VE230 Electromagnetics

Chapter 4

September 12, 2022



Exercise 4.1

The upper and lower conducting plates of a large parallel-plate capacitor are separated by a distance d and maintained at potentials V_0 and 0, respectively. A dielectric slab of dielectric constant 6.0 and uniform thickness 0.8d is placed over the lower plate. Assuming negligible fringing effect, determine

- a) the potential and electric field distribution in the dielectric slab,
- b) the potential and electric field distribution in the air space between the dielectric slab and the upper plate,
 - c) the surface charge densities on the upper and lower plates.
 - d) Compare the results in part (b) with those without the dielectric slab.

Answer:

Use subscripts d and $\overline{\nabla}^2$ to denote dielectric and air regions respectively, $\overline{\nabla}^2 V = 0$ in both regions.

$$V_d = c_1 y + c_2, \quad \bar{E}_d = -\bar{a}_y c_1, \bar{D}_d = -\bar{a}_y \epsilon_0 \epsilon_r c_1$$

 $V_a = c_3 y + c_4, \quad \bar{E}_a = -\bar{a}_y c_3, \bar{D}_a = -\bar{a}_y \epsilon_0 c_3$

B.C: At
$$y=0, V_d=0$$
; at $y=d, V_a=V_0$; at $y=0.8d$: $V_d=V_a, \bar{D}_d=\bar{D}_a$. Solving:

$$c_1 = \frac{V_0}{(0.8 + 0.2\epsilon_r) d}, \quad c_2 = 0, \quad c_3 = \frac{\epsilon_r V_0}{(0.8 + 0.2\epsilon_r) d}, \quad c_4 = \frac{(1 - \epsilon_r) V_0}{1 + 0.25\epsilon_r}$$

a)
$$V_d = \frac{5yV_0}{(4+\epsilon_r)d}, \quad \bar{E}_d = -\bar{a}_y \frac{5V_0}{(4+\epsilon_r)d}$$

b)
$$V_a = \frac{5\epsilon_r y - 4(\epsilon_r - 1) d}{(4 + \epsilon_r) d} V_b, \quad \bar{E}_a = -\bar{a}_y \frac{5\epsilon_r V_0}{(4 + \epsilon_r) d}$$

c)
$$(\rho_s)_{y=d} = -(D_a)_{y=d} = \frac{5\epsilon_0 \epsilon_r V_0}{(4+\epsilon_r) d}$$

$$(\rho_s)_{y=0} = (D_d)_{y=0} = -\frac{5\epsilon_0 \epsilon_r V_0}{(4+\epsilon_r) d}$$

Exercise 4.2

Prove that the scalar potential V in Eq. (3-61)

$$V = \frac{1}{4\pi\epsilon_0} \int_{V'} \frac{\rho}{R} dv'$$

satisfies Poisson's equation, Eq. (4-6)

$$\nabla^2 V = -\frac{\rho}{\epsilon}$$

Answer:

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Exercise 4.3

Prove that a potential function satisfying Laplace's equation in a given region possesses no maximum or minimum within the region.

Answer:

At a point where V is a maximum (minimum) the second derivatives of V with respect to x, y, and z would. all be negative (positive); their sum could not vanish, as required by Laplace's equation.

Exercise 4.4

Verify that

$$V_1 = C_1/R$$
 and $V_2 = C_2 z / (x^2 + y^2 + z^2)^{3/2}$,

where C_1 and C_2 are arbitrary constants, are solutions of Laplace's equation.

Answer:

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Exercise 4.5

Assume a point charge Q above an infinite conducting plane at y=0.

- a) Prove that V(x, y, z) in Eq. (4-37) satisfies Laplace's equation if the conducting plane is maintained at zero potential.
- b) What should the expression for V(x, y, z) be if the conducting plane has a nonzero potential V_0 ?
- c) What is the electrostatic force of attraction between the charge Q and the conducting plane?

Answer:

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Exercise 4.6

Assume that the space between the inner and outer conductors of a long coaxial cylindrical structure is filled with an electron cloud having a volume density of charge $\rho = A/r$ for a < r < b, where a and b are, the radii of the inner and outer conductors, respectively. The inner conductor is maintained at a potential V_0 , and the outer conductor is grounded. Determine the potential distribution in the region a < r < b by solving Poisson's equation.

Poisson's eq.
$$\bar{\nabla}^2 V = -\frac{A}{\epsilon r} \longrightarrow \frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial V}{\partial r} \right) = -\frac{A}{\epsilon r}.$$

Solution: $V = -\frac{A}{\epsilon} r + c_1 \ln r + c_2.$
B.C.:
$$\begin{cases} \text{At } r = a, \quad V_0 = -\frac{A}{\epsilon} a + c_1 \ln a + c_2. \quad c_1 = \frac{\frac{A}{\epsilon} (b-a) - V_0}{\ln(b/a)}, \\ \text{At } r = b, \quad 0 = -\frac{A}{\epsilon} b + c_1 \ln b + c_2. \quad c_2 = \frac{V_0 \ln b + \frac{A}{\epsilon} (a \ln b - b \ln a)}{\ln(b/a)}. \end{cases}$$

A point charge Q exists at a distance d above a large grounded conducting plane. Determine

- a) the surface charge density ρ_s ,
- b) the total charge induced on the conducting plane.

