

# MAE 158 Lecture 15

Nov 18 2024

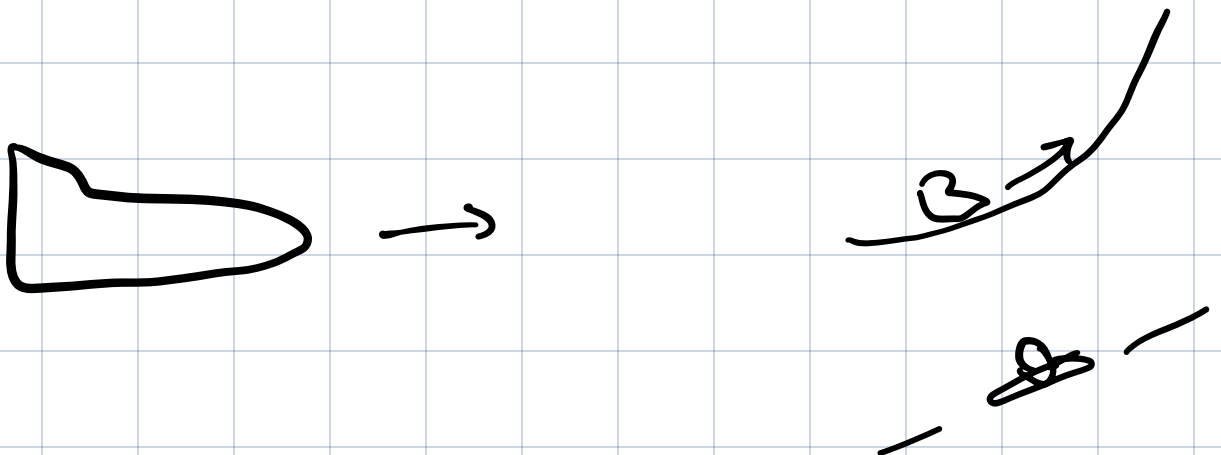
Announcements: Week 8 HW posted

Today's objectives: Turning performance

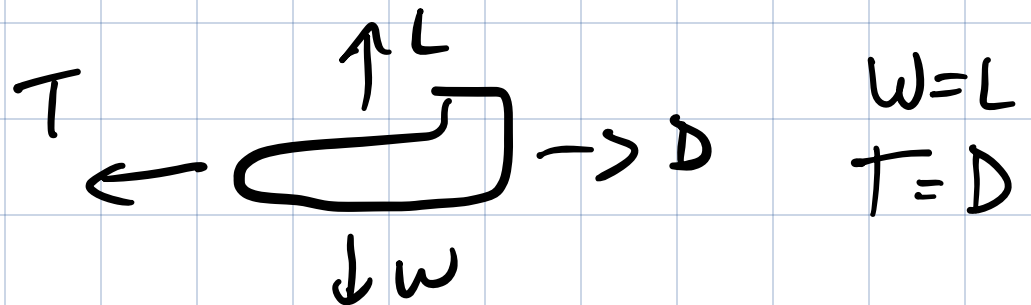
turning Performance:

- pilots use controls in order to manipulate flight path

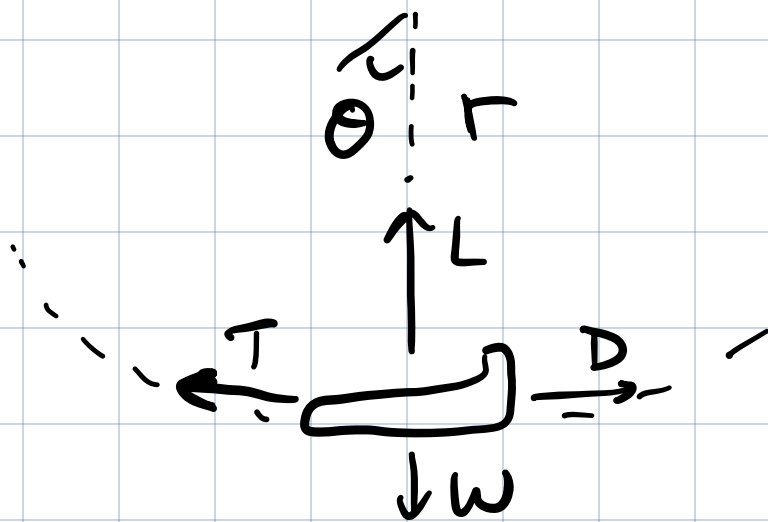
- ↳ Rudders, elevators, ailerons, differential thrust etc...



