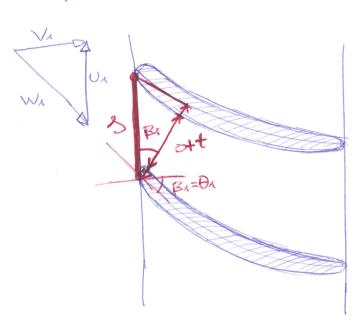
## Impeller throat area derivation

at the throat near the impeller can be calculated cosine rule in combination with the blade thickness near the impeller leading edge:



Euler equation W = Voz.Uz - Voz.U1

(Section M.S of Cosey and Robinson 2021)

The cosine rule gives:

(A better estimation is possible is the Bin distribution is known)

where

- S is the blade spacing
- 0 is the blade opening
- t is the blade thirthess near the leading edge
- v is the radial coordinate
- Z is the number of blades:

Evaluating the spring throat area from the opening gives

At = 
$$\frac{1}{2} \cdot 0 \cdot (r_t - r_h) = \frac{1}{2} \cdot (r_t - r_h) \cdot [s \cdot \cos \theta_n - t]$$

$$AH = Z.0.0.(r+r+) = t.(r+r+)$$

$$AH = Z(r+r+).[32\pi(r+r+) - t] = \pi(r-r+) - t-2(r+r+)$$

$$Z= Z(r+r+).[32\pi(r+r+) - t] = \pi(r-r+) - t-2(r+r+)$$

$$Ath = Ain - \frac{t}{s} \pi(rt^2 - rh^2) = Ain - (\frac{t}{s}) \cdot Ain$$

$$Ath = \left(\frac{3}{3} - \frac{t}{3}\right) Ain$$

$$Ath = (\cos\theta_1 - \frac{t}{3})Ain$$

Therefore the area at the throat is reduced with respect to the area at the impeller inlet because of:

- Metal argle Dr

- Blade thickness SHAHAGE to spacing ratio (metal blockage)

- (Fossibly additional aerodynamic blockage) 5\*

acceleration from the impeller inlet to the throat an be estimated as: assume DU=0

(1) 
$$ht + \frac{wt^2}{z} = hin + \frac{wi^2}{z}$$

From conservation of mass we have that:

m = pin Ain Wmin = Oth. Ath. Wth

Oin Ain Wir cos(Rin) = Oth Ath. Wth

i= B-0 Wth = (Bin ). (Ain ). COS(Bin)

$$\frac{Wh}{Win} = \frac{1}{2} \frac{1}{2}$$

With and (0th/hth) are computed from (1) and (2) assuming [Sin=St]