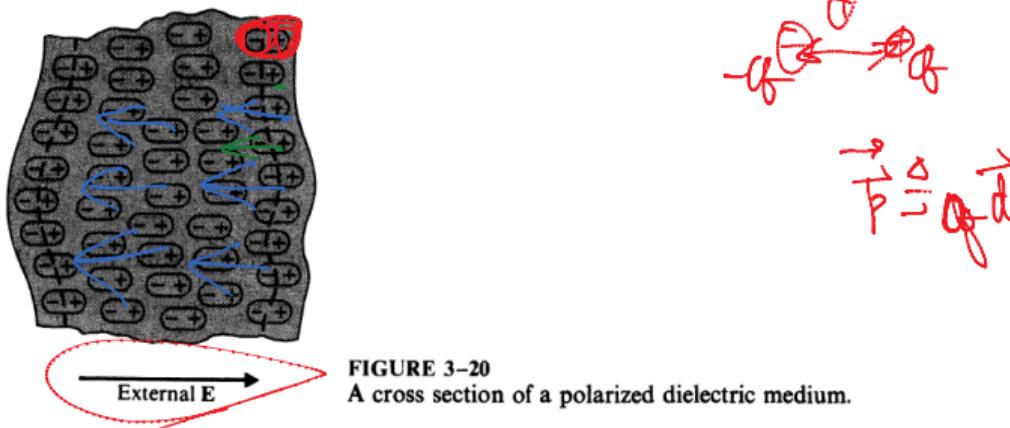


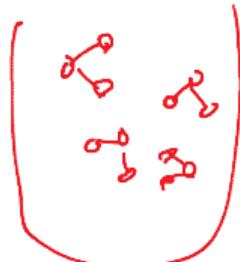
3-7 Dielectrics in Static Electric Field

- Dielectrics: Bound charges
- A dielectric material placed under $\mathbf{E}_{\text{external}}$
 - polarize a dielectric material and create electric dipoles, which is $\mathbf{E}_{\text{induced}}$
 - modify \mathbf{E} both inside and outside the dielectric material



Permanent Dipole Moments

- Some materials have non-zero dipole moments in the absence of E_{external} field
 - E.g., H_2O (polar molecule)
 - Macroscopic viewpoint of H_2O
 - ❖ Without E_{external} : No net dipole moment
 - ❖ With E_{external} : Molecules aligned due to E_{external} → nonzero net dipole moment



$E_{\text{ext}} \Rightarrow$ ordered orientation of water molecules
→ net \vec{P}_{e}

3-7.1 Equivalent Charge Distributions of Polarized Dielectrics

- Macroscopic effect
- Polarization vector:

total number of dipoles

$$N = n\Delta v$$

where N is the total # in a volume (Δv);
 n is the number density

$$\mathbf{P} = \lim_{\Delta v \rightarrow 0} \frac{\sum_{k=1}^{n\Delta v} \mathbf{p}_k}{\Delta v} \quad (\text{C/m}^2), \quad \text{vector addition}$$



P: Volume density of electric dipole moment p

$$d\mathbf{p} = \mathbf{P} dv'$$

$$dm = P dv$$

- Derivation for dielectrics:

$$V = \frac{\mathbf{p} \cdot \mathbf{a}_R}{4\pi\epsilon_0 R^2} \quad (\text{V}),$$

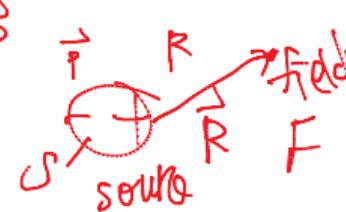
$dV = \frac{\mathbf{P} \cdot \mathbf{a}_R}{4\pi\epsilon_0 R^2} dv'.$

$\int \downarrow$

$$V = \frac{1}{4\pi\epsilon_0} \int_V \frac{\mathbf{P} \cdot \hat{\mathbf{a}}_R}{R^2} dv'$$

$\hat{\mathbf{a}}_R = \frac{\mathbf{r}}{|\mathbf{r}|} = \frac{\mathbf{r}}{|\mathbf{r}|}$

Primed is the coordinate of source



field

$$R^2 = (x - x')^2 + (y - y')^2 + (z - z')^2$$

$$\nabla' \left(\frac{1}{R} \right) = \frac{\hat{\mathbf{a}}_R}{R^2}$$

source:

related to distribution of dipoles

$$\frac{1}{R} = -\frac{\hat{\mathbf{a}}_R}{R^2}$$

Gradient w.r.t the primed coordinate. Thus, no “-” sign at the right side (see slide#20).

$$\begin{aligned} & \hat{\mathbf{a}}_x \frac{\partial}{\partial x} \\ & + \hat{\mathbf{a}}_y \frac{\partial}{\partial y} \\ & + \hat{\mathbf{a}}_z \frac{\partial}{\partial z} \end{aligned}$$

$$V = \frac{1}{4\pi\epsilon_0} \int_V \mathbf{P} \cdot \nabla' \left(\frac{1}{R} \right) dv'$$

$$\nabla' \left(\frac{1}{R} \right) = -\frac{\hat{\mathbf{a}}_R}{R^2}$$



$$\nabla' \cdot (\mathbf{fA}) = \mathbf{f} \nabla' \cdot \mathbf{A} + \mathbf{A} \cdot \nabla' \mathbf{f}$$

letting $\mathbf{A} = \mathbf{P}$ and $f = 1/R$,

$$V = \frac{1}{4\pi\epsilon_0} \left[\int_{V'} \nabla' \cdot \left(\frac{\mathbf{P}}{R} \right) dv' - \int_{V'} \frac{\nabla' \cdot \mathbf{P}}{R} dv' \right]$$

$$\hat{\mathbf{a}}_x \frac{\partial}{\partial x} + \hat{\mathbf{a}}_y \frac{\partial}{\partial y} + \hat{\mathbf{a}}_z \frac{\partial}{\partial z}$$



$$V = \frac{1}{4\pi\epsilon_0} \oint_{S'} \frac{\mathbf{P} \cdot \mathbf{a}'}{R} dS' + \frac{1}{4\pi\epsilon_0} \int_{V'} \frac{(-\nabla' \cdot \mathbf{P})}{R} dv',$$

By divergence theorem



Comparison with

$$V = \frac{1}{4\pi\epsilon_0} \int_{V'} \frac{\rho}{R} dv' \quad (\text{V}).$$

$$V = \frac{1}{4\pi\epsilon_0} \int_{S'} \frac{\rho_s}{R} ds' \quad (\text{V});$$

V = contribution of surface charge distribution

+

contribution of volume charge distribution

$$\rho_{ps} = \mathbf{P} \cdot \mathbf{a}_n$$

$$\rho_p = -\nabla \cdot \mathbf{P}$$

- ' has been dropped for simplicity
- Polarization charge densities or bound-charge densities

polarization

$$V = \frac{1}{4\pi\epsilon_0} \oint_{S'} \frac{\rho_{ps}}{R} ds' + \frac{1}{4\pi\epsilon_0} \int_{V'} \frac{\rho_p}{R} dv'.$$

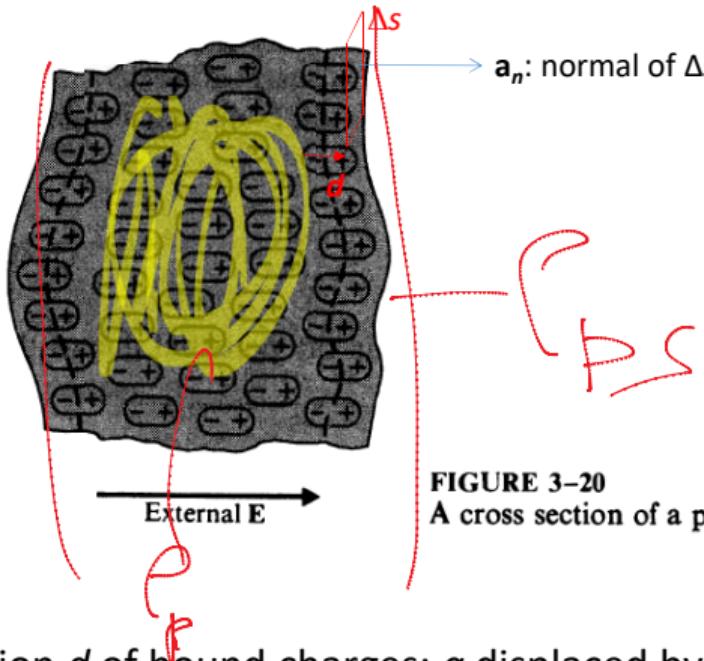


FIGURE 3–20

A cross section of a polarized dielectric medium.

