

SCUOLA DI INGEGNERIA INDUSTRIALE E DELL'INFORMAZIONE

MSc in Space Engineering

Authors:

10723712Marcello Pareschi(BSc Aerospace Engineering - Politecnico di Milano)10836125Daniele Paternoster(BSc Aerospace Engineering - Politecnico di Milano)10711624Alex Cristian Turcu(BSc Aerospace Engineering - Politecnico di Milano)10884250Tamim Harun Or(BSc Aerospace Engineering - International Islamic University Malaysia)

Professor: Camilla Colombo Academic year: 2023-2024

Interplanetary trajectory design

Contents

		planetary mission
1	.1	Symbols
		1.1.1 Analisi della missione
		1.1.2 Analisi della missione 2
1	.2	Introduction
		1.2.1 Description of the problem
		1.2.2 Assigned data and constraints
1	.3	Algorithms description
		1.3.1 Brute force algorithm
		1.3.2 Gradient method algorithm
1	.4	Reduction of the time windows
		1.4.1 Resonance period analysis
		1.4.2 Cost-plot analysis
		1.4.3 Final time window selection
1	.5	Conclusion and results

1. Interplanetary mission

1.1. Symbols

1.1.1 Analisi della missione

 A_e $[m^2]$ area di efflusso totale

 ϕ [rad] angolo di traiettoria del razzo

1.1.2 Analisi della missione 2

 A_e [m^2] area di efflusso totale

φ [rad] angolo di traiettoria del razzo

1.2. Introduction

1.2.1 Description of the problem

The first part of the assignment aims at designing an interplanetary transfer from Mars to asteroid 1036 Ganymede exploiting a powered gravity assist on Earth. The problem is analyzed through the patched conics method, without considering the injection and arrival hyperbolas. The initial and final velocity vector of the satellite are assumed to be the same of the respective celestial body. The two heliocentric legs are calculated through the Lambert problem. The trajectory is selected with the only criteria of minimizing the cost of the mission, assessed through the total ΔV . The latter is computed by summing different contributions:

$$\Delta V_{tot} = \Delta V_1 + \Delta V_2 + \Delta V_3 \tag{1}$$

Where the three terms are defined as:

- ΔV_1 injection in the first heliocentric leg;
- ΔV_2 exit from the second heliocentric leg;
- ΔV_3 impulse given by the engine at pericentre of hyperbola fly-by;

All the manoeuvres are assumed to be impulsive, i.e. they change only the velocity vector of the spacecraft, mantaining invariated the position vector. Note that ΔV_1 and ΔV_2 are related to heliocentric velocities, while ΔV_3 is calculated through relative geocentric velocities.

For each manoeuvre the cost is computed as:

$$\Delta V_i = \|V_{+,i} - V_{-,i}\| \tag{2}$$

1.2.2 Assigned data and constraints

A few constraints were considered:

- earliest departure date $t_{min,dep} = [01/01/2028 \ 00:00:00]$ in Gregorian calendar
- latest arrival date $t_{max,arr} = [01/01/2058 \ 00:00:00]$ in Gregorian calendar
- time of flights of the two heliocentric arcs must be greater than the associated parabolic time
- minimum pericentre radius of the fly-by hyperbola $r_p = r_E + 500 \text{ km}$
- single-revolution Lambert problem was considered
- reasonable total time of the mission

Note that the constraint on the pericentre radius of the fly-by is considered both for avoid impact on Earth and to prevent undesired atmoshperic drag effects.

1.3. Algorithms description

1.3.1 Brute force algorithm

1.3.2 Gradient method algorithm

1.4. Reduction of the time windows

1.4.1 Resonance period analysis

1.4.2 Cost-plot analysis

1.4.3 Final time window selection

1.5. Conclusion and results

Bibliography