



# POLITECNICO

## MILANO 1863

### Reverse Engineering of Juno Mission

#### Homework 2

Course of Space System Engineering & Operations  
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#### Group 5

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# Notation

<b>ME</b>	Main engine	<b>MEF</b>	Main engine flush
<b>RCS</b>	Reaction Control System	<b>TRL</b>	Technology readiness level
<b>DSM</b>	Deep space maneuver	<b>RW</b>	Reaction wheel
<b>TCM</b>	Trajectory correction maneuver	<b>COM</b>	Centre of mass
<b>SK</b>	Station keeping	<b>MAG</b>	Magnetometer
<b>PRM</b>	Period reduction maneuver	<b>PC</b>	Plane change
<b>JOI</b>	Jupiter orbit insertion	$\tau$	Burn time
<b>REM</b>	Rocket engine module	$I_s$	Specific impulse

# 1 Mission analysis and $\Delta V$ budget

Manuevers	Design [m/s]	Perf. [m/s]	Sim. [m/s]	$\tau_{ME}$ Design [min]	$\tau_{ME}$ Perf. [min]
TCM <sup>[1]</sup> -1 $\div$ 2 (RCS)	4.4	1.71	-	-	-
DSM <sup>[1]</sup> -1 (ME)	360.1	344.16	722.51	30.97	29.71
DSM <sup>[1]</sup> -2 (ME)	394.8	387.94		30.07	29.77
TCM <sup>[1]</sup> -4 $\div$ 15 (RCS)	32.5	7.89	-	-	-
MEF <sup>[1]</sup> (ME)	3.3	3.3	-	-	-
JOI <sup>[2]</sup> (ME)	424.07 <sup>I</sup>	541.73	424.07	27.86	35.65
JOI <sup>[2]</sup> clean-up (RCS)	4.92	6.39	-	-	-
PRM <sup>[2]</sup> (ME)	636	-	602.45	35.19	-
OTM <sup>[3]</sup> pre-PC (RCS)	120 <sup>II</sup>	94.88	-	-	-
PC (RCS)	-	56.39	69.97 <sup>III</sup>	-	-
OTM post-PC (RCS)	-	108.08	-	-	-
De-Orbit <sup>[4]</sup> (RCS)	75 <sup>IV</sup>	30.89 <sup>V</sup>	87.93	-	-

Table 1: Comparison between estimated and real masses

<sup>I</sup> This value has been assumed equal to the one calculated from the insertion on the 107-days orbit.

<sup>II</sup> This value has been calculated as each of the 30 nominal science orbits require 4 m/s of  $\Delta V$ .

<sup>III</sup> This value is referred to the plane change of the 53-days orbit as no other trajectories required this maneuver.

<sup>IV</sup> Value assumed to be equal between the 11-days orbit and the 14-days orbit.

<sup>V</sup> This value has been updated from the nominal 75 m/s since the De-orbit maneuver will be performed from a 53-days orbit and not from a 14-days orbit.

## 2 Propulsion system architecture

The spacecraft axes are defined as shown in Figure 1: the spacecraft is spinning along the +Z-axis, aligned with the HGA. The +X-axis is aligned with the MAG boom while the +Y-axis is in the direction of cross product between +Z-axis and +X-axis.

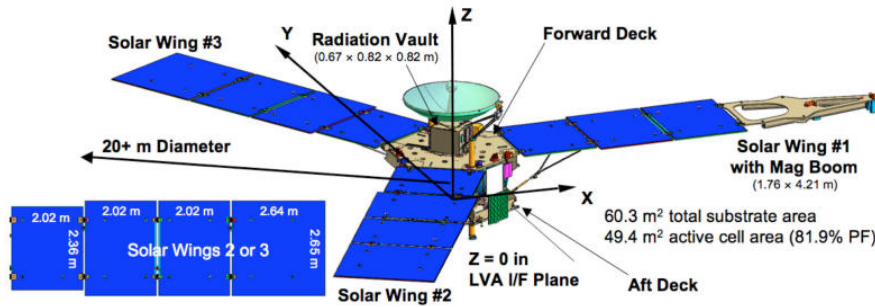


Figure 1: Axis description

### 2.1 Main Engine and RCS

Juno is equipped with a dual mode propulsion subsystem: the bi-propellant ME uses the hypergolic couple hydrazine and nitrogen tetroxide ( $N_2H_4 - N_2O_4$ ) and RCS uses hydrazine as monopropellant. This choice has been made to simplify the design: fewer tanks are needed as fuel ones are shared between the two systems. Moreover, the choice of this specific hypergolic couple is dictated by the storage requirements of the mission: in a five-year cruise reliability and sturdiness of the propulsive system were among the main drivers of the mission. Electric thrusters were discarded as TRL 9 technologies were required: other limitations such as power budget, an highly radioactive environment, weight and space inside the spacecraft required a more simple and light solution.

