On the Behavior of Natural Circulation Loops with Phase Change

Troy C. Haskin

University of Wisconsin–Madison

2016/09/20

Outline

Outline

1. Background
2. Thermohydraulics
3. Discretization of Conservation Equations
4. JFNK
5. Stability
6. Results
7. Future Work

Goals

Simulate a simple closed-loop with naturally circulating water in both single and two-phase regimes using

- Non-ideal equation of state for water
- Simple but accurate models for frictional pressure losses
- Modern, nonlinear solver with complete residual convergence
- Rigorous discretization that allows for exact integration of conservation equations over physical domain

And ultimately determine the linear stability of the system under consideration.

Stability

What is stability?

- Often used term
- Used with many definitions (both implicit and explicit)

Stability

One definition:

Transient (possibly oscillatory) thermal hydraulic phenomenon stemming from nonlinear-geometric-multiphase feedback that could lead to system excursions causing dangerous mechanical or thermal damage and possibly human harm.

Stability

Another definition:

A system of the form

$$\partial_t q = f(t, q) \tag{1}$$

is stable if $q \in [q_{\text{low}}, q_{\text{hi}}]$ for all time.

Stability

Another definition:

A system of the form

$$\partial_t q = f(t, q) \tag{1}$$

is stable if $q \in [q_{\text{low}}, q_{\text{hi}}]$ for all time.

Definition for here:

A system of the form

$$\partial_t q = Aq \tag{2}$$

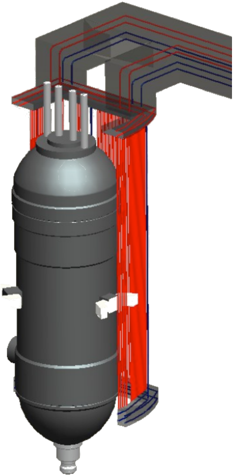
is stable if all eigenvalues of A are less than or equal to zero.

Stability

Applications?

- Thermosiphon
- Power cycle loops
- And...

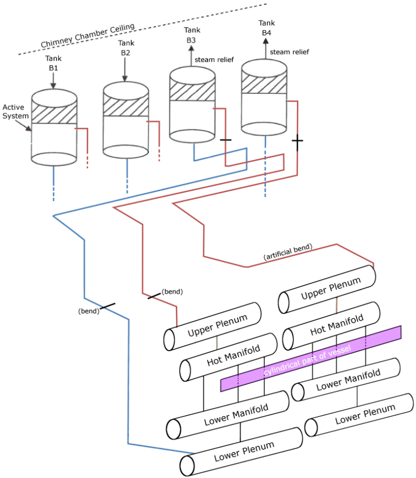
Reactor Cavity Cooling System



Purpose:
Naturally-driven cooling of reactor under accident conditions

Accident conditions:
Loss of onsite, offsite power (station blackout)

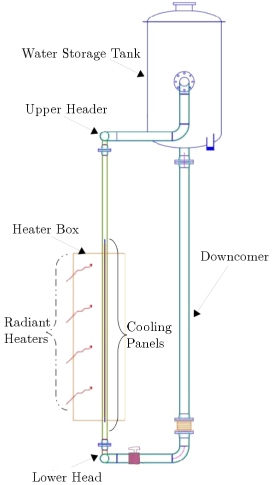
Reactor Cavity Cooling System: Big picture

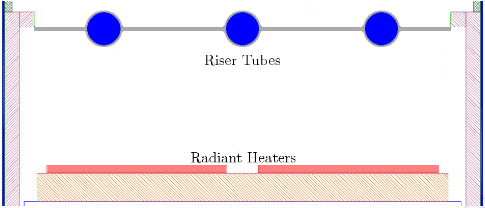


Selected specifications:

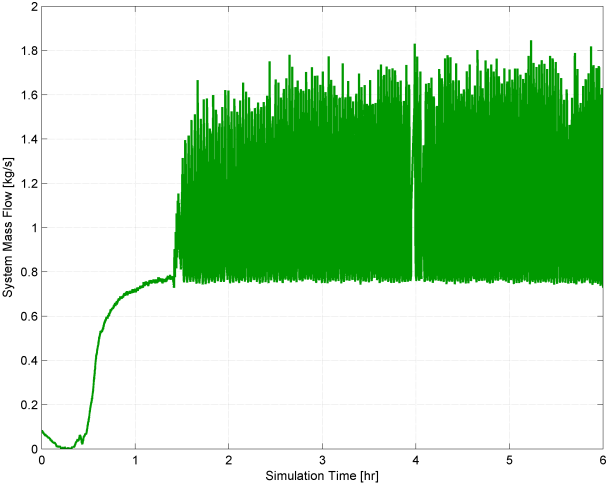
- Trains: 2
- Lines/Tanks: 8
- Elevation change: 35 meters
- Path length: 200 meters
- Heated length: 20 meters
- Risers: 200+
- Heat transfer:
  - Radiation: 80%
  - Convection: 20%

RCCS Experiment





Experimental data: flow oscillations during boiling



Been done before?

Two-phase, natural circulation stability in the literature exists (see thesis). But...

- Analytical work limited to simple equations-of-state
- Large volumes with piece-wise properties (non-dimensional numbers abound)
- System code usage hindered by simple discretization scheme and confounded by complicated models

What will be done here?

Use of RELAP, MELCOR, etc. for investigation was deemed unsound.

- Complicated models, without easy determination by user in some cases;
- Needed derivatives for stability not given and difficult to determine;
- Non-rigorous grid derivation or implementation of conservation law;
- Heuristic convergence methods instead of residual based determination.

Therefore, this work will cover the following

- Derive the conservation laws with careful consideration of uni-directional flow.
- Discuss the discretization and solution of those nonlinear equations;
- Outline the methodology used to determine the stability of the system;
- Apply all of the above to a test loop under single and two-phase conditions.

Outline

General Conservation Law (CLaw)

Conservation laws balance a vector of conserved variables **q**over a control volume.