External \mathbf{E}

- Causes a separation d of bound charges; q displaced by d along the direction of the external \mathbf{E}
- Total charge crossing the surface Δs : $nq d(\Delta s)$, for $\mathbf{d} \parallel \mathbf{a}_n$

$$\Delta Q = nq(\mathbf{d} \cdot \mathbf{a}_n)(\Delta s), \text{ for } \mathbf{d} \not\parallel \mathbf{a}_n$$

$$\mathbf{p} = q\mathbf{d}$$

$$\mathbf{P} = n\mathbf{p} = nq\mathbf{d}$$



$$\Delta Q = \mathbf{P} \cdot \mathbf{a}_n (\Delta s) \quad \rho_{ps} = \frac{\Delta Q}{\Delta s} = \mathbf{P} \cdot \mathbf{a}_n,$$



The net charge remaining within the volume V is the negative of the integral

$$\begin{aligned} Q &= - \oint_S \mathbf{P} \cdot \mathbf{a}_n ds \\ &= \int_V (-\nabla \cdot \mathbf{P}) dv = \int_V \rho_p dv, \end{aligned}$$

$$\rho_p = -\nabla \cdot \mathbf{P}.$$

Since starting with an electrically neutral dielectric body, the total charge of the body after polarization must remain zero.

$$\begin{aligned} \text{Total charge} &= \oint_S \rho_{ps} ds + \int_V \rho_p dv \\ &= \oint_S \mathbf{P} \cdot \mathbf{a}_n ds - \int_V \nabla \cdot \mathbf{P} dv = 0, \end{aligned}$$

3-8 Electric Flux Density and Dielectric Constant

- In 3-7, polarization \mathbf{P} or bound volume charge density ρ_p
→ produces \mathbf{E} field due to ρ_p
- Modification of divergence postulates:

$$\boxed{\nabla \cdot \mathbf{E} = \frac{\rho}{\epsilon_0}} \quad \rightarrow \quad \nabla \cdot \mathbf{E} = \frac{1}{\epsilon_0} (\rho + \underline{\rho_p}).$$
$$\downarrow \quad \boxed{\rho_p = -\nabla \cdot \mathbf{P}.}$$
$$\nabla \cdot (\epsilon_0 \mathbf{E} + \mathbf{P}) = \rho.$$
$$\boxed{\mathbf{D} = \epsilon_0 \mathbf{E} + \mathbf{P} \quad (\text{C/m}^2).}$$

Where \mathbf{D} : electric flux density, electric displacement



$$\nabla \cdot \mathbf{D} = \rho \quad (\text{C/m}^3),$$



$$\int_V \nabla \cdot \mathbf{D} dv = \int_V \rho dv$$

$$\oint_S \mathbf{D} \cdot d\mathbf{s} = Q \quad (\text{C})$$

Integral form

Another form of Gauss's law: The total outward flux of the electric displacement (or, simply, the total outward electric flux) over any closed surface is equal to the total *free* charge enclosed in the surface.

χ_e and ϵ_r

- Electric susceptibility
 - For linear and isotropic medium,

$$\mathbf{P} = \epsilon_0 \chi_e \mathbf{E}, \quad \chi_e \text{ dimensionless quantity called } \textit{electric susceptibility}$$

- Relative permittivity (dielectric constant)

$$\mathbf{D} = \epsilon_0 \mathbf{E} + \mathbf{P} \quad (\text{C/m}^2).$$



$$\begin{aligned}\mathbf{D} &= \epsilon_0(1 + \chi_e)\mathbf{E} \\ &= \epsilon_0 \epsilon_r \mathbf{E} = \epsilon \mathbf{E} \quad (\text{C/m}^2),\end{aligned}$$

$$\epsilon_r = 1 + \chi_e = \frac{\epsilon}{\epsilon_0}$$

ϵ : absolute permittivity (or simply permittivity)

	$\epsilon_r = \epsilon/\epsilon_0$
Carbon Tetrachloride ^a	2.2
Ethanol ^a	24
Methanol ^a	33
<i>n</i> -Hexane ^a	1.9
Nitrobenzene ^a	35
Pure Water ^a	80
Barium Titanate ^b (with 20% Strontium Titanate)	>2100
Borosilicate Glass ^b	4.0
Ruby Mica (Muscovite) ^b	5.4
Polyethylene ^b	2.2
Polyvinyl Chloride ^b	6.1
Teflon ^b (Polytetrafluoroethylene)	2.1
Plexiglas ^b	3.4
Paraffin Wax ^b	2.2

^a From Lange's Handbook of Chemistry, 10th ed., McGraw-Hill, New York, 1961, pp. 1234-37.

^b From A. R. von Hippel (Ed.) Dielectric Materials and Applications, M.I.T., Cambridge, Mass., 1966, pp. 301-370

A Simple Medium

- Linear: χ_e is dependent of \mathbf{E} only (not $|\mathbf{E}|^2$, $|\mathbf{E}|^3\ldots$)
- Homogeneous: χ_e is independent of space
- Isotropic: χ_e is a scalar, not a tensor $\rightarrow \mathbf{P}/\mathbf{E}$
- A simple medium: linear, homogeneous, and isotropic
- ϵ_r in a simple medium is a constant

Anisotropic Medium

- The ϵ_r is different for different directions of the electric field
 - \mathbf{D} and \mathbf{E} vectors generally have different directions (i.e., not parallel)
 - $\overline{\overline{\epsilon}}$ is a tensor
- For crystals, choosing a proper coordinate system, $\overline{\overline{\epsilon}}$ can be simplified

$$\begin{bmatrix} D_x \\ D_y \\ D_z \end{bmatrix} = \begin{bmatrix} \epsilon_{11} & \epsilon_{12} & \epsilon_{13} \\ \epsilon_{21} & \epsilon_{22} & \epsilon_{23} \\ \epsilon_{31} & \epsilon_{32} & \epsilon_{33} \end{bmatrix} \begin{bmatrix} E_x \\ E_y \\ E_z \end{bmatrix}.$$

Anisotropic: Biaxial and Uniaxial

- Biaxial: $\epsilon_1 \neq \epsilon_2 \neq \epsilon_3$

$$\begin{bmatrix} D_x \\ D_y \\ D_z \end{bmatrix} = \begin{bmatrix} \epsilon_1 & 0 & 0 \\ 0 & \epsilon_2 & 0 \\ 0 & 0 & \epsilon_3 \end{bmatrix} \begin{bmatrix} E_x \\ E_y \\ E_z \end{bmatrix}. \quad \begin{aligned} D_x &= \epsilon_1 E_x, \\ D_y &= \epsilon_2 E_y, \\ D_z &= \epsilon_3 E_z. \end{aligned}$$

- Uniaxial: $\epsilon_1 = \epsilon_2 \neq \epsilon_3$

- In this book, only deal with isotropic media

3-8.1 Dielectric Strength

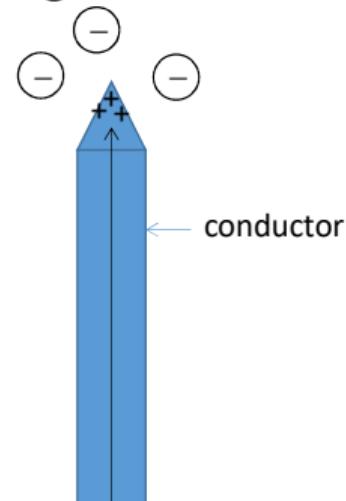
- External $\mathbf{E} \rightarrow$ Displacement of bound charges \rightarrow Polarization \mathbf{P}
- Dielectric breakdown: If very strong external \mathbf{E} causes permanent dislocation of electrons and damage in the material, avalanche effect of ionization due to collisions may occur. The material becomes conducting and may result in large currents.
- Dielectric strength: The maximum \mathbf{E} intensity that a dielectric material can withstand without breakdown

TABLE 3-1
Dielectric Constants and Dielectric Strengths of Some Common Materials

Material	Dielectric Constant	Dielectric Strength (V/m)
Air (atmospheric pressure)	1.0	3×10^6
Mineral oil	2.3	15×10^6
Paper	2–4	15×10^6
Polystyrene	2.6	20×10^6
Rubber	2.3–4.0	25×10^6
Glass	4–10	30×10^6
Mica	6.0	200×10^6

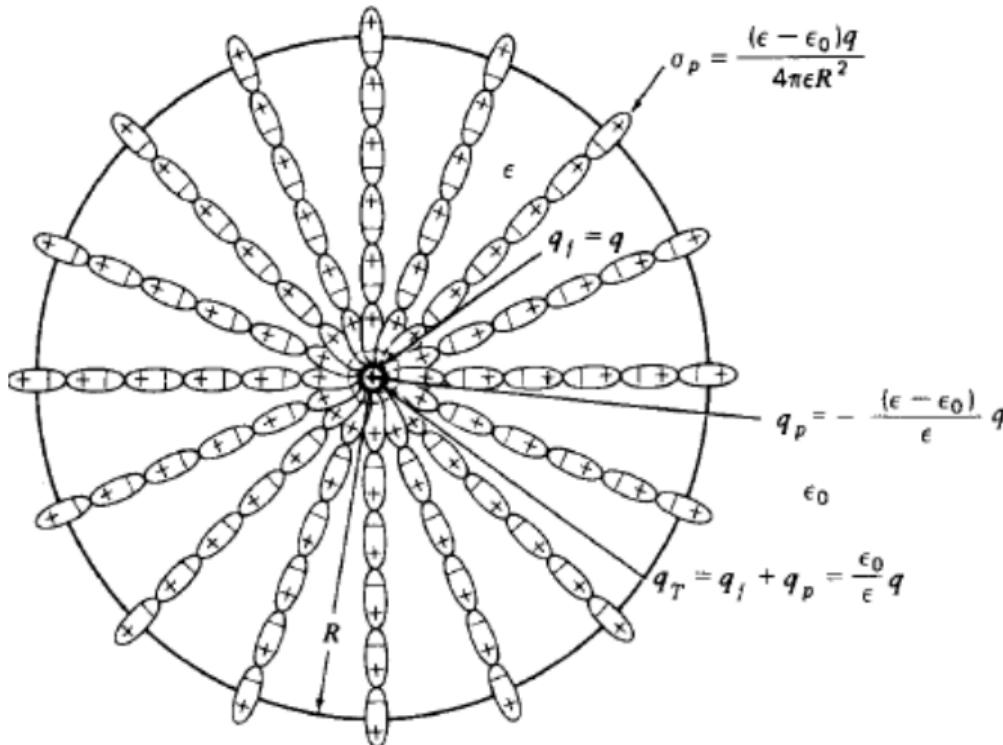
A Lighting Arrester with a Sharp Rod

- Example 3-13: The electric field intensities are inversely proportional to the radii. That is, \mathbf{E} is higher at the surface with a larger curvature.
- A cloud containing an abundance of electric charges
 - ➔ charges of opposite sign are attracted from the ground to the tip
 - ➔ \mathbf{E} is very strong at the tip (sharp points)
 - ➔ When \mathbf{E} at tip > $E_{\text{breakdown, wet air}}$
 - ➔ Air ionized, becomes conducting
 - ➔ $(-)$ in the cloud are discharged safely to the ground



Example: Point Charge Embedded in a Dielectric Sphere

Let's use Maxwell's equations to solve the fields inside materials.



