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End-Sem

[Mass - Transfer]

(1) For benzene Antoine's equation constants are:

$$A = 6.91, \quad B = 1211, \quad C = 221.$$

For toluene Antoine's equation constants are:

$$A = 6.95, \quad B = 1344, \quad C = 215.$$

Now using Raoult's Law:

$$P = x_A P_A^{\text{sat}} + x_B P_B^{\text{sat}} \quad A \rightarrow \text{Benzene.}$$
$$x_A = x_B = 0.5 \quad B \rightarrow \text{Toluene.}$$

Now $x_A = x_B = 0.5$

Let

$$f(T) = \frac{1}{2} \left[\frac{6.91}{10} \right]$$
$$f(T) = \frac{1}{2} \left[\left(10 - \frac{(6.91 - 1211)}{T+211} \right) + 10 \left(6.95 - \frac{1344}{T+215} \right) \right] - 760$$

$$\therefore f(r) = \frac{1}{2} \left[10 \left(\frac{6.91 - 12.11}{r+24} \right) + 10 \left(\frac{6.95 - 12.41}{r+215} \right) \right] - 760$$

Now

$$f(100) = 191 \text{ mm of Hg}$$

$$f(90) = (-40 \text{ mm of Hg})$$

$$f(95) = (69.2 \text{ mm of Hg})$$

$$f(92) = -(0.269), \quad f(92.01) = (-0.046)$$

$$\therefore T_{\text{bubble of } \text{H}_2}$$

$(T)_{\text{bubble of mixture}} \approx 92^\circ\text{C}$

$\therefore T_{\text{bubble}} = 92.1^\circ\text{C}$

(b)

$$x_1 P_A^{\text{sat}} = y_1 P \quad (\text{Raoult's Law})$$

$$x_2 P_B^{\text{sat}} = y_2 P \quad (\text{Raoult's Law})$$

$$x_1 + x_2 \approx 1$$

$$\frac{y_1 P}{P_A^{\text{sat}}} + \frac{y_2 P}{P_B^{\text{sat}}} = 1$$

Now :

$P = 760 \text{ mm of Hg}$

$$760 \left[\frac{y_{\text{Benzene}}}{10 \left(6.21 - \frac{1211}{T+211} \right)} + \frac{y_{\text{toluene}}}{10 \left(6.25 - \frac{1344}{T+215} \right)} \right] = 1$$

Now

$$g(T) = 760 \left[\frac{y_{\text{Benzene}}}{10 \left(6.21 - \frac{1211}{T+211} \right)} + \frac{y_{\text{toluene}}}{10 \left(6.25 - \frac{1344}{T+215} \right)} \right] - 1$$

Now

$$\boxed{y_{\text{Benzene}} = y_{\text{toluene}} = 0.5}$$

$$g(100) = (-0.036)$$

$$g(99) = (-0.007)$$

$$g(98) = (0.023)$$

$$g(98.5) = 0.008$$

$$\boxed{g(98.75) = 0.00042}$$

$$\therefore \boxed{T_{\text{dew}} = 98.75}$$

Q-2

(a) $F = 100 \text{ kmol/hr}$ ($R_{\text{Benzene}} = 80\%$)
 $(R_{\text{Toluene}} = 20\%)$

\therefore Benzene is more volatile as in distillate it is recovered $\therefore (\gamma_f = 0.2)$

Now In distillate product ($R_{\text{Benzene core.}} = 0.95$)
 $\therefore (x_D = 0.95)$

B \because Reflux fluid is at bubble pt $\therefore (z_{21})$ and vertical line from (β_f, z_f)

From - graph:

$$\frac{x_D}{(R_{m+1})} = 0.299$$

$$\therefore \frac{0.95}{(R_{m+1})} = 0.299$$

$$\therefore (R_{m+1}) = \cancel{3.17}$$

$$R_{m+1} = \frac{0.95}{0.299}$$

$$\therefore \boxed{(R_{m+1} = \cancel{2.77})}$$

$$\boxed{R_m = 2.275}$$

(b) From the data given in book ($\gamma = 2.34$) for
(benzene-toluene) system

∴ equation of curve,

$$y = \frac{2.34x}{1 + 1.34x}$$

Now from (\bar{x}_f, \bar{y}_f) a vertical line is drawn as $(\bar{x}=1)$
∴ at intersection with curve $(x=0.2)$

$$\therefore y = \frac{2.34 \times 0.2}{1 + 1.34 \times 0.2} = [0.51]$$

∴ on curve (q-line meets at $(0.3, 0.51)$)

