

# Final Report

Course: MAE 159 - Aircraft Performance

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Winter 2025 specifications:

Number of passengers 210

(2-class, domestic rules)

Weight of cargo 8000 pounds

(10 pounds/ft<sup>3</sup>)

Maximum Payload Weight 55,000 lbs

Range (still air) 3500 nautical miles

Takeoff field length 6900 feet

(sea-level, hot day 84° f)

Landing approach speed 135 knots

Cruise Mach number 0.80

Initial cruise altitude 35,000 feet

Maximum wingspan 125 feet

Maximum landing weight with 45% fuel

Engine Configuration: 2 JT9D-class engines, wing-mounted

**Seating Layout:** 6 abreast

Wing Design: Taper ratio = 0.35

Date: March 1st, 2025

## 1. Approach

In this study, commercial transport conventional aircraft design and advanced technology aircraft design are compared for economic performance. Both designs have to satisfy all the specifications requirements and safety requirements while keeping Direct Operating Cost (DOC) as low as possible.

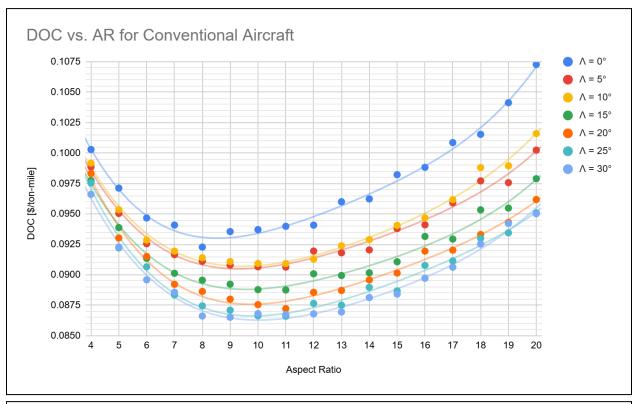
#### 1.1 Design Specifications

Specification	Value
Number of Passengers	210 (2-class, domestic rules)
Cargo Weight	8,000 lbs (10 lbs/ft³)
Maximum Payload Weight	55,000 lbs
Range (still air)	3,500 nautical miles
Takeoff Field Length	6,900 feet (sea-level, hot day 84°F)
Landing Approach Speed	135 knots
Cruise Mach Number	0.8
Initial Cruise Altitude	35,000 feet
Maximum Wingspan	125 feet
Maximum Percent Fuel Weight at Landing	45%

Table 1: Aircraft Design Specifications

Table 1 shows the specifications that the two aircrafts are required to meet. These design parameters define the aircraft's operational capabilities, including passenger and cargo capacity, cruise range, takeoff field length, landing performance, and other aerodynamic constraints. Besides these explicit specifications, the two aircrafts also have to meet all safety requirements such as minimum 1.3 stall velocity operation and passing safety gradients in all flight segments. Optimization is performed by parallelly clearing all requirements and iterating aspect ratio (AR) and swept angle ( $\Lambda$ ) for minimum DOC. Other properties of the aircraft are then extracted and calculated from the MATLAB code for further sizing procedure and final design in Solidworks. This process is done twice for the conventional aircraft design and the advanced technology design.

