

## Chapter 1

# Theory

The theory encompassed by this work can be divided into four basic parts: conservation laws, thermohydraulics, numerical methods, and stability. Conservation laws, such as those for momentum and energy, form a fundamental basis of analysis in all branches of science. Therefore, a precise definition for a generic conserved quantity and an associated conservation law will be given. Following this generic treatment, the specific conservation laws for thermohydraulics will be presented. Numerical methods for solving the thermohydraulic conservation laws will then be derived. Finally, the stability theory for the thermohydraulic system will be discussed.

## 1.1 Conservation Laws

### 1.1.1 Scalar Form

A conserved quantity  $q$  refers to any physical property whose time evolution within an arbitrary, closed volume exactly balances with its surface fluxes and volume sources. For the purpose of mathematical discussion and analysis, the conserved quantity  $q$  will simultaneously represent a function of space and time that conforms to the requirements of the physical property. These definitions define the following scalar conservation law over a volume  $\Omega$  with a closed surface  $\Gamma$ :

$$\partial_t \int_{\Omega} q(x_i, t) \partial\Omega = \int_{\Gamma} -F_i(q, x_i, t) n_i \partial\Gamma + \int_{\Omega} S(q, x_i, t) \partial\Omega, \quad (1.1)$$

where  $F_i$  is the surface flux of  $q$ ,  $n_i$  is the outward unit normal of the surface  $\Gamma$ , and  $S$  is the volume source of  $q$ . Such that the units in the equation agree, both  $q$  and  $S$  are taken on a per volume basis and  $F_i$  on a per area basis. The negative sign in the surface integral ensures that outward fluxes act as sinks and inward fluxes as sources to the time evolution of  $q$ 's volume integral. Equation 1.1 is the most general scalar conservation law that will be presented and is always physically valid regardless of the functions' behavior.

A general conservation law can also be presented in differential form (i.e., as a differential equation). First the Divergence Theorem is used to equate the surface integral in equation 1.1 to a volume integral:

$$\int_{\Gamma} -F_i(q, x_i, t) n_i \partial\Gamma = \int_{\Omega} -\partial_i F_i(q, x_i, t) \partial\Omega. \quad (1.2)$$

Substituting equation 1.2 into equation 1.1 and moving all terms to the left-hand side gives:

$$\int_{\Omega} \partial_t q(x_i, t) + \partial_i F_i(q, x_i, t) - S(q, x_i, t) \partial\Omega = 0, \quad (1.3)$$

where the time derivative operator could be moved into the integral since the volume is taken to be time-independent. Since the integration volume in equation 1.3 is arbitrary, we take limit of the equality as the volume shrinks to a zero.

$$\lim_{\Omega \rightarrow 0} \left[ \int_{\Omega} \partial_t q(x_i, t) + \partial_i F_i(q, x_i, t) - S(q, x_i, t) \partial\Omega \right] = 0. \quad (1.4)$$

In this limit, the enforcement of the equality changes from one over a finite volume into one that is enforced at a particular point. To ensure point-wise enforcement over a given domain, the integrand itself is required to be equally zero at every point in the domain; this yields

the differential conservation law

$$\partial_t q(x_i, t) + \partial_i F_i(q, x_i, t) - S(q, x_i, t) = 0. \quad (1.5)$$

When equipped with adequate boundary and initial data, this differential equation defines the requirement for all sufficiently smooth functions that describe how the conserved quantity evolves at every point in space-time.

The differential form may seem cleaner than the integral form, but *it is not valid for all functional forms of  $q$* . In transitioning from equation 1.4 to equation 1.5, it is assumed that all functions in the integrand remain bounded. If any of the terms within the limit become infinite, the balance cannot be satisfied. In particular, if  $q$  has an area where it undergoes a discontinuous jump, called a shock, the gradient of the flux is infinite and the differential form is rendered invalid. While methods that handle shocks in a robust fashion (shock-capturing schemes) are not the focus of this work, it is presented for completeness and consideration.

### 1.1.2 Vector Form

The simulation of real world problems often involves the solution of a system of conservations laws. In general, the systems are nonlinear and tightly coupled. The actual solution of these problems will be discussed in future sections, but the notation used will be introduced now.

The integral conservation law for a vector of conserved quantities  $q_i$  is

$$\partial_t \int_{\Omega} q_i(x_i, t) \partial\Omega = \int_{\Gamma} -F_{ij}(q_i, x_i, t) n_j \partial\Gamma + \int_{\Omega} S_i(q_i, x_i, t) \partial\Omega, \quad (1.6)$$

where  $F_{ij}$  is a matrix of surface fluxes of  $q_i$  in the  $j$ -th direction,  $n_j$  is the outward unit normal of the surface  $\Gamma$ , and  $S_i$  is the volume source of  $q_i$ . The integrals of the vector

quantities represent element-wise integration. A process similar to the scalar case also yields the differential form of the system conservation law:

$$\partial_t q_i(x_i, t) + \partial_j F_{ij}(q_i, x_i, t) - S_i(q_i, x_i, t) = 0, \quad (1.7)$$

where  $\partial_j F_{ij}$  represents a row-wise divergence operation.

