

# **PHYS 161: Homework 5**

Due on Wednesday February 25, 2015

*Professor Landee 11:00am*

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## Problem 1

(6.10) *Rings with opposite currents*

Two parallel rings have the same axis and are separated by a small distance  $\epsilon$ . They have the same radius  $a$ , and they carry the same current  $I$  but in opposite directions. Consider the magnetic field at points on the axis of the rings. The field is zero midway between the rings, because the contributions from the rings cancel. And the field is zero very far away. So it must reach a maximum value at some point in between. Find this point. Work in the approximation where  $\epsilon \ll a$ .

**Solution**

From the equation for field on axis

$$B_z = \frac{\mu_0 I b^2}{2(b^2 + z^2)^{3/2}} \quad (6.53)$$

the field for this set up on the  $z$  axis would be

$$B_z = \frac{\mu_0 I a^2}{2} \left( \frac{1}{(a^2 + (z - \epsilon/2)^2)^{3/2}} - \frac{1}{(a^2 + (z + \epsilon/2)^2)^{3/2}} \right)$$

the first order Taylor expansion is

$$B_z \approx \frac{\mu_0 I a^2}{2} \frac{3z\epsilon}{(a^2 + z^2)^{5/2}}$$

Now let constant  $k = \frac{\mu_0 I a^2}{2}$ ,

$$\frac{B_z}{k} = \frac{3z\epsilon}{(a^2 + z^2)^{5/2}}$$

So take derivative,

$$\frac{d}{dz} \frac{B_z}{k} = \frac{3\epsilon(a^2 - 4z^2)}{(a^2 + z^2)^{7/2}}$$

and let it equals zero. It yields that  $z = a/2$ . Put this result into the equation, the maximum value is:

$$\frac{24\epsilon\mu_0 I}{25\sqrt{5}a^2}$$

## Problem 2

(6.44) *Line integral along the axis*

Consider the magnetic field of a circular current ring, at points on the axis of the ring, given by Eq. (6.53). Calculate explicitly the line integral of the field along the axis from  $-\infty$  to  $\infty$ , to check the general formula

$$\int \mathbf{B} \cdot d\mathbf{s} = \mu_0 I \quad (6.97)$$

Why may we ignore the “return” part of the path which would be necessary to complete a closed loop?

**Solution**

Let us mention the equation

$$B_z = \frac{\mu_0 I b^2}{2(b^2 + z^2)^{3/2}} \quad (6.53)$$

So the integral

$$\int \mathbf{B} \cdot d\mathbf{s} = \int_{-\infty}^{\infty} \frac{\mu_0 I b^2}{2(b^2 + z^2)^{3/2}} dz = \frac{\mu_0 I}{2} \int_{-\infty}^{\infty} \frac{b^2}{(b^2 + z^2)^{3/2}} dz = \frac{\mu_0 I}{2} \frac{z}{\sqrt{b^2 + z^2}} \Big|_{-\infty}^{\infty} = \mu_0 I$$

This integral goes from  $-\infty$  to  $\infty$ , therefore the return part would be infinitesimally small, which could be ignored.

### Problem 3

(6.54) *Force between a wire and a loop*

Figure 6.47 shows a horizontal infinite straight wire with current  $I_1$  pointing into the page, passing a height  $z$  above a square horizontal loop with side length  $l$  and current  $I_2$ ... (problem omitted)

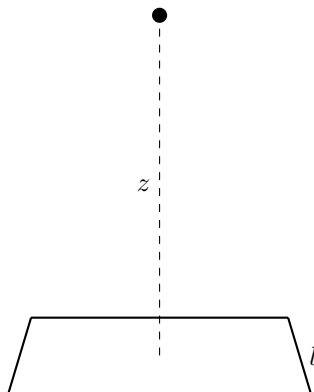
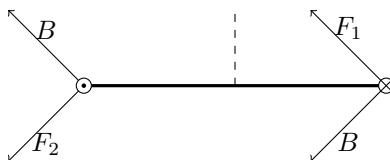