Answer:

All swer.
$$\bar{E}\big|_{y=0} = -\bar{a}_y \frac{Q}{4\pi\epsilon R^2} (2\sin\theta) = -\bar{a}_y \frac{Qd}{2\pi\epsilon (d^2 + r^2)^{3/2}}$$
a)
$$\rho_s = \bar{a}_y \cdot \epsilon \bar{E}\big|_{y=0} = -\frac{Qd}{2\pi (d^2 + r^2)^{3/2}}$$
b)
$$\int_0^\infty \rho_s 2\pi r dr = -Q$$

Exercise 4.8

For a positive point charge Q located at distances d_1 and d_2 , respectively, from two grounded perpendicular conducting half-planes shown in Fig. 4-4(a), find the expressions for

- a) the potential and the electric field intensity at an arbitrary point P(x, y) in the first quadrant,
- b) the surface charge densities induced on the two half-planes. Sketch the variations of the surface charge densities in the xy-plane.

Answer:

Consider the conditions in the xy-plane (z = 0).

a)
$$V_p = \frac{Q}{4\pi\epsilon} \left(\frac{1}{R_1} - \frac{1}{R_2} + \frac{1}{R_3} - \frac{1}{R_4} \right)$$
, where
$$R_1 = \left[(x - d_1)^2 + (y - d_2)^2 \right]^{1/2}, \quad R_2 = \left[(x - d_1)^2 + (y + d_2)^2 \right]^{1/2},$$

$$R_3 = \left[(x + d_1)^2 + (y + d_2)^2 \right]^{1/2}, \quad R_4 = \left[(x + d_1)^2 + (y - d_2)^2 \right]^{1/2}.$$

$$\bar{E}_p = -\bar{\nabla}V_p = -\bar{a}_x \frac{\partial V_P}{\partial x} - \bar{a}_y \frac{\partial V_P}{\partial y}$$

$$= \bar{a}_x \frac{Q}{4\pi\epsilon} \left[-\frac{x - d_1}{R_1^3} + \frac{x - d_1}{R_2^3} - \frac{x + d_1}{R_3^3} + \frac{x + d_1}{R_4^3} \right]$$

$$+ \bar{a}_y \frac{Q}{4\pi\epsilon} \left[-\frac{y - d_2}{R_1^3} + \frac{y + d_2}{R_2^3} - \frac{y + d_2}{R_3^3} + \frac{y - d_2}{R_3^3} \right].$$

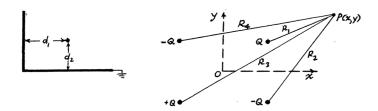
 E_p will have a z-component if the point P does not lie in the xy-plane.

b) On the conducting half-planes, $\rho_s = D_n = \epsilon E_n$. Along the x-axis, y = 0: $R_1 = \left[(x - d_1)^2 + d_2^2 \right]^{1/2} = R_2$, and $R_3 = \left[(x + d_1)^2 + d_2^2 \right]^{1/2} = R_2$ $R_4. E_x = 0, E_y = \frac{Q}{2\pi E} \left[\frac{d_2}{R_1^3} - \frac{d_2}{R_2^3} \right].$

$$\therefore \rho_s(y=0) = \frac{Qd_2}{2\pi} \left\{ \frac{1}{\left[(x-d_1)^2 + d_2^2 \right]^{3/2}} - \frac{1}{\left[(x+d_1)^2 + d_2^2 \right]^{3/2}} \right\}$$

$$= \begin{cases} 0, & \text{at } x=0.\\ & \text{max, at } x=d_1. \end{cases}$$

Similarly for $\rho_s(x=0)$ on the vertical conducting Conducting plane by changing x to y and $d_1 \leftrightarrow d_2$.



Exercise 4.9

Determine the systems of image charges that will replace the conducting boundaries that are maintained at zero potential for

- a) a point charge Q located between two large, grounded, parallel conducting planes as shown in Fig. 4-22(a),
- b) an infinite line charge ρ_{ℓ} located midway between two large, intersecting conducting planes forming a 60-degree angle, as shown in Fig. 4-22(b).

Answer:

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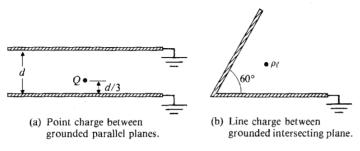


FIGURE 4-22 Diagrams for Problem P.4-9.

A straight conducting wire of radius a is parallel to and at height h from the surface of the earth. Assuming that the earth is perfectly conducting, determine the capacitance and the force per unit length between the wire and the earth.

Answer:

Refer to Example 4-4.

$$C' = \frac{2\pi\epsilon_0}{\ln\left[(h/a) + \sqrt{(h/a)^2 - 1}\right]} = \frac{2\pi\epsilon_0}{\cosh^{-1}(h/a)}$$
 (F/m)

Exercise 4.11

A very long two-wire transmission line, each wire of radius a and separated by a distance d, is supported at a height h above a flat conducting ground. Assuming both d and h to be much larger than a, find the capacitance per unit length of the line.

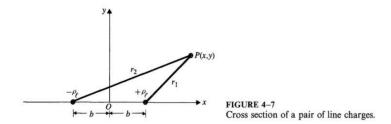
Answer:

Same as
$$C_{12}$$
 in problem $P3 - 38$

Exercise 4.12

For the pair of equal and opposite line charges shown in Fig. 4-7,

- a) write the expression for electric field intensity **E** at point P(x,y) in Cartesian coordinates,
 - b) find the equation of the electric field lines sketched in Fig. 4-8.