## 1.2 Wing Sizing Results



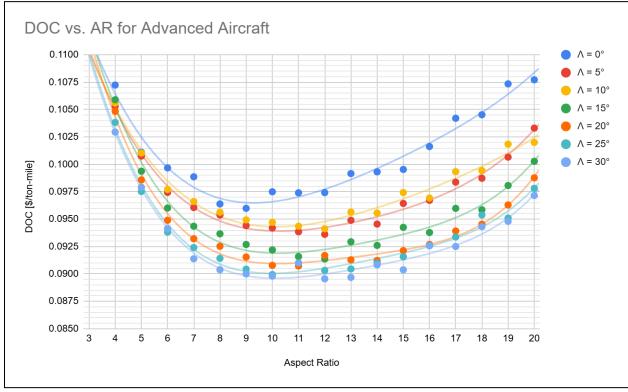
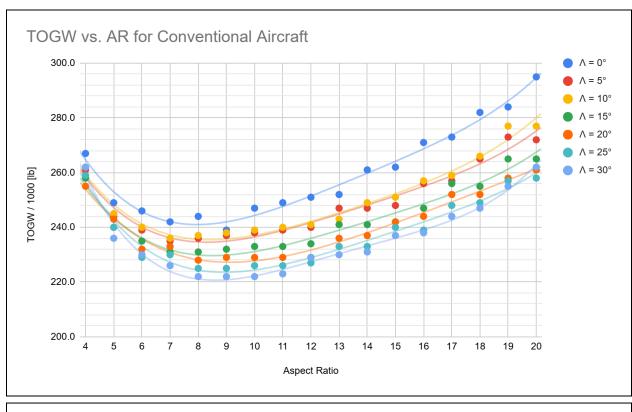


Figure 1: DOC vs. AR for All Aluminum (top) and for All Composite (bottom)



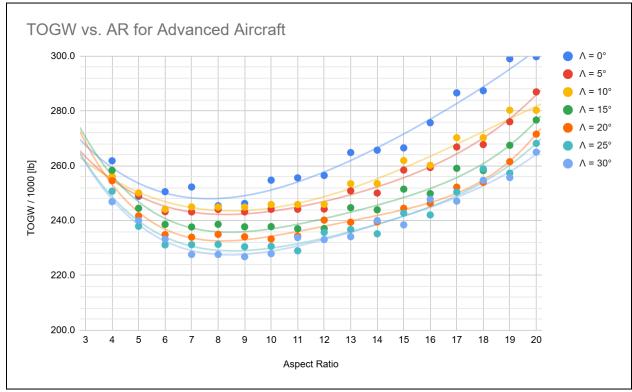


Figure 2: TOGW vs. AR for All Aluminum (top) and for All Composite (bottom)

It's worth noting that both DOC vs. AR graphs and TOGW vs. AR graphs converge at the same AR and  $\Lambda$ . Therefore, minimizing DOC is the same as minimizing Takeoff Gross Weight (TOGW). This makes sense because TOGW and DOC have a linear relationship. As TOGW increases, DOC increases and as TOGW decreases, DOC also decreases.

Aspect ratio trend is in U shape. At extreme low AR, 4, and extreme high AR, 20, the DOC is significantly higher than mid range AR, 7-11. The AR that gives the lowest DOC is around 9, which is expected for most current commercial aircrafts [1]. However, due to the Maximum Wingspan requirement in Table 1, AR is chosen to be 8. At AR value at 9 and above, the wingspan is greater than 125 [ft], thus disqualifying them from design consideration.

Swept angle trend is opposite to DOC. As  $\Lambda$  increases, DOC decreases. Therefore,  $\Lambda$  should be as high as possible to minimize DOC. However, when  $\Lambda$  is too high, the designs cannot pass all specifications and safety requirements. This leads to  $\Lambda$  stops at 30° for both designs because higher  $\Lambda$  values aren't able to pass safety gradients.

#### 1.3 Primary Analysis: Detailed Composite vs Aluminum

WEIGHT [lb]	Conventional	Advanced	
Wing	22,077.63	22,559.16	
Fuselage	2,542.66	2,557.72	
Nacelle + Pylon	4,661.90	4,842.47	
Tail	4,342.67	4,437.39	
Power Plant	23,463.19	25,809.51	
Fixed Equipment	37,630.00	37,827.83	
Fuel	64,994.09	72,136.82	

Table 2: Components Weight Comparison Between Conventional and Advanced Designs

Specific fuel consumption (SFC) for conventional aircraft design is 0.68 while SFC for advanced aircraft design is 0.61 because advanced engines provide a 10% decrease in SFC.