Figure 1: Figure 6.47

#### Solution

From this front view



the net force  $F_1 + F_2$  on the square is indeed to the left. Because the circular magnetic field due to  $I_1$  is

$$B = \frac{\mu_0 I_1}{2\pi R}$$

the force  $F_1$  on the right side is

$$F_1 = I_2 l B = \frac{\mu_0 I_1 I_2 l}{2\pi R}$$

with the angle  $\theta$  to the  $x$  direction, where  $\cos \theta = \frac{l/2}{R}$ . So its  $x$  component is

$$F_{1x} = \frac{\mu_0 I_1 I_2 l}{2\pi R} \frac{l/2}{R} = \frac{\mu_0 I_1 I_2 l^2}{4\pi R^2}$$

and  $F_{2x}$  could be shown as the same. Therefore the net force equals

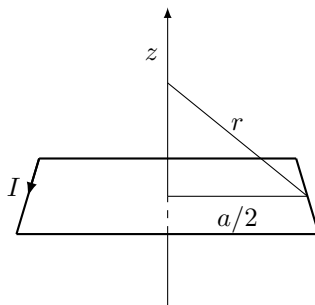
$$F = F_{1x} + F_{2x} = \frac{\mu_0 I_1 I_2 l^2}{2\pi R^2}$$

### Problem 4

The square coil.

Consider a square coil with the length of each side is  $a$ . A current  $I$  is passed through the ring. Calculate the magnetic field on the vertical axis that passes through the center of the square. Compare this field to that of a circular loop with the same current and a diameter  $a$ .

**Solution**



The Biot-Savart law says that

$$\mathbf{B}(\mathbf{r}) = \frac{\mu_0 I}{4\pi} \int \frac{d\mathbf{l} \times \mathbf{r}}{|\mathbf{r}|^3}$$

where  $\mathbf{r}$  is the displacement vector. Now consider the right edge.  $\mathbf{r} = (0 - a/2)\hat{x} + (0 - y)\hat{y} + (z - 0)\hat{z}$ .  $d\mathbf{l} = dy\hat{y}$ . Therefore  $d\mathbf{l} \times \mathbf{r} = (z\hat{x} + \frac{a}{2}\hat{z}) dy$ . So the integral

$$\mathbf{B}_1 = \frac{\mu_0 I}{4\pi} \left( z\hat{x} + \frac{a}{2}\hat{z} \right) \int_{-a/2}^{a/2} \frac{dy}{(\frac{a^2}{4} + y^2 + z^2)^{3/2}} = \frac{\mu_0 I}{4\pi} \left( z\hat{x} + \frac{a}{2}\hat{z} \right) \frac{4a}{\sqrt{\frac{a^2}{2} + z^2} (a^2 + 4z^2)}$$

By symmetry of the configuration, the segment on left would contribute the same  $\hat{z}$  component but opposite  $\hat{x}$  component. By the same reason, the two top and bottom segments will do the same. Therefore the total field would be

$$\mathbf{B} = 4 \times \frac{\mu_0 I}{4\pi} \frac{a}{2} \hat{z} \frac{4a}{\sqrt{\frac{a^2}{2} + z^2} (a^2 + 4z^2)} = \frac{2a^2 \mu_0 I}{\pi \sqrt{\frac{a^2}{2} + z^2} (a^2 + 4z^2)} \hat{z}$$

Comparing to the field on axis for a circular loop which is

$$\mathbf{B}' = \frac{a^2 \mu_0 I}{(a^2 + z^2)^{3/2}} \hat{z}$$

Their ratio

$$\lim_{z \rightarrow \infty} \frac{\mathbf{B}}{\mathbf{B}'} = \lim_{z \rightarrow \infty} \frac{2(a^2 + z^2)^{3/2}}{\pi \sqrt{\frac{a^2}{2} + z^2} (a^2 + 4z^2)} = \frac{1}{2\pi}$$

## Problem 5

(III-8) In the text (pages 82-86) we obtained... (problem omitted)

**Solution**

For the  $r$  coordinate, mark the side on the left going down as 1, and so on.

$$\oint_{C_1} \mathbf{F} \cdot \hat{\mathbf{t}} ds \simeq -F_z \left( r, \theta - \frac{\Delta\theta}{2}, z \right) \Delta z$$

$$\oint_{C_3} \mathbf{F} \cdot \hat{\mathbf{t}} ds \simeq F_z \left( r, \theta + \frac{\Delta\theta}{2}, z \right) \Delta z$$