Nonlinear form:

$$\frac{\partial q_i}{\partial t} + \frac{\partial f_i(q_i; x_i, t)}{\partial x_i} = s_i(q_i, z, t) \tag{1}$$

Quasilinear form:

$$\frac{\partial q_i}{\partial t} + \frac{\partial f_i(q_i; z, t)}{\partial q_i} \frac{\partial q_i(x_i, t)}{\partial z} = s_i(q_i, x_i, t) \tag{2}$$

Characteristic speeds:

$$\Lambda = \mathrm{Eig}\left[\frac{\partial f_i(q_i; z, t)}{\partial q_i} \right] \tag{3}$$

Conservation of Mass

Integral form:

$$\partial_t \int_\Omega \rho \, \mathrm{d}\Omega = \int_\Gamma -u_j \rho n_j \, \mathrm{d}\Gamma + \int_\Omega s^\rho \, \mathrm{d}\Omega \tag{4}$$

Differential form:

$$\partial_t \rho + \partial_j (u_j \rho) = s^\rho \tag{5}$$

Conservation of Momentum

Integral form:

$$\partial_t \int_\Omega \rho u_i \,\mathrm{d}\Omega = \int_\Gamma (-u_j \rho u_i) n_j \,\mathrm{d}\Gamma + \int_\Gamma (-\delta_{ij} P + \tau_{ij}) n_j \,\mathrm{d}\Gamma + \int_\Omega \rho g_i + s^u \,\mathrm{d}\Omega \qquad (6)$$

Differential form:

$$\partial_t(\rho u_i) + \partial_j(u_j \rho u_i) = -\partial_i P + \partial_i \tau_{ij} + \rho g_i + s^u \qquad (7)$$

Conservation of Energy

Integral form:

$$\partial_t \int_\Omega \rho e \, \mathrm{d}\Omega = \int_\Gamma [-(\rho e + P) u_j + u_i \tau_{ij} - q_j] n_j \, \mathrm{d}\Gamma + \int_\Omega \rho g_j u_j + s^e \, \mathrm{d}\Omega \qquad (8)$$

Differential form:

$$\partial_t (\rho e) + \partial_j [(\rho e + P) u_j] = \partial_j (u_i \tau_{ij} - q_j) + \rho g_j u_j + s^e \qquad (9)$$

Conservation of Bulk Momentum

Only want to track one momentum per cell.

Dot the Conservation of Momentum equation with bulk flow direction z_i:

$$\partial_t \int_\Omega \rho u_i z_i \,\mathrm{d}\Omega = \int_\Gamma (-u_j \rho u_i) n_j z_i \,\mathrm{d}\Gamma + \int_\Gamma (-\delta_{ij} P + \tau_{ij}) n_j z_i \,\mathrm{d}\Gamma + \int_\Omega \rho g_i z_i + s_z^u \,\mathrm{d}\Omega \quad (10)$$

Let $u_z = u_i z_i$:

$$\partial_t \int_\Omega \rho u_z \,\mathrm{d}\Omega = \int_\Gamma (-u_j \rho u_z) n_j \,\mathrm{d}\Gamma + \int_\Gamma (-\delta_{ij} P + \tau_{ij}) n_j z_i \,\mathrm{d}\Gamma + \int_\Omega \rho g_i z_i + s_z^u \,\mathrm{d}\Omega \quad (11)$$

Conservation of Bulk Momentum

Only want to track one momentum per cell.

Dot the Conservation of Momentum equation with bulk flow direction z_i:

$$\partial_t \int_\Omega \rho u_i z_i \, \mathrm{d}\Omega = \int_\Gamma (-u_j \rho u_i) n_j z_i \, \mathrm{d}\Gamma + \int_\Gamma (-\delta_{ij} P + \tau_{ij}) n_j z_i \, \mathrm{d}\Gamma + \int_\Omega \rho g_i z_i + s_z^u \, \mathrm{d}\Omega \quad (10)$$

Let $u_z = u_i z_i$:

$$\partial_t \int_\Omega \rho u_z \, \mathrm{d}\Omega = \int_\Gamma (-u_j \rho u_z) n_j \, \mathrm{d}\Gamma + \int_\Gamma (-\delta_{ij} P + \tau_{ij}) n_j z_i \, \mathrm{d}\Gamma + \int_\Omega \rho g_i z_i + s_z^u \, \mathrm{d}\Omega \quad (11)$$

Channel flow conservation:

$$\frac{\mathrm{d}}{\mathrm{d}t} \int_\Omega \rho u_z \, \mathrm{d}\Omega = \int_{\Gamma_1 + \Gamma_2} \pm (P + u_z \rho u_z) \, \mathrm{d}\Gamma + \int_{\Gamma_w} \tau_{ij} z_i n_j \, \mathrm{d}\Gamma + \int_\Omega \rho g \ \mathrm{Cos}(\theta) + s_z^u \, \mathrm{d}\Omega, \quad (12)$$

Other Assumptions

- Heat conduction and viscous heating is negligible compared to enthalpy flow
- Fluid-fluid friction is negligible compared to fluid-wall friction and form losses
- Time-rate of change of potential and kinetic energy is negligible to the thermal energy change

Results to equations

$$\rho e \approx \rho i \tag{13}$$

$$q_j \approx 0 \tag{14}$$

$$u_i \tau_{ij} \approx 0 \tag{15}$$

$$\tau_{ij} z_i n_j \approx \frac{1}{2} f_{\text{darcy}} \frac{L_{\text{char}}}{D_h} \operatorname{Abs}(\rho u_z)\, u_z \tag{16}$$

Equation of State

- IAPWS-95 non-ideal equation of state for water
- Magnificently huge curve fit of Helmholtz free energy potential
- Natural variables are ρ and T
- Back calculate T from ρ and i (plot)

Outline

Purpose

Derive quasi-two-dimensional thermohydraulic equations to enable adequate modeling of a branched system.

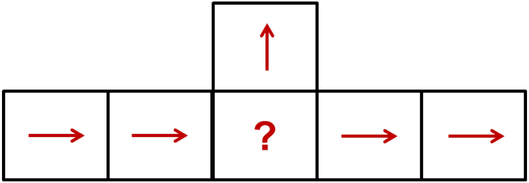
Consider only conservation of mass, momentum, and energy.