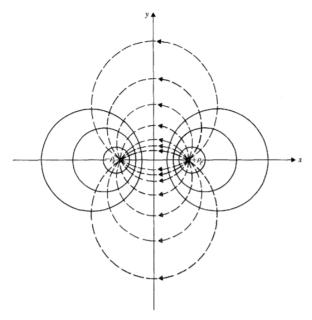


FIGURE 4-8
Equipotential (solid) and electric field (dashed) lines around a pair of line charges.

Answer:

a)

From
$$V_P = \frac{\rho_\ell}{2\pi\epsilon_0} \ln \frac{r_2}{r_1}$$
 and $\frac{r_2}{r_1} = \frac{\sqrt{(x+b)^2 + y^2}}{\sqrt{(x-b)^2 + y^2}} = k$:
$$V_p = \frac{\rho_l}{2\pi\epsilon_0} \ln \frac{\sqrt{(x+b)^2 + y^2}}{\sqrt{(x-b)^2 + y^2}}.$$

$$\bar{E}_p = -\bar{a}_x \frac{\partial V_p}{\partial x} - \bar{a}_y \frac{\partial V_p}{\partial y} = \frac{\rho_l}{2\pi\epsilon_0} \left\{ \frac{\bar{a}_x 2b (y^2 + b^2 - x^2) - \bar{a}_y 4bxy}{[(x+b)^2 + y^2] [y^2 + (x-b)^2]} \right\}$$

b) Equation for lines everywhere tangent to the electric field lines is obtained by requiring

$$\frac{dy}{dx} = \frac{E_y}{E_x} = -\frac{2xy}{y^2 + b^2 - x^2},$$

Which reduces to $\frac{d(x^2+y^2)}{(x^2+y^2)-b^2} = \frac{dy}{y}$. Integrating, we obtain $x^2+y^2-2ky=b^2$, or $x^2+(y-k)^2=b^2+k^2$, where K is a constant. Circles of radii $\sqrt{b^2+k^2}$ having centers at (0,K).

Exercise 4.13

Determine the capacitance per unit length of a two-wire transmission line with parallel conducting cylinders of different radii a_1 and a_2 , their axes being separated by a distance D (where $D > a_1 + a_2$).

Answer:

$$V_1 = -\frac{\rho_l}{2\pi r \epsilon_0} \ln \frac{a_1}{d_1}, \quad V_2 = \frac{\rho_l}{2\pi \epsilon_0} \ln \frac{a_2}{d_2}$$

Capacitance per unit length

$$C' = \frac{\rho_l}{V_1 - V_2} = \frac{2\pi\epsilon_0}{\ln\frac{d_1 d_2}{a_1 a_2}}.$$

Four equations:

$$a_1^2 = d_{i1}d_1,$$
 $a_2^2 = d_{i2}d_2,$
 $d_1 + d_{i2} = D,$ $d_2 + d_{i1} = D.$

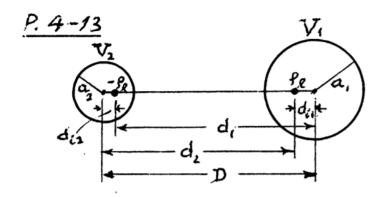
We obtain

$$\frac{d_1 d_2}{a_1 a_2} = \frac{a_1 a_2}{d_{i_1} d_{i_2}} \text{ and } a_1^2 + a_2^2 + d_1 d_2 + d_{i_1} d_{i_2} = D^2$$

$$\frac{d_1 d_2}{a_1 a_2} = \frac{D^2}{2a_1 a_2} - \frac{a_1}{2a_2} - \frac{a_2}{2a_1} + \sqrt{\left(\frac{D^2}{2a_1 a_2} - \frac{a_1}{2a_2} - \frac{a_2}{2a_1}\right)^2 - 1}$$

$$\therefore C' = \frac{2\pi \epsilon_0}{\ln\left[\frac{1}{2}\left(\frac{D^2}{a_1 a_2} - \frac{a_1}{a_2} - \frac{a_2}{a_1}\right) + \sqrt{\frac{1}{4}\left(\frac{D^2}{a_1 a_2} - \frac{a_1}{a_2} - \frac{a_2}{a_1}\right)^2 - 1}\right]}$$

$$= \frac{2\pi \epsilon_0}{\cosh^{-1}\left[\frac{1}{2}\left(\frac{D^2}{a_1 a_2} - \frac{a_1}{a_2} - \frac{a_2}{a_1}\right)\right]} \quad (F/m).$$



Exercise 4.14

A long wire of radius a_1 lies inside a conducting circular tunnel of radius a_2 , as shown in Fig. 4-10(a). The distance between their axes is D.

- a) Find the capacitance per unit length.
- b) Determine the force per unit length on the wire if the wire and the tunnel carry equal and opposite line charges of magnitude ρ_{ℓ} .

Eq.
$$(4-61)$$
: $c_1 = \frac{1}{2D} (a_2^2 - a_1^2 - D^2)$; $E_q(4-62)$: $c_2 = \frac{1}{2D} (a_2^2 - a_1^2 + D^2)$.

