

3D Printing Support Reduction via Skinning Deformation

Extended Abstract

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Figure 1: Our method generates natural skinning deformation with reduced support structures

ABSTRACT

In layer-based 3D fabrication, supporting materials are fabricated to support overhanging regions and are discarded later; reducing supports save time and material cost. We introduce a deformation-based method that minimizes supporting structures. The method searches globally in the space of linear blending transformations on skeleton handles, minimizing distortion, overhang, and self-intersection. Our method produces natural deformations requiring minimal supporting structures while avoiding artifacts such as self-intersection. Our method can be generalized to include arbitrary constraint by incorporating additional objectives, such as accounting for center of mass for balancing and physical property of the printing material for self-support.¹

CCS CONCEPTS

- Computing methodologies → Mesh geometry models.

KEYWORDS

geometry processing, shape deformation, 3D fabrication

Introduction

Fused filament fabrication is a popular 3D fabrication process whereby the molten materials are deposited layer by layer. Supporting structures are fabricated concurrently and act as a fixture to support the weights of material that constitute the overhanging regions. Supporting structures introduce material waste and prolong the time required for fabrication. Additionally, they often require manual removal and could potentially introduce damage to the model itself. It is desirable to print models with minimal supporting structures.

There are several approaches to the problem. [5] One approach focuses on finding the best printing orientation and designing better support generation algorithms. [9] Alternatively, people have

¹Code is available at https://github.com/tt6746690/fast_support_reduction

incorporated support structure constraints to topology optimization during model design. [6] The most relevant approach to this abstract relies on deforming the shape itself for self-support in situation where the geometry of the shape is not critical. There has been attempt to reduce the number of overhanging regions iteratively by deforming an enclosing coarser volumetric mesh. [1].

Linear blend skinning is a fast deformation method. Recent work shown impressive result in automatically generating weights for smooth and intuitive deformation [4] and in efficiently computing as-rigid-as-possible deformations by searching in the subspace of skinning deformations. [3].

This abstract presents a method for finding natural deformations with reduced support structures. We pose the problem of support reduction as a global optimization problem over the space of linear blend skinning deformations minimizing several objectives, namely

- (1) local distortion [8]
- (2) support structures
- (3) self-intersection

We implemented a prototype and fabricated some model for visualization.

Method

Let $\mathcal{M} = (\mathbf{V}, \mathbf{F})$ be rest-pose mesh living in dimension $d \in \{2, 3\}$. Let $\mathbf{V} = \{\mathbf{v}_1^T, \dots, \mathbf{v}_n^T\}^T \in \mathbb{R}^{n \times d}$ be the rest-pose vertex positions. Let $\mathcal{M}' = (\mathbf{V}', \mathbf{F})$ be deformed mesh.

Linear Blend Skinning. Given a set of handles $\mathcal{H} = \{\mathbf{h}_1, \dots, \mathbf{h}_m\}$, we can apply an affine transformation $\mathbf{T}_j \in \mathbb{R}^{d \times (d+1)}$ on each handle \mathbf{h}_j . Let $\mathbf{T} = \{\mathbf{T}_1^T, \dots, \mathbf{T}_m^T\}^T \in \mathbb{R}^{(d+1)m \times d}$. Linear blend skinning is a deformation method whereby the vertex positions on the deformed shape are represented as a weighted linear combination of the handles' transformations,

$$\mathbf{v}'_i = \sum_{j=1}^m w_j(\mathbf{v}_i) \mathbf{T}_j \begin{pmatrix} \mathbf{v}_i \\ 1 \end{pmatrix}$$

where $w_j : \mathcal{M} \rightarrow \mathbb{R}$ is computed using bounded biharmonic weights.[4] Equivalently, $\mathbf{V}' = \mathbf{M}\mathbf{T}$, where $\mathbf{M} \in \mathbb{R}^{n \times (d+1)m}$ is a matrix combining \mathbf{V} and \mathbf{W} as noted in [3].

As-rigid-as-possible Energy. To obtain natural deformations, we minimize a distortion energy $E_{arap} : \mathbb{R}^{n \times d} \rightarrow \mathbb{R}$ which measures local deviation from rigidity and acts to preserve shape detail. [8]

$$E_{arap}(\mathbf{V}') = \frac{1}{2} \sum_{f \in \mathcal{F}} \sum_{(i,j) \in f} c_{ijf} \|(\mathbf{v}'_i - \mathbf{v}'_j) - \mathbf{R}_f(\mathbf{v}_i - \mathbf{v}_j)\|^2$$

where $\mathbf{R}_f \in SO(d)$ are per-face rotations and $c_{ijk} \in \mathbb{R}$ are cotangent weights. Let $\mathbf{R} = \{\mathbf{R}_1^T, \dots, \mathbf{R}_f^T, \dots, \mathbf{R}_n^T\}^T \in \mathbb{R}^{dn \times d}$. We can find \mathbf{R} in local step before computing E_{arap} ,

$$\mathbf{R} = \arg \min_{\mathbf{R}} \text{tr}(\tilde{\mathbf{R}} \mathbf{T})$$

as specified in [3] via singular value decomposition.