consider a few turn procedures  
compared to SLF



pullup maneuver (flare maneuver)



pilot pull back  
on control stick,  
& A/C move  
in a curved  
flight path,  
 $L > W$

define  $n \equiv \text{load factor} = \frac{L}{W}$

if  $n=1$  ( $L=W$ ) means

A/c experiences 1 "g" of load

if  $n = 3 \rightarrow 3$  "g's"

$$r = \frac{V^2}{g(n-1)}$$

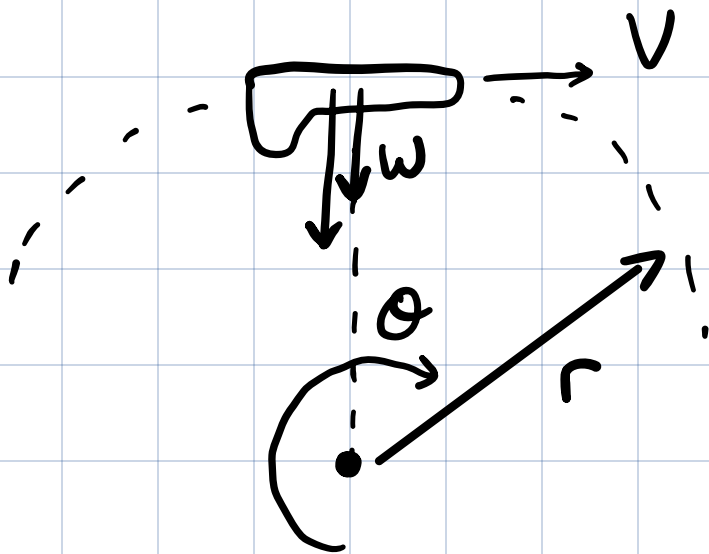
turn Radius

$$\frac{d\theta}{dt} = \omega = \frac{V}{r} = g \frac{(n-1)}{V}$$

$\uparrow$   
omega

turn Rate

pull-down maneuver:



turn Rate &  $r$ ?