Methodology

- Consider a collection of control volumes and momentum cells.
- Information is exchanged through surface fluxes.
- Control volumes and momentum cells cover same physical space; but are off-set.

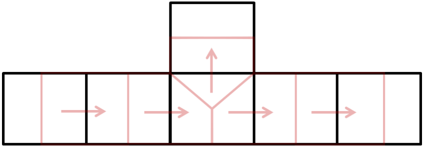
Coincident Spatial Grid

All equations solved on same grid:

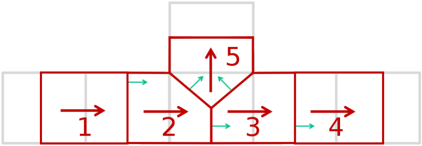


Staggered Spatial Grid

Mass and energy grid:



Momentum grid:



Semi-Discretized Control Volume Equations

Mass and energy for control k:

$$\frac{\mathrm{d}}{\mathrm{d}t}\int_{\Omega}\rho_k \,\mathrm{d}\Omega = s_k^{\rho} V_k + \sum_{n=1}^{N} u_n \rho_{d,n} A_n \tag{17}$$

$$\frac{\mathrm{d}}{\mathrm{d}t}\int_{\Omega}\rho i \,\mathrm{d}\Omega = s_k^{e} V_k + \sum_{n=1}^{N} u_n \rho h_{d,n} A_n \tag{18}$$

Semi-Discretized Momentum Cell Equation

Momentum for momentum cell k:

$$\frac{\mathrm{d}}{\mathrm{d}t}\int_{\Omega}\rho u_k \,\mathrm{d}\Omega = (\rho_k g_k + s_k^u)\, V_k - \sum_{n=1}^{N}(P_n z_n + u_{\mathrm{I},n}\rho u_{d,n})A_n - \frac{1}{2} f_{\mathrm{D},k}\,\frac{L_{\mathrm{char,k}}}{D_{\mathrm{eff,k}}}\,\mathrm{Abs}(\rho u_k)u_k A_k \tag{19}$$

Time Stepping

Semi-discrete equations are now of the form:

$$\partial_t q_i = D_i(q_i) \tag{20}$$

Various choices of stepping over a time step p:

$$q_i^p - q_i^{p-1} = \Delta t \, D_i(q_i^{p-1}) \tag{21}$$

$$q_i^p - q_i^{p-1} = \Delta t \, D_i(q_i^p) \tag{22}$$

$$q_i^p - q_i^{p-1} = \tfrac{1}{2} \Delta t \left[D_i(q_i^{p-1}) + D_i(q_i^p) \right] \tag{23}$$

$$q_i^p - q_i^{p-1} = \Delta t \left[D_i(q_i^{p-1}) + \partial_{q_i^{p-1}} D_i(q_i^{p-1}) \, (q_i^p - q_i^{p-1}) \right] \tag{24}$$

Outline

Full discretized equations

Consider the Implicit Euler full discretization:

$$q_i^p - q_i^{p-1} = \Delta t \, D_i(q_i^p) \tag{25}$$

How do you find q_i^p to satisfy that equations assuming D_i is nonlinear?

Newton-Raphson: Procedure

Put the equation into "residual" form

$$r(q_i^p) = q_i^p - q_i^{p-1} - \Delta t \, D_i(q_i^p) \tag{26}$$

and search for the vector q_i^p that makes $r(q_i^p)$ equal to 0 (or close enough).

Common search technique is Newton-Raphson method:

$$\text{Solve } \partial_{q_i} r(q_i^p) \, \Delta q_i^p = -r(q_i^p) \tag{27}$$

$$q_i^p = q_i^p + \Delta q_i^p \tag{28}$$

Newton-Raphson: Problems

- Calculating the Jacobian $\partial_{q_i} r(q_i^p)$ can be time and memory intensive.
- Solving the linear system is likewise difficult

JFNK

JFNK: Jacobian-Free Newton-Krylov method.

Krylov method

A particular way of solving the linear system $Ax = b$:

1. Compute a search direction z_n:

$$z_n = \begin{cases} r_{n-1} & \text{if } r_{n-1} < r_{n-2} \\ v_{n-1} & \text{otherwise} \end{cases} \tag{29}$$

2. Update a QR factorization:

$$[A\,z_1, A\,z_2, ..., A\,z_n] = V_n R_n \tag{30}$$

3. Update residual:

$$r_n = r_{n-1} - v_n^{\mathsf{T}} r_{n-1} v_n \tag{31}$$

4. Solve the system

$$R_n w_n = [v_1^{\mathsf{T}} r_1, ..., v_n^{\mathsf{T}} r_{n-1}]^{\mathsf{T}}; \quad x_n = x_0 + [z_1, ..., z_n] w_n \tag{32}$$

Approximate Jacobian

Important part to notice

$$[A\,z_1, A\,z_2, ..., A\,z_n] \tag{33}$$

The only new computation every iteration is Az_n (matrix-vector product).

Jacobian-Free method uses the following finite difference relation:

$$\partial_{q_i} r(q_i^p) z_n \approx \frac{r(q_i^p + \varepsilon z_n) - r(q_i^p)}{\varepsilon} \tag{34}$$

Instead of creating the Jacobian, approximate its existence using this formula (Jacobian-free) in a Krylov Method.

