

## EEEN 322 PS 2 QUESTIONS

### Q1

- 3.3-8** A signal  $g(t)$  is band-limited to  $B$  Hz. Show that the signal  $g^n(t)$  is band-limited to  $nB$  Hz. Hint:  $g^2(t) \iff [G(\omega) * G(\omega)]/2\pi$ , and so on. Use the width property of convolution.

\* \* \* \* \*

### Q2

- 3.4-1** Signals  $g_1(t) = 10^4 \text{rect}(10^4 t)$  and  $g_2(t) = \delta(t)$  are applied at the inputs of the ideal low-pass filters  $H_1(\omega) = \text{rect}(\omega/40,000\pi)$  and  $H_2(\omega) = \text{rect}(\omega/20,000\pi)$  (Fig. P3.4-1). The outputs  $y_1(t)$  and  $y_2(t)$  of these filters are multiplied to obtain the signal  $y(t) = y_1(t)y_2(t)$ .
- Sketch  $G_1(\omega)$  and  $G_2(\omega)$ .
  - Sketch  $H_1(\omega)$  and  $H_2(\omega)$ .
  - Sketch  $Y_1(\omega)$  and  $Y_2(\omega)$ .
  - Find the bandwidths of  $y_1(t)$ ,  $y_2(t)$ , and  $y(t)$ .

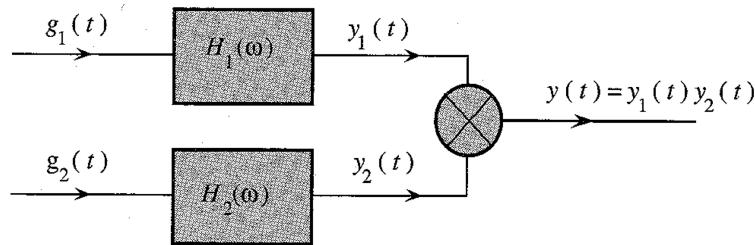


Figure P3.4-1

\* \* \* \* \*

### Q3

- EXAMPLE 3.19** Verify Parseval's theorem for the signal  $g(t) = e^{-at} u(t)$  ( $a > 0$ ).

\* \* \* \* \*

### Q4

- EXAMPLE 3.20** Estimate the essential bandwidth  $W$  rad/s of the signal  $e^{-at} u(t)$  if the essential band is required to contain 95% of the signal energy.

\* \* \* \* \*

### Q5

- EXAMPLE 3.24** A noise signal  $n_i(t)$  with PSD  $S_{n_i}(\omega) = K$  is applied at the input of an ideal differentiator (Fig. 3.43a). Determine the PSD and the power of the output noise signal  $n_o(t)$ .

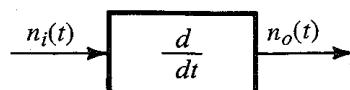
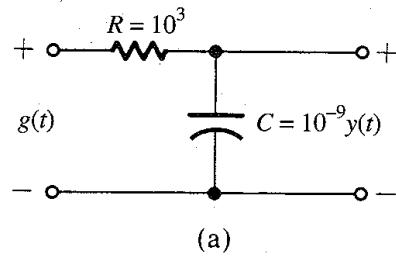


Figure 3.43 (a)

\* \* \* \* \*

**Q6**

- 3.5.3 Determine the maximum bandwidth of a signal that can be transmitted through the low-pass  $RC$  filter in Fig. 3.27a with  $R = 1000$  and  $C = 10^{-9}$  if, over this bandwidth, the amplitude response (gain) variation is to be within 5% and the time delay variation is to be within 2%.



(a)

Figure 3.27 Simple  $RC$  filter,

## EEEN 322 PS 2 SOLUTIONS

**Q1**

3.3-8 From the frequency convolution property, we obtain

$$g^2(t) \iff \frac{1}{2\pi} G(\omega) * G(\omega)$$

The width property of convolution states that if  $c_1(x) * c_2(x) = y(x)$ , then the width of  $y(x)$  is equal to the sum of the widths of  $c_1(x)$  and  $c_2(x)$ . Hence, the width of  $G(\omega) * G(\omega)$  is twice the width of  $G(\omega)$ . Repeated application of this argument shows that the bandwidth of  $g^n(t)$  is  $nB$  Hz ( $n$  times the bandwidth of  $g(t)$ ).