Point Charge Embedded in a Dielectric Sphere

$$\iint_V \vec{D} \cdot \hat{n} dS = \iiint_s \rho dV_s$$

$$D_r 4\pi r^2 = Q$$

$$\therefore \vec{D} = \frac{Q}{4\pi r^2} \hat{r}$$

$$\vec{E} = \frac{Q}{4\pi} \begin{cases} \frac{1}{\epsilon r^2} \hat{r} & r < R \\ \frac{1}{\epsilon_0 r^2} \hat{r} & r > R \end{cases}$$

$$\vec{P} = \vec{D} - \epsilon_0 \vec{E} =$$

$$\vec{P} = \frac{Q}{4\pi r^2} \begin{cases} \left(\frac{\epsilon - \epsilon_0}{\epsilon} \right) \hat{r} & r < R \\ 0 & r > R \end{cases}$$

$$\vec{E} = -\nabla V$$

$$V(\vec{r}) = \frac{Q}{4\pi} \begin{cases} \frac{1}{\epsilon r} + \frac{1}{\epsilon R} \left(\frac{\epsilon - \epsilon_0}{\epsilon_0} \right) & r < R \\ \frac{1}{\epsilon_0 r} & r > R \end{cases}$$

Polarization Induced Charge on Sphere Surface

At the outer surface of the sphere $\mathbf{P}(\mathbf{R}) \cdot \hat{\mathbf{n}} = P_r(\mathbf{R}) = \rho_{ps} = \frac{Q(\epsilon - \epsilon_0)}{4\pi\epsilon R^2}$

In order to maintain charge neutrality, we must have an equal and opposite polarization induced point charge at the center of the sphere. The total polarization charge must sum to zero.

At the center: $q_p = -Q \left(\frac{\epsilon - \epsilon_0}{\epsilon} \right)$  $q_p + q_{ps} = 0$

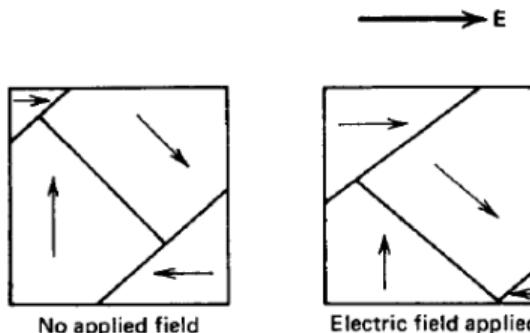
Thus the sphere can be modeled as the combination of the true and polarization charge at the center along with the polarization charge on the outer surface.

At the center: $q_T = q + q_p = Q \frac{\epsilon_0}{\epsilon} = \frac{Q}{\epsilon_r}$ 

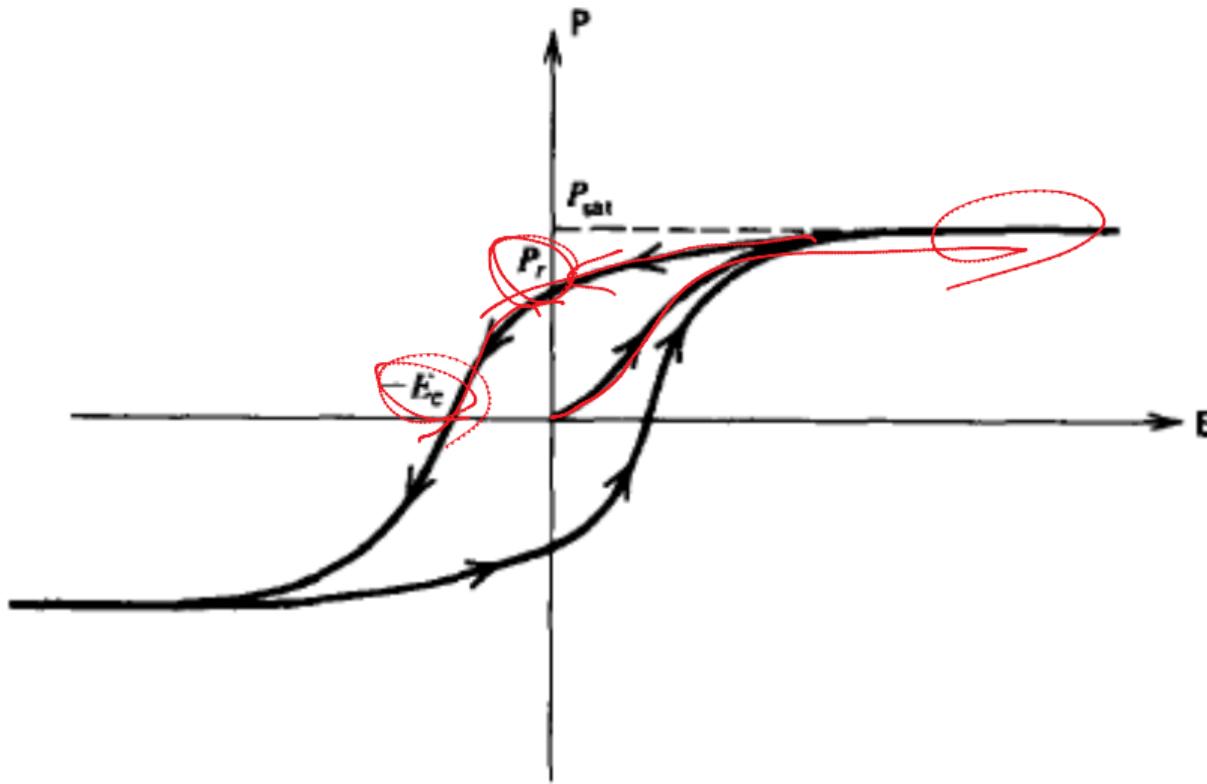
The effect of the dielectric is therefore ***the displacement of some of the original charge to its outer surface.***

Non-Linear Materials: Hysteresis

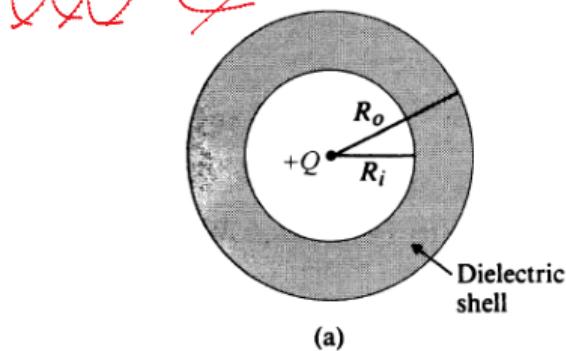
- Ferroelectric materials: such materials exists ***spontaneous polarization*** even when there is no external field. Ferromagnetic materials (permanent magnets) also display similar behavior.
- Domains: There is a whole field for describing how the material changes its polarization when an external field is applied. It is also well known that there are “domains” inside material that have constant polarization and well defined boundaries. The application of an electric field amounts to the ***shrinking or growing*** of these domains.



Ferroelectric Hysteresis Curve

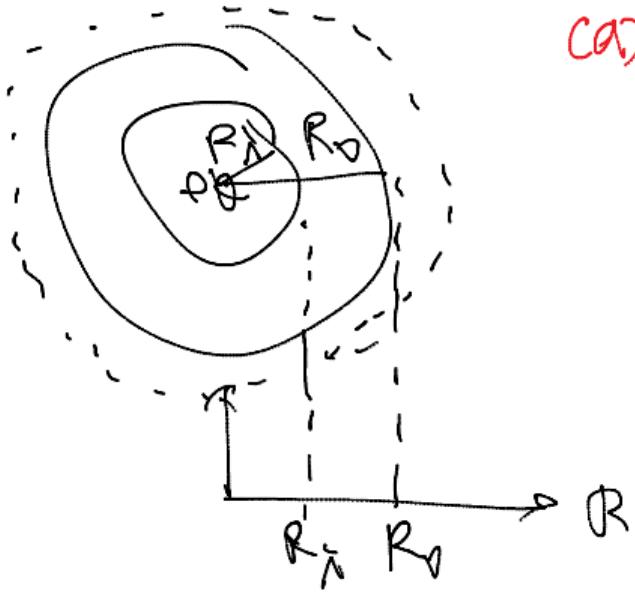


EXAMPLE 3–12 A positive point charge Q is at the center of a spherical dielectric shell of an inner radius R_i and an outer radius R_o . The dielectric constant of the shell is ϵ_r . Determine E , V , D , and P as functions of the radial distance R .



$$\oint_S \mathbf{D} \cdot d\mathbf{s} = Q \quad (\text{C.})$$

Gauss's law: E , $D \rightarrow V$ and P



(a) $R > R_O$

$$\oint E \cdot dS = \frac{Q}{\epsilon_0} \Rightarrow E_{R_I} 4\pi R^2 = \frac{Q}{\epsilon_0}$$