And the area enclosed is  $r\Delta\theta\Delta z$ . So

$$\frac{1}{\Delta S} \int_{C_1+C_3} \mathbf{F} \cdot \hat{\mathbf{t}} ds = \frac{1}{r\Delta\theta} \left[ F_z \left( r, \theta + \frac{\Delta\theta}{2}, z \right) - F_z \left( r, \theta - \frac{\Delta\theta}{2}, z \right) \right]$$

Take the limit to  $\Delta\theta \rightarrow 0$ , this becomes

$$\frac{1}{r} \frac{\partial F_z}{\partial \theta}$$

Then

$$\begin{aligned} \oint_{C_2} \mathbf{F} \cdot \hat{\mathbf{t}} ds &\simeq F_\theta \left( r, \theta, z - \frac{\Delta z}{2} \right) r \Delta\theta \\ \oint_{C_4} \mathbf{F} \cdot \hat{\mathbf{t}} ds &\simeq -F_\theta \left( r, \theta, z + \frac{\Delta z}{2} \right) r \Delta\theta \end{aligned}$$

so

$$\frac{1}{\Delta S} \int_{C_2+C_4} \mathbf{F} \cdot \hat{\mathbf{t}} ds = -\frac{1}{\Delta z} \left[ F_\theta \left( r, \theta, z + \frac{\Delta z}{2} \right) - F_\theta \left( r, \theta, z - \frac{\Delta z}{2} \right) \right]$$

Take the limit to  $\Delta z \rightarrow 0$ , this becomes

$$-\frac{\partial F_\theta}{\partial z}$$

Therefore we could conclude

$$(\nabla \times \mathbf{F})_r = \frac{1}{r} \frac{\partial F_z}{\partial \theta} - \frac{\partial F_\theta}{\partial z}$$

Similarly for the  $\theta$  coordinate, mark the side closest to  $z$  axis going up as 1, and so on.

$$\begin{aligned} \oint_{C_1} \mathbf{F} \cdot \hat{\mathbf{t}} ds &\simeq F_z \left( r - \frac{\Delta r}{2}, \theta, z \right) \Delta z \\ \oint_{C_3} \mathbf{F} \cdot \hat{\mathbf{t}} ds &\simeq -F_z \left( r + \frac{\Delta r}{2}, \theta, z \right) \Delta z \end{aligned}$$

And the area enclosed is  $\Delta r \Delta z$ . So

$$\frac{1}{\Delta S} \int_{C_1+C_3} \mathbf{F} \cdot \hat{\mathbf{t}} ds = -\frac{1}{\Delta r} \left[ F_z \left( r + \frac{\Delta r}{2}, \theta, z \right) - F_z \left( r - \frac{\Delta r}{2}, \theta, z \right) \right]$$

Take the limit to  $\Delta r \rightarrow 0$ , this becomes

$$-\frac{\partial F_z}{\partial r}$$

Then

$$\begin{aligned} \oint_{C_2} \mathbf{F} \cdot \hat{\mathbf{t}} ds &\simeq F_r \left( r, \theta, z + \frac{\Delta z}{2} \right) \Delta r \\ \oint_{C_4} \mathbf{F} \cdot \hat{\mathbf{t}} ds &\simeq -F_r \left( r, \theta, z - \frac{\Delta z}{2} \right) \Delta r \end{aligned}$$

so

$$\frac{1}{\Delta S} \int_{C_2+C_4} \mathbf{F} \cdot \hat{\mathbf{t}} ds = \frac{1}{\Delta z} \left[ F_r \left( r, \theta, z + \frac{\Delta z}{2} \right) - F_r \left( r, \theta, z - \frac{\Delta z}{2} \right) \right]$$

Take the limit to  $\Delta z \rightarrow 0$ , this becomes

$$\frac{\partial F_r}{\partial z}$$

Therefore we could conclude

$$(\nabla \times \mathbf{F})_\theta = \frac{\partial F_r}{\partial z} - \frac{\partial F_z}{\partial r}$$

## Problem 6

(III-9) Following the procedure... (problem omitted)

