

MAE 158 Lecture 13

Nov. 12th 2024

Announcements: Week 7 HW posted

Today's Objectives: Takeoff (accelerated flight)

Last time: $E_{\text{prop}} = \frac{\eta}{C_P} (2\rho S)^{1/2} \frac{C_L^{3/2}}{C_D} \left(\frac{1}{W^{1/2}} - \frac{1}{W_0^{1/2}} \right)$

from week 7 HW:

$$E_{\text{prop}} = 37.9 \frac{\eta}{C_P} \frac{C_L^{3/2}}{C_D} \sqrt{\frac{\sigma S}{W_0}} \left(\sqrt{\frac{W_0}{W_1}} - 1 \right)$$

$$\sigma = \frac{P}{P_{SL}}$$

move $\frac{1}{W_0^{1/2}}$ outside

$$E_{\text{prop}} = \frac{\eta}{C_P} \left(\frac{2\rho S}{W_0} \right)^{1/2} \frac{C_L^{3/2}}{C_D} \left(\left(\frac{W_0}{W_1} \right)^{1/2} - 1 \right)$$

$$\sigma \cdot \rho_{sl} = \rho$$

Note $550 \frac{\text{ft} \cdot \text{lb}}{\text{s}} = 1 \text{ hp}$

$$= \underbrace{2^{1/2} \rho_{sl}^{1/2}}_{\substack{\uparrow \\ \frac{\text{lb}}{\text{BHP} \cdot \text{hr}}}} \frac{\eta}{C_P} \left(\frac{\sigma S}{W_0} \right)^{1/2} \frac{C_L^{3/2}}{C_D} \left(\left(\frac{W_0}{W_1} \right)^{1/2} - 1 \right)$$

$\frac{\text{lb}}{\text{BHP} \cdot \text{hr}}$, multiply by $550 \frac{\text{ft} \cdot \text{lb}}{\text{s}}$

to convert
from BHP to

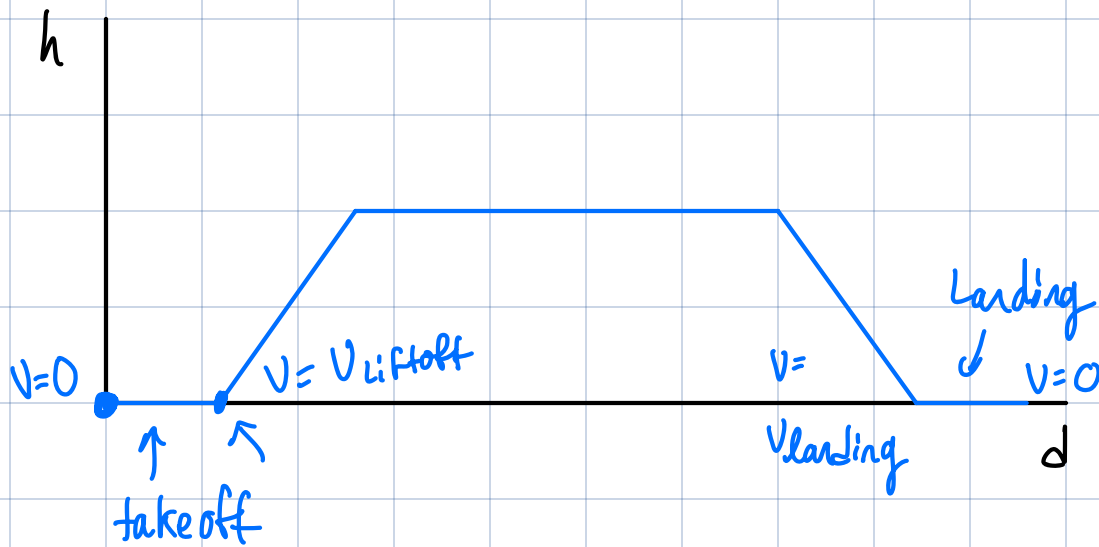
english units
 $\frac{\text{ft} \cdot \text{lb}}{\text{s}}$