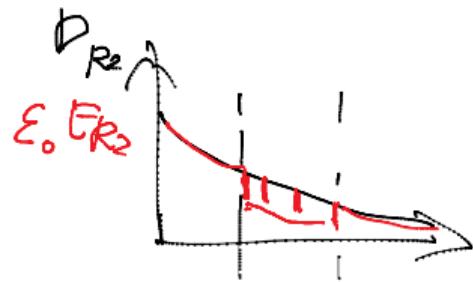
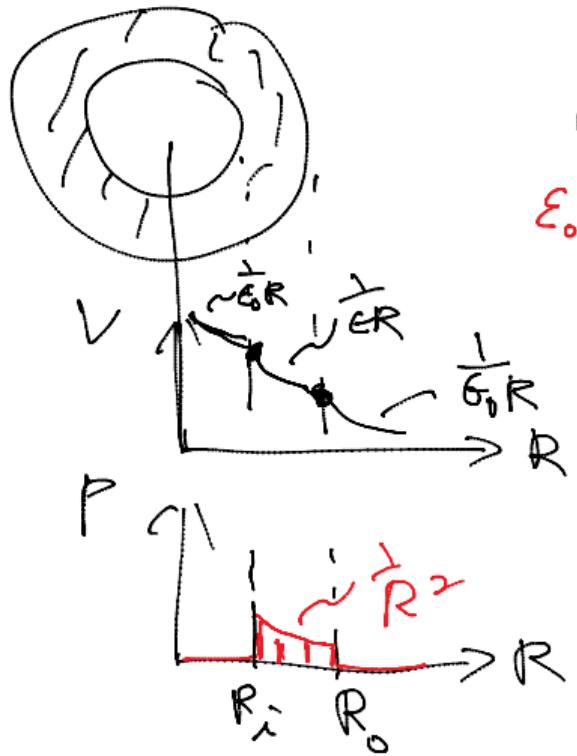
$$E_{R_I} = \frac{Q}{4\pi \epsilon_0 R^2}$$

$$V_I - V = \int_R^R E_{R_I} dR = \dots = \frac{Q}{4\pi \epsilon_0 R}$$

$$P_{R_I} = \epsilon_0 E_{R_I} = \frac{Q}{4\pi R^2}$$

$$P_R = P_{R_I} - \epsilon_0 E_{R_I} = 0$$

(b)



$$P_{R2} = D_{R2} - \epsilon_0 E_{R2}$$

EXAMPLE 3–13 Consider two spherical conductors with radii b_1 and b_2 ($b_2 > b_1$) that are connected by a conducting wire. The distance of separation between the conductors is assumed to be very large in comparison to b_2 so that the charges on the spherical conductors may be considered as uniformly distributed. A total charge Q is deposited on the spheres. Find (a) the charges on the two spheres, and (b) the electric field intensities at the sphere surfaces.

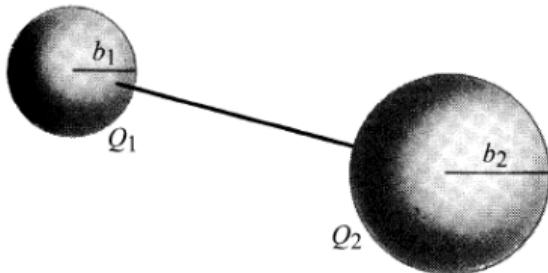
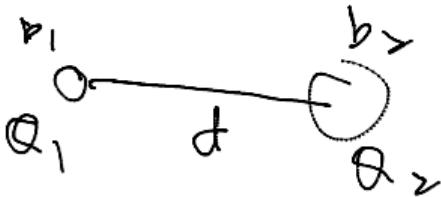


FIGURE 3–22
Two connected conducting spheres (Example 3–13).



$$\theta_1 + \theta_2 = \theta$$

(a) Q_1, Q_2 ?

(b) E_1, E_2 ?

$b_1 < b_2 \ll d$

Q1

$$E_{1n} = \frac{Q_1}{4\pi\epsilon_0 b_1^2}$$

$$E_{2n} = \frac{Q_2}{4\pi\epsilon_0 b_2^2}$$

$$\Rightarrow \frac{E_{1n}}{E_{2n}} = \frac{Q_1}{Q_2} \left(\frac{b_2}{b_1} \right)^2 \\ = \frac{b_2^2}{b_1^2} \approx$$

$$(a) V_1 = V_2$$

~~pot~~ $\therefore b_1 < b_2 \ll d$, \therefore potential on each ball will not be affected by the charge of the other ball

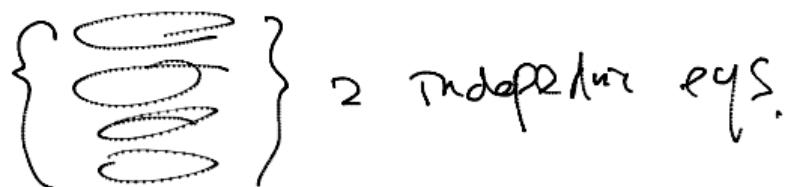
$$V_1 = \frac{Q_1}{4\pi\epsilon_0 b_1} = V_2 = \frac{Q_2}{4\pi\epsilon_0 b_2} \Rightarrow \frac{Q_1}{b_1} = \frac{Q_2}{b_2}$$

$$Q_1 = Q \left(\frac{b_1}{b_1 + b_2} \right); Q_2 = Q \left(\frac{b_2}{b_1 + b_2} \right) \approx$$

3-9 Boundary Conditions for Electrostatic Fields

- Knowledge of the relations of the ***field quantities at an interface*** between two media is of importance for electromagnetic problems.

\vec{E} , \vec{D} , \vec{H} , \vec{B}



B.C.: Tangential Component

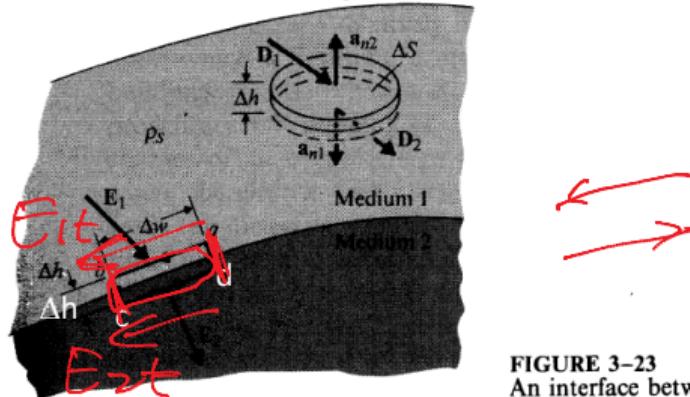


FIGURE 3-23
An interface between two media.

let sides $bc = da = \Delta h$ approach zero

$$\oint_{abeda} \mathbf{E} \cdot d\ell = \mathbf{E}_1 \cdot \Delta w + \mathbf{E}_2 \cdot (-\Delta w) = E_{1t} \Delta w - E_{2t} \Delta w = 0.$$

$$\rightarrow E_{1t} = E_{2t} \quad (\text{V/m}),$$

The tangential component of an \mathbf{E} field is continuous across an interface.

B.C.: Tangential Component

- A conductor/free space interface:

$$E_{2t, \text{conductor}} = 0 \rightarrow E_{1t, \text{free space}} = 0$$

P.C.

free space



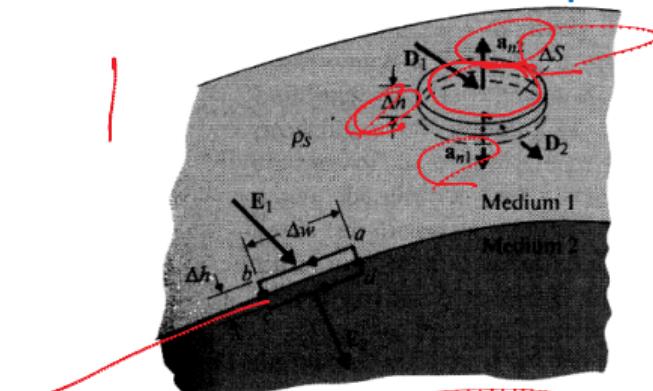
- Two dielectrics:

$$E_{1t} = E_{2t} \quad (\text{V/m}), \quad \rightarrow \quad \frac{D_{1t}}{\epsilon_1} = \frac{D_{2t}}{\epsilon_2}$$

dielect. 1

dielect. 2

B.C.: Normal Component



$$\hat{a}_{n2} \cdot \vec{P}_1 = \downarrow P_{1n}$$

$$\hat{a}_{n2} \cdot \vec{D}_2 = \uparrow D_{2n}$$

FIGURE 3-23
An interface between two media.

Gauss's law: $\oint_S \mathbf{D} \cdot d\mathbf{s} = (\mathbf{D}_1 \cdot \mathbf{a}_{n2} + \mathbf{D}_2 \cdot \mathbf{a}_{n1}) \Delta S$

$$= \mathbf{a}_{n2} \cdot (\mathbf{D}_1 - \mathbf{D}_2) \Delta S$$

$$= \rho_s \Delta S = Q$$

$$\mathbf{a}_{n2} = -\mathbf{a}_{n1}$$

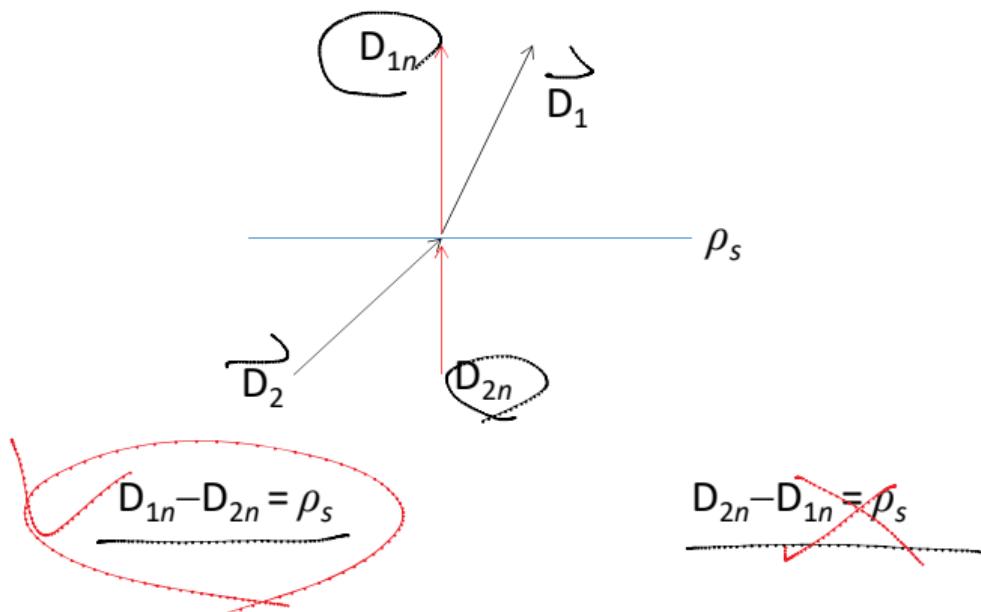
$$\rightarrow \mathbf{a}_{n2} \cdot (\mathbf{D}_1 - \mathbf{D}_2) = \rho_s$$

$$\mathbf{D}_{1n} - \mathbf{D}_{2n} = \rho_s \quad (\text{C/m}^2)$$

Ref.: \mathbf{a}_{n2}

The normal of \mathbf{D} field is **discontinuous** across an interface where **a surface charge** exists—the amount of discontinuity being equal to the surface charge density.