In conventional aircraft design, all components are in aluminum while in advanced aircraft design, all components are in composite material. In particular, wing and tail components weight decrease 30%, fuselage weight decreases 15%, fixed equipment weight decreases by 10%, nacelles and pylons decrease by 20%.

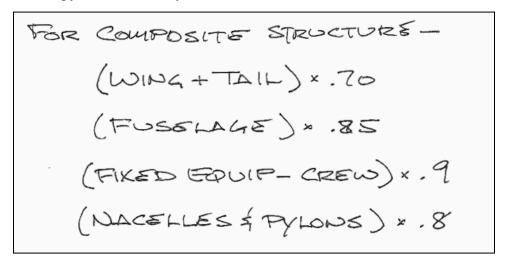


Figure 3: Course Manual Advanced Technology Weight Change

The only exception is the power plant because for advanced technology, the power plant weight is 10% higher to trade off for the 10% decrease of the SFC. Composite material is lighter than aluminum, so theoretically advanced aircraft design should have lower weight compared to conventional aircraft design. However, because of the increase in power plant weight and decreases in SFC, the design optimization loop changed the configuration into a different optimal TOGW thus changing the weight of all components.

#### 1.4 Aircraft Comparison Specs

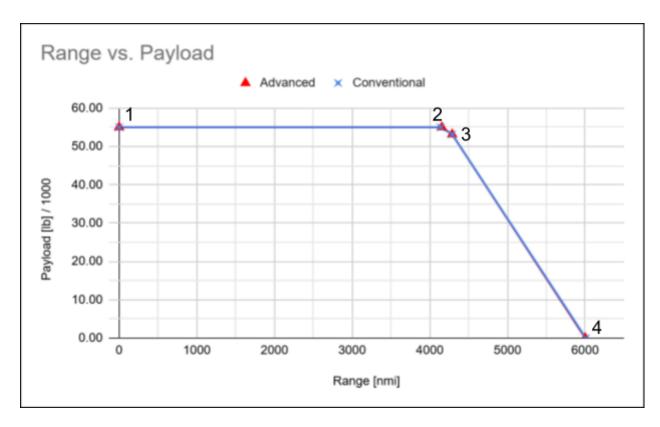
	Conventional	Advanced		
WING				
Wingspan [ft]	123.02	122.40		
MAC [ft]	16.57	16.48		
Planform Area [ft^2]	1,891.67	1,872.76		