\*\*\*\*\*

**Q2**

3.4-1

$$G_1(\omega) = \text{sinc}\left(\frac{\omega}{20000}\right) \quad \text{and} \quad G_2(\omega) = 1$$

Figure S3.4-1 shows  $G_1(\omega)$ ,  $G_2(\omega)$ ,  $H_1(\omega)$  and  $H_2(\omega)$ . Now

$$Y_1(\omega) = G_1(\omega)H_1(\omega)$$

$$Y_2(\omega) = G_2(\omega)H_2(\omega)$$

The spectra  $Y_1(\omega)$  and  $Y_2(\omega)$  are also shown in Fig. S3.4-1. Because  $y(t) = y_1(t)y_2(t)$ , the frequency convolution property yields  $Y(\omega) = Y_1(\omega) * Y_2(\omega)$ . From the width property of convolution, it follows that the bandwidth of  $Y(\omega)$  is the sum of bandwidths of  $Y_1(\omega)$  and  $Y_2(\omega)$ . Because the bandwidths of  $Y_1(\omega)$  and  $Y_2(\omega)$  are 10 kHz, 5 kHz, respectively, the bandwidth of  $Y(\omega)$  is 15 kHz.

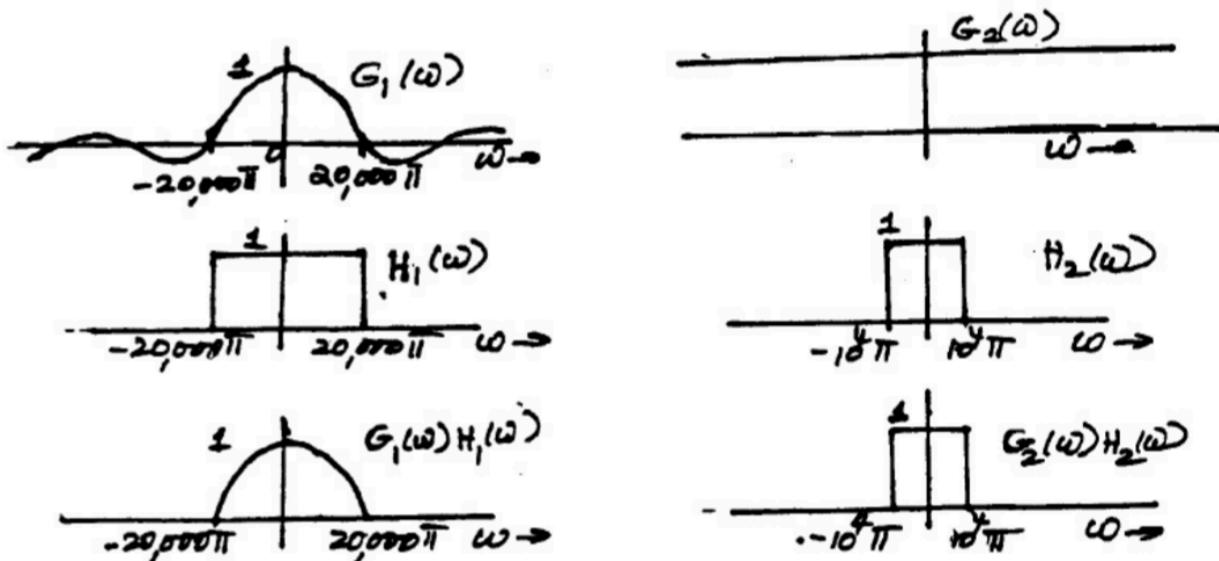


Fig. S3.4-1

\*\*\*\*\*

**Q3**

**EXAMPLE 3.19**

We have

$$E_g = \int_{-\infty}^{\infty} g^2(t) dt = \int_0^{\infty} e^{-2at} dt = \frac{1}{2a} \quad (3.65)$$