The ME is a Leros-1b, built by Nammo<sup>[5]</sup>, and produces about 662 N of thrust with a  $I_{s,ME}$  of 318.6 s. This particular engine is certified for a 42 minutes continuous burn and has a cumulative life of 342 minutes. This engine is utilized during the DSMs, JOI and PRM. RIFERIMENTO ALLA SEZIONE PRECEDENTE It is mounted inside the body of the spacecraft along the -Z-axis, centred between the propellant tanks and under the electronic vault. This solution

has probably been adopted due to space requirements inside the Atlas V fairing and safety precautions during the cruise phase. The ME is also shielded by a hatch that opens when a maneuver is needed. The RCS is used for TCMs, attitude control and general SK. The catalyst used to decompose the hydrazine is the S-405, based on iridium and aluminum<sup>[6]</sup>. The whole RCS is composed by four REMs, each of them mounted along the  $\pm Y$ -axis on a pylon, as shown in Figure 2. Each pylon houses three thrusters, the MR-111C by Aerojet Rocketdyne<sup>[7]</sup>, pointed in different directions, providing a thrust of 4.5 N with  $I_{s,RCS}$  of 220 s each. Electrical power is required to operate the feeding valves, heating valves and the catalytic bed, amounting to a maximum of around 13 W<sup>[8]</sup>.

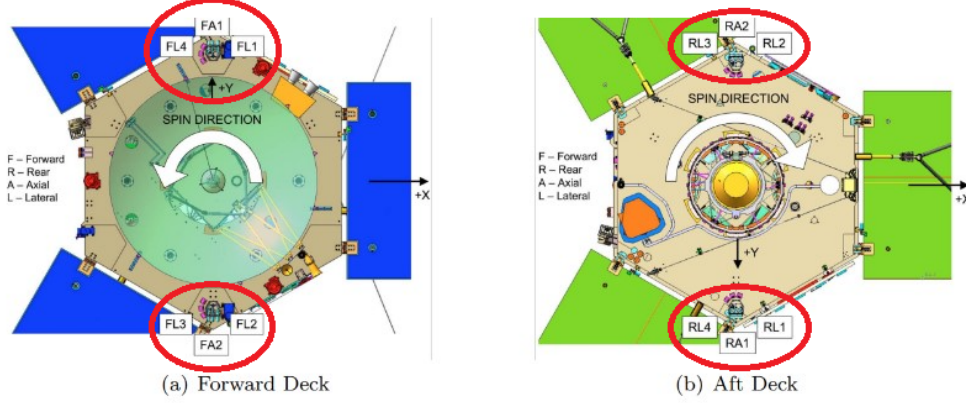


Figure 2: Forward and Aft deck view

The pylons are raised respectively by 74 cm on the forward deck and about 26 cm on the aft deck as shown in Figure 4. With the need of limiting even more the interaction of the exhaust gasses with the on board instruments, mainly mounted on the top deck, the HGA and solar panels, the axial thrusters are canted  $10^\circ$  away from the Z-axis while the lateral thrusters are canted  $5^\circ$  away from the X-axis and  $12.5^\circ$  toward the Z-axis<sup>[1]</sup>. This particular configuration of RCS is required since no RW nor any other type of active attitude control is present on board the spacecraft: the ability of decoupling the forces and the momentum was thus needed. Lateral thrusters are denominated with letter "L" while axial thrusters are denominated with letter "A", as can be seen both from Figure 2 and Figure 4. This configuration increased the overall reliability of the propulsion system as "A" thrusters could be used as replacement of the ME for small maneuvers. A simplified scheme of the propulsion system has been developed in Figure 3.