coefficient in front

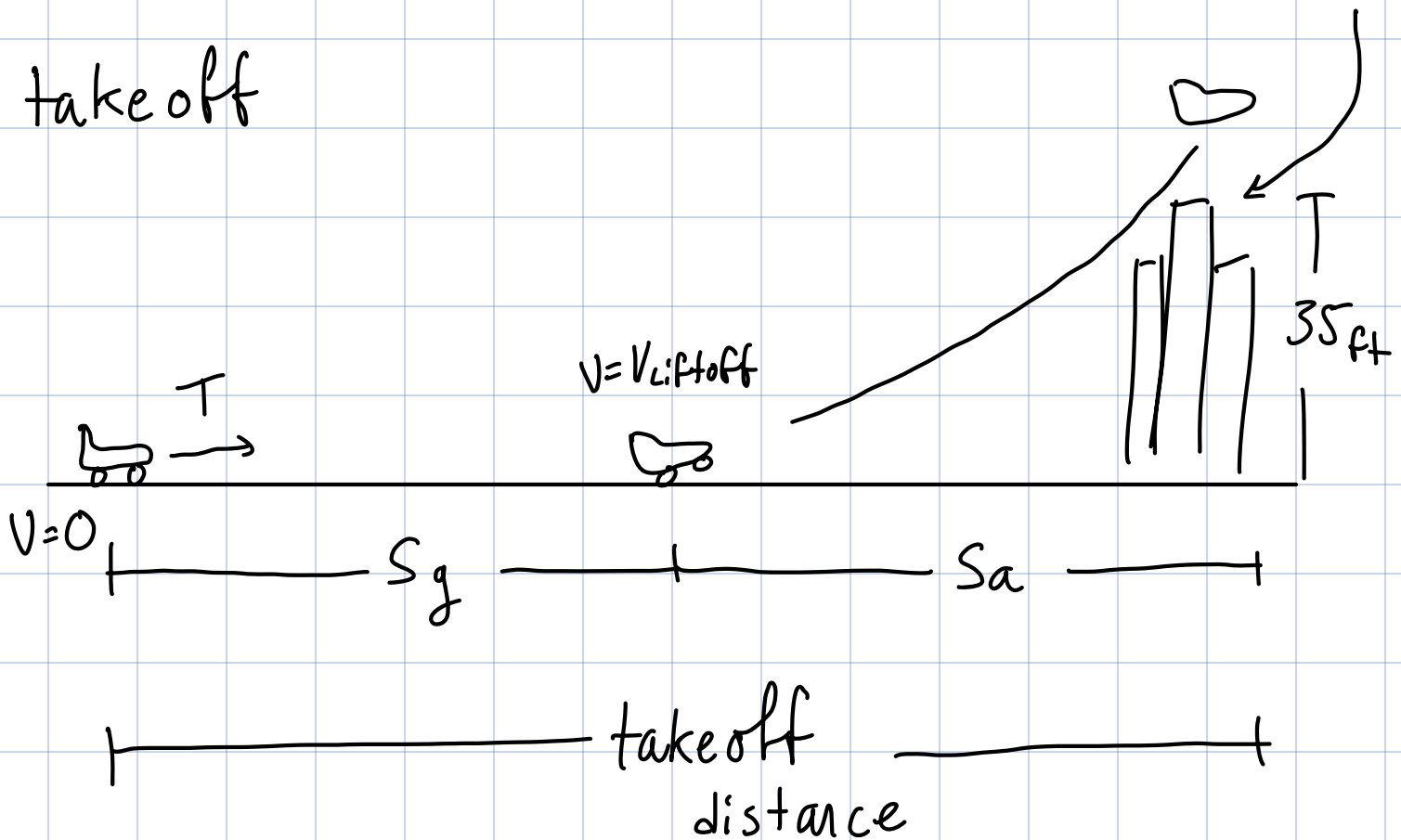
$$\Rightarrow 2^{1/2} \cdot \rho_{sl}^{1/2} \cdot 550$$