We now determine  $E_g$  from the signal spectrum  $G(\omega)$  given by

$$G(\omega) = \frac{1}{j\omega + a}$$

and from Eq. (3.64),

$$E_g = \frac{1}{2\pi} \int_{-\infty}^{\infty} |G(\omega)|^2 d\omega = \frac{1}{2\pi} \int_{-\infty}^{\infty} \frac{1}{\omega^2 + a^2} d\omega = \frac{1}{2\pi a} \tan^{-1} \frac{\omega}{a} \Big|_{-\infty}^{\infty} = \frac{1}{2a}$$

which verifies Parseval's theorem.

**Q4**

**EXAMPLE 3.20**

In this case,

$$G(\omega) = \frac{1}{j\omega + a}$$

and the ESD is

$$|G(\omega)|^2 = \frac{1}{\omega^2 + a^2}$$

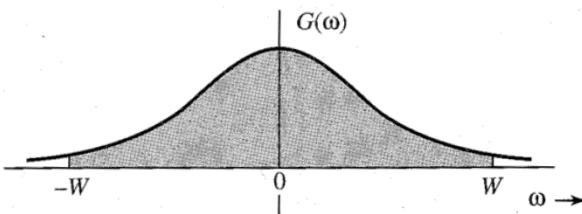
This ESD is shown in Fig. 3.37. Moreover, the signal energy  $E_g$  is  $1/2\pi$  times the area under this ESD, which has already been found to be  $1/2a$ . Let  $W$  rad/s be the essential bandwidth, which contains 95% of the total signal energy  $E_g$ . This means  $1/2\pi$  times the shaded area in Fig. 3.37 is  $0.95/2a$ , that is,

$$\begin{aligned} \frac{0.95}{2a} &= \frac{1}{2\pi} \int_{-W}^{W} \frac{d\omega}{\omega^2 + a^2} \\ &= \frac{1}{2\pi a} \tan^{-1} \frac{\omega}{a} \Big|_{-W}^{W} = \frac{1}{\pi a} \tan^{-1} \frac{W}{a} \end{aligned}$$

or

$$\frac{0.95\pi}{2} = \tan^{-1} \frac{W}{a} \implies W = 12.706a \text{ rad/s}$$

This means that the spectral components of  $g(t)$  in the band from 0 (dc) to  $12.706$  rad/s ( $2.02$  Hz) contribute 95% of the total signal energy; all the remaining spectral components (in the band from  $12.706$  rad/s to  $\infty$ ) contribute only 5% of the signal energy.\*



**Figure 3.37** Estimating the essential bandwidth of a signal.

\* Although the ESD exists over the range from  $-\infty$  to  $\infty$ , the concept of bandwidth is only meaningful for positive frequencies. Therefore, the essential bandwidth is not from  $-W$  to  $W$ , but from  $0$  to  $W$ .

Q5

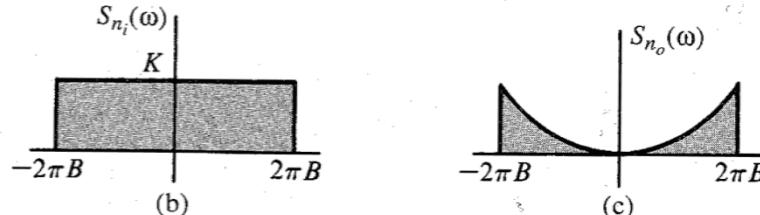
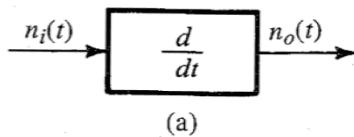
### **EXAMPLE 3.24**

