

3D Printing Support Reduction via Skinning Deformation

Extended Abstract

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Figure 1: Our method generates natural skinning deformation with reduced support structures

ABSTRACT

In layer-based 3D fabrication, supporting materials are fabricated to support overhanging regions yet discarded later. Reducing supports saves both time and material cost. In this abstract, we propose a skinning-based deformation method that slims down the supporting structure. We achieve this by searching globally in the space of linear blending transformations on skeleton handles, making a trade-off among as-rigid-as-possible, overhang, and self-intersection energies. Beyond minimizing supports, our method generates semantically meaningful deformation while avoiding artifacts e.g. self-intersection. This approach could be generalized to include arbitrary constraints by incorporating additional objectives, such as the center of mass for balancing and physical properties of printing material for self-support. With precomputed skinning weights, our method has the potential to be GPU accelerated and employed as a real-time user interface that helps model design and fabrication.¹

CCS CONCEPTS

- Computing methodologies → Mesh geometry models.

KEYWORDS

geometry processing, shape deformation, 3D fabrication

INTRODUCTION

Fused filament fabrication is a popular 3D fabrication process whereby the molten materials are deposited layer by layer. Supporting structures are fabricated concurrently and act as a fixture to support the weight of the material in overhanging regions. However, supporting structures introduce material waste and prolong the time required for fabrication. Additionally, the support removal step is performed manually or by dissolution, which are easy to

damage the model and leave visual artifacts on the surface. Thus, it is desirable to print models with minimal supporting structures.

There are several approaches to tackle the problem [5]. One approach focuses on finding the best printing orientation and designing better support generation algorithms [9]. There has also been work on incorporating support structure constraints in topology optimization during model design [6]. The approach most relevant to this abstract relies on deforming the shape itself for self-support in situations where the geometry of the shape is not necessary to be perfectly preserved. There has been an attempt to reduce the number of overhanging regions iteratively by deforming an enclosing coarser volumetric mesh [1].

Linear blend skinning is a fast deformation method. Recent work has shown impressive results in automatically generating weights for smooth and intuitive deformations [4] and in efficiently computing as-rigid-as-possible deformations by searching the subspace of skinning deformations [3].

This abstract presents a method for finding natural deformations with reduced support structures. We pose the problem of support reduction as a global optimization problem over the space of linear blend skinning deformations minimizing a weighted combination of several objectives, namely

- (1) local distortion [8]
- (2) support structures
- (3) self-intersection

We implemented a prototype and fabricated some models for visualization.

METHOD

Let $\mathcal{M} = (\mathbf{V}, \mathbf{F})$ be a rest-pose mesh living in dimension $d \in \{2, 3\}$. Let $\mathbf{V} = \{\mathbf{v}_1^T, \dots, \mathbf{v}_n^T\}^T \in \mathbb{R}^{n \times d}$ be the rest-pose vertex positions. Let $\mathcal{M}' = (\mathbf{V}', \mathbf{F})$ be the deformed mesh.

LINEAR BLEND SKINNING. Given a set of handles $\mathcal{H} = \{\mathbf{h}_1, \dots, \mathbf{h}_m\}$, we can apply an affine transformation $\mathbf{T}_j \in \mathbb{R}^{d \times (d+1)}$ on each handle \mathbf{h}_j . Let $\mathbf{T} = \{\mathbf{T}_1^T, \dots, \mathbf{T}_m^T\}^T \in \mathbb{R}^{(d+1)m \times d}$. Linear blend skinning is a deformation method whereby the vertex positions on the deformed shape are represented as a weighted linear combination of

¹Code is available at https://github.com/tt6746690/fast_support_reduction

the handles' transformations,

$$\mathbf{v}'_i = \sum_{j=1}^m w_j(\mathbf{v}_i) \mathbf{T}_j \begin{pmatrix} \mathbf{v}_i \\ 1 \end{pmatrix}$$

where $w_j : \mathcal{M} \rightarrow \mathbb{R}$ is computed using bounded biharmonic weights.[4] Equivalently, $\mathbf{V}' = \mathbf{MT}$, where $\mathbf{M} \in \mathbb{R}^{n \times (d+1)m}$ is a matrix combining \mathbf{V} and \mathbf{W} as noted in [3].

AS-RIGID-AS-POSSIBLE ENERGY. To obtain natural deformations, we minimize a distortion energy $E_{arap} : \mathbb{R}^{n \times d} \rightarrow \mathbb{R}$ which measures local deviation from rigidity and acts to preserve shape details [8]

$$E_{arap}(\mathbf{V}') = \frac{1}{2} \sum_{f \in \mathcal{F}} \sum_{(i,j) \in f} c_{ijf} \|(\mathbf{v}'_i - \mathbf{v}'_j) - \mathbf{R}_f(\mathbf{v}_i - \mathbf{v}_j)\|^2$$

where $\mathbf{R}_f \in SO(d)$ are per-face rotations and $c_{ijf} \in \mathbb{R}$ are cotangent weights. Let $\mathbf{R} = \{\mathbf{R}_1^T, \dots, \mathbf{R}_f^T, \dots, \mathbf{R}_n^T\}^T \in \mathbb{R}^{dn \times d}$. We can find \mathbf{R} in a local step before computing E_{arap} ,

$$\mathbf{R} = \arg \min_{\mathbf{R}} \text{tr}(\mathbf{R} \tilde{\mathbf{K}} \mathbf{T})$$

as specified in [3] via singular value decomposition.