Eq.
$$(4-55): b^2 = c_1^2 - a_1^2;$$

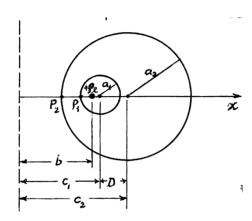
Eq. $(4-56): b^2 = c_2^2 - a_2^2.$
a) $V = \frac{\varphi_l}{2\pi\epsilon_0} \ln \frac{r_2}{r_1}$
At $P_1: r_2 = b + (c_1 - a_1), r_1 = b - (c_1 - a_1).$
At $P_2: r_2 = b + (c_2 - a_2), r_1 = b - (c_2 - a_2).$
 $V_1 - V_2 = \frac{\rho_l}{2\pi\epsilon_0} \ln \left[\frac{b + (c_1 - a_1)b - (c_2 - a_2)}{b - (c_1 - a_1)b + (c_2 - a_2)} \right].$

Expressing $b, c_1 \& c_2$ in terms of $D, a_1 \& a_2$

and simplifying:
$$V_1 - V_2 = \frac{\rho_l}{2\pi\epsilon_0} \ln \left\{ \left(\frac{a_1^2 + a_2^2 - D^2}{2a_1 a_2} \right) + \left[\left(\frac{a_1^2 + a_2^2 - D^2}{2a_1 a_2} \right)^2 - 1 \right]^{1/2} \right\}$$

$$C' = \frac{\rho_l}{V_1 - V_2} = \frac{2\pi\epsilon_0}{\ln\left\{\left(\frac{a_1^2 + a_2^2 - D^2}{2a_1 a_2}\right) + \left[\left(\frac{a_1^2 + a_2^2 - D^2}{2a_1 a_2}\right)^2 - 1\right]^{1/2}} = \frac{2\pi\epsilon_0}{\cosh^{-1}\left(\frac{a_1^2 + a_2^2 - D^2}{2a_1 a_2}\right)} \quad (F/m).$$

b) Force per unit length
$$F' = \frac{\rho_l^2}{2\pi\epsilon_0(4b^2)} = \frac{D^2\rho_l^2}{2\pi\epsilon_0\left[\left(a_1^2 + a_2^2 - D^2\right)^2 - 4a_1^2D^2\right]} (N/m).$$



Exercise 4.15

A point charge Q is located inside and at distance d from the center of a grounded spherical conducting shell of radius b (where b>d). Use the method of images to determine

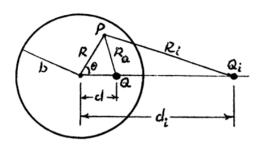
- a) the potential distribution inside the shell,
- b) the charge density ρ_s induced on the inner surface of the shell.

$$Q_i = -\frac{b}{d}Q, \quad d_i = \frac{b^2}{d}.$$

a)
$$V_p = \frac{Q}{4\pi\epsilon_0} \left(\frac{1}{R_Q} - \frac{b}{dR_i} \right);$$

$$R_Q = \left(R^2 + d^2 - 2Rd\cos\theta\right)^{1/2}$$

$$R_i = \left(R^2 + d_i^2 - 2Rd_i \cdot \cos \theta\right)^{1/2}$$
b) $\rho_s = -\epsilon_0 \frac{\partial V}{\partial R}\Big|_{R=b} = -\frac{Q(b^2 - d^2)}{4\pi b(b^2 + d^2 - 2bd\cos \theta)^{3/2}}.$



Two conducting spheres of equal radius a are maintained at potentials V_0 and 0, respectively. Their centers are separated by a distance D.

- a) Find the image charges and their locations that can electrically replace the two spheres.
 - b) Find the capacitance between the two spheres.

Answer:

a) Q_0 and system of image changes: In left sphere Q_0 at $d_0 = 0$.

$$Q_2 = \frac{a^2}{D(D - d_1)} Q_0 \text{ at } d_2$$

$$Q_4 = \frac{a^4}{D(D-d_1)(D-d_2)(D-d_3)}Q_0$$
 at d_4

In right sphere

$$-Q_1 = -\frac{a}{D}Q_0 \text{ at } d_1$$

$$-Q_3 = -\frac{a}{D-d_2}Q_2 = -\frac{a^3}{D(D-d_1)(D-d_2)}Q_0 \text{ at } d_3$$

$$Q_{Ln} = Q_0 \prod_{\substack{m=1\\(n=2,4,6,\cdots)}}^n \frac{a}{D-d_{m-1}} \text{ at } d_n$$

$$-Q_{Rn} = -Q_0 \prod_{m=1}^n \frac{a}{D-d_{m-1}} \text{ at } d_n$$

$$d_m = \frac{a^2}{D-d_{m-1}}, m = 1, 2, 3, \cdots; d_0 = 0$$

(b)
$$C = \frac{Q_0 + \sum_{n} Q_{Ln}}{V_0} = 4\pi\epsilon_0 a \left[1 + \sum_{n=2.4} \left(\prod_{m=1}^{n} \frac{a}{D - d_{m-1}} \right) \right]$$

Two dielectric media with dielectric constants ϵ_1 and ϵ_2 are separated by a plane boundary at x = 0, as shown in Fig. 4-23. A point charge Q exists in medium 1 at distance d from the boundary.

- a) Verify that the field in medium 1 can be obtained from Q and an image charge $-Q_1$, both acting in medium 1.
- b) Verify that the field in medium 2 can be obtained from Q and an image charge $+Q_2$ coinciding with Q, both acting in medium 2.
- c) Determine Q_1 and Q_2 . (Hint: Consider neighboring points P_1 and P_2 in media 1 and 2, respectively, and require the continuity of the tangential component of the E-field and of the normal component of the D-field.)