### Solution

For the  $r$  coordinate,

$$\oint_{C_1} \mathbf{F} \cdot \hat{\mathbf{t}} ds \simeq F_\phi \left( r, \phi, \theta - \frac{\Delta\theta}{2} \right) r \Delta\phi$$

$$\oint_{C_3} \mathbf{F} \cdot \hat{\mathbf{t}} ds \simeq -F_\phi \left( r, \phi, \theta + \frac{\Delta\theta}{2} \right) r \Delta\phi$$

And the area enclosed is  $r^2 \Delta\theta \Delta\phi \sin \phi$ . So

$$\frac{1}{\Delta S} \int_{C_1+C_3} \mathbf{F} \cdot \hat{\mathbf{t}} ds = -\frac{1}{r \Delta\theta \sin \phi} \left[ F_\phi \left( r, \phi, \theta + \frac{\Delta\theta}{2} \right) - F_\phi \left( r, \phi, \theta - \frac{\Delta\theta}{2} \right) \right]$$

Take the limit to  $\Delta\theta \rightarrow 0$ , this becomes

$$-\frac{1}{r \sin \phi} \frac{\partial F_\phi}{\partial \theta}$$

Then

$$\oint_{C_2} \mathbf{F} \cdot \hat{\mathbf{t}} ds \simeq -F_\theta \left( r, \phi - \frac{\Delta\phi}{2}, \theta \right) r \sin \left( \phi - \frac{\Delta\phi}{2} \right) \Delta\pi$$

$$\oint_{C_4} \mathbf{F} \cdot \hat{\mathbf{t}} ds \simeq F_\theta \left( r, \phi + \frac{\Delta\phi}{2}, \theta \right) r \sin \left( \phi + \frac{\Delta\phi}{2} \right) \Delta\phi$$

so

$$\frac{1}{\Delta S} \int_{C_2+C_4} \mathbf{F} \cdot \hat{\mathbf{t}} ds = \frac{1}{r \Delta\theta \sin \phi} \left[ F_\theta \left( r, \phi + \frac{\Delta\phi}{2}, \theta \right) \sin \left( \phi + \frac{\Delta\phi}{2} \right) - F_\theta \left( r, \phi - \frac{\Delta\phi}{2}, \theta \right) \sin \left( \phi - \frac{\Delta\phi}{2} \right) \right]$$

Take the limit to  $\Delta\theta \rightarrow 0$ , this becomes

$$\frac{1}{r \sin \phi} \frac{\partial}{\partial \phi} (\sin \phi F_\theta)$$

Therefore we could conclude

$$(\nabla \times \mathbf{F})_r = \frac{1}{r \sin \phi} \frac{\partial}{\partial \phi} (\sin \phi F_\theta) - \frac{1}{r \sin \phi} \frac{\partial F_\phi}{\partial \theta}$$

For the  $\phi$  coordinate, enclosed area is  $r \Delta r \Delta\theta \sin \phi$

$$\oint_{C_1} \mathbf{F} \cdot \hat{\mathbf{t}} ds \simeq -F_\theta \left( r + \frac{\Delta r}{2}, \phi, \theta \right) \left( r + \frac{\Delta r}{2} \right) \Delta\theta \sin \phi$$

$$\oint_{C_2} \mathbf{F} \cdot \hat{\mathbf{t}} ds \simeq -F_r \left( r, \phi, \theta - \frac{\Delta\theta}{2} \right) \Delta r$$

$$\oint_{C_3} \mathbf{F} \cdot \hat{\mathbf{t}} ds \simeq F_\theta \left( r - \frac{\Delta r}{2}, \phi, \theta \right) \left( r - \frac{\Delta r}{2} \right) \Delta\theta \sin \phi$$

$$\oint_{C_4} \mathbf{F} \cdot \hat{\mathbf{t}} ds \simeq F_r \left( r, \phi, \theta + \frac{\Delta\theta}{2} \right) \Delta r$$