Jacobian-Free Newton-Krylov

A particular way of solving the linear system $Ax = b$:

1. Compute a search direction z_n:

$$z_n = \begin{cases} r_{n-1} & \text{if } r_{n-1} < r_{n-2} \\ v_{n-1} & \text{otherwise} \end{cases} \tag{35}$$

2. Update a QR factorization:

$$[A\, z_1, A\, z_2, ..., A\, z_n] = V_n R_n \tag{36}$$

3. Update residual:

$$r_n = r_{n-1} - v_n^{\mathrm{T}} r_{n-1} v_n \tag{37}$$

4. Solve the system

$$R_n w_n = [v_1^{\mathrm{T}} r_1, ..., v_n^{\mathrm{T}} r_{n-1}]^{\mathrm{T}}; \quad x_n = x_0 + [z_1, ..., z_n] w_n \tag{38}$$

Jacobian-Free Newton-Krylov

A particular way of solving the linear system $Ax = b$:

1. Compute a search direction z_n:

$$z_n = \begin{cases} r_{n-1} & \text{if } r_{n-1} < r_{n-2} \\ v_{n-1} & \text{otherwise} \end{cases} \tag{35}$$

2. Update a QR factorization:

$$[z_1, \frac{r(q_i^p + \varepsilon z_2) - r(q_i^p)}{\varepsilon}, ..., \frac{r(q_i^p + \varepsilon z_n) - r(q_i^p)}{\varepsilon}] = V_n R_n \tag{36}$$

3. Update residual:

$$r_n = r_{n-1} - v_n^{\mathsf{T}} r_{n-1} v_n \tag{37}$$

4. Solve the system

$$R_n w_n = [v_1^{\mathsf{T}} r_1, ..., v_n^{\mathsf{T}} r_{n-1}]^{\mathsf{T}}; \quad x_n = x_0 + [z_1, ..., z_n] w_n \tag{38}$$

Outline

Perturbation equations

Assumed that the true solution is a summation of a steady-state and a transient

$$q_i(x_i, t) = q_i^{\mathrm{ss}}(x_i) + \delta q_i(x_i, t). \tag{39}$$

Perturbation equations

Assumed that the true solution is a summation of a steady-state and a transient

$$q_i(x_i, t) = q_i^{\text{ss}}(x_i) + \delta q_i(x_i, t). \tag{39}$$

General nonlinear perturbation equation (diagrams):

$$\frac{\partial \delta q_i}{\partial t} + \frac{\partial}{\partial x_j}[f_{ij}(q_i^{\text{ss}} + \delta q_i)] = s_i(q_i^{\text{ss}} + \delta q_i) \tag{40}$$

Perturbation equations

Assumed that the true solution is a summation of a steady-state and a transient

$$q_i(x_i, t) = q_i^{ss}(x_i) + \delta q_i(x_i, t). \tag{39}$$

General nonlinear perturbation equation (diagrams):

$$\frac{\partial \delta q_i}{\partial t} + \frac{\partial}{\partial x_j}[f_{ij}(q_i^{ss} + \delta q_i)] = s_i(q_i^{ss} + \delta q_i) \tag{40}$$

Taylor expansion about perturbation (neglecting H.O.T.) yields general linear perturbation equation:

$$\frac{\partial \delta q_i}{\partial t} + \frac{\partial}{\partial x_j}\left[\frac{\partial f_{ij}}{\partial q_k^{ss}} \delta q_k\right] = \frac{\partial s_i}{\partial q_k^{ss}} \delta q_k \tag{41}$$

Solution method of general linear equations

Perturbations still part of spatially varying PDE.

Discretizing like full transient equations will yield spurious, positive eigenvalues from mass/energy advection.

Solution: integration over entire system and isolate global time-evolution on left-hand side:

$$\partial_t \delta q_i(t) = \frac{1}{\int_\Omega \mathrm{d}\Omega} \left[\int_\Omega \frac{\partial s_i}{\partial q_k^{\mathrm{ss}}} \, \mathrm{d}\Omega - \int_\Gamma \frac{\partial f_{ij}}{\partial q_k^{\mathrm{ss}}} n_j \, \mathrm{d}\Gamma \right] \delta q_k(t) \tag{42}$$

Solution method of thermohydraulic system

Apply to mass, energy, momentum system:

$$\frac{\mathrm{d}}{\mathrm{d}t}\begin{bmatrix}\delta\rho\\ \delta\rho i\\ \delta\rho u_z\end{bmatrix} = -\partial_j\left(\begin{bmatrix}\partial_{q_k}(\rho u_j)\\ \\ \partial_{q_k}[(\rho i + P)u_j]\\ \\ \partial_{q_k}(u_j\rho u_z + P\delta_{ij}z_i - \tau_{ij}z_i)\end{bmatrix}\delta q_k\right) + \left(\begin{bmatrix}\partial_{q_k}(s^\rho)\\ \partial_{q_k}(s^e)\\ \partial_{q_k}(\rho g_z + s_z^u)\end{bmatrix}\delta q_k\right) \tag{43}$$

Solution method of thermohydraulic system

Integrating to the skin of the system and eliminating terms that vanish:

$$\frac{\mathrm{d}}{\mathrm{d}t}\begin{bmatrix}\delta\rho\\ \delta\rho i\\ \delta\rho u_z\end{bmatrix} = \frac{1}{V_{\text{sys}}}\begin{bmatrix}0 & 0 & 0\\ 0 & 0 & 0\\ \alpha_\rho & \alpha_{\rho i} & \alpha_{\rho u_z}\end{bmatrix}\begin{bmatrix}\delta\rho\\ \delta\rho i\\ \delta\rho u_z\end{bmatrix}, \tag{43}$$

where $\alpha_* = -\int_\Gamma \partial_* \Delta P_{\text{dar}}\,\mathrm{d}\Gamma$

Solution method of thermohydraulic system

Integrating to the skin of the system and eliminating terms that vanish:

$$\frac{\mathrm{d}}{\mathrm{d}t}\begin{bmatrix}\delta\rho\\ \delta\rho i\\ \delta\rho u_z\end{bmatrix} = \frac{1}{V_{\text{sys}}}\begin{bmatrix}0 & 0 & 0\\ 0 & 0 & 0\\ \alpha_\rho & \alpha_{\rho i} & \alpha_{\rho u_z}\end{bmatrix}\begin{bmatrix}\delta\rho\\ \delta\rho i\\ \delta\rho u_z\end{bmatrix}, \tag{43}$$

where $\alpha_* = -\int_\Gamma \partial_* \Delta P_{\text{dar}}\,\mathrm{d}\Gamma$

With the solution

$$\begin{bmatrix}\delta\rho(t)\\ \delta\rho i(t)\\ \delta\rho u_z(t)\end{bmatrix} = \begin{bmatrix}1 & 0 & 0\\ 0 & 1 & 0\\ \frac{\alpha_\rho}{\alpha_{\rho u_z}}\left(e^{\tilde{\alpha}t}-1\right) & \frac{\alpha_{\rho i}}{\alpha_{\rho u_z}}\left(e^{\tilde{\alpha}t}-1\right) & e^{\tilde{\alpha}t}\end{bmatrix}\begin{bmatrix}\delta\rho(0)\\ \delta\rho i(0)\\ \delta\rho u_z(0)\end{bmatrix}, \tag{44}$$

where $\tilde{\alpha} = \alpha_{\rho u_z}/V_{\text{sys}}$.