Overhang Energy. An overhanging region that can be 3D printed without support is called *self-supported*. We call the angle between the region's tangent plane and printing direction the *self-supported angle* α . Let α_{max} be the maximum supporting angle. Let $\tau = \sin(\alpha_{max})$ be the *maximal supporting coefficient*. A surface $f \in \mathcal{F}$ is considered *risky* and thus requires support if,

$$\arccos(\mathbf{n}_f \cdot \mathbf{d}_p) > \pi + \alpha_{max} \rightarrow \mathbf{n}_f \cdot \mathbf{d}_p < -\tau$$

where \mathbf{n}_f is unit normal of face f and \mathbf{d}_p is the printing direction. Let $\partial \mathcal{M}' \subset \mathcal{F}$ be surface faces of the deformed mesh. Let $A(\cdot)$ be the area function and $c(\cdot)$ be the centroid function for a face f . We can approximate the volume of support required for any face risky f by computing the volume of a rectangular prism,

$$\lambda(f) = \begin{cases} A_{base}h = A_f |\mathbf{n}_f \cdot \mathbf{d}_p| (\mathbf{c}_f \cdot \mathbf{d}_p) & \text{if } \mathbf{n}_f \cdot \mathbf{d}_p < -\tau \\ 0 & \text{otherwise} \end{cases}$$

where A_f is the area of the face, \mathbf{c}_f is the centroid of the face. We define an overhang energy $E_{overhang} : \mathbb{R}^{n \times d} \rightarrow \mathbb{R}$ which measures the volume of support required,

$$E_{overhang}(\mathbf{V}') = \sum_{f \in \partial \mathcal{M}'} \lambda(f)$$

Self-intersection Energy. One dominant artifact in skinning deformation is self-intersection, which renders the shape not 3D printable. We call a subset of mesh \mathcal{M} bordered by intersecting tetrahedra the *self-intersecting region*. To quantify the total volume V_i of each self-intersecting region, we define a $k \times k$ grid below the mesh and trace rays up in direction of the printing direction from every grid point. A ray is inside a self-intersecting region if $\mathbf{d}_p \cdot \mathbf{n}_f < 0$ for 2 consecutively incident faces. Summation of distances d_j that j -th ray traversed inside a self-intersecting region approximates the volume. We can define a self-intersection energy $E_{intersect} : \mathbb{R}^{n \times d} \rightarrow \mathbb{R}$ which measures the total volume of the self-intersecting regions as follows,

$$E_{intersect}(\mathbf{V}') = \sum_i V_i = \sum_{j=1}^{k \times k} d_j$$

Optimization. We perform global optimization over the space of linear blend skinning transformations using particle swarm optimization, as noted in [2]. We define a single objective function $E : \mathbb{R}^{3m} \rightarrow \mathbb{R}$ as a weighted sum of 3 energy functions,

$$E(\mathbf{x}) = \omega_1 E_{arap}(\mathbf{V}') + \omega_2 E_{overhang}(\mathbf{V}') + \omega_3 E_{intersect}(\mathbf{V}')$$

where $\mathbf{x} = \{\phi_j, \theta_j, \psi_j\}_{j=1}^m$ are Euler's angles describing the local rotation for each handle $h_j \in \mathcal{H}$. We use forward kinematics to propagate local rotations \mathbf{x} in order to compute the transformation matrix \mathbf{T} . We apply linear blend skinning formula $\mathbf{V}' = \mathbf{MT}$ to determine vertex positions for the deformed mesh, from which we can determine the value for as-rigid-as-possible, overhang, and self-intersection energy. $\omega_1, \omega_2, \omega_3$ are hyperparameters used to adjust relative weight of different objectives and are chosen a posteriori.

Experiments & Results

We use the same default settings for particle swarm optimization as specified in [2] with 200 random initial particles and 120 iterations for both Figure. 1 and Figure. 2. By observing the viewer and fabricated model, we observe a reduction in the number of *risky* faces as well as support materials used. The generated deformation are natural and have some but negligible self-intersection.

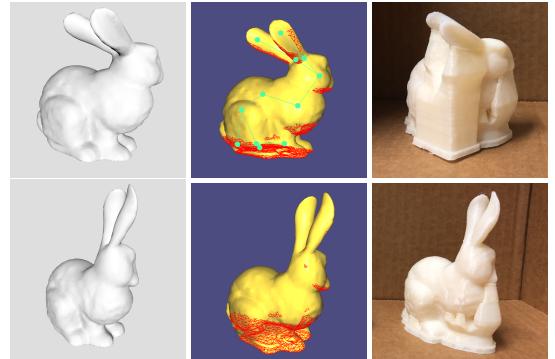


Figure 2: Our method reduces support material usage by 37% on the bunny

Limitations and Future Work

Hyperparameters $\omega_1, \omega_2, \omega_3$ are tuned manually by experimentation and there is no clear way to pick sensible values because the objectives are tradeoffs and often act in conflict with each other. For example, overhang free deformation may introduce a large amount of distortions. In future work, we would like to investigate more on multi-objective optimization.

Currently, an entire run of the optimization procedure took several minutes for Figure. 1 and Figure. 2. There are huge potential in moving linear blend skinning and energy computation to vertex shaders for fast and parallel computation. In future work, we want to re-implement bottleneck steps using OpenGL for real time computation to allow for interactive design.

Although we have decided to look at support reduction, the method can be easily adapted to incorporate additional constraints. For example, we can formulate another energy term to account for center of mass for self-balancing. [7] or to account for the physical strength of the fabrication material. In future work, we want to include additional constraint to make 3D model self-support itself in a variety of scenarios.

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