Which one is correct?



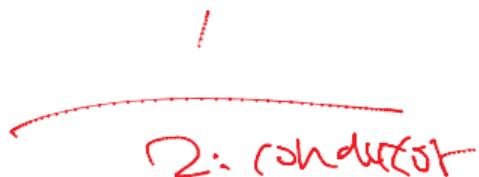
B.C.: Normal Component

$$E_{1n} = \frac{\rho_s}{\epsilon}$$

- For a dielectric (Medium 1)/conductor (Medium 2) interface:

$$\underbrace{D_2 = 0}_{\text{1: dielectric}} \quad \rightarrow \quad D_{1n} = \epsilon_1 E_{1n} = \rho_s,$$

$$\cancel{D_{1n} - D_{2n}}$$



- For no charge existing at the interface

$$\rho_s = 0, \quad \rightarrow \quad D_{1n} = D_{2n} \\ \epsilon_1 E_{1n} = \epsilon_2 E_{2n}.$$

Continuity of D_n and E_n

$$\underbrace{(\mathbf{D}_1 - \mathbf{D}_2) \cdot \hat{\mathbf{n}}}_{\text{red underline}} = \underbrace{(\mathbf{P}_1 + \varepsilon_0 \mathbf{E}_1 - \mathbf{P}_2 - \varepsilon_0 \mathbf{E}_2) \cdot \hat{\mathbf{n}}}_{\text{red underline}} = \rho_s$$

$$(\varepsilon_0 \mathbf{E}_1 - \varepsilon_0 \mathbf{E}_2) \cdot \hat{\mathbf{n}} = \rho_s - \underbrace{(\mathbf{P}_1 - \mathbf{P}_2) \cdot \hat{\mathbf{n}}}_{\text{red underline}} = \rho_s - \rho_{ps}$$

$$(\mathbf{E}_1 - \mathbf{E}_2) \cdot \hat{\mathbf{n}} = \frac{\rho_s - \rho_{ps}}{\varepsilon_0}$$

- The normal component of the \mathbf{D} field is discontinuous by the amount of TRUE charge on the surface.
- The normal component of the \mathbf{E} field is discontinuous by the amount of TOTAL charge (true plus polarization charge).
- Therefore, the D_n field may be continuous (when $\rho_s = 0$).

$\rho_s = \rho_{ps}$ is rate

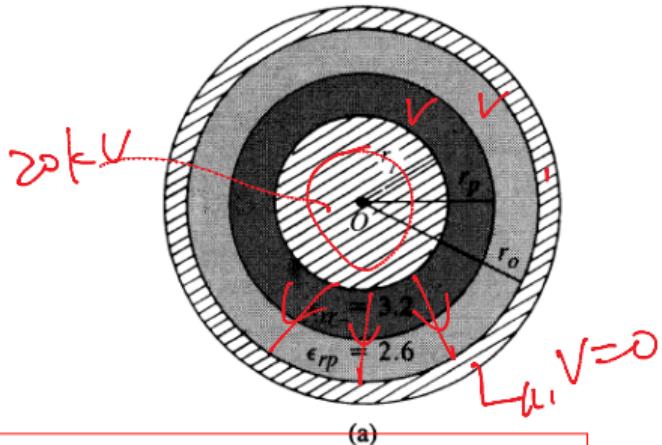
Continuity of D_t and E_t

$$\underline{(\mathbf{E}_1 - \mathbf{E}_2) \times \hat{\mathbf{n}}} = \left(\frac{\mathbf{D}_1 - \mathbf{P}_1}{\epsilon_0} - \frac{\mathbf{D}_2 - \mathbf{P}_2}{\epsilon_0} \right) \times \hat{\mathbf{n}} = \mathbf{0}$$

$$\underline{(\mathbf{D}_1 - \mathbf{D}_2) \times \hat{\mathbf{n}}} = (\mathbf{P}_1 - \mathbf{P}_2) \times \hat{\mathbf{n}} = \epsilon_0 (\Delta \chi_e) \mathbf{E} \times \hat{\mathbf{n}}$$

- The tangential component of the \mathbf{E} field is continuous across EVERY interface.
- The tangential component of the \mathbf{D} field is discontinuous by the amount of **susceptibility difference** of the interface.

EXAMPLE 3–16 When a coaxial cable is used to carry electric power, the radius of the inner conductor is determined by the load current, and the overall size by the voltage and the type of insulating material used. Assume that the radius of the inner conductor is 0.4 (cm) and that concentric layers of rubber ($\epsilon_{rr} = 3.2$) and polystyrene ($\epsilon_{rp} = 2.6$) are used as insulating materials. Design a cable that is to work at a voltage rating of ~~20 (kV)~~. In order to avoid breakdown due to voltage surges caused by lightning and other abnormal external conditions, the maximum electric field intensities in the insulating materials are not to exceed 25% of their dielectric strengths.



(a)

$$E \leq 0.25 \times E_{\max, \text{rubber}}$$

$$E \leq 0.25 \times E_{\max, \text{ps}}$$

The E field from an infinitely long conductor = $\rho_i / (2\pi\epsilon)$

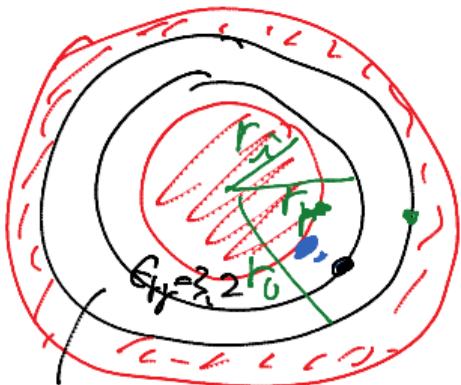
V by taking integration of E field

$$\uparrow E = \frac{\uparrow V}{\uparrow d}$$

$$E = \frac{Q}{2\pi R^2 \epsilon}$$

$$r_i = 0.4 \text{ cm}$$

$$r_p? \quad r_o$$



$$\epsilon_{rp} = 2.6$$

$$2^{\circ} V_{max} = \underline{20k}$$

$$= - \int_{r_0}^{r_i} E_r dr$$

$$= - \int_{r_0}^{r_p} E_{r,ps} dr - \int_{r_p}^{r_i} E_{r,rubber} dr$$

$$1^{\circ} E_{max, rubber} = \frac{1}{4} \times 25 \times 10^6 = \frac{\rho_e}{2\pi \epsilon_0 \cdot G_F \cdot r_i}$$

$$E_{max, ps} = \frac{1}{4} \times 20 \times 10^6 = \frac{\rho_e}{2\pi \epsilon_0 \cdot G_F \cdot r_p} \Rightarrow r_p = 0.616 \text{ cm}$$

$$\frac{\Phi}{\Theta} = \dots$$

$$= \frac{\rho_e}{2\pi \epsilon_0} \left[\frac{1}{G_F} \ln \left(\frac{r_o}{r_p} \right) + \frac{1}{G_F} \ln \left(\frac{r_p}{r_i} \right) \right] \Rightarrow r_0 = 0.832 \text{ cm}$$

3-10 Capacitance and Capacitors

- Deposit charges Q on a conductor $\rightarrow V$
- $kQ \rightarrow k\rho_s \rightarrow kV$

$$V = \frac{1}{4\pi\epsilon_0} \int_{S'} \frac{\rho_s}{R} ds' \quad (V);$$

$$V = \frac{Q}{4\pi\epsilon_0 R} \Rightarrow V \sim Q$$

- The ratio Q/V unchanged

$$Q = CV,$$

C : capacitance (C/V , or Farad)

$$\uparrow C = \frac{Q}{V}$$

Capacitor

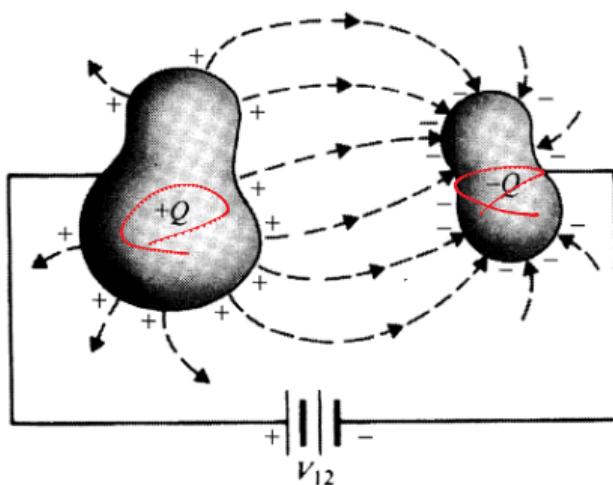


FIGURE 3–27
A two-conductor capacitor.