so

$$\frac{1}{\Delta S} \int_{C_1+C_3} \mathbf{F} \cdot \hat{\mathbf{t}} ds = -\frac{1}{r \Delta r} \left[ F_\theta \left( r + \frac{\Delta r}{2}, \phi, \theta \right) \left( r + \frac{\Delta r}{2} \right) - F_\theta \left( r - \frac{\Delta r}{2}, \phi, \theta \right) \left( r - \frac{\Delta r}{2} \right) \right]$$

$$\frac{1}{\Delta S} \int_{C_2+C_4} \mathbf{F} \cdot \hat{\mathbf{t}} ds = \frac{1}{r \Delta\theta \sin \phi} \left[ F_r \left( r, \phi, \theta + \frac{\Delta\theta}{2} \right) - F_r \left( r, \phi, \theta - \frac{\Delta\theta}{2} \right) \right]$$

Take the limits, we could conclude

$$(\nabla \times \mathbf{F})_\phi = \frac{1}{r \sin \phi} \frac{\partial F_r}{\partial \theta} - \frac{1}{r} \frac{\partial}{\partial \theta} (r F_\theta)$$

For the  $\theta$  coordinate, enclosed area is  $r \Delta r \Delta \phi$

$$\begin{aligned} \oint_{C_1} \mathbf{F} \cdot \hat{\mathbf{t}} ds &\simeq F_\phi \left( r + \frac{\Delta r}{2}, \phi, \theta \right) \left( r + \frac{\Delta r}{2} \right) \Delta \phi \\ \oint_{C_2} \mathbf{F} \cdot \hat{\mathbf{t}} ds &\simeq -F_r \left( r, \phi - \frac{\Delta \phi}{2}, \theta \right) \Delta r \\ \oint_{C_3} \mathbf{F} \cdot \hat{\mathbf{t}} ds &\simeq -F_\phi \left( r - \frac{\Delta r}{2}, \phi, \theta \right) \left( r - \frac{\Delta r}{2} \right) \Delta \phi \\ \oint_{C_4} \mathbf{F} \cdot \hat{\mathbf{t}} ds &\simeq F_r \left( r, \phi + \frac{\Delta \phi}{2}, \theta \right) \Delta r \end{aligned}$$

so

$$\begin{aligned} \frac{1}{\Delta S} \int_{C_1+C_3} \mathbf{F} \cdot \hat{\mathbf{t}} ds &= \frac{1}{r \Delta r} \left[ F_\phi \left( r + \frac{\Delta r}{2}, \phi, \theta \right) \left( r + \frac{\Delta r}{2} \right) - F_\phi \left( r - \frac{\Delta r}{2}, \phi, \theta \right) \left( r - \frac{\Delta r}{2} \right) \right] \\ \frac{1}{\Delta S} \int_{C_2+C_4} \mathbf{F} \cdot \hat{\mathbf{t}} ds &= -\frac{1}{r \Delta \phi} \left[ F_r \left( r, \phi + \frac{\Delta \phi}{2}, \theta \right) - F_r \left( r, \phi - \frac{\Delta \phi}{2}, \theta \right) \right] \end{aligned}$$

Take the limits, we could conclude

$$(\nabla \times \mathbf{F})_\theta = \frac{1}{r} \frac{\partial}{\partial r} (r F_\phi) - \frac{1}{r} \frac{\partial F_r}{\partial \phi}$$

## Problem 7

(III-15) Verify Stokes' theorem

$$\oint_C \mathbf{F} \cdot \hat{\mathbf{t}} ds = \iint_S \hat{\mathbf{n}} \cdot \nabla \times \mathbf{F} dS$$

in each of the following cases... (problem omitted)

**Solution**

(a)

$$\nabla \times \mathbf{F} = \begin{vmatrix} i & j & k \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ F_x & F_y & F_z \end{vmatrix} = 2z \hat{\mathbf{j}}$$

Therefore, at  $y = 0$

$$\iint_S \hat{\mathbf{n}} \cdot \nabla \times \mathbf{F} dS = \int_0^1 \int_0^1 \hat{\mathbf{j}} \cdot 2z \hat{\mathbf{j}} dx dz = \int_0^1 \int_0^1 2z dx dz = 1$$

And

$$\begin{aligned} \oint_C \mathbf{F} \cdot \hat{\mathbf{t}} ds &= \int_0^1 \mathbf{F}(x, y, z=1) \cdot \hat{\mathbf{i}} dx - \int_0^1 \mathbf{F}(x=1, y, z) \cdot \hat{\mathbf{k}} dz \\ &\quad - \int_0^1 \mathbf{F}(x, y, z=0) \cdot \hat{\mathbf{i}} dx + \int_0^1 \mathbf{F}(x=0, y, z) \cdot \hat{\mathbf{k}} dz \\ &= 1 - 0 - 0 + 0 = 1 \end{aligned}$$

As shown, Stokes' theorem holds in this case.