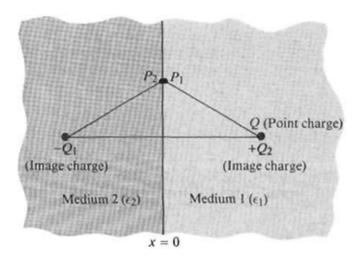


FIGURE 4-23 Image charges in dielectric media (Problem P.4-17).

Answer: 略

Exercise 4.18

Describe the geometry of the region in which the potential function can be represented by a single term as follows:

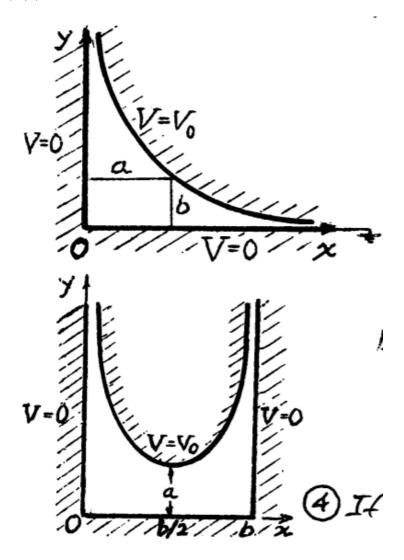
- a) $V(x, y) = c_1 x y$,
- b) $V(x,y) = c_2 \sin kx \sinh ky$.

Find c_1, c_2 , and k in terms of the dimensions and a fixed potential V_0

- a) V(x,y) = c, xy Required boundary conditions:
- (1) $V(0,y) = 0 \rightarrow$ Grounded conducting plane at x = 0.
- (2) $V(x,0) = 0 \rightarrow$ Grounded conducting plane at y = 0.
- If V(a,b) = c, $ab = V_0 \longrightarrow c_1 = \frac{V_0}{ab} \longrightarrow V(x,y) = \frac{V_0}{ab}xy$
- (3) Shape of curved boundary defined by:
- $V(x,y) = V_0 = \left(\frac{V_0}{ab}\right) xy$, or xy = ab (a hyperbola).
- b) $V(x,y) = c_2 \sin kx \sinh y$. Required boundary conditions:

- (1) $V(0,y) = 0 \longrightarrow \text{Grounded plane at } x = 0.$
- (2) $V(\pi/k, y) = 0 \rightarrow \text{Grounded plane at } x = \pi/k = b.$
- (3) $V(x,0) = 0 \longrightarrow \text{Grounded plane at } y = 0.$
- (4) If $V(b/2, a) = c_2 \sin\left(\frac{\pi}{b}\right) \left(\frac{b}{2}\right) \sinh\left(\frac{\pi}{b}\right) a = c_2 \sinh(a\pi/b) = V_0$,

 $V(x,y) = \frac{V_0}{\sinh(a\pi/b)}\sin(\pi x/b)\sinh(\pi y/b)$. curved bounded = $\sinh\left(\frac{\pi}{b}y\right) = \frac{\sinh(a\pi/b)}{\sin(\pi x/b)}$.



Exercise 4.19

In what way should we modify the solution in Eq. (4-114)

$$V(x,y) = \sum_{n=1}^{\infty} C'_n \sinh \frac{n\pi}{b} (x-a) \sin \frac{n\pi}{b} y$$

$$= \frac{4V_0}{\pi} \sum_{n=\text{ odd}}^{\infty} \frac{\sinh[n\pi(a-x)/b]}{n \sinh(n\pi a/b)} \sin \frac{n\pi}{b} y,$$

$$n = 1, 3, 5, \dots,$$

$$0 < x < a \quad \text{and} \quad 0 < y < b.$$

for Example 4-7 if the boundary conditions on the top, bottom, and right planes in Fig. 4-17 are $\partial V/\partial n=0$?

Answer:

$$V_n(x,y) = C'_n \cosh \frac{n\pi}{b} (x-a) \cos \frac{n\pi}{b} y$$

Exercise 4.20

In what way should we modify the solution in Eq. (4-114)

$$V(x,y) = \sum_{n=1}^{\infty} C'_n \sinh \frac{n\pi}{b} (x-a) \sin \frac{n\pi}{b} y$$

$$= \frac{4V_0}{\pi} \sum_{n=\text{ odd}}^{\infty} \frac{\sinh[n\pi(a-x)/b]}{n \sinh(n\pi a/b)} \sin \frac{n\pi}{b} y,$$

$$n = 1, 3, 5, \dots,$$

$$0 < x < a \quad \text{and} \quad 0 < y < b.$$

for Example 4-7 if the top, bottom, and left planes in Fig. 4-17 are grounded (V = 0) and an end plate on the right is maintained at a constant potential V_0 ?

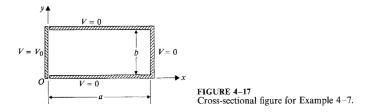
Answer:

$$V_n(x,y) = C_n \sinh \frac{n\pi}{b} x \sin \frac{n\pi}{b} y$$
B.C.
$$\text{at } x = a : V_0 = \sum_{n=1}^{\infty} V_n(a,y) = \sum_{n=1}^{\infty} C_n \sinh \frac{n\pi}{b} a \sin \frac{n\pi}{b} y$$

$$V(x,y) = \frac{4V_0}{\pi} \sum_{n=\text{ odd}}^{\infty} \frac{\sinh(n\pi x/b)}{n \sinh(n\pi a/b)} \sin \frac{n\pi}{b} y$$