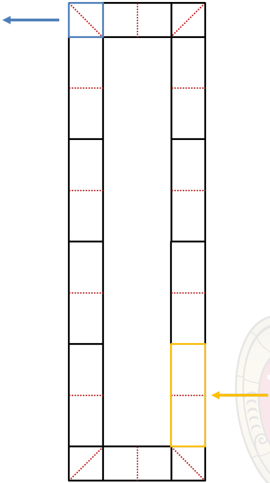
Outline

Methodology

- All closed-loop systems exhibit a singular steady-state solution.
- Solution: perform a transient calculation that provided diagonal regularity and run transient to a stationary-state using all previous equations and tools.
- Once the steady-state is attained, computer the eigenvalues and examine.

Primary Test Loop

- 14 control volume / momentum cells
- 1.4 meters high, 0.4 meters wide (3.5 aspect ratio)
- 0.1 meter hydraulic diameter



Single Phase Test Region

The single phase region was investigated over a rectangle in P-T space:

- $P \in [101\,325\,\mathrm{Pa}, 202\,650\,\mathrm{Pa}]$
- $T \in [300\,\mathrm{K}, 372\,\mathrm{K}]$

at heat loads of 1, 2, 4, 8, and 16 kW.

All values, such as pressure and temperature, refer the state of the cooling volume at steady-state, unless otherwise noted.

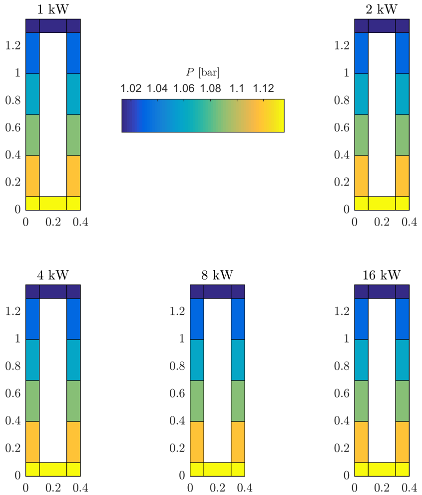
Single Phase Thermohydraulic Summary

Parameters	Heat Load kW				
	1	2	4	8	16
Avg. Temperature Rise [ΔK]	0.2392	0.3677	0.5428	0.7944	1.26
Avg. Pressure Difference [ΔkPa]	12.504	12.501	12.501	12.500	12.500
Avg. Mass Flow Rate [$\mathrm{kg\,s^{-1}}$]	1.012	1.33	1.80	2.44	3.08
$\dot{m}c_p\Delta T$ [kW]*	1.02	2.05	4.08	8.10	16.2