$$\uparrow \quad 0.00238 \frac{\text{slugs}}{\text{ft}^3} \rightsquigarrow 37.9$$

takeoff Procedures



takeoff

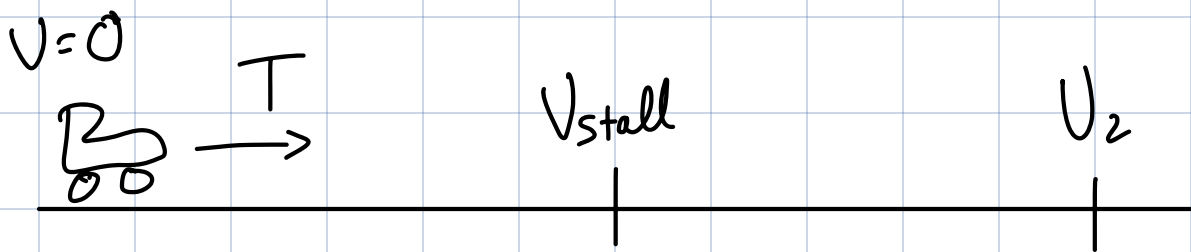


$S_g \equiv$ ground Roll distance between brake Release & lift off

$S_a \equiv$ air borne distance b/t Liftoff
& clearance of obstacle

total TO distance $S_g + S_a$

looking specifically @ S_g



- start to accelerate to V_{stall}
- accelerate to $V_2 \equiv$ "take off safety speed"

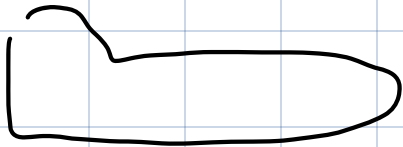
for typical civil transport A/C

$$V_2 = 1.2 \sqrt{\frac{2W}{\rho S C_{L_{max}}}}$$

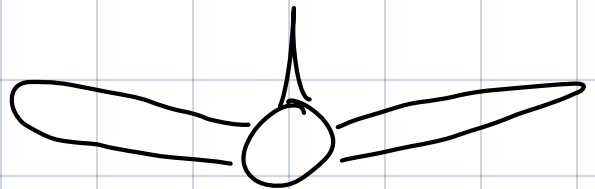
↑

take off configuration

"clean" configuration

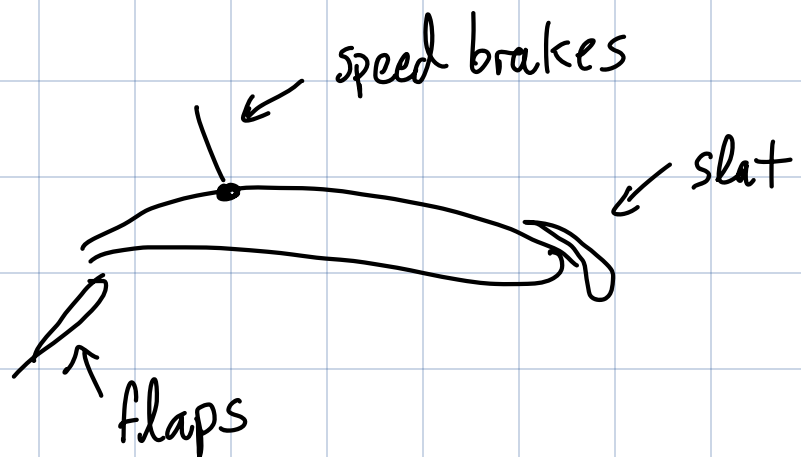
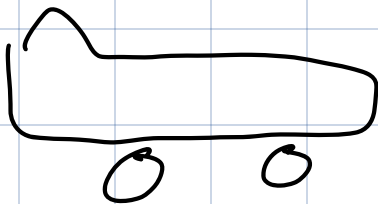