OVERHANG ENERGY. An overhanging region that can be 3D printed without support is called *self-supported*. We call the angle between the region's tangent plane and printing direction the *self-supported angle* α . Let α_{max} be the maximum supporting angle. Let $\tau = \sin(\alpha_{max})$ be the *maximal supporting coefficient*. A surface $f \in \mathcal{F}$ is considered *risky* and thus requires support if,

$$\arccos(\mathbf{n}_f \cdot \mathbf{d}_p) > \pi + \alpha_{max} \rightarrow \mathbf{n}_f \cdot \mathbf{d}_p < -\tau$$

where \mathbf{n}_f is unit normal of face f and \mathbf{d}_p is the printing direction. Let $\partial \mathcal{M}' \subset \mathcal{F}$ be surface faces of the deformed mesh. We can approximate the volume of support required for any risky face f by computing the volume of a rectangular prism,

$$\lambda(f) = \begin{cases} A_{base}h = A_f |\mathbf{n}_f \cdot \mathbf{d}_p| (\mathbf{c}_f \cdot \mathbf{d}_p) & \text{if } \mathbf{n}_f \cdot \mathbf{d}_p < -\tau \\ 0 & \text{otherwise} \end{cases}$$

where A_f is the area of the face, \mathbf{c}_f is the centroid of the face. We define an overhang energy $E_{overhang} : \mathbb{R}^{n \times d} \rightarrow \mathbb{R}$ which measures the volume of support required,

$$E_{overhang}(\mathbf{V}') = \sum_{f \in \partial \mathcal{M}'} \lambda(f)$$

SELF-INTERSECTION ENERGY. One dominant artifact in skinning deformations is self-intersection, which renders the shape unprintable. We call a subset of mesh \mathcal{M} bordered by intersecting tetrahedra a *self-intersecting region*. To measure the volume V_i of self-intersecting region i , we define a $k \times h$ grid below the mesh and trace rays up in the printing direction from every grid point. A ray is inside a self-intersecting region if $\mathbf{d}_p \cdot \mathbf{n}_f < 0$ for 2 consecutively incident faces. The sum of distances d_j that the j -th ray traversed inside a self-intersecting region approximates the volume. We define a self-intersection energy $E_{intersect} : \mathbb{R}^{n \times d} \rightarrow \mathbb{R}$ which measures the total volume of the self-intersecting regions as follows,

$$E_{intersect}(\mathbf{V}') = \sum_i V_i = \sum_{j=1}^{k \times h} d_j$$

OPTIMIZATION. We perform global optimization over the space of linear blend skinning transformations using particle swarm optimization, as described in [2]. We define a single objective function $E : \mathbb{R}^{3m} \rightarrow \mathbb{R}$ as a weighted sum of the three energy functions,

$$E(\mathbf{x}) = \omega_1 E_{arap}(\mathbf{V}') + \omega_2 E_{overhang}(\mathbf{V}') + \omega_3 E_{intersect}(\mathbf{V}')$$

where $\mathbf{x} = \{\phi_j, \theta_j, \psi_j\}_{j=1}^m$ are Euler's angles describing the local rotation for each handle $h_j \in \mathcal{H}$. We use forward kinematics to propagate local rotations \mathbf{x} in order to compute the transformation matrix \mathbf{T} . We apply the linear blend skinning formula $\mathbf{V}' = \mathbf{MT}$ to determine vertex positions for the deformed mesh, from which we can work out the value of the as-rigid-as-possible, overhang, and self-intersection energies. $\omega_1, \omega_2, \omega_3$ are hyperparameters used to adjust the relative weight of different objectives and are fixed a priori.

EXPERIMENTS & RESULTS

We use the same default settings for particle swarm optimization as specified in [2] with 200 random initial particles and 120 iterations for both Figure. 1 and Figure. 2. By quantitatively comparing the viewer and fabricated models, we observe a reduction in the number of *risky* faces as well as support materials used. The generated deformations are natural and have negligible self-intersections.

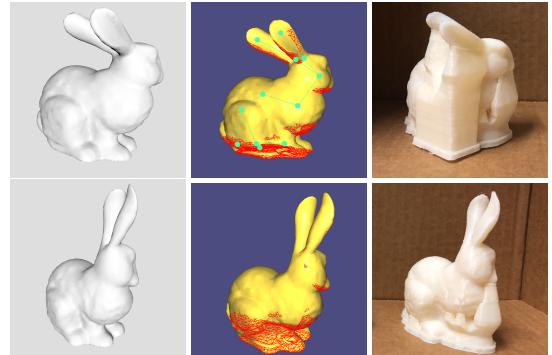


Figure 2: Our method reduces support material usage by 37% on the Stanford bunny

Table 1: Statistics of Support Reduction Performance

Model	Before	After	Reduced By
Big Buck Bunny Figure 1	$0.98in^3$	$0.83in^3$	15%
Stanford Bunny Figure 2	$0.79in^3$	$0.50in^3$	37%

LIMITATIONS AND FUTURE WORK

Hyperparameters $\omega_1, \omega_2, \omega_3$ are tuned manually by experimentation and there is no clear way to pick sensible values because the objectives are tradeoffs and often act in conflict with each other. For example, an overhang free deformation may introduce a large amount of distortion. In future work, we would like to investigate more on multi-objective optimization.

Currently, an entire run of the optimization procedure takes several minutes for Figure. 1 and Figure. 2. There is huge potential in moving the linear blend skinning and energy computations to

vertex shaders for fast and parallel execution. In future work, we want to re-implement bottleneck steps using OpenGL for real time computation to allow for interactive design.

Although we have decided to look at support reduction, the method can be easily adapted to incorporate additional constraints. For example, we can formulate another energy term to account for center of mass for self-balancing [7] or to account for the physical strength of the fabrication material. In future work, we want to include additional constraints to make the 3D model support itself in a variety of scenarios.

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