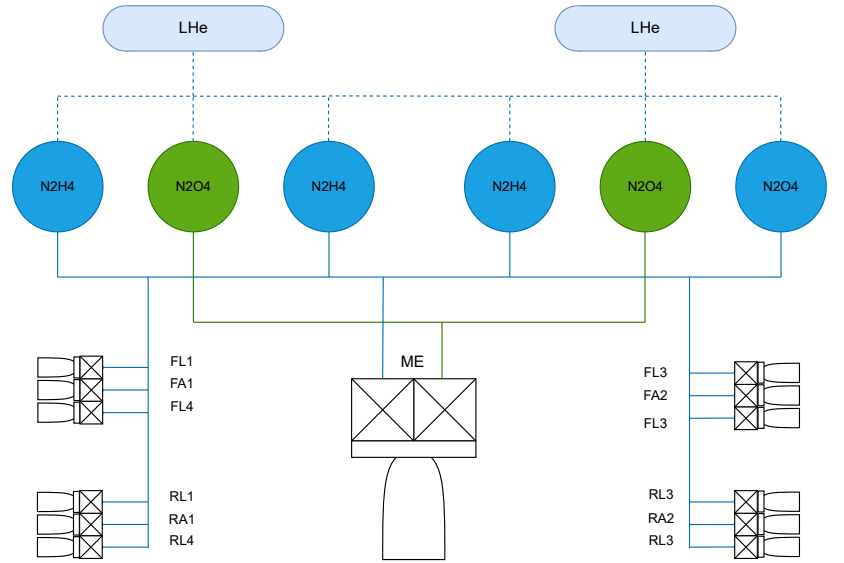


Figure 3: Propulsion system architecture

## 2.2 Maneuver Implementation Modes

Juno's maneuver can be performed in two different modes: *vector – mode* and *turn – burn – turn*.

The *vector – mode* consists of separated and coordinated axial and lateral burns from RCS thrusters. As seen in subsection 2.1 the thrusters are not exactly perpendicular one to the other, so during a *vector – mode* maneuver an induced axial  $\Delta V$  is generated and must be compensated.

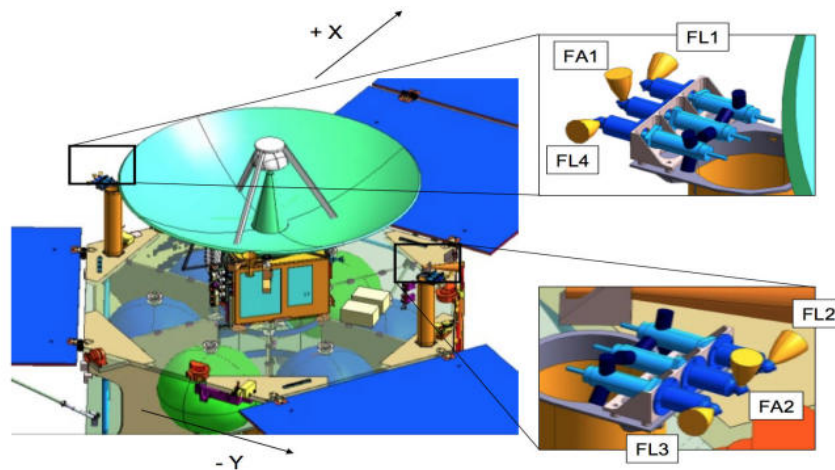


Figure 4: RCS forward mount

The *turn – burn – turn* mode consists in a sequence of RCS and ME burns: first the spacecraft slews to the design spinning rate of 5 RPM, then the ME is ignited and the maneuver is performed. At last, the spacecraft slews back to its nominal spinning rate. This mode is used during all the ME burns. In this kind of maneuver the RCS uses the "L" thrusters on the REMs. All ME maneuvers are so performed.

### 2.3 Tanks

Juno's tanks are equally distributed throughout its hexagonal shaped body. Four tanks are needed to store hydrazine and two tanks are needed to store the oxidizer. As can be seen from Figure 4, the oxidizer ones (green tanks) are located along the X-axis, while fuel ones (blue ones) are placed in the remaining bays. All six tanks have a sphere-like shape for two main reasons: the sphere allows to have the most internal volume with the lowest possible surface and so both weight and heat exchange are limited.