* $c_p = 4182\,\mathrm{J\,kg^{-1}\,K^{-1}}$

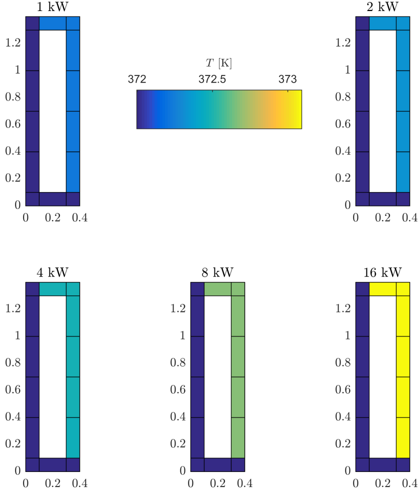
Single Phase Characterization

Pressure distribution at {372 K,101 325 Pa}



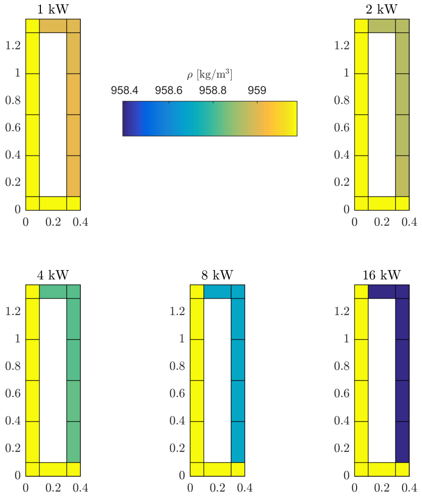
Single Phase Characterization

Temperature distribution at $\{372\,\mathrm{K}, 101\,325\,\mathrm{Pa}\}$

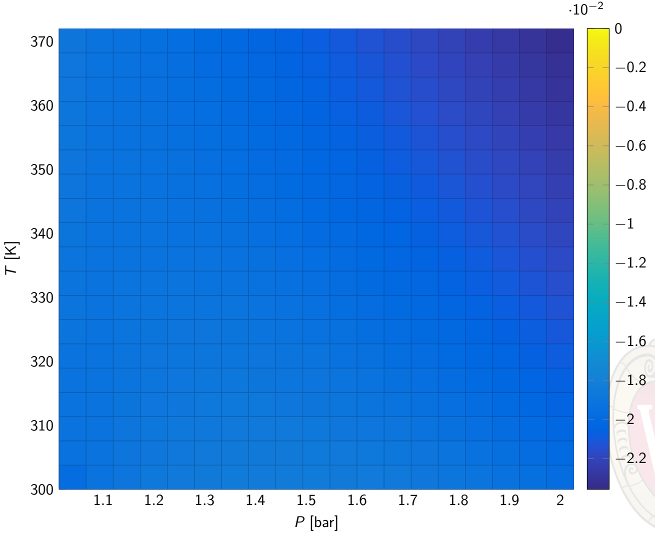


Single Phase Characterization

Density distribution at $\{372\,\mathrm{K}, 101\,325\,\mathrm{Pa}\}$

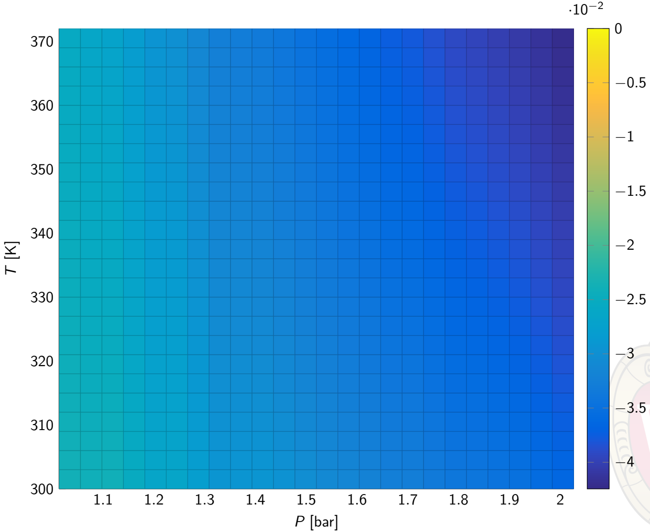


Single Phase Eigenvalue Plots



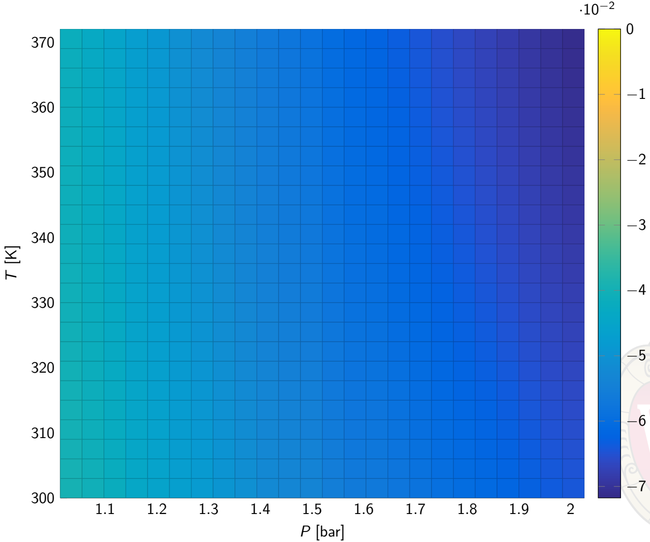
Heat load: 1 kW

Single Phase Eigenvalue Plots



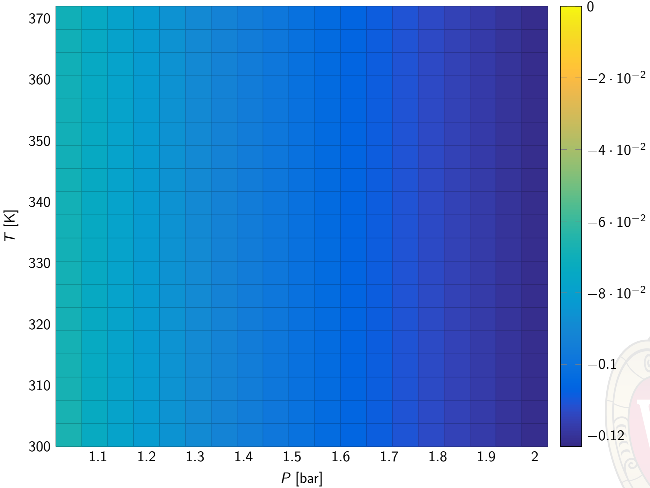
Heat load: 2 kW

Single Phase Eigenvalue Plots



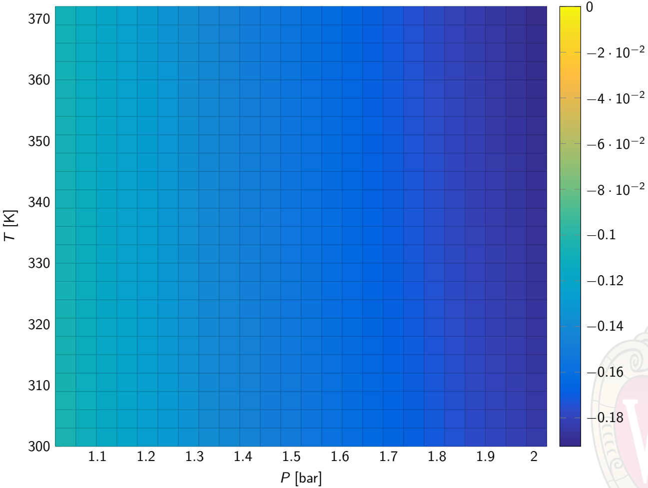
Heat load: 4 kW

Single Phase Eigenvalue Plots



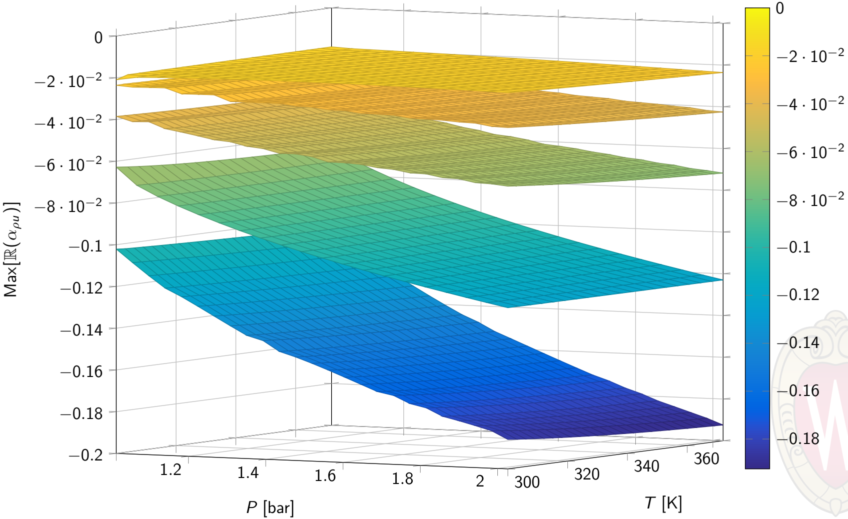
Heat load: 8 kW

Single Phase Eigenvalue Plots



Heat load: 16 kW

Single Phase All Eigenvalue Plots



Two-Phase Results

The two-phase region was investigated along the liquid saturation from 372 K (0.97 bar) to 390 K (1.7964 bar) at heat loads of 1, 2, 4, and 6 kW. The temperature range corresponds roughly to the tank saturation conditions investigated at the UW–Madison Experiment: 1 bar to 1.75 bar.