(b)

$$\oint_C \mathbf{F} \cdot \hat{\mathbf{t}} ds = \int_{C_1} \mathbf{F} \cdot \hat{\mathbf{t}} ds + \int_{C_2} \mathbf{F} \cdot \hat{\mathbf{t}} ds + \int_{C_3} \mathbf{F} \cdot \hat{\mathbf{t}} ds$$

Parametrize the paths.

For  $C_1$ ,  $r = 1$ ,  $\theta = \pi/2$ , so  $\hat{\mathbf{r}}(\phi) = (\cos \phi, \sin \phi, 0)$ , where  $0 \leq \phi \leq \pi/2$ . And  $\mathbf{f}(\phi) = (\sin \phi, 0, \cos \phi)$ . The integral becomes

$$\int_{C_1} \mathbf{F} \cdot \hat{\mathbf{t}} ds = \int_0^{\pi/2} \mathbf{f} \cdot \hat{\mathbf{r}}' d\phi = \int_0^{\pi/2} -\sin^2 \phi d\phi = -\frac{\pi}{4}$$

For  $C_2$ ,  $r = 1$ ,  $\phi = \pi/2$ , so  $\hat{\mathbf{r}}(\theta) = (0, \cos \theta, \sin \theta)$ , where  $0 \leq \theta \leq \pi/2$ . And  $\mathbf{f}(\theta) = (\cos \theta, \sin \theta, 0)$ . The integral becomes

$$\int_{C_2} \mathbf{F} \cdot \hat{\mathbf{t}} ds = \int_0^{\pi/2} \mathbf{f} \cdot \hat{\mathbf{r}}' d\theta = \int_0^{\pi/2} -\sin^2 \theta d\theta = -\frac{\pi}{4}$$

For  $C_3$ ,  $r = 1$ ,  $\phi = 0$ , so  $\hat{\mathbf{r}}(\theta) = (\cos \theta, 0, \sin \theta)$ , where  $0 \leq \theta \leq \pi/2$ . And  $\mathbf{f}(\theta) = (0, \sin \theta, \cos \theta)$ . The integral becomes

$$\int_{C_3} \mathbf{F} \cdot \hat{\mathbf{t}} ds = \int_0^{\pi/2} \mathbf{f} \cdot \hat{\mathbf{r}}' d\theta = \int_0^{\pi/2} -\cos^2 \theta d\theta = -\frac{\pi}{4}$$

So adding these up,

$$\oint_C \mathbf{F} \cdot \hat{\mathbf{t}} ds = -\frac{3\pi}{4}$$

$\nabla \times \mathbf{F} = (-1, -1, -1)$ . Change into spherical coordinates,  $\nabla \times \mathbf{F} = (\sqrt{3}, \pi - \tan^{-1}(\sqrt{2}), -\frac{3\pi}{4})$ . The normal vector  $\hat{\mathbf{n}} = x\hat{\mathbf{i}} + y\hat{\mathbf{j}} + z\hat{\mathbf{k}}$ , therefore  $\hat{\mathbf{n}} \cdot \nabla \times \mathbf{F} = -x - y - z$ . So when  $r = 1$

$$\begin{aligned} \iint_S \hat{\mathbf{n}} \cdot \nabla \times \mathbf{F} dS &= \iint_S (-x - y - z) dS \\ &= - \int_0^{\pi/2} \int_0^{\pi/2} (x + y + z) r^2 \sin \theta d\phi d\theta \\ &= - \int_0^{\pi/2} \int_0^{\pi/2} (\sin \phi \sin \theta + \cos \phi \sin \theta + \cos \theta) \sin \theta d\phi d\theta \\ &= -\frac{3\pi}{4} \end{aligned}$$

Stokes' theorem holds in this case.