Now from $(0.95, 0.95)$ to $(0.3, 0.51)$
operating line passes



∴ on equating slopes:

$$\left(\frac{0.95 - 0.51}{0.95 - 0.30} \right) = \frac{R_m}{R_{m+1}} = 0.692$$

$$\therefore R_m = 2.25$$

it is ~~at~~ analytical
Value of (R)

∴ R_m from analytical solⁿ, $\boxed{2.25}$

R_m from graph, $\boxed{2.27}$

$$\textcircled{a} \quad R = R_{\min} \times 1.5$$

$$R = 1.5 \times 2.27 = \boxed{3.405}$$

Now : For derivation :

\textcircled{b} Overall balance :

$$F = D + W \quad \text{--- (1)}$$

component balance

$$F x_f = D x_D + W x_W \quad \text{--- (2)}$$

$$x_D = 0.25$$

$$x_W = 0.05$$

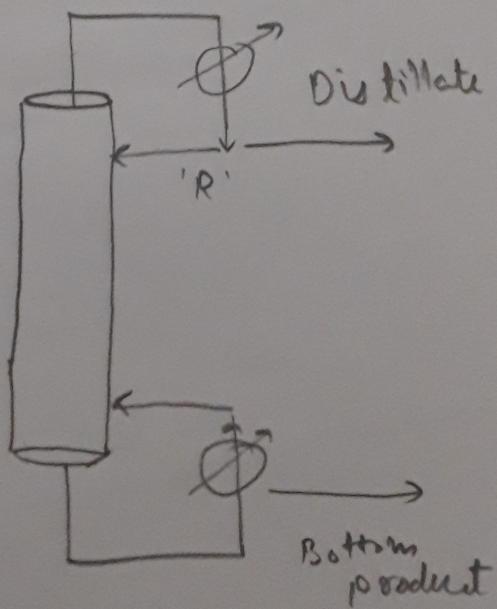
$$x_f = 0.5$$

$$F = 100 \text{ kmol/hr}$$

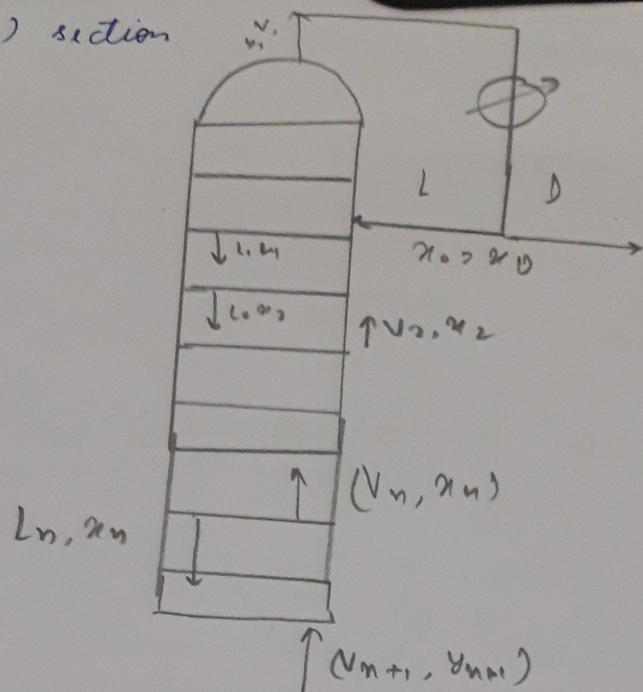
\therefore from (1) and (2)

$$\boxed{\begin{aligned} D &= 27.38 \text{ kmol/hr} \\ W &= 72.22 \text{ kmol/hr} \end{aligned}}$$

(b) Now for (ROL)