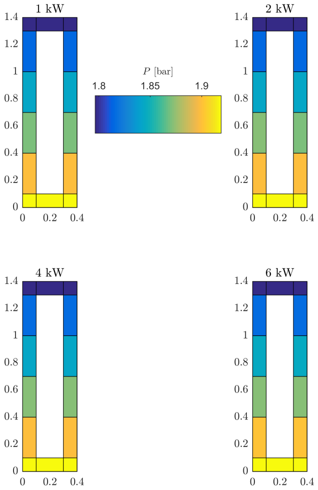
All values, such as pressure and temperature, refer the state of the cooling volume at steady-state, unless otherwise noted.

Two-Phase Thermohydraulic Summary

Parameters	Heat Load			
	1 kW	2 kW	4 kW	6 kW
Avg. Temperature Rise [ΔK]	0.034	0.0352	0.0951	0.13
Avg. Pressure Difference [ΔkPa]	12.17	12.17	12.29	12.38
Avg. Mass Flow Rate [$\mathrm{kg\,s^{-1}}$]	6.89	6.97	9.92	10.89
Avg. Maximum Quality [10^4]	0.648	0.671	1.68	2.22

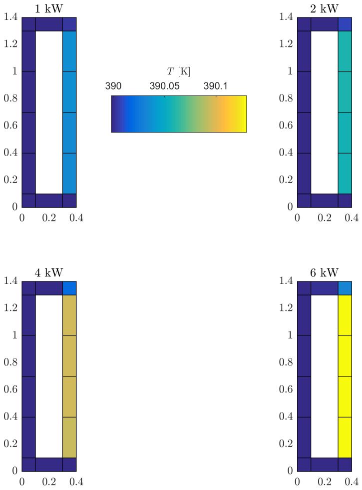
Two Phase Characterization

Pressure distribution at {390 K,179 645 Pa}



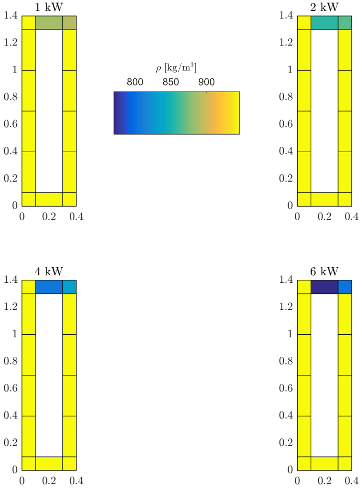
Two Phase Characterization

Temperature distribution at $\{390\,\mathrm{K}, 179\,645\,\mathrm{Pa}\}$



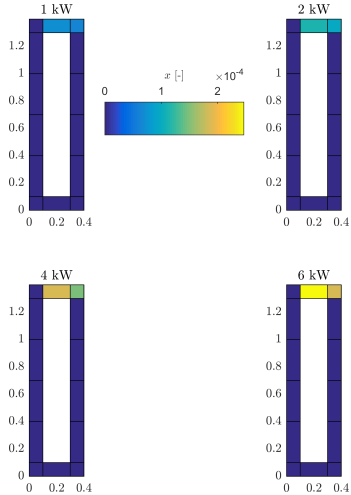
Two Phase Characterization

Density distribution at $\{390\,\mathrm{K}, 179\,645\,\mathrm{Pa}\}$

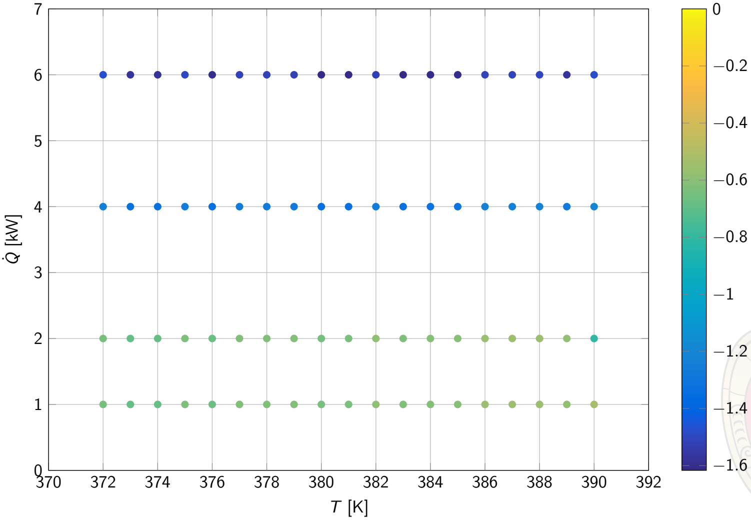


Two Phase Characterization

Quality distribution at $\{390\,\mathrm{K}, 179\,645\,\mathrm{Pa}\}$



Two Phase Eigenvalue Plot



Conclusions

- Test loop is stable under all tested states and phases under the assumptions made.
- Pressure and increased heat load are stablizing forces for the system.

Outline

Future Work

- **Modeling:** Explore different, larger, and more complicated geometries with the current toolset.
- **Programming:** Re-write thermodynamics package in a compiled form for increased speed.
- **Numerics:** Improve JFNK solver with built-in fallback routine so full system time-step fallbacks aren't so costly; explore higher-order time stepping algorithms (TR-BDF2).
- **Physics:** Add in more physics to improve on the modeling: boil-off, heat diffusion, true two-phase models.
- **Mathematics:** Examine the non-normal stability matrix using pseudospectra analysis to better assess the effects of short-time transients on the stability of the system.