$\mathbf{E} \perp$ conductor surfaces (equipotential surfaces)

$$C = \frac{Q}{V_{12}} \quad (\text{F})$$

Capacitance

- C depends on
 - The geometry of the conductors
 - The permittivity of the medium between conductors
 - ***Independent of Q and V***
 - Measurement of C
 - Method 1: V_{12} known, determine Q (Chap.4)
 - Method 2: Q known, determine V_{12}
 - ❖ 1. Choose a proper coordinate system
 - ❖ 2. Assume $+Q, -Q$ on the conductors
 - ❖ 3. Find \mathbf{E} from Q (Gauss's law, etc.); Find V_{12} by
$$V_{12} = - \int_2^1 \mathbf{E} \cdot d\ell$$
 - ❖ 4. $C = Q/V_{12}$
- See examples 3-17, 3-18, 3-19

3-10.1 Series and Parallel Connections of Capacitors

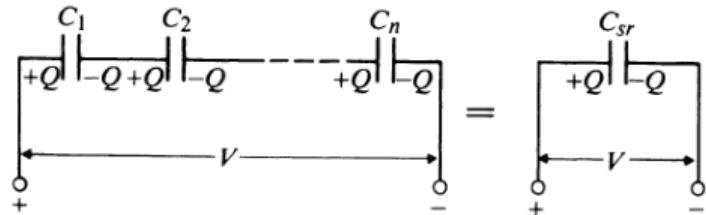


FIGURE 3-31
Series connection of capacitors.

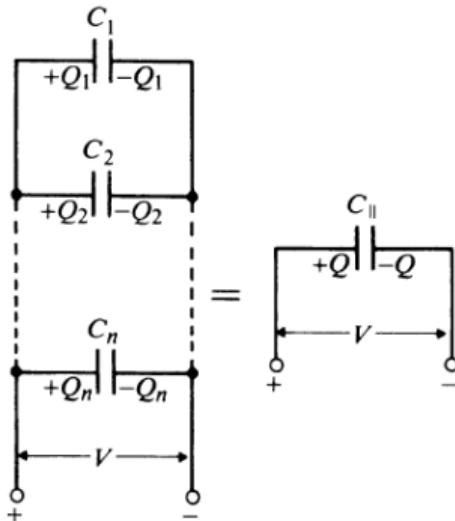


FIGURE 3-32
Parallel connection of capacitors.

Series

- V
 - $+Q$ and $-Q$ on two external terminals
 - $+Q$ and $-Q$ also induced internally

$$\rightarrow V = \frac{Q}{C_{sr}} = \frac{Q}{C_1} + \frac{Q}{C_2} + \cdots + \frac{Q}{C_n},$$

$$\boxed{\frac{1}{C_{sr}} = \frac{1}{C_1} + \frac{1}{C_2} + \cdots + \frac{1}{C_n}.}$$

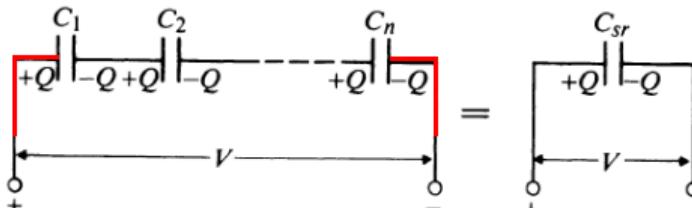
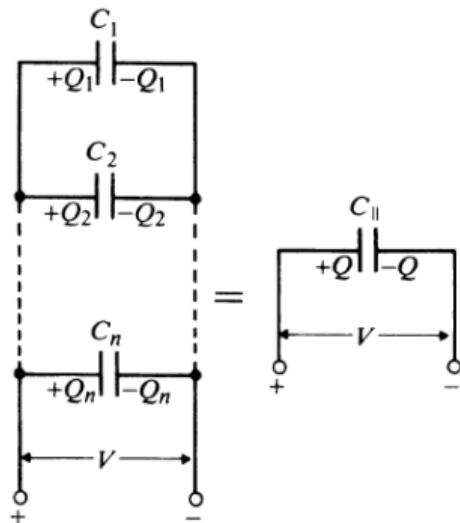


FIGURE 3-31
Series connection of capacitors.

Parallel

- V
→ Q_1, Q_2, Q_3, \dots on each capacitor



$$\begin{aligned}Q &= Q_1 + Q_2 + \cdots + Q_n \\&= C_1 V + C_2 V + \cdots + C_n V = C_{\parallel} V\end{aligned}$$

$$C_{\parallel} = C_1 + C_2 + \cdots + C_n.$$

FIGURE 3–32
Parallel connection of capacitors.

3-10.2 Capacitances in Multiconductor Systems

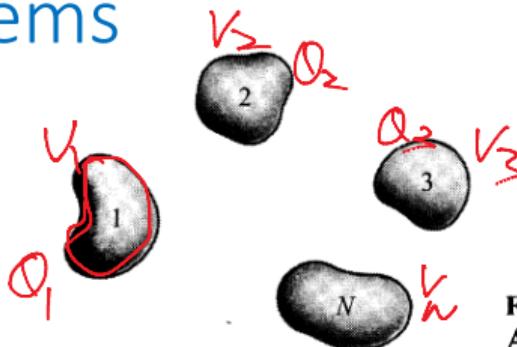


FIGURE 3-34
A multiconductor system.

Presence of a charge on any one of the conductors affects potential of all the other conductors

$$V_1 = p_{11}Q_1 + p_{12}Q_2 + \cdots + p_{1N}Q_N,$$

$$V_2 = p_{21}Q_1 + p_{22}Q_2 + \cdots + p_{2N}Q_N,$$

⋮

$$V_N = p_{N1}Q_1 + p_{N2}Q_2 + \cdots + p_{NN}Q_N.$$

p_{ij} : coefficients of potential; depends on
1. Shape and position of the conductor
2. Permittivity of surroundings

For an isolated system $Q_1 + Q_2 + Q_3 + \cdots + Q_N = 0$.

$$\bar{V} = \begin{bmatrix} \bar{P} \\ \vdots \end{bmatrix} \bar{q}$$

$$Q_1 = c_{11}V_1 + c_{12}V_2 + \cdots + c_{1N}V_N,$$

$$Q_2 = c_{21}V_1 + c_{22}V_2 + \cdots + c_{2N}V_N,$$

⋮

$$Q_N = c_{N1}V_1 + c_{N2}V_2 + \cdots + c_{NN}V_N,$$

c_{ii} : coefficients of capacitance

c_{ij} : coefficients of induction ($i \neq j$)

$$\bar{Q}_r = \bar{P}^{-1} \bar{V}$$

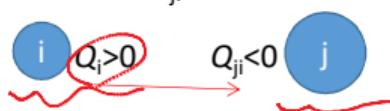
c_{ii} : ground all other conductors, then $c_{ii} = Q_i/V_i$

c_{ji} : Induced charge $Q_{ji} = c_{ji}V_i$



If Q_i on ith conductor and $Q_i > 0$, then $V_i > 0$ and induced $Q_{ji} < 0$

Thus, $c_{ii} > 0$; $c_{ji} < 0$



By reciprocity, $p_{ij} = p_{ji}$ and $c_{ij} = c_{ji}$

A Four-conductor System

$$Q_1 = c_{11}V_1 + c_{12}V_2 + \cdots + c_{1N}V_N,$$

$$Q_2 = c_{21}V_1 + c_{22}V_2 + \cdots + c_{2N}V_N,$$

⋮

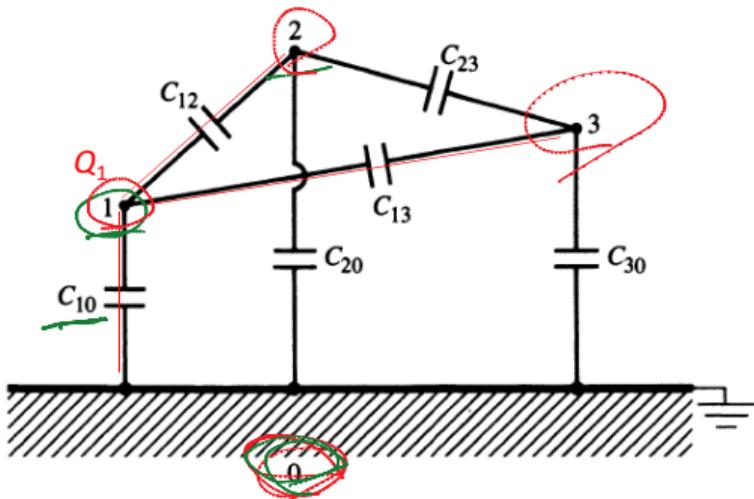
$$Q_N = c_{N1}V_1 + c_{N2}V_2 + \cdots + c_{NN}V_N,$$



Conductors 0, 1, 2, 3. Let conductor 0 be grounded (i.e., $V_0 = 0$).

$$\left\{ \begin{array}{l} Q_0 = 0 \\ Q_1 = c_{11}V_1 + c_{12}V_2 + c_{13}V_3, \\ Q_2 = c_{21}V_1 + c_{22}V_2 + c_{23}V_3, \\ Q_3 = c_{31}V_1 + c_{32}V_2 + c_{33}V_3, \end{array} \right.$$

A Four-conductor System



c: capacitance of coefficients
C: partial capacitance

c: Coefficient of capacitance
C: Capacitance

FIGURE 3–35
Schematic diagram of three conductors and the ground.