## 1.2 Conservation Derivations

The derivations of the main equations used in thermohydraulics will be presented using the definitions above. Mass, momentum, and energy are the primary quantities of interest and will be presented on a per unit volume basis. It is noted that dependence will be omitted for clarity; however, all quantities and functions as assumed to be functions of any variable in the system.

### 1.2.1 Conservation of Mass

Mass or, on a per volume basis, density is conserved as a simple scalar. The density of material in a given control volume is controlled by the background flow field moving it from one point to another. Therefore, the integral conservation law for density is

$$\partial_t \int_{\Omega} \rho \, \partial\Omega = \int_{\Gamma} -(u_i \rho) n_i \, \partial\Gamma + \int_{\Omega} S^\rho \, \partial\Omega, \quad (1.8)$$

with the more familiar differential form being

$$\partial_t \rho(x_i, t) + \partial_i(u_i \rho) = S^\rho. \quad (1.9)$$

### 1.2.2 Conservation of Momentum

A control volume's momentum  $\rho u_i$  is more complicated than density because it is inherently a vector quantity. Since all of the components of the vector can affect one another, the flux function is necessarily a tensor quantity.

One part of the flux function is a so-called normal component

$$F_{ij}^{\text{N}} = \delta_{ij}P + u_j\rho u_i, \quad (1.10)$$

where  $\delta_{ij}$  is the Kronecker delta and  $P$  is the thermodynamic pressure. This function is distinguished as normal since both of the terms involve quantities that move through the boundary of the control volume.

The other, orthogonal portion of the function is the tangential component

$$F_{ij}^{\text{T}} = -\tau_i j, \quad (1.11)$$

### 1.2.3 Conservation of Energy

## 1.3 Thermohydraulics

### 1.3.1 Base Equations

### 1.3.2 Generic Bulk Flow

The set of conservation equations for a fluid in three dimensional form using index notation is

$$\partial_t \rho + \partial_j(\rho u_j) = S_\rho \quad (1.12a)$$

$$\partial_t \rho u_i + \partial_j(\rho u_i u_j - \sigma_{ij}) + \partial_i P = \rho g_i + S_{\rho u} \quad (1.12b)$$

$$\partial_t \rho e + \partial_j[u_j(\rho e + P)] - \partial_j(u_i \sigma_{ij}) = S_{\rho e}, \quad (1.12c)$$

where  $\rho$  is density,  $u$  is velocity,  $g$  is the gravity vector,  $e$  is the total energy of flow,  $P$  is the thermodynamic pressure,  $\sigma_{ij}$  is the viscous stress tensor, and  $S_*$  are arbitrary sinks or sources. Integration of equation 1.12 over some arbitrary, time-independent volume  $\Omega$  with boundary  $\Gamma$  yields

$$\partial_t \int_{\Omega} \rho \partial\Omega + \int_{\Omega} \partial_j(\rho u_j) \partial\Omega = \int_{\Omega} S_\rho \partial\Omega \quad (1.13a)$$

$$\partial_t \int_{\Omega} \rho u_i \partial\Omega + \int_{\Omega} \partial_j(\rho u_i u_j - \sigma_{ij}) + \partial_i P \partial\Omega = \int_{\Omega} \rho g_i + S_{\rho u} \partial\Omega \quad (1.13b)$$

$$\partial_t \int_{\Omega} \rho e \partial\Omega + \int_{\Omega} \partial_j[u_j(\rho e + P)] - \partial_j(u_i \sigma_{ij}) \partial\Omega = \int_{\Omega} S_{\rho e} \partial\Omega. \quad (1.13c)$$

The unweighted volume average of a quantity  $\alpha$  is denoted by  $\bar{\alpha}$  and defined as

$$\bar{\alpha} = \frac{1}{\Omega} \int_{\Omega} \alpha \partial\Omega. \quad (1.14)$$

Using this definition, division of equation 1.13 by  $\Omega$  and transformation of the volume integrals of spatial derivatives into surface integrals via the Divergence Theorem gives

$$\partial_t \bar{\rho} + \frac{1}{\Omega} \int_{\Gamma} \rho u_j n_j \partial\Gamma = \bar{S}_{\rho} \quad (1.15a)$$

$$\partial_t \bar{\rho u_i} + \frac{1}{\Omega} \int_{\Gamma} (\rho u_i u_j - \sigma_{ij}) n_j \partial\Gamma + \frac{1}{\Omega} \int_{\Gamma} P n_i \partial\Gamma = \bar{\rho} g_i + \bar{S}_{\rho u} \quad (1.15b)$$

$$\partial_t \bar{\rho e} + \frac{1}{\Omega} \int_{\Gamma} [u_j (\rho e + P) - u_i \sigma_{ij}] n_j \partial\Gamma = \bar{S}_{\rho e}, \quad (1.15c)$$

where  $n$  denotes the outward unit normal of the surface  $\Gamma$ . Equation 1.15 is the general, three-dimensional control volume form of the considered conservation equations.

### 1.3.3 Channel Flow

## 1.4 Numerical Methods

## 1.5 Stability Theory