Questions

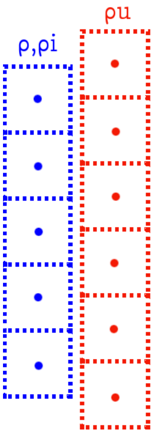
"The key to wisdom is this: constant and frequent questioning. For by doubting we are led to question, and by questioning we arrive at the truth."

— Peter Abelard

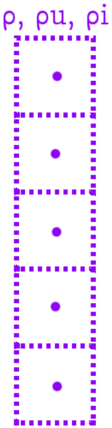
Outline

Staggered/Collocated

Staggered mesh:

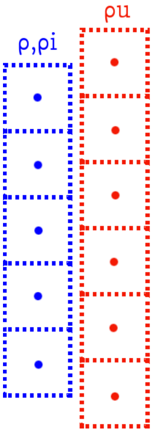


Collocated mesh:

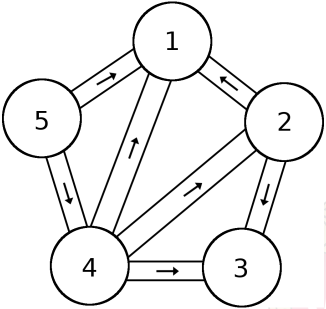


Rigorous vs. Non-Rigorous

Rigorous staggered mesh (CFD):

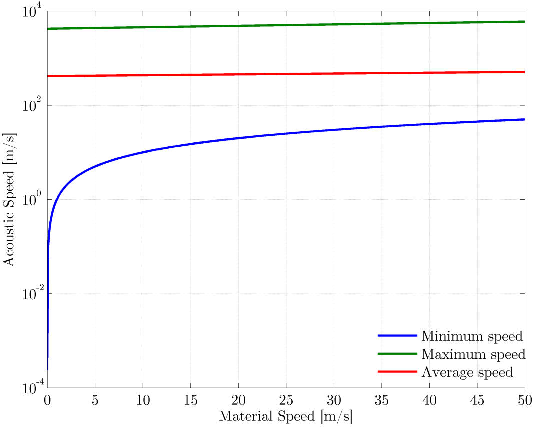


Non-rigorous staggered mesh (System codes):



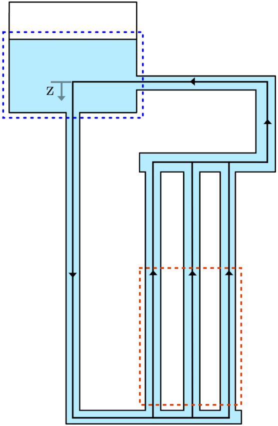
return

Acoustic Speeds

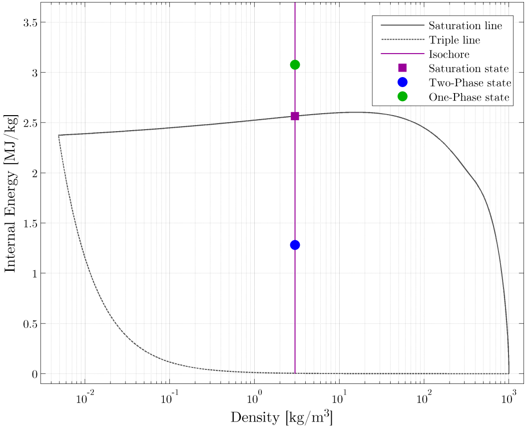


return

Non-simple, closed loop



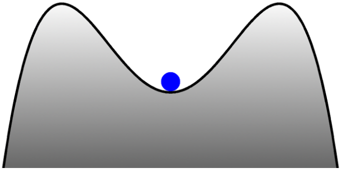
i-ρDiagram



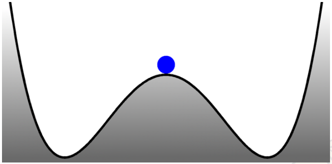
return

Stability Diagrams

Linearly stable, nonlinearly unstable:

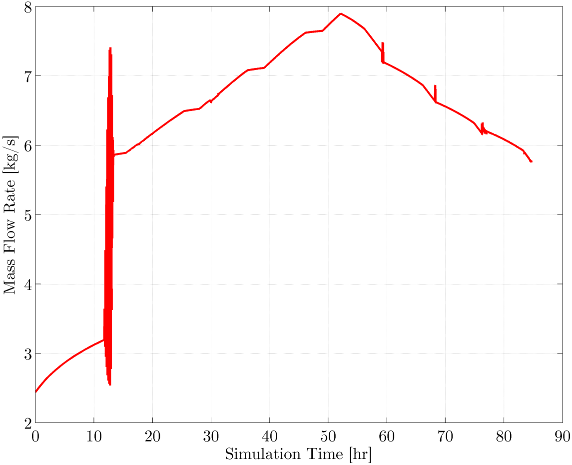


Linearly unstable, nonlinearly stable:



return

System Mass flow: 4 days



return

Multiphase Model

$$\frac{\partial}{\partial t}\begin{bmatrix} \alpha\rho_\phi \\ \alpha\rho u_\phi \\ \alpha\rho i_\phi \end{bmatrix} + \frac{\partial}{\partial z}\begin{bmatrix} \alpha\rho u_\phi \\ u_\phi\,\alpha\rho u_\phi + P(\rho_\phi, i_\phi) \\ u_\phi[\alpha\rho i_\phi + P(\rho_\phi, i_\phi)] \end{bmatrix} = \tag{45}$$

$$\begin{bmatrix} \mathbb{M}_\phi \\ \alpha\rho_\phi g(z) - \frac{K_{\mathrm{eff},\phi}(\mathbf{q})}{2} u_\phi \left|\alpha\rho u_\phi\right| + \mathbb{P}_\phi \\ \dot{Q}_{\mathrm{add},\phi}(\mathbf{q}, z, t) + \mathbb{E}_\phi \end{bmatrix}$$