Rewrite the $Q \sim V$ relation (by definition of capacitance)

$$Q_1 = C_{10}V_1 + \underline{C_{12}(V_1 - V_2)} + C_{13}(V_1 - V_3),$$

$$Q_2 = C_{20}V_2 + C_{12}(V_2 - V_1) + \underline{C_{23}(V_2 - V_3)},$$

$$Q_3 = C_{30}V_3 + C_{13}(V_3 - V_1) + C_{23}(V_3 - V_2),$$

C_{10}, C_{20}, C_{30} : self-partial capacitance
 $C_{ij} (i \neq j)$: mutual partial capacitance

Compare:

$$Q_1 = c_{11}V_1 + c_{12}V_2 + c_{13}V_3, \quad Q_1 = C_{10}V_1 + C_{12}(V_1 - V_2) + C_{13}(V_1 - V_3),$$

$$Q_2 = c_{12}V_1 + c_{22}V_2 + c_{23}V_3, \quad Q_2 = C_{20}V_2 + C_{12}(V_2 - V_1) + C_{23}(V_2 - V_3),$$

$$Q_3 = c_{13}V_1 + c_{23}V_2 + c_{33}V_3, \quad Q_3 = C_{30}V_3 + C_{13}(V_3 - V_1) + C_{23}(V_3 - V_2),$$



Coefficient of capacitance:

$$\underline{c_{11} = C_{10} + C_{12} + C_{13},}$$

$$\underline{c_{22} = C_{20} + C_{12} + C_{23},}$$

$$\underline{c_{33} = C_{30} + C_{13} + C_{23},}$$

Coefficient of inductance:

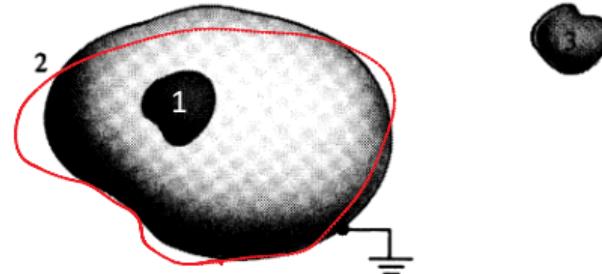
$$c_{12} = -C_{12},$$

$$c_{23} = -C_{23},$$

$$c_{13} = -C_{13}.$$

$$\begin{aligned} C_{10} &= c_{11} + c_{12} + c_{13}, \\ C_{20} &= c_{22} + c_{12} + c_{23}, \\ C_{30} &= c_{33} + c_{13} + c_{23}. \end{aligned}$$

3-10.3 Electrostatic Shielding



$$\begin{aligned}Q_1 &= C_{10}V_1 + C_{12}(V_1 - V_2) + C_{13}(V_1 - V_3), \\Q_2 &= C_{20}V_2 + C_{12}(V_2 - V_1) + C_{23}(V_2 - V_3), \\Q_3 &= C_{30}V_3 + C_{13}(V_3 - V_1) + C_{23}(V_3 - V_2),\end{aligned}$$

FIGURE 3-37
Illustrating electrostatic shielding.

Following the previous system, we ground the conductor #2.
(i.e., $V_2=0$)

$$\rightarrow Q_1 = C_{10}V_1 + \cancel{C_{12}V_1} + \cancel{C_{13}(V_1 - V_3)}.$$

When $\cancel{Q_1 = 0} \rightarrow E \text{ inside } \#2 = 0 \rightarrow V_1 = V_2 = 0 \rightarrow 0 = -C_{13}V_3 \rightarrow C_{13} = 0$

Gauss's law

A change of V_3 will not affect Q_1 .

EXAMPLE 3–18 A cylindrical capacitor consists of an inner conductor of radius a and an outer conductor whose inner radius is b . The space between the conductors is filled with a dielectric of permittivity ϵ , and the length of the capacitor is L . Determine the capacitance of this capacitor.

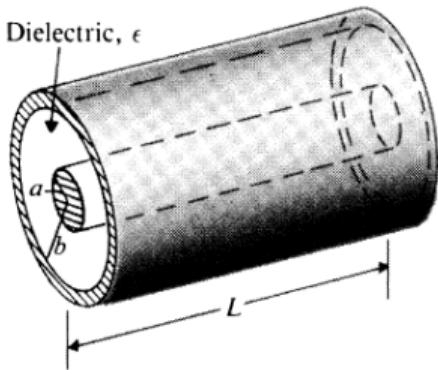


FIGURE 3–29
A cylindrical capacitor (Example 3–18).



1° Assume \vec{E} , \rightarrow

2° Gauss's law: $\vec{E} = \hat{\alpha}_r \frac{\rho_0}{\epsilon_0 r} = \hat{\alpha}_r \frac{Q}{2\pi\epsilon_0 L}$

3° $V_{ab} = - \int_b^a E_r dr$

$$= \dots = \frac{Q}{2\pi\epsilon_0 L} \ln\left(\frac{b}{a}\right)$$



4° $C = \frac{Q}{V_{ab}} = \frac{2\pi\epsilon_0 L}{\ln\left(\frac{b}{a}\right)}$

EXAMPLE 3–21 Three horizontal parallel conducting wires, each of radius a and isolated from the ground, are separated from one another as shown in Fig. 3–36. Assuming $d \gg a$, determine the partial capacitances per unit length between the wires.

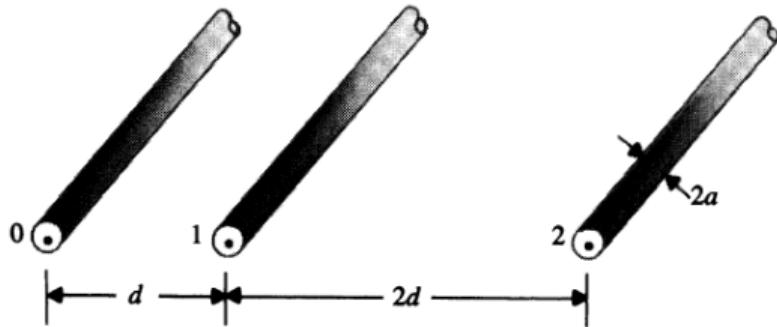
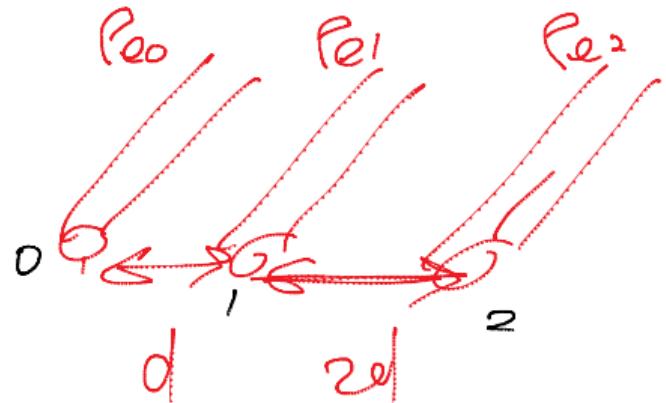


FIGURE 3–36
Three parallel wires (Example 3–21).

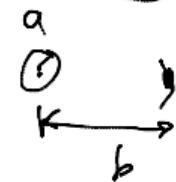


radius = a

C per unit length?

Ex3-18

$$V_{ab} = \frac{Q}{2\pi\epsilon_0 L} \ln\left(\frac{b}{a}\right)$$



$\langle \sigma_0 \rangle$

$$\begin{aligned} V_{10} &= V_{10, R_{e1}} + V_{0, R_{e2}} + \underline{V_{10, R_{e3}}} \\ &= -V_{01} + \frac{R_{e1}}{2\pi\epsilon_0} \ln\left(\frac{d}{a}\right) + \left[\frac{R_{e3}}{2\pi\epsilon_0} \ln\left(\frac{3d}{a}\right) - \frac{R_{e2}}{2\pi\epsilon_0} \ln\left(\frac{2d}{a}\right) \right] \\ &\quad - \left(\frac{R_{e0}}{2\pi\epsilon_0} \ln\left(\frac{d}{a}\right) \right) \end{aligned}$$

3-11 Electrostatic Energy and Forces

- From Eq. 3-44 $V_{21} \equiv \frac{W}{q} = - \int_{P_1}^{P_2} \mathbf{E} \cdot d\ell$ (J/C or V).
 - Work required to bring a charge q from P_1 to P_2
 $W = qV_{21}$
- A charge Q_1 in free space. Work required to bring a **second** charge Q_2 from infinity to a distance R_{12} : $W = Q_2 V_{2\infty} = Q_2 V_2$

$$W_2 = Q_2 V_2 = Q_2 \left(\frac{Q_1}{4\pi\epsilon_0 R_{12}} \right) \text{ due to } Q_1$$

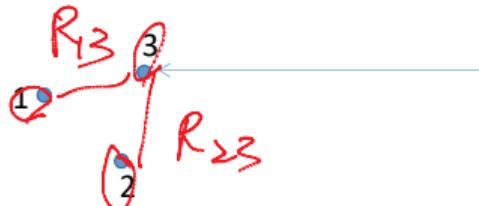
$$W_2 = Q_1 \frac{Q_2}{4\pi\epsilon_0 R_{12}} = Q_1 V_1.$$

$$Q_1 V_1 = Q_2 V_2; Q_1 V_1 + Q_2 V_2 = 2W_2$$

$$W_2 = \frac{1}{2}(Q_1 V_1 + Q_2 V_2).$$

Against \mathbf{E} field of charge Q_1
(V_2 is due to charge Q_1)





- Another charge Q_3 . Work required to bring a **third** charge Q_3 from infinity to a distance R_{13} from Q_1 and R_{23} from Q_2 : $\Delta W = Q_3 V_{3\infty}$

$$\Delta W = Q_3 V_3 = Q_3 \left(\frac{Q_1}{4\pi\epsilon_0 R_{13}} + \frac{Q_2}{4\pi\epsilon_0 R_{23}} \right).$$

Against E field of charge Q_1 and E field of charge Q_2
(V_3 is due to charges Q_1 and Q_2)