Exercise 4.21

Consider the rectangular region shown in Fig. 4-17 as the cross section of an enclosure formed by four conducting plates. The left and right plates are grounded, and the top and bottom plates are maintained at constant potentials V_1 and V_2 , respectively. Determine the potential distribution inside the enclosure.



$$V(x,y) = \sum_{n} \sin \frac{n\pi}{a} x \left[A_n \sinh \frac{n\pi}{a} y + B_n \cosh \frac{n\pi}{a} y \right]$$
At $y = 0$, $V(x,0) = V_2 = \sum_{n} B_n \sin \frac{n\pi}{a} x \to B_n = \begin{cases} \frac{4V_2}{n\pi}, n = \text{ odd.} \\ 0, n = \text{ even.} \end{cases}$
At $y = b, V(x,b) = V_1 = \sum_{n} \sin \frac{n\pi}{a} x \left[A_n \sinh \frac{n\pi}{a} b + B_n \cosh \frac{n\pi}{a} b \right]$

$$\therefore A_n \sinh \frac{n\pi}{a} b + B_n \cosh \frac{n\pi}{a} b = \begin{cases} \frac{4V_1}{n\pi}, n = \text{ odd.} \\ 0, n = \text{ even.} \end{cases}$$

$$\therefore A_n = \begin{cases} \frac{4}{n\pi \sinh(n\pi b/a)} \left(V_1 - V_2 \cosh \frac{n\pi}{a} b \right), n = \text{ odd.} \\ 0, n = \text{ even.} \end{cases}$$

Consider a metallic rectangular box with sides a and b and height c. The side walls and the bottom surface are grounded. The top surface is isolated and kept at a constant potential V_0 . Determine the potential distribution inside the box.

Answer:

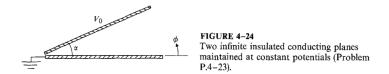
$$V(x,y,z) = \sum_{m} \sum_{n} C_{mn} \sin \frac{m\pi}{a} x \sin \frac{n\pi}{b} y \sinh k_{mn} z, \text{ Where } k_{mn} = \sqrt{\left(\frac{m\pi}{a}\right)^{2} + \left(\frac{n\pi}{b}\right)^{2}}.$$
At $z = c$

$$V(x,y,c) = V_{0} = \sum_{m} \sum_{n} C_{mn} \sin \frac{m\pi}{a} x \sin \frac{n\pi}{b} y \sinh k_{mn} c.$$

$$\longrightarrow C_{mn} = \begin{cases} \frac{16V_{0}}{mn\pi^{2} \sinh k_{mn} c}; m, n = odd. \\ 0, m, n = even. \end{cases}$$

Exercise 4.23

Two infinite insulated conducting planes maintained at potentials 0 and V_0 form a wedge-shaped configuration, as shown in Fig. 4-24. Determine the potential distributions for the regions: (a) $0 < \phi < \alpha$, and (b) $\alpha < \phi < 2\pi$.



Solution:
$$V(\phi) = A_0 \phi + B_0$$

a) B.C. (1): $V(0) = 0 \longrightarrow B_0 = 0$.
B.C. (2): $V(\alpha) = V_0 = A_0 \alpha \longrightarrow A_0 = \frac{V_0}{\alpha}$.

$$V(\phi) = \frac{V_0}{\alpha} \phi$$

$$0 \leqslant \phi \leqslant \alpha$$
b)

B.C. (1):
$$V(\alpha) = V_0 = A_1 \alpha + B_1$$
B.C. (2):
$$V(2\pi) = 0 = 2\pi A_1 + B$$

$$A_1 = -\frac{V_0}{2\pi - \alpha}, B_1 = \frac{2\pi V_0}{2\pi - \alpha}$$

$$V(\phi) = \frac{V_0}{2\pi - \alpha} (2\pi - \phi), \quad \alpha \leqslant \phi \leqslant 2\pi$$

An infinitely long, thin conducting circular cylinder of radius b is split in four quarter-cylinders, as shown in Fig. 4-25. The quarter-cylinders in the second and fourth quadrants are grounded, and those in the first and third quadrants are kept at potentials V_0 and $-V_0$, respectively. Determine the potential distribution both inside and outside the cylinder.

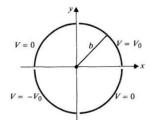


FIGURE 4-25 Cross section of long circular cylinder split in four quarters (Problem P.4-24).

Answer:

The solution is the superposition of that for Example 4-9 and that for Fig.4-19 rotated 90° in the clockwise direction. (In both cases V_0 should be replaced by $V_0/2$.) Inside:

$$V(r,\phi) = \frac{2V_0}{\pi} \sum_{n=odd} \frac{1}{n} \left(\frac{r}{b}\right)^n \left[\sin n\phi + \sin n\left(\phi + \frac{\pi}{2}\right)\right], \quad r < b$$

Outside:

$$V(r,\phi) = \frac{2V_0}{\pi} \sum_{n=odd} \frac{1}{n} \left(\frac{b}{r}\right)^n \left[\sin n\phi + \sin n\left(\phi + \frac{\pi}{2}\right)\right], \quad r > b$$

Exercise 4.25

A long, grounded conducting cylinder of radius b is placed along the z-axis in an initially uniform electric field $\mathbf{E}_0 = \mathbf{a}_x E_0$. Determine potential distribution $V(r, \phi)$ and electric field intensity $\mathbf{E}(r, \phi)$ outside the cylinder. Show that the electric field intensity at the surface of the cylinder may be twice as high as that in the distance, which may cause a local

breakdown or corona. (This phenomenon of corona discharge along the rigging and spars of ships and on airplanes near storms is known as St. Elmo's fire. †)

Answer:

$$V(r,\phi) = -E_0 r \cos \phi + \sum_{n=1}^{\infty} B_n r^{-n} \cos n\phi. \left(\begin{array}{c} \text{At } r >> b \\ E = \bar{a}_k E_0, V = -E_0 r \cos \phi \end{array} \right)$$

$$\text{At } r = b, V(b,\phi) = -E_0 b \cos \phi + \sum_{n=1}^{\infty} B_n b^{-n} \cos n\phi$$

$$\longrightarrow B_1 = E_0 b^2; \quad B_n = 0$$

for

$$n \neq 1$$
.