gear, flaps, slats
are all Retracted

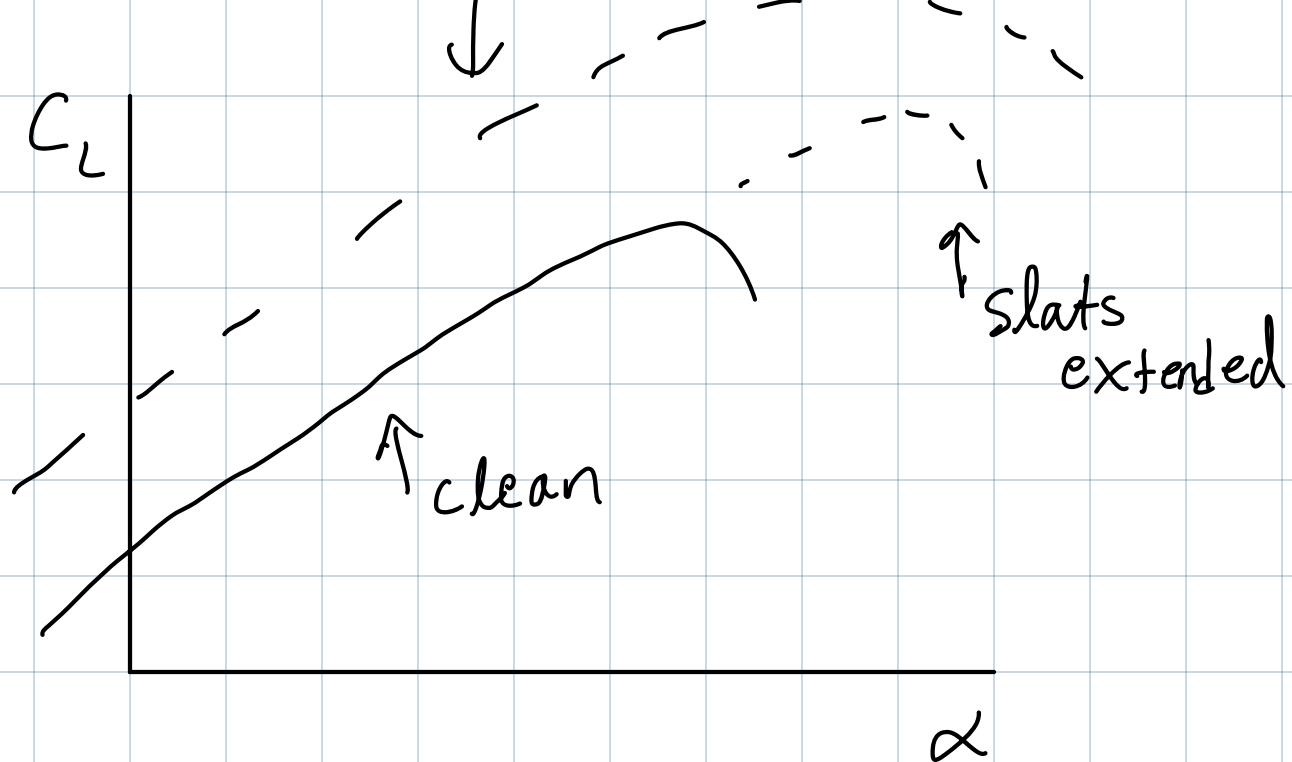


cruise, climb,
descent

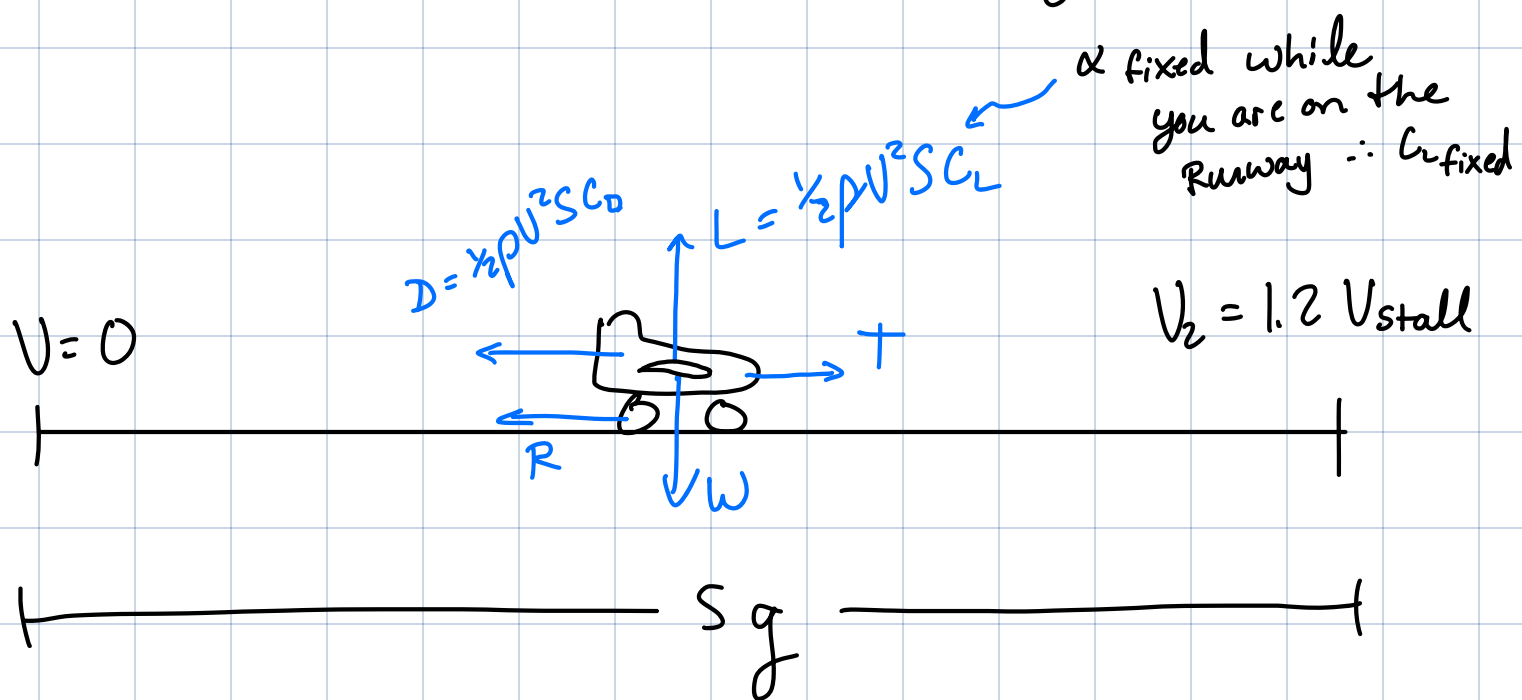
Takeoff Configuration



flaps & slats
extended



Shevell Fig 14.15 gives C_L
for various configurations



$$\text{Rolling Resistance} = R = \mu_r (W - L)$$

$\mu_r \equiv$ Rolling friction coefficient
depends on surface

$= 0.05$ for grass

$= 0.015$ for asphalt

$$a = \frac{\sum F}{m} = \frac{T - D - R}{W/g} = \frac{T - qSC_D - \mu(W - qSC_L)}{W/g}$$

$T(v)$, $D(v)$, $R(v)$

\leadsto function of v
not ϕ !

suppose $a \approx \phi$

then $Sg = \frac{v_2^2 - v_0^2}{2a}$

from kinematics

\uparrow only works
if a
is constant

① Riemann Sum

$V_0 V_1 V_{i+1} V_{i+2} \dots V_N = V_2$

$\Delta x \approx \Delta$ for each segment

2) assume $D \approx \Delta$ using V @ start of the segment
 $R \approx \Delta$
 $T \approx \Delta$ to compute forces

then compute a for an incremental distance along segment

if $V_N = V_2$, that is TO distance

② assume an average value for a along entire TO distance

use a obtained when calculating $T-D-R$
@ $V = 0.7 V_2$

in other words, compute T, D, R
@ $V = 0.7 V_2$

plug into $a = \frac{\Sigma F}{m}$

first calculate $V_{\text{stall}} = \sqrt{\frac{2W}{\rho S C_{L_{\text{max}}}}}$
↑
to config

