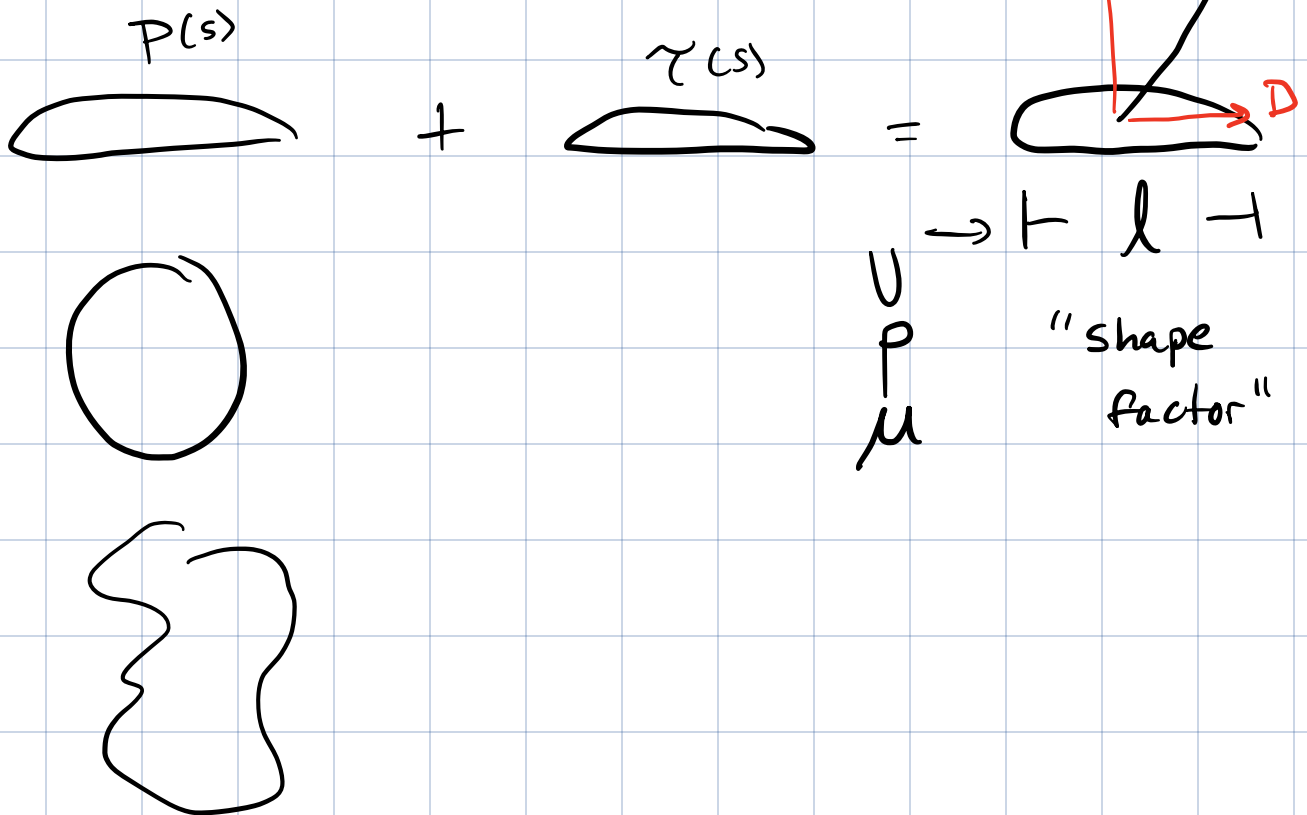
gradient Region

$$\frac{P}{P_1} = \frac{\cancel{P} \cancel{R} T}{\cancel{P_1} \cancel{R} T_1} = \frac{P T}{P_1 T_1}$$

thus,

$$\boxed{\frac{P}{P_1} = \left(\frac{T}{T_1}\right)^{-(\gamma/\alpha R + 1)}}$$

Nature of Aerodynamic forces (ch 3)