Outside the cylinder,

$$r \geqslant b : V(r,\phi) = -E_0 r \left(1 - \frac{b^2}{r^2}\right) \cos \phi$$

$$\bar{E}(r,\phi) = -\bar{\nabla}V = \bar{a}_r E_0 \left(\frac{b^2}{r^2} + 1\right) \cos \phi + \bar{a}_\phi E_0 \left(\frac{b^2}{r^2} - 1\right) \sin \phi.$$

$$(\text{At } r = b, \phi = 0, \pi : |E| = 2E_0.)$$

Exercise 4.26

A long dielectric cylinder of radius b and dielectric constant ϵ_r is placed along the z-axis in an initially uniform electric field $\mathbf{E}_0 = \mathbf{a}_x E_0$. Determine $V(r, \phi)$ and $\mathbf{E}(r, \phi)$ both inside and outside the dielectric cylinder.

Answer:

$$r \ge b$$
, $V_0(r,\phi) = -E_0 r \cos \phi + \sum_{n=1}^{\infty} B_n r^{-n} \cos n\phi$
 $r \le b$, $V_i(r,\phi) = \sum_{n=1}^{\infty} A_n r^n \cos n\phi$.

At
$$r = b : V_0(b, \phi) = V_i(b, \phi) \longrightarrow -E_0b + B, b^{-1} = A_1b; B_nb^{-n} = A_nb_n^n n \neq 1$$

$$-\frac{\partial V_0}{\partial r}\bigg|_{r=b} = -\epsilon_r \frac{\partial V_i}{\partial r}\bigg|_{r=b} \longrightarrow E_0 + B_1 b^{-2} = -\epsilon_r A_1; nB_n b^{-(n+1)} = -\epsilon_r nA_n b^{n-1}, n \neq 1.$$

Solving:

$$A_1 = -\frac{2E_0}{\epsilon_r + 1}, B_1 = \frac{\varepsilon_r - 1}{\epsilon_r + 1}b^2 E_0$$

$$A_n = B_n = 0$$
 for $n \neq 1$

$$V_0(r,\phi) = -\left(1 - \frac{\epsilon_r - 1}{\epsilon_r + 1} \frac{b^2}{r^2}\right) E_0 r \cos \phi$$

$$V_i(r,\phi) = -\frac{2}{\epsilon_r + 1} E_0 r \cos \phi$$

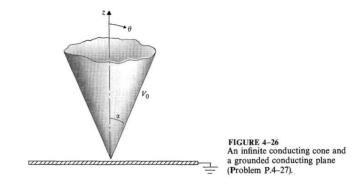
$$\bar{E} = -\bar{\nabla}V = -\bar{a}_r \frac{\partial V}{\partial r} - \bar{a}_\phi \frac{\partial V}{r \partial \phi}$$

$$\bar{E}_0 = \bar{a}_r E_0 \left(1 + \frac{\epsilon_r - 1}{\epsilon_r + 1} \frac{b^2}{r^2}\right) \cos \phi - \bar{a}_\phi E_0 \left(1 - \frac{\epsilon_r - 1}{\epsilon_r + 1} \frac{b^2}{r^2}\right) \sin \phi$$

$$\bar{E}_i = \frac{2}{\epsilon_r + 1} E_0 \left(\bar{a}_r \cos \phi - \bar{a}_\phi \sin \phi\right)$$

An infinite conducting cone of half-angle α is maintained at potential V_0 and insulated from a grounded conducting plane, as illustrated in Fig. 4-26. Determine

- a) the potential distribution $V(\theta)$ in the region $\alpha < \theta < \pi/2$,
- b) the electric field intensity in the region $\alpha < \theta < \pi/2$,
- c) the charge densities on the cone surface and on the grounded plane.



$$V$$
 and \bar{E} depend only on θ . $\to E_q(4-9): \frac{d}{d\theta} \left(\sin \theta \frac{dV}{d\theta}\right) = 0$

a) Solution:
$$\frac{dV}{d\theta} = \frac{C_1}{\sin \theta} \longrightarrow V(\theta) = C_1 \ln \left(\tan \frac{\theta}{2} \right) + C_2$$
$$(1)V(\alpha) = V_0 = C_1 \ln \left(\tan \frac{\theta}{2} \right) + C_2$$
$$(2)V\left(\frac{\pi}{2}\right) = 0 = C_1 \ln \left(\tan \frac{\pi}{4} \right) + C_2 \longrightarrow C_2 = 0$$
$$C_1 = \frac{V_0}{\ln[\tan(\alpha/2)]} \longrightarrow V(\theta) = \frac{V_0 \ln[\tan(\theta/2)]}{\ln[\tan(\alpha/2)]}$$
b)
$$\bar{E} = -\bar{a}_{\theta} \frac{dV}{Rd\theta} = -\bar{a}_{\theta} \frac{V_0}{R \ln[\tan(\alpha/2)] \sin \theta}$$

c) On the cone:
$$\theta = \alpha, \rho_s = \epsilon_0 E(\alpha) = -\frac{t_0 V_0}{R \sin[\tan(\alpha/2)] \sin \theta}$$