calculate $V_2 = 1.2 \cdot V_{\text{stall}}$

calculate $0.7V_2$


calculate forces $\rightarrow a$

$$S_g = \frac{V_2^2}{2 a_{0.7V_2}}$$


$$= \frac{1.44 W^2}{g \rho S C_{L_{\text{max}}} (T-D-R)_{V=0.7V_2}}$$

Note when Taking Off,

V_z, C_L not be C_{Lmax}



$V_z = 1.2 V_{stall}$



when taking off

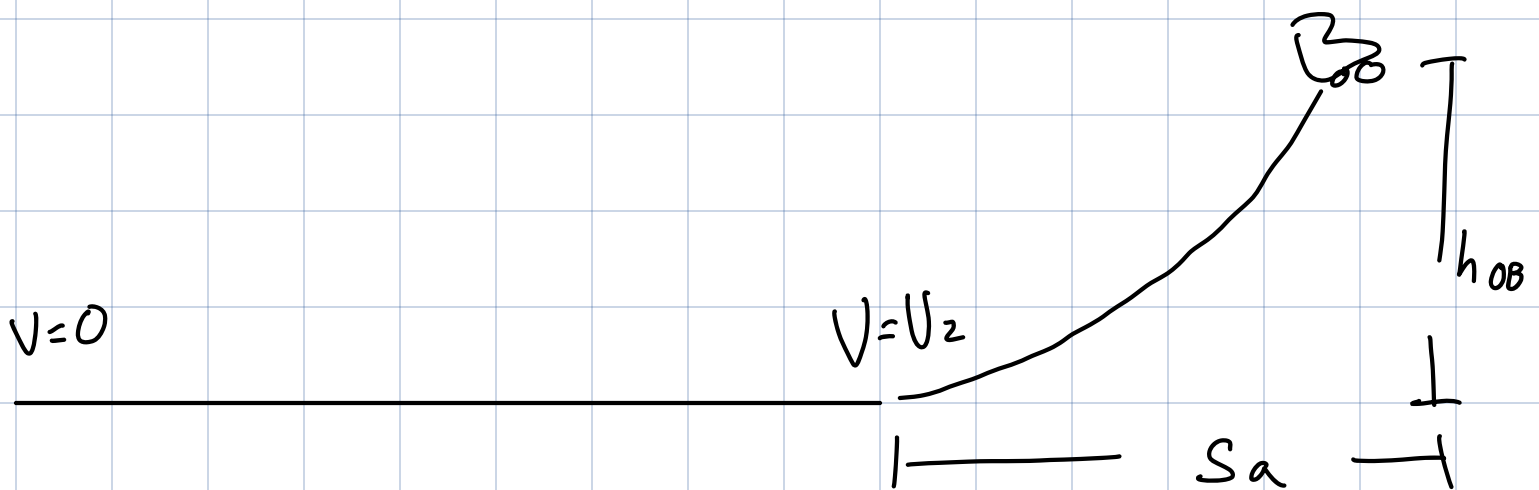
A/C pitches
up right
at $Lift off$

on ground

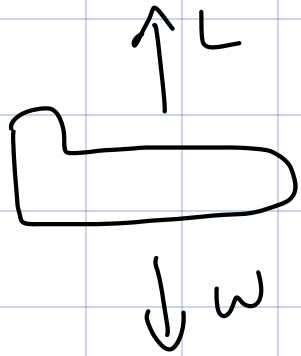
$$C_D = C_{Dp} + KC_L^2$$

$C_{Dp0} + \Delta C_{Dp configuration}$
 \uparrow
 "clean"
 C_{Dp}
 \uparrow
 gear, flaps,
 slats etc....