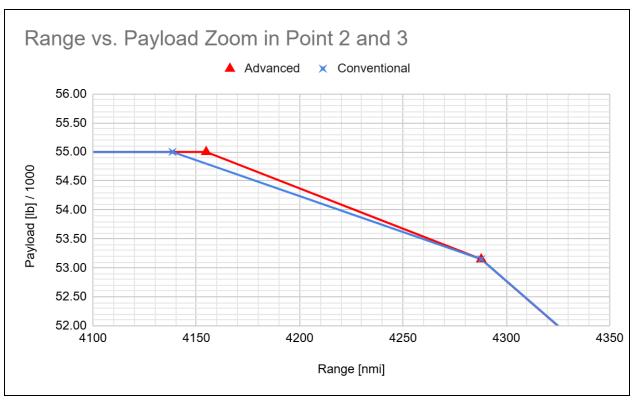
Airfoil Type	Supercritical	Supercritical
Aspect Ratio (AR)	8	8
Swept Angle (°)	30	30
FUSELAGE		
Length [ft]	165.78	165.78
Diameter [ft]	14	14
Seats Abreast	6	6
MATERIAL		
Wing	Aluminum	Composite
Fuselage	Aluminum	Composite
Nacelle + Pylon	Aluminum	Composite
Tail	Aluminum	Composite
Fixed Equipment	Aluminum	Composite
WEIGHT [lb]	Conventional	Advanced
Wing	22,077.63	22,559.16
Fuselage	2,542.66	2,557.72
	_,e :=:••	<b>'</b>
Nacelle + Pylon	4,661.90	4,842.47
Nacelle + Pylon Tail	· ·	·
•	4,661.90	4,842.47
Tail	4,661.90 4,342.67	4,842.47 4,437.39
Tail Power Plant	4,661.90 4,342.67 23,463.19	4,842.47 4,437.39 25,809.51
Tail Power Plant Fixed Equipment	4,661.90 4,342.67 23,463.19 37,630.00	4,842.47 4,437.39 25,809.51 37,827.83
Tail Power Plant Fixed Equipment Fuel	4,661.90 4,342.67 23,463.19 37,630.00	4,842.47 4,437.39 25,809.51 37,827.83
Tail Power Plant Fixed Equipment Fuel ENGINES	4,661.90 4,342.67 23,463.19 37,630.00 64,994.09	4,842.47 4,437.39 25,809.51 37,827.83 72,136.82
Tail  Power Plant  Fixed Equipment  Fuel  ENGINES  Flat Plate Drag Area [ft^2]	4,661.90 4,342.67 23,463.19 37,630.00 64,994.09 30.77	4,842.47 4,437.39 25,809.51 37,827.83 72,136.82
Tail  Power Plant  Fixed Equipment  Fuel  ENGINES  Flat Plate Drag Area [ft^2]  Engine Type	4,661.90 4,342.67 23,463.19 37,630.00 64,994.09 30.77 JT9D	4,842.47 4,437.39 25,809.51 37,827.83 72,136.82 30.60 JT9D
Tail  Power Plant  Fixed Equipment  Fuel  ENGINES  Flat Plate Drag Area [ft^2]  Engine Type  Number of Engines	4,661.90 4,342.67 23,463.19 37,630.00 64,994.09 30.77 JT9D 2	4,842.47 4,437.39 25,809.51 37,827.83 72,136.82 30.60 JT9D 2
Tail Power Plant Fixed Equipment Fuel ENGINES Flat Plate Drag Area [ft^2] Engine Type Number of Engines Max Thrust per Engine [lb]	4,661.90 4,342.67 23,463.19 37,630.00 64,994.09 30.77 JT9D 2 43,857.47	4,842.47 4,437.39 25,809.51 37,827.83 72,136.82 30.60 JT9D 2 44,154.67

DOC [\$/ton-mile]	0.0865	0.0900
SFC	0.68	0.61
Powerplant Weight [lb]	24,501.38	26,951.52

Table 3: Specification Comparison Between Conventional and Advanced Designs

The comparison between the conventional (full aluminum) and advanced (full composite) aircraft designs reveals a nuanced balance of performance, efficiency, and economic considerations. Both configurations use a supercritical airfoil with similar wing dimensions, maintaining an aspect ratio (AR) of 8 and a swept angle of 30 degrees. This consistency ensures aerodynamic efficiency is primarily determined by structural materials rather than geometric differences. The full composite wing, though slightly heavier (22,559.16 lb) than the aluminum wing (22,077.63 lb), may offer better durability and reduced life-cycle maintenance. The small increase in weight might reflect enhanced structural integrity offered by composites. Both configurations employ JT9D engines, but the advanced design achieves slightly higher thrust per engine (44,154.67 lb vs. 43,857.47 lb). This reflects the ability of composite materials to endure greater stress, possibly enhancing propulsion efficiency. The composite design, with its sophisticated material technology, results in higher fuel capacity (72,136.82 lb vs. 64,994.09 lb) to potentially expand operational range under heavier payloads. However, this benefit comes with an increased Direct Operating Cost (DOC) of \$0.0900/ton-mile compared to the aluminum design's \$0.0865/ton-mile. This suggests that while composites offer performance improvements, they might slightly elevate operational expenses without significant cost-offsetting measures.