The transfer function of an ideal differentiator is  $H(\omega) = j\omega$ . If the noise at the demodulator output is  $n_o(t)$ , then from Eq. (3.90),

$$S_{n_o}(\omega) = |H(\omega)|^2 S_{n_i}(\omega) = |j\omega|^2 K$$

The output PSD  $S_{n_o}(\omega)$  is parabolic, as shown in Fig. 3.43c. The output noise power  $N_o$  is  $1/2\pi$  times the area under the output PSD. Therefore,

$$N_o = \frac{1}{2\pi} \int_{-2\pi B}^{2\pi B} K\omega^2 d\omega = K \int_{-2\pi B}^{2\pi B} \omega^2 d\omega = \frac{8\pi^2 B^3 K}{3}$$



**Figure 3.43** Power spectral densities at the input and the output of an ideal differentiator.

Q6

### 3.5-3 From the results in Example 3.16

$$|H(\omega)| = \frac{a}{\sqrt{\omega^2 + a^2}} \quad a = \frac{1}{RC} = 10^6$$

Also  $H(0) = 1$ . Hence if  $\omega_1$  is the frequency where the amplitude response drops to 0.95, then

$$|H(\omega_1)| = \frac{10^6}{\sqrt{\omega_1^2 + 10^{12}}} = 0.95 \implies \omega_1 = 328.684$$

Moreover, the time delay is given by (see Example 3.16)

$$t_d(\omega) = \frac{a}{\omega^2 + a^2} \Rightarrow t_d(0) = \frac{1}{a} = 10^{-6}$$

If  $\omega_2$  is the frequency where the time delay drops to 0.98% of its value at  $\omega = 0$ , then

$$t_d(\omega_2) = \frac{10^6}{\omega_2^2 + 10^{12}} = 0.98 \times 10^{-6} \implies \omega_2 = 142,857$$

We select the smaller of  $\omega_1$  and  $\omega_2$ , that is  $\omega = 142,857$ , where both the specifications are satisfied. This yields a frequency of 22.736.4 Hz.

**Table 3.1****Short Table of Fourier Transforms**

	$g(t)$	$G(\omega)$	
1	$e^{-at}u(t)$	$\frac{1}{a+j\omega}$	$a > 0$
2	$e^{at}u(-t)$	$\frac{1}{a-j\omega}$	$a > 0$
3	$e^{-a t }$	$\frac{2a}{a^2+\omega^2}$	$a > 0$
4	$te^{-at}u(t)$	$\frac{1}{(a+j\omega)^2}$	$a > 0$
5	$t^n e^{-at}u(t)$	$\frac{n!}{(a+j\omega)^{n+1}}$	$a > 0$
6	$\delta(t)$	1	
7	1	$2\pi\delta(\omega)$	
8	$e^{j\omega_0 t}$	$2\pi\delta(\omega - \omega_0)$	
9	$\cos \omega_0 t$	$\pi[\delta(\omega - \omega_0) + \delta(\omega + \omega_0)]$	
10	$\sin \omega_0 t$	$j\pi[\delta(\omega + \omega_0) - \delta(\omega - \omega_0)]$	
11	$u(t)$	$\pi\delta(\omega) + \frac{1}{j\omega}$	
12	$\text{sgn } t$	$\frac{2}{j\omega}$	
13	$\cos \omega_0 t u(t)$	$\frac{\pi}{2}[\delta(\omega - \omega_0) + \delta(\omega + \omega_0)] + \frac{j\omega}{\omega_0^2 - \omega^2}$	
14	$\sin \omega_0 t u(t)$	$\frac{\pi}{2j}[\delta(\omega - \omega_0) - \delta(\omega + \omega_0)] + \frac{\omega_0}{\omega_0^2 - \omega^2}$	
15	$e^{-at} \sin \omega_0 t u(t)$	$\frac{\omega_0}{(a+j\omega)^2 + \omega_0^2}$	$a > 0$
16	$e^{-at} \cos \omega_0 t u(t)$	$\frac{a+j\omega}{(a+j\omega)^2 + \omega_0^2}$	$a > 0$
17	$\text{rect}\left(\frac{t}{\tau}\right)$	$\tau \text{sinc}\left(\frac{\omega\tau}{2}\right)$	
18	$\frac{W}{\pi} \text{sinc}(Wt)$	$\text{rect}\left(\frac{\omega}{2W}\right)$	
19	$\Delta\left(\frac{t}{\tau}\right)$	$\frac{\tau}{2} \text{sinc}^2\left(\frac{\omega\tau}{4}\right)$	
20	$\frac{W}{2\pi} \text{sinc}^2\left(\frac{Wt}{2}\right)$	$\Delta\left(\frac{\omega}{2W}\right)$	
21	$\sum_{n=-\infty}^{\infty} \delta(t - nT)$	$\omega_0 \sum_{n=-\infty}^{\infty} \delta(\omega - n\omega_0)$	$\omega_0 = \frac{2\pi}{T}$