For (ROL) section



Rectifying section

$$V_{n+1} = L_n + D \quad \text{--- ① (Overall balance)}$$

$$(V_{n+1})y_{n+1} = L_n x_n + D x_0 \quad \text{--- ② [component balance]}$$

$$\therefore (L_n + D)y_{n+1} = L_n x_n + D x_0$$

$$\therefore (y_{n+1}) = \frac{L_n x_n}{(L_n + D)} + \frac{D x_0}{(L_n + D)}$$

Assumptions
 $L_1 = L_2 = L_3 = \dots = L_n = L$

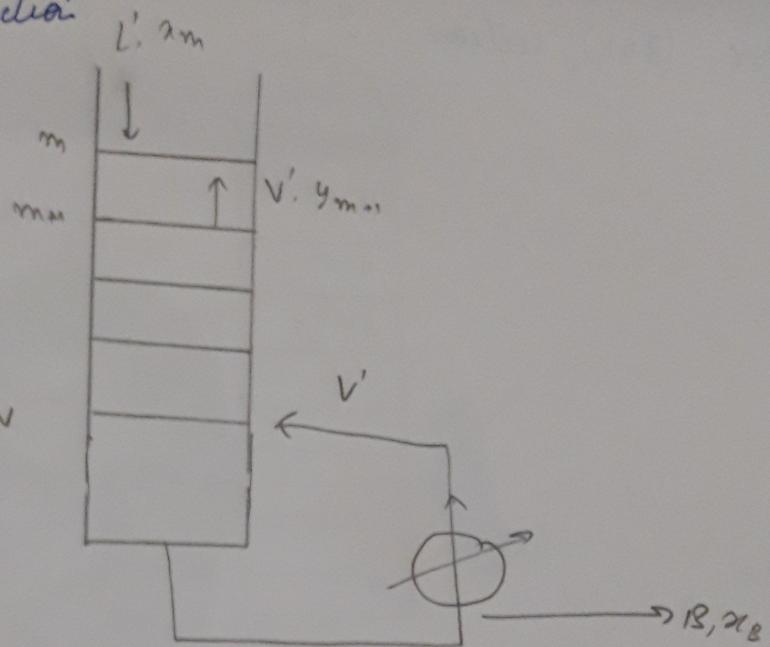
Defining,

$$(R = \frac{L}{D})$$

$$y_{n+1} = \left(\frac{R x_n}{R + 1} + \frac{x_0}{R + 1} \right)$$

→ equation of (ROL)

For stripping section



$$\begin{aligned} L' &= L + 2F \\ V' &= V + (1-2)F \end{aligned}$$

Assuming

$$L'_m = L'_{m+1} = L'_{m+2} = \dots \therefore L_n = L'$$

$$\text{and } V'_m = V'_{m+1} = V'_{m+2} = \dots \quad V'_n = V'$$

Overall balance

$$V' + B = L' \quad \text{--- (1)}$$

Material balance

$$L' x_m = V' y_{m+1} + B x_B \quad \text{--- (2)}$$

$$\therefore (y_{m+1}) = \left(\frac{L'}{V'}\right)x - \left(\frac{B}{V'}\right)x_B \quad \text{and } V' = L' - B$$

$$\therefore \boxed{y = \left(\frac{L'}{L' - B}\right)x - \left(\frac{B}{L' - B}\right)} \quad \text{--- (SOL - Eqn)}$$

\therefore For Raffining section

$$(y = \frac{R x}{R+1} + \frac{u_B}{R+1})$$

and for stripping section

$$y = \left(\frac{L' x}{L' - B} \right) - \left(\frac{B u_B}{L' - B} \right)$$

$$\boxed{y = \left(\frac{L'}{L' - B} \right) x - \left(\frac{B}{L' - B} \right) u_B}$$

where

$$B = w$$

$$\text{and } \boxed{u_B = w_w}$$

for $R = 3.405$

$$\boxed{y = 0.27x + 0.21} \longrightarrow (\text{ROL-line})$$

and

$$R = \frac{L}{B}$$

$$\therefore L = 3.405 \times 27.77$$

$$\therefore \boxed{L = 94.59} \text{ kmol/hr}$$

$$\therefore L' = L + 2F$$

$$= 94.59 + 100 \Rightarrow 194.59 \text{ kmol/hr}$$

$$\bar{V} = \underline{V} \quad \therefore \boxed{y = 1.59x - 0.005} \text{ (SOL-line)}$$

\\ ROI Line :

$$y = 0.79x + 0.31$$

SOL Line

$$y = 1.58x - 0.008$$

From graph: No. of theoretical stages (≈ 10)

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