The two tanks<sup>[9]</sup> containing the supercritical helium needed to pressurize the propellant system are placed near solar wing one and solar wing two. Unlike fuel and oxidizer tanks, helium ones do not have a sphere like shape due to volume management inside the bays<sup>[10]</sup>: cylindrical tanks allows to fill better the gaps present under the main tanks. The positioning of the pressurant tanks breaks even more the symmetry of the mass distribution: this feature, in concomitance with the distribution of the propellant tanks, will make the COM not shifting only along the Z-axis unless other precautions were made in placing other internal components.

A system of valves regulates the pressure inside the tanks to allow nominal operations of the ME and RCS. All the tanks are insulated from their surroundings and heating elements are present on both tanks and feeding lines to ensure safe and nominal temperature inlet for the ME<sup>[5]</sup>. One of the main problems with managing liquid in space is the need of guiding the fuel to the feeding lines of the engines to avoid mixture of gas in the combustion chamber and thus reducing the mass flow, compromising the correct functioning of the propulsion system. Moreover, liquid propellants produce sloshing movement that apply a small amount of forces and moments inside the tanks, causing an unsteady oscillatory spin. Juno is a spin stabilized spacecraft so the induced forces causes a movement of nutation. A Propellant Expulsion Device (PED) is thus needed: the spinning of the spacecraft helps guiding the fuel to the most exterior part of the tanks where fuel lines are located<sup>[11]</sup>. MEFs are planned to flush the main propellant line and to increase the precision of the different maneuvers. In order to accomplish its mission, Juno holds about 2.000 Kg of propellant: about 1280 kg of fuel and 720 kg of oxidizer<sup>[1]</sup>. A more detailed analysis of tanks will be conducted in QUI METTIAMO IL RIFERIMENTO AL SIZING

## 3 Reverse engineering of propulsion system

## Bibliography

- [1] Thomas A. Pavlak et al. *Maneuver Design for the Juno Mission: Inner Cruise*. AIAA space forum. Site: <https://arc.aiaa.org/>. 2018.
- [2] Paul W. Stumpf et al. *MANEUVER OPERATIONS DURING JUNO'S APPROACH, ORBIT INSERTION, AND EARLY ORBIT PHASE*. JPL open repository. Site: <https://dataverse.jpl.nasa.gov/file.xhtml?fileId=58768&version=1.1&toolType=PREVIEW>. 2017.
- [3] S. Stephens. *Juno Mission Plan Document*. Planetary Data System. Site: [https://pds.nasa.gov/ds-view/pds/viewMissionProfile.jsp?MISSION\\_NAME=JUNO](https://pds.nasa.gov/ds-view/pds/viewMissionProfile.jsp?MISSION_NAME=JUNO). 2011.
- [4] Various. *Juno Mission and Trajectory Design*. Website. Site: <https://spaceflight101.com/juno/juno-mission-trajectory-design/>. 2024.
- [5] Nammo. *Leros-1b engine*. Journal of Geophysical Research: Planet. Site: <https://www.nammo.com/wp-content/uploads/2021/03/2021-Nammo-Westcott-Liquid-Engine-LEROS1B.pdf>.
- [6] Dr. Edward. J. Wucherer al. *Improving and Testing S-405 Catalyst*. AIAA space forum. Site: <https://arc.aiaa.org/doi/epdf/10.2514/6.2013-4053>. 2013.
- [7] *Aerojet Rocketdyne Propulsion plays role in Juno mission*. Online Communication. Site: <https://www.proquest.com>. 2016.
- [8] *MR-111C datasheet*. Site: <http://www.astronautix.com/m/mr-111.html>.
- [9] *Launch*. Site: <https://www.missionjuno.swri.edu/launch>.
- [10] Dr. Mary M. Mellott et al. *NSSDCA/COSPAR ID: 2011-040A*. Nasa SSDCA. Site: <https://nssdc.gsfc.nasa.gov/nmc/spacecraft/display.action?id=2011-040A>. 2022.
- [11] Sathya Gangadharan et al. *Modeling of Fuel Slosh in a Spin Stabilized Spacecraft with On-Axis Propellant Tanks Implemented with Diaphragms*. AIAA Modeling and Simulation Technologies Conference 10 - 13 August 2009, Chicago, Illinois. Site: <https://arc.aiaa.org/>. 2009.