forces  $\perp$  to  
flight path

$$\frac{mV^2}{r} = L - W \cos \theta$$

$$\theta = 180^\circ$$

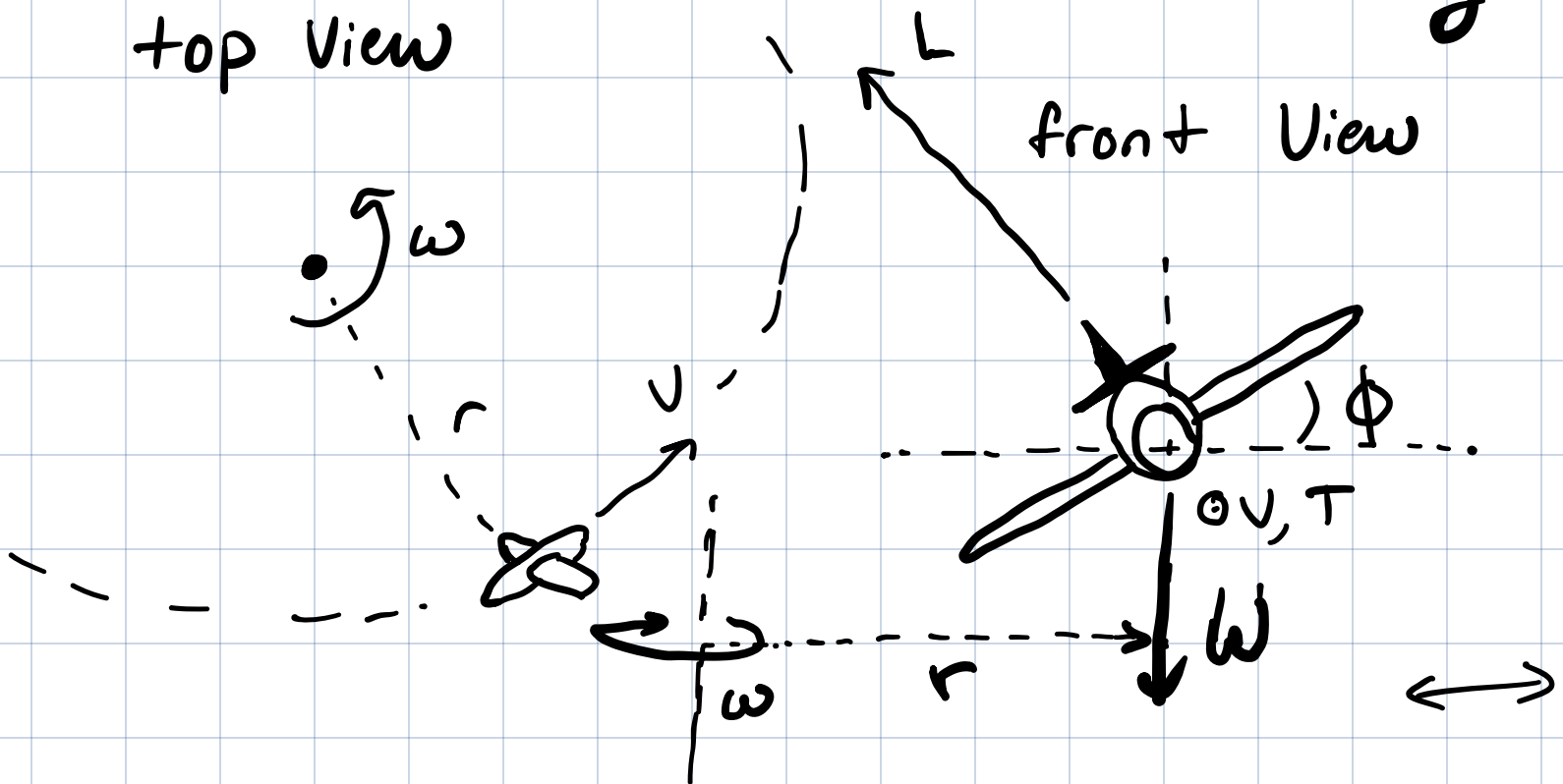
$$\rightarrow \frac{mV^2}{r} = L + W$$

$$\left. \begin{aligned} r &= \frac{mv^2}{(L+W)} = \frac{1}{g} \frac{v^2}{(n+1)} \\ \omega &= \frac{g(n+1)}{v} \end{aligned} \right\} \text{pull down maneuver}$$

turning in a level plane  
(Banking)

top View

## front + View



- Lift vector turn inwards
- Wing @  $\phi$  w.r.t the horizontal

$$\therefore L \cos \phi = W \quad \phi \equiv \text{Bank angle}$$

lateral forces

$$L \sin \phi = \frac{mV^2}{r}$$

also  $\cos \phi = \frac{W}{L} = \frac{1}{n}$

bank angle corresponds directly  
to load factor

$$r = \frac{mV^2}{L \sin \phi} = \frac{1}{n} \frac{V^2}{g \sin \phi}$$

Recall  $\cos^2 \phi + \sin^2 \phi = 1$

thus  $\left(\frac{1}{n}\right)^2 + \sin^2 \phi = 1$

then  $r = \frac{V^2}{g\sqrt{n^2-1}}$   $\omega = \frac{V}{r} = \frac{g\sqrt{n^2-1}}{V}$

turn Radius

turn Rate

total distance traveled in  
a turn on level  
plane?