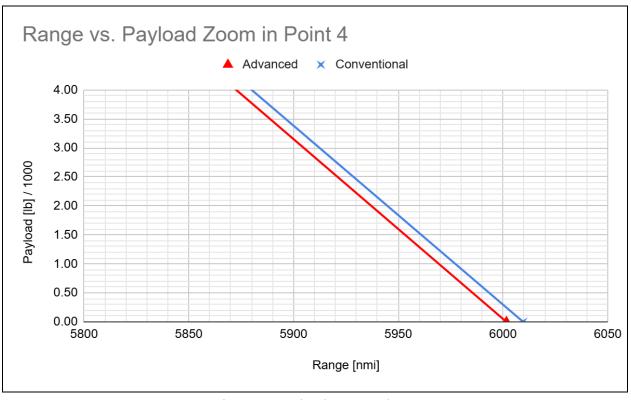


Figure 4: Payload Range Chart

#### 2. Results and Conclusions

After a thorough analysis and comparison of the conventional aluminum and advanced composite configurations, the decision is made in favor of the full aluminum configuration. This choice is based on a combination of efficiency, cost-effectiveness, and familiarity that aligns well with operational and strategic goals.

Aluminum has a long history in the aerospace industry, providing proven reliability and durability. The material's known performance characteristics reduce the risk associated with adopting new technologies and support consistent operational outcomes. The production and material costs for aluminum are markedly lower than those for advanced composites. This results in substantial savings upfront, allowing airlines to allocate resources to other critical areas such as training, maintenance, and expansion. Aluminum's extensive use means simplified maintenance procedures and a wide availability of repair expertise and parts. This leads to reduced maintenance downtimes and costs throughout the aircraft's lifecycle, enhancing overall operational efficiency.

DOC for conventional aircraft is lower compared to advanced aircraft. Therefore, by continuing with aluminum, airlines capitalize on a well-understood material while remaining competitive in markets dominated by cost-sensitive decisions. This choice also supports a conservative risk profile, appealing to stakeholders prioritizing stability and predictability.

## 3. Description of the Configuration

#### 3.1 Wing and Tails

Wing AR,  $\Lambda$ , and reference area ( $S_{ref}$ ) is taken from MATLAB code and analysis above. Then using equations in Schaufele textbook, the rest of the information of the wing can be calculated.

Name	Value / Equation
☐ Global Variables	
"Root Chord W"	= 2 * "S_ref" / ( "Span W" * (1 + "Taper Ratio W" ) )
"Tip Chord W"	= "Root Chord W" * "Taper Ratio W"
"Swept Angle W"	= 30
"Span W"	= sqr ( "S_ref" * "AR W" )
"AR W"	= 8
"S_ref"	= 1872.75746643
"Taper Ratio W"	= 0.35
"MAC W"	= (2/3) * "Root Chord W" * (1 + "Taper Ratio W" - ("Taper Ratio W" / (1 + "Taper Ratio W")))
"Y W"	= ("Span W" / 6) * ((1 + 2 * "Taper Ratio W") / (1 + "Taper Ratio W"))

Table 4: Equations for Wing in Solidworks

Here the calculation was computed inside Solidworks Equations so that they can be directly implemented in the 3D design as variables. In later design and sizing process, when these parameters need to be changed, they can be changed easily and updated systematically in Solidworks to smooth out the design process.

For tail sizing, Schaufele is heavily ultilized.