On the grounded plane:

$$\theta = \pi/2, \rho_s = -\epsilon_0 E\left(\frac{\pi}{2}\right) = \frac{\epsilon_0 V_0}{R \ln[\tan(\alpha/2)]}$$

Exercise 4.28

Rework Example 4 – 10, assuming that $V(b,\theta) = V_0$ in Eq. (4-155a) $V(b,\theta) = 0^{\dagger}$ EXAMPLE 4-10 An uncharged conducting sphere of radius b is placed in an initially uniform electric field $\mathbf{E}_0 = \mathbf{a}_z E_0$. Determine (a) the potential distribution $V(R, \theta)$, and (b) the electric field intensity $\mathbf{E}(R,\theta)$ after the introduction of the sphere.

Answer:

Starting from Eq. (4-157) and applying the b.c. $V(b,\theta)=V_0$:

$$V_0 = \frac{B_0}{b} + \left(\frac{B_1}{b^2} - E_0 b\right) \cos \theta - \sum_{n=2}^{\infty} B_n b^{-(n+1)} P_n(\cos \theta), \quad R \ge b.$$

$$\longrightarrow B_0 = bV_0, \quad B_1 = E_0 b^3, \quad B_n = 0 \text{ for } n \geqslant 2. \therefore V(R, \theta) = \frac{b}{R} V_0 - E_0 \left[1 - \left(\frac{b}{R} \right)^3 \right] R \cos \theta, \quad R \geqslant b$$

$$\bar{E}(R,\theta) = \bar{a}_R \left\{ \frac{bV_0}{R^2} + E_0 \left[1 + 2\left(\frac{b}{R}\right)^3 \right] \cos \theta \right\} - \bar{a}_\theta E_0 \left[1 - \left(\frac{b}{R}\right)^3 \right] R \sin \theta, R \ge b.$$

$$\rho_s = \epsilon_0 E_R|_{R=b} = \epsilon_0 \frac{V_0}{b} + 3\epsilon_0 E_0 \cos \theta.$$

Exercise 4.29

A dielectric sphere of radius b and dielectric constant ϵ_r is placed in an initially uniform electric field, $\mathbf{E}_0 = \mathbf{a}_z E_0$, in air. Determine $V(R,\theta)$ and $\mathbf{E}(R,\theta)$ both inside and outside the dielectric sphere.

Answer:

$$R \leq b: V_{i}(R,\theta) = \sum_{n=0}^{\infty} A_{n}R^{n}P_{n}(\cos\theta); R \geq b, V_{0}(R,\theta) = \sum_{n=0}^{\infty} \left(B_{n}R^{n} + C_{n}R^{-(n+1)}\right)P_{n}(\cos\theta).$$
For $R \gg b, V_{0}(R,\theta) = -E_{0}Z = -E_{0}R\cos\theta \longrightarrow B_{1} = -E_{0}; B_{n} = c_{n} = 0 \text{ for } n \neq 1.$

$$\therefore V_{0}(R,\theta) = -E_{0}R\cos\theta + C_{1}R^{-2}\cos\theta.$$
B.C. (1) $V_{i}(b,\theta) = V_{0}(b,\theta) \longrightarrow A_{1}b = -E_{0}b + C, b^{-2}\}A_{1} = -\frac{3E_{0}}{\epsilon_{r} + 2},$
(2) $\epsilon_{r}\frac{\partial V_{i}}{\partial R}\Big|_{R=b} = \frac{\partial V_{0}}{\partial R}\Big|_{k=b} \longrightarrow \epsilon_{r}A_{1} = -E_{0} - 2c_{1}b^{-3}\}c_{1} = \frac{\epsilon_{r} - 1}{\epsilon_{r} + 2}E_{0}b^{3}.$

$$V_{i}(R,\theta) = -\frac{3E_{0}}{\epsilon_{r} + 2}R\cos\theta, \quad V_{0}(R,\theta) = -E_{0}R\cos\theta + \frac{(\epsilon_{r} - 1)b^{3}}{(\epsilon_{r} + 2)R^{2}}E_{0}\cos\theta.$$

$$\bar{E}_{i}(R,\theta) = -\bar{\nabla}V_{i} = \frac{3E_{0}}{\epsilon_{r} + 2}\left(\bar{a}_{R}\cos\theta - \bar{a}_{\theta}\sin\theta\right) = \bar{a}_{z}\frac{3\epsilon_{0}}{\epsilon_{r} + 2}.$$

$$\bar{E}_{0}(R,\theta) = -\bar{\nabla}V_{0} = \bar{a}_{R}\left[1 + \frac{2(\epsilon_{r} - 1)b^{3}}{(\epsilon_{r} + 2)R^{3}}\right]E_{0}\cos\theta - \bar{a}_{\theta}\left[1 - \frac{(\epsilon_{r} - 1)b^{3}}{(\epsilon_{r} + 2)R^{3}}\right]E_{0}\sin\theta.$$

Reference

1. Cheng, David Keun. Field and wave electromagnetics. Pearson Education India, 1989.