## Energy Spectral Density (ESD) and Power Spectral Density (PSD)

### Energy

$$E_g = \int_{-\infty}^{+\infty} |g(t)|^2 dt = \frac{1}{2\pi} \int_{-\infty}^{+\infty} |G(\omega)|^2 d\omega \quad (\text{Parseval})$$

### Energy Spectral Density (ESD)

$$\begin{aligned}\Psi_g(\omega) &= |G(\omega)|^2 \\ \Rightarrow E_g &= \frac{1}{2\pi} \int_{-\infty}^{+\infty} \Psi_g(\omega) d\omega\end{aligned}$$

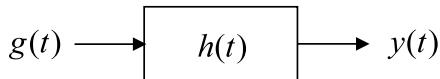
### Relationship with time autocorrelation

$$\psi_g(\tau) = \int_{-\infty}^{+\infty} g(t)g(t+\tau)dt$$

$$\psi_g(\tau) \Leftrightarrow \Psi_g(\omega) \quad (\text{FT pair})$$

$$E_g = \psi_g(0)$$

### ESD of Input / Output

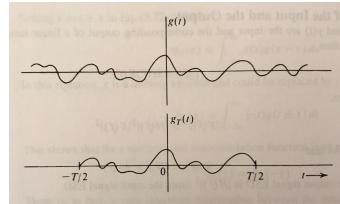


$$\Psi_y(\omega) = |H(\omega)|^2 \Psi_g(\omega)$$

### Energy Spectrum of $x(t)=g(t)\cos\omega_0 t$

$$\Psi_x(\omega) = \frac{1}{4} [\Psi_g(\omega + \omega_0) + \Psi_g(\omega - \omega_0)]$$

$$E_x = \frac{1}{2} E_g$$



### Power

$$P_g = \lim_{T \rightarrow \infty} \frac{1}{T} \int_{-T/2}^{+T/2} |g(t)|^2 dt$$

### Power Spectral Density (PSD)

$$\begin{aligned}S_g(\omega) &= \lim_{T \rightarrow \infty} \frac{|G_T(\omega)|^2}{T} \quad (*) \\ \Rightarrow P_g &= \frac{1}{2\pi} \int_{-\infty}^{+\infty} S_g(\omega) d\omega\end{aligned}$$

The power spectrum can be computed this way as long as the limit exists

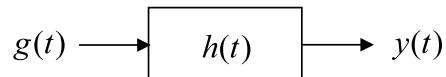
### Relationship with time autocorrelation

$$R_g(\tau) = \lim_{T \rightarrow \infty} \frac{1}{T} \int_{-T/2}^{+T/2} g(t)g(t+\tau) dt$$

$$R_g(\tau) \Leftrightarrow S_g(\omega) \quad (\text{FT pair})$$

$$P_g = R_g(0) \quad \text{and} \quad \text{RMS} = \sqrt{P_g}$$

### PSD of Input / Output



$$\Psi_y(\omega) = |H(\omega)|^2 \Psi_g(\omega)$$

### Power Spectrum of $x(t)=g(t)\cos\omega_0 t$

$$S_x(\omega) = \frac{1}{4} [S_g(\omega + \omega_0) + S_g(\omega - \omega_0)]$$

$$P_x = \frac{1}{2} P_g$$

(\*)  $g_T(t)$  is  $g(t)$  truncated to  $\left[-\frac{T}{2}, \frac{T}{2}\right]$