Drag \rightarrow force impeding forward motion

Lift \rightarrow force serving to lift body upward

$$F = f(\rho, \mu, V, l, \text{shape})$$

dimensional analysis, Π -theorem,
can get an algebraic expression
for this Relation

$$F = \rho^a \mu^b V^c l^d \cdot C$$

\uparrow shape factor

dimensions : M = mass
 L = length
 T = time

$$F = ma \Rightarrow \frac{ML}{T^2}$$

$$\rho = \text{mass/volume} \Rightarrow \frac{M}{L^3}$$

$$V = \text{length} / \text{time} \Rightarrow L / T$$

$$l = \text{length} \Rightarrow L$$

$$\mu = \tau / \frac{du}{dy} \Rightarrow \frac{MLT^{-2}L^{-2}}{LT^{-1}L^{-1}}$$

$$\Rightarrow \frac{M}{LT}$$

$$\tau = \mu \frac{du}{dy}$$

$$\text{dimensions } F = \text{dimensions } \rho^a \mu^b V^c l^d$$

$$\frac{ML}{T^2} = \left(\frac{M}{L^3}\right)^a \left(\frac{M}{LT}\right)^b \left(\frac{L}{T}\right)^c L^d$$

$$M : 1 = a + b$$

$$L : 1 = c + d - 3a - b$$

$$T : -2 = -b - c$$

solve in terms of b :

$$a = 1 - b$$

$$c = 2 - b$$

$$d = 2 - b$$

} Plug in to F

$$F = \rho^{1-b} \mu^b V^{2-b} l^{2-b} \cdot C$$

$$= \underbrace{\rho V^2 l^2} \left(\underbrace{\frac{\mu}{\rho V l}} \right)^b \cdot C$$

$$\frac{\rho V l}{\mu} \equiv \text{Reynolds Number} = \frac{Re}{RU}$$

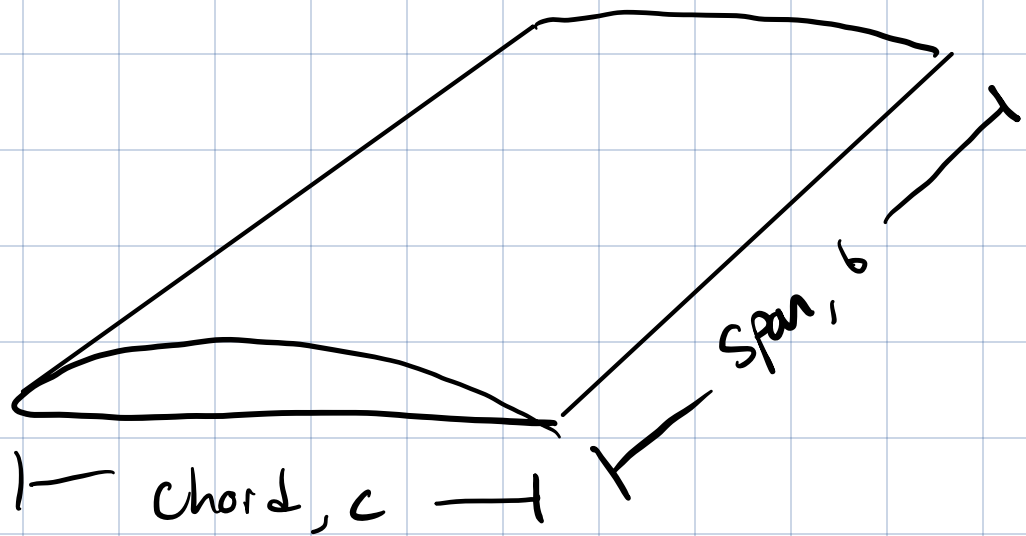
call $C \cdot \left(\frac{\mu}{\rho V l} \right)^b \rightarrow$ some coefficient
that is a function
of shape, Re

$$C_F \equiv \text{force coefficient}$$

$$2 \cdot C \left(\frac{\mu}{\rho V l} \right)^b$$

$$F = \frac{1}{2} \rho V^2 \cdot \underset{\substack{\downarrow \\ S_{REF}}}{l^2} \cdot C_F$$

in general for an aircraft wing
 S_{REF} is planform area



if wing is Rectangular, no fuse
 $S_{REF} = C \cdot b$