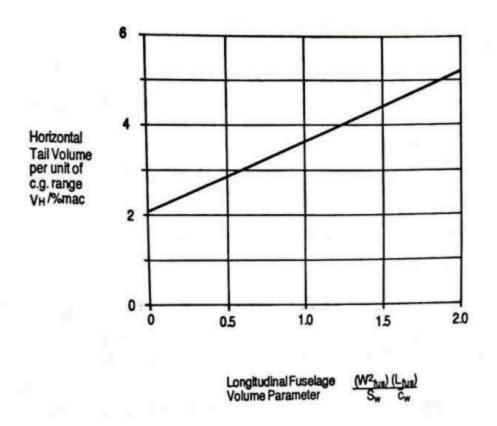


Fig. 6-9 Preliminary Design Chart ~ Horizontal Tail Volume Determination

Aircraft Type	V <sub>H</sub> Range
Personal/Utility	.4892
Commuters	.46-1.07
Regional Turboprops	.83-1.47
Business Jets	.5199
Jet Transports	.54-1.48
Military Fighter/Attack	.2075

Fig. 6-10 Representative Horizontal Tail Volume Ranges

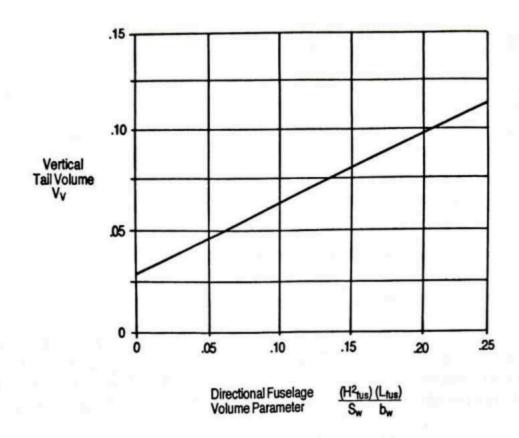


Fig. 6-15 Preliminary Design Chart ~ Vertical Tail Volume Determination

Aircraft Type	V <sub>v</sub> Range
Personal/Utility	.024086
Commuters	.041097
Regional Turboprops	.065121
Business Jets	.061093
Jet Transports	.038120
Military Fighter/attack	.041130

Fig. 6-16 Representative Vertical Tail Volume Ranges

Aircraft Type	AR	λ	c,/c	t/c
Personal/Utility	3.5-5.0	.50-1.0	.3545	.0609
Commuters	3.5-5.0	.5080	.3545	.0609
Regional Turboprops	3.5-5.0	.5080	.3045	.0609
Business Jets	3.5-5.0	.3550	.3040	.0609
Jet Transports	3.5-5.0	.2545	.3035	.0609
Military Fighter/Attack	3.0-4.0	.2540	.30-1.0	.0304

Fig. 6-17 Summary of Horizontal Tail Geometric Characteristics

Aircraft Type	AR	λ	c,/c	t/c
Personal/Utility	1.2-1.8	.3050	.2545	.0609
Commuters	1.2-1.8	.3080	.3545	.0609
Regional Turboprops	1.4-1.8	.3070	.2545	.0609
Business Jets	0.8-1.6	.3060	.2535	.0609
Jet Transports	1.4-1.8	.3080	.2540	.0810
Military Fighter/Attack	1.2-1.6	.2540	.2035	.0309

Fig. 6-18 Summary of Vertical Tail Geometric Characteristics

### 3.2 Fuselage and Exterior Configuration

Although fuselage length can be taken from MATLAB code, it was cut back to avoid unnecessary weight and material cost.

#### 3.3 C.G Design

This follows CG sizing procedure to make sure the aircraft CG location is always around MAC quarter chord for a tolerance of 10%.

### 3.4 Interior Configuration

Course manual specificies how interior layout needs to be done. Also PAX is the constraining parameter in this step.

## 3.5 Selected Aircraft Configuration

TBlahblahblah

# 4. Configuration Drawings

## 5. Conclusion

Blah blah blah

## 6. Work Cited

- [1] Performance predictor Aerospace America.
- [2] MAE 159 Appendix Hand Cal.pdf
- [3] AR vs DOC.m
- [4] Weight\_takeoff\_vs\_DOC.m
- [5] AR\_vs\_Weight\_takeoff.m
- [6] Course\_Manual.pdf
- [7] Psuedo Code 2.m
- [8] Sample Calculation.m
- [9] Schaufele.pdf