- Total work to assemble the 3 charges Q_1 , Q_2 , and Q_3 : $W_3 = W_2 + \Delta W$

$$W_3 = W_2 + \Delta W = \frac{1}{4\pi\epsilon_0} \left(\frac{Q_1 Q_2}{R_{12}} + \frac{Q_1 Q_3}{R_{13}} + \frac{Q_2 Q_3}{R_{23}} \right).$$

Rewrite: 3 terms divided into 6 terms

$$W_3 = \frac{1}{2} \left[Q_1 \left(\frac{Q_2}{4\pi\epsilon_0 R_{12}} + \frac{Q_3}{4\pi\epsilon_0 R_{13}} \right) + Q_2 \left(\frac{Q_1}{4\pi\epsilon_0 R_{12}} + \frac{Q_3}{4\pi\epsilon_0 R_{23}} \right) + Q_3 \left(\frac{Q_1}{4\pi\epsilon_0 R_{13}} + \frac{Q_2}{4\pi\epsilon_0 R_{23}} \right) \right]$$

work
required
by Q_1
to bring Q_3

$$= \frac{1}{2} (Q_1 V_1 + Q_2 V_2 + Q_3 V_3).$$

- Potential V_1 is caused by charges Q_2 and Q_3
- Different from the previous V_1 due to Q_2 only

General expression

Self energy: work required to assemble the individual point charges

Initially, Q_1 in space

Introduce Q_2

$$\Delta W = Q_2 V_{2\infty}$$

Introduce Q_3

$$\Delta W = Q_3 V_{3\infty}$$

$$Q_4 \quad \Delta W = Q_4 V_{4\infty}$$

Mutual energy: the interacting energy

$$W_2 = \frac{1}{2}(Q_1 V_1 + Q_2 V_2).$$

$$W_3 = \frac{1}{2}(Q_1 V_1 + Q_2 V_2 + Q_3 V_3).$$

$$W_4 = \sum_{i=1}^4 Q_i V_i$$

$$W_e = \frac{1}{2} \sum_{k=1}^N Q_k V_k \quad (\text{J}),$$

Potential V_k is caused by all the other charges

$$V_k = \frac{1}{4\pi\epsilon_0} \sum_{\substack{j=1 \\ (j \neq k)}}^N \frac{Q_j}{R_{jk}}.$$

3-11.1 Electrostatic Energy in terms of Field Quantities

- For a continuous charge distribution of density ρ

$$W_e = \frac{1}{2} \int_{V'} \rho V dv \quad (\text{J}).$$

Volume

Electrical potential

$$\rho(r) V(r)$$



$$W_e = \frac{1}{2} \int_{V'} (\nabla \cdot \mathbf{D}) V dv.$$



$$\nabla \cdot (V \mathbf{D}) = V \nabla \cdot \mathbf{D} + \mathbf{D} \cdot \nabla V,$$

$$W_e = \frac{1}{2} \int_{V'} \nabla \cdot (V \mathbf{D}) dv - \frac{1}{2} \int_{V'} \mathbf{D} \cdot \nabla V dv$$

$$= \frac{1}{2} \oint_S V \mathbf{D} \cdot \mathbf{a}_n ds + \frac{1}{2} \int_{V'} \mathbf{D} \cdot \mathbf{E} dv,$$

o When $R \rightarrow \infty$



- V' can be any volume
- Choose its radius $R \rightarrow \infty \rightarrow$ 1st term disappears because of $V_\infty = 0$

$$W_e = \frac{1}{2} \int_{V'} \mathbf{D} \cdot \mathbf{E} dv \quad (\text{J}).$$

Electrostatic Energy Density w_e

$$W_e = \frac{1}{2} \int_{V'} \mathbf{D} \cdot \mathbf{E} dv \quad (\text{J}).$$

 $\mathbf{D} = \epsilon \mathbf{E}$ For a linear medium

$$\cancel{W_e} = \frac{1}{2} \int_{V'} \epsilon E^2 dv \quad (\text{J})$$

$\cancel{\text{J/m}^3}$

$$W_e = \frac{1}{2} \int_{V'} \frac{D^2}{\epsilon} dv \quad (\text{J}).$$

Electrostatic

 $W_e = \int_{V'} w_e dv.$

$$w_e = \frac{1}{2} \mathbf{D} \cdot \mathbf{E} \quad (\text{J/m}^3)$$

$$w_e = \frac{1}{2} \epsilon E^2 \quad (\text{J/m}^3)$$

$$w_e = \frac{D^2}{2\epsilon} \quad (\text{J/m}^3).$$

Definition of density form is artificial.
Volume integral form can be verified.

3-11.2 Electrostatic Forces

- Using Coulomb's law to determine the force on one body that is caused by the charges on other bodies would be very tedious.
- Thus, a simple method of ***principle of virtual displacement*** is introduced.
 - System of bodies with ***fixed charges*** 
 - System of conducting bodies with ***fixed potentials*** 

$$\vec{F} = \hat{a}_{12} \frac{q_1 q_2}{4\pi\epsilon_0 R_{12}^2}$$

System of Bodies with Fixed Charges

- An isolated system consisting of charged conductor and dielectric bodies.
- Condition: Charges are constant.
- Electric force displaces one of the bodies by $d\ell$ (a virtual displacement)

- Mechanical **work** done by the system: $dW = \mathbf{F}_Q \cdot d\ell$, \mathbf{F}_Q : total electric force acting on the body
- In other words, **reduced stored electrostatic energy** produces the mechanical **work**

$$dW + dW_e = 0 \rightarrow dW = -dW_e = \mathbf{F}_Q \cdot d\ell.$$

$$dW_e = (\nabla W_e) \cdot d\ell$$

$$\mathbf{F}_Q = -\nabla W_e \quad (\text{N}).$$

A very simple formula for the calculation of \mathbf{F}_Q from the **electrostatic energy** of the system

- Electric torque rotates one of the bodies by $d\phi$ (a virtual rotation) about an axis (e.g., z axis)
 - Work done by the system:

$$dW = (T_Q)_z d\phi$$



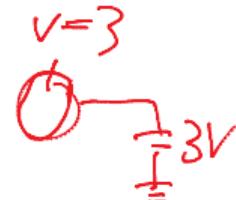
.



$$(T_Q)_z = -\frac{\partial W_e}{\partial \phi} \quad (\text{N}\cdot\text{m}).$$

System of Conducting Bodies with Fixed Potentials

- Condition: potentials are fixed. ✓ const.
- System connected to external sources to maintain fixed potentials
- A displacement $d\ell \rightarrow dW_e, dQ_k$ to maintain fixed potentials V_k



- 1. Work done by **the external sources**: $dW_s = \sum_k V_k dQ_k$

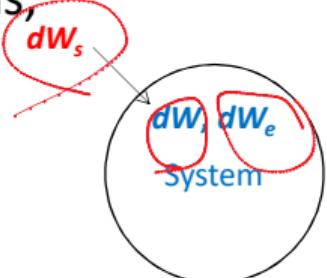
dQ_k : Due to charge transfer between external sources and the system

- 2. Produced mechanical **work**: $dW = \underline{\mathbf{F}_v \cdot d\ell}$

\mathbf{F}_v : Electric force acting on the body

- 3. Change of **electrostatic energy** due to dQ_k : $dW_e = \frac{1}{2} \sum_k V_k dQ_k = \frac{1}{2} dW_s$

- Thus,



$$dW + dW_e = dW_s.$$



$$dW = dW_e$$



$$\begin{aligned} \mathbf{F}_V \cdot d\ell &= dW_e \\ &= (\nabla W_e) \cdot d\ell \end{aligned}$$



$\mathbf{F}_V = \nabla W_e \quad (\text{N}).$

$F_V = -\nabla W_e$

↑
Fixed charges

Fixed potential

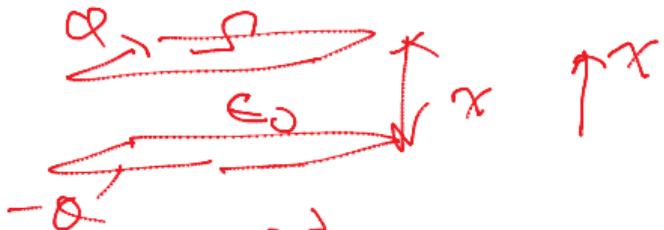
- Similarly, a displacement $d\phi \rightarrow dW_e, dQ_k$



$$(T_V)_z = \frac{\partial W_e}{\partial \phi} \quad (\text{N}\cdot\text{m}),$$

The difference in formulas for fixed potentials and for fixed charges is only a sign change.

EXAMPLE 3-26 Determine the force on the conducting plates of a charged parallel-plate capacitor. The plates have an area S and are separated in air by a distance x .



$$C = \frac{\epsilon_0 S}{x} = \frac{Q}{V} \Rightarrow Q = \frac{V\epsilon_0 S}{x} \quad (2)$$

$$1^{\circ} \vec{F}_Q = -\nabla W_e$$

Q is fixed \Rightarrow express W_e in terms of Q

$$E_x = \frac{V}{x}$$

$$W_e = \frac{1}{2} QV = \frac{1}{2} QE_x X$$

$$\vec{F}_Q = -\nabla W_e = -\hat{x} \frac{\partial}{\partial x} \left(\frac{1}{2} QE_x X \right) = -\frac{1}{2} QE_x \hat{a}_x$$

$$2^{\circ} \vec{F}_r = \nabla W_e$$

$$W_e = \frac{1}{2} QV = \frac{1}{2} CV^2 = \frac{\sqrt{\epsilon_0} S}{2x}$$

$$\vec{F}_r = \nabla W_e = \dots = -\frac{V^2 \epsilon_0 S}{2x^2} \hat{a}_x$$

$$E_x = \frac{V}{x} = 0$$