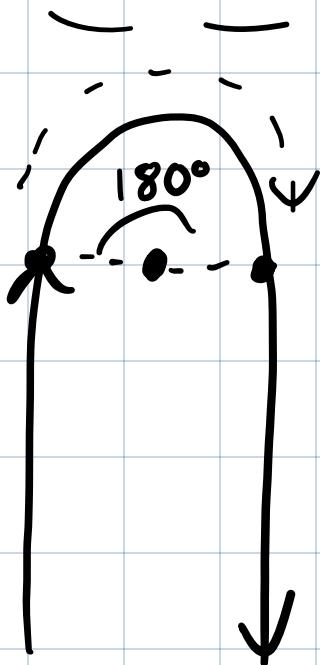
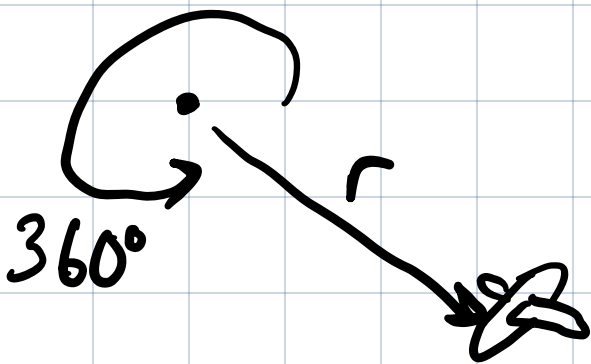
total distance

$2\pi r$  if  
travel  $360^\circ$

can get time from  
 $\omega$

if I want to  
minimize  $r$   
& maximize  $\omega$

- low  $V$   
- high  $n$  } what  
are  
these



limits?

## n constraints

- structural limits of aircraft

1. limit load factor:  
permanent damage occurs

2. ultimate load factor:  
structural failure occurs  
(AKA, something breaks)

$n_{\max, \text{structural}}$   $\sim 2$  commercial  
 $\sim 7-8$  military

- thrust constraint:

· in a level turn, lift will increase by a ratio of  $1/\cos\phi$

· if you increase  $L$ , induced drag  $\uparrow$

@ a given  $V$ ,  $T_R \uparrow$  in the turn as a function of  $1/\cos\phi$  in the induced drag

$\phi$  limited by thrust available

$n_{\text{thrust constraint}}$ ,  $\text{Drag} = \text{Thrust}$   
 $= \frac{1}{2}\rho V^2 S (C_{DP} + K C_L^2)$

$$C_L = \frac{n \cdot 2W}{\rho V^2 S}, \quad K = \frac{1}{\pi A e}$$

$\downarrow$

$$\text{Thrust} = \frac{1}{2}\rho V^2 S \left( C_{DP} + K \left( \frac{n \cdot 2W}{\rho V^2 S} \right)^2 \right)$$

$\uparrow$   $T_{A, \text{max}}$   $\uparrow$   $n_{\text{thrust constraint}}$



$$\underline{n_{\text{thrust constraint}}} = \left[ \left( \frac{\frac{1}{2} \rho V^2}{K \frac{W}{S}} \right) \left( \frac{T_{A \max}}{W} - \frac{\frac{1}{2} \rho V^2 C_{Dp}}{W/S} \right) \right]^{\frac{1}{2}}$$

$n_{C_{L \max}, \text{constraint}}$

@ a given  $V$  in the turn  
you need corresponding  
 $C_L$  to get necessary lift