\uparrow
 use C_L
 on ground
 (Not $C_{Lmax}!!$)

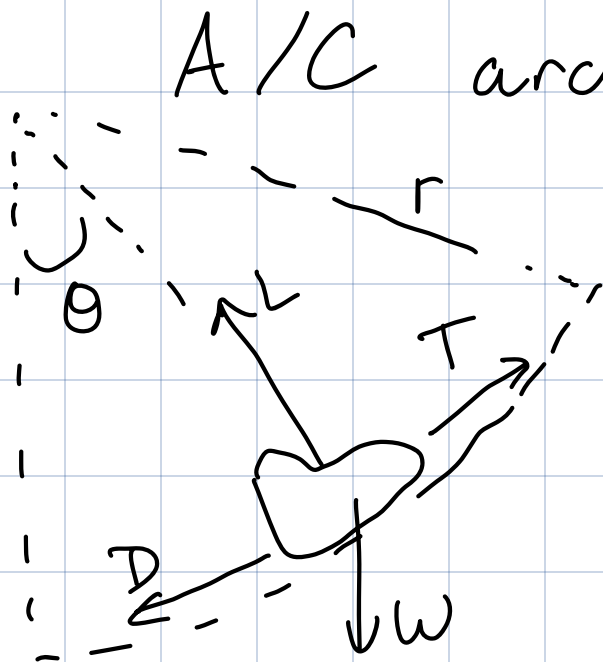


in order to get Sa , pull-up maneuver



$$SLF \quad L = W$$

When pitching A/c for Liftoff, typically
Need α higher than needed for
SLF, sudden increase in
 L such that
 $L > W$



$r \equiv$ Radius of
curved arch

$\frac{d\theta}{dt} \equiv$ Rate of change
of turn
angle θ

looking @ instantaneous moment
where pullup is initiated
 $\theta = 0^\circ$

in vertical direction

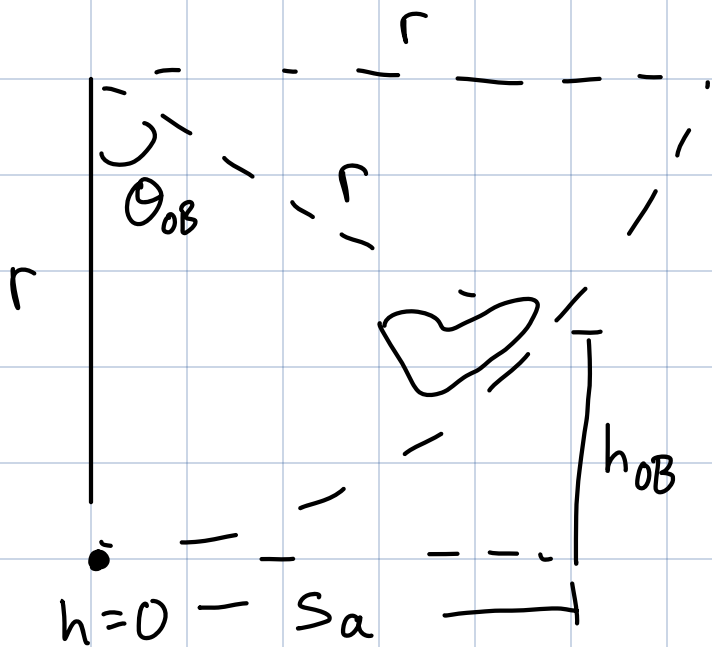
$$L - W = \frac{m V^2}{r} \quad \leftarrow \begin{array}{l} \text{centripetal} \\ \text{force} \end{array}$$

$$r = \frac{m V^2}{L - W} = \frac{V^2}{g \left(\frac{L}{W} - 1 \right)}$$

$\frac{W}{g}$

$L/W \equiv \text{load factor} = n$

$$r = \frac{V^2}{g(n-1)}$$



$$\cos \theta_{OB} = \frac{r - h_{OB}}{r}$$

$$\theta_{OB} = \cos^{-1} \left(1 - \frac{h_{OB}}{r} \right)$$

$$S_a = r \sin \theta_{OB}$$

↑
need to know
 n , & $V_{Liftoff}$

Summary