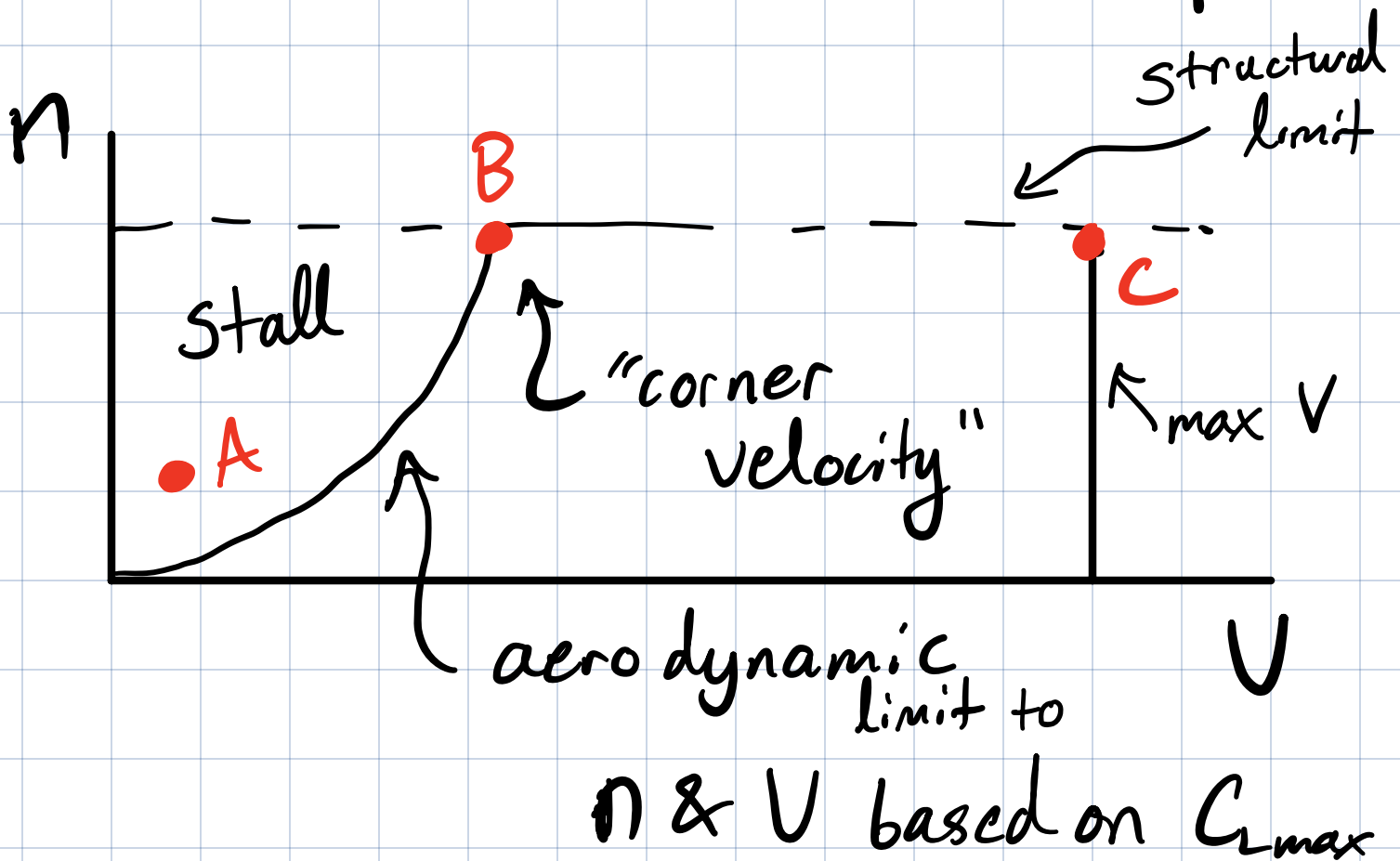
@ desired  $\phi$

$$n = \frac{L}{W} = \frac{\frac{1}{2} \rho V^2 S C_L}{W}$$

@ a given  $\uparrow$  Velocity constrained by  $C_{L \max}$

$$\underline{n_{C_{L \max} \text{ constraint}}} = \frac{\frac{1}{2} \rho V^2 S C_{L \max}}{W}$$

$V$ - $n$  diagram  $\rightarrow$  "flight envelope"



Which point leads to  
"Best turn performance?"

$A$  = Stalling

$B = \text{high } n \ \& \ \text{low } V$

$\rightarrow$  best turn performance

$C = \text{high } V$   
 $\quad \quad \& \ \text{high } n$

for a given problem,

It asked to determine

lowest  $r$  or fastest  $\omega$

$\rightarrow$  check  $n_{\text{struct}}$

$n_{\text{thrust}}$

$n_{C, \text{max}}$

} whichever  
is lowest  
is  
constraint

$\rightarrow$  @ a given  $V$

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because there is a tradeoff  
with  $n$  &  $V$ ,  
how do we get theoretical  
 $r_{\min}$  &  $\omega_{\max}$ ?

- $r_{\min}$  doesn't necessarily happen  
@  $n_{\max}$  because of  
dependence on  $V$

$$\frac{dr}{dV} = 0 = \frac{d}{dV} \left( \frac{V^2}{g\sqrt{n^2-1}} \right)$$

$\uparrow$   
 $n$  also  
depends on  $V$

full mathematical derivation  
Anderson ch. 6

$$\Rightarrow V_{rmin} = \sqrt{\frac{4K(\omega/s)}{P(T/\omega)}}$$

this is  $V$  @ theoretical  
minimum turn Radius

$$\text{also: } n_{rmin} = \sqrt{2 - \left[ \frac{4K C_{DP}}{(T/\omega)^2} \right]}$$

$$r_{min} = \frac{V_{rmin}^2}{g \sqrt{n_{rmin}^2 - 1}} = \frac{4K(\omega/s)}{g P(T/\omega) \sqrt{1 - 4K \frac{C_{DP}}{(T/\omega)^2}}}$$

↑ min turn Radius conditions

① a given  $T/W$  ratio

- but - iff  $V_{rmin}$  is below  
Stall velocity,  
then have to adjust  $V$  &  $n$   
& turn @ a higher radius

for max  $\omega$ :

$$\frac{d\omega}{dV} = 0 = \frac{d}{dV} \left( g \frac{\sqrt{n^2 - 1}}{V} \right)$$

Anderson ch. 6

$$\underline{V_{\omega_{\max}}} = \left[ \frac{2 \left( \frac{W}{S} \right)}{\rho} \right]^{\frac{1}{2}} \left( \frac{K}{C_{Dp}} \right)^{\frac{1}{4}}$$

$$\underline{n_{\omega_{\max}}} = \left( \frac{\frac{T/W}{\sqrt{K C_{Dp}}} - 1}{\sqrt{K C_{Dp}}} \right)^{\frac{1}{2}}$$

$$\underline{\omega_{\max}} = g \cdot \sqrt{\frac{\rho}{W/S} \left[ \frac{T/W}{2 \cdot K} - \left( \frac{C_{Dp}}{K} \right)^{\frac{1}{2}} \right]}$$


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determine "theoretical min  
turn Radius"

$$W/S = 76.84 \text{ lb/ft}^2$$

$$K = 0.08$$

Sea level conditions

$$\rightarrow \rho = 0.00238 \text{ slug/ft}^3$$

$$T/w = 0.3795$$

$$C_{D,P} = 0.015$$

$$r_{\min} = \frac{V_{r_{\min}}^2}{g \sqrt{n_{r_{\min}}^2 - 1}} = \frac{4K (w/s)}{g \rho \left(\frac{T}{w}\right) \sqrt{1 - 4K \frac{C_{D,P}}{(T/w)^2}}}$$

$$= \frac{4 \cdot 0.08 (76.84 \text{ lb/ft}^2)}{(32.2 \frac{\text{ft}}{\text{s}^2}) (0.00238 \frac{\text{slug}}{\text{ft}^3}) (0.3795) \cdot}$$

$$\sqrt{1 - 4(0.08) \frac{0.015}{(0.3795)^2}}$$

$$= \underline{861 \text{ ft}}$$

"theoretical min"



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