(c)  $\nabla \times \mathbf{F} = (0, 0, -2)$ , so in cylindrical coordinates

$$\begin{aligned} \iint_S \hat{\mathbf{n}} \cdot \nabla \times \mathbf{F} dS &= \iint_S \hat{\mathbf{n}} \cdot (0, 0, -2) dS \\ &= \iint_{S_1} \hat{\rho} \cdot \nabla \times \mathbf{F} dS + \iint_{S_2} \hat{\mathbf{z}} \cdot \nabla \times \mathbf{F} dS \\ &= 0 + \int_0^R \int_0^{2\pi} -2\rho d\phi d\rho \\ &= -2\pi R^2 \end{aligned}$$

And then for the line integral, parametrize the path  $\hat{\mathbf{r}}(\phi) = (R \cos \phi, R \sin \phi, 0)$ . And  $\mathbf{f} = (R \sin \phi, -R \cos \phi, 0)$ . So

$$\int_C \mathbf{F} \cdot \hat{\mathbf{t}} ds = \int_0^{2\pi} \mathbf{f} \cdot \hat{\mathbf{r}}' d\phi = \int_0^{2\pi} -R^2 d\phi = -2\pi R^2$$

Verified.



## Problem 8

(III-16) (a) Consider a vector function with the property  $\nabla \times \mathbf{F} = 0$ ... (problem omitted)

**Solution**

(a) Use Stokes' theorem. Because

$$\oint_C \mathbf{F} \cdot \hat{\mathbf{t}} ds = \iint_S \hat{\mathbf{n}} \cdot \nabla \times \mathbf{F} dS = 0$$

on this donut shape, the upper and lower halves could be seen as having circulation of opposite directions, while  $C_1$  or  $C_2$  belongs to one of them.

$$\oint_{C_1} \mathbf{F} \cdot \hat{\mathbf{t}} ds - \oint_{C_2} \mathbf{F} \cdot \hat{\mathbf{t}} ds = 0$$

So

$$\oint_{C_1} \mathbf{F} \cdot \hat{\mathbf{t}} ds = \oint_{C_2} \mathbf{F} \cdot \hat{\mathbf{t}} ds$$

(b) When assuming  $r > 0$ , the curl

$$\nabla \times \mathbf{B} = \nabla \times \left( 0, \frac{\mu_0 I}{2\pi r}, 0 \right) = \left( 0, 0, \frac{\mu_0 I}{2\pi r^2} - \frac{\mu_0 I}{2\pi r^2} \right) = (0, 0, 0)$$

When  $r = 0$ , the calculation becomes indeterminate.

(c) Let

$$a = \oint_C \mathbf{B} \cdot d\mathbf{l}$$

a small element of this is

$$da = \mathbf{B} \cdot d\mathbf{r} = B \cos \theta dr$$

When considering a circular loop centered at  $z$  axis,  $\theta = 0$ ,

$$B \cos \theta dr = B dr = \frac{\mu_0 I}{2\pi r} dr$$

So

$$\oint_C \mathbf{B} \cdot d\mathbf{l} = a = 2\pi r \frac{\mu_0 I}{2\pi r} = \mu_0 I$$

which is the Ampère's circuital law.

## Problem 9

(III-19) Determine the value of the line integral  $\int_C \mathbf{F} \cdot \hat{\mathbf{t}} ds$  where

$$\mathbf{F} = (e^{-y} - ze^{-x})\hat{\mathbf{i}} + (e^{-z} - xe^{-y})\hat{\mathbf{j}} + (e^{-x} - ye^{-z})\hat{\mathbf{k}}$$

and  $C$  is the path... (problem omitted)

**Solution**

Firstly, calculated  $\nabla \times \mathbf{F} = 0$ . As shown in problem 8, for a field of zero curl, two closed curves enclosing one capping surface would have the same circulation. So the path  $C$  could be converted to  $(0, 0, 0)$ ,  $(1, 0, 0)$ ,  $(1, 1, 0)$ , and  $(1, 1, 1)$ , and still gives the same result. Therefore at  $y = z = 0$

$$\int_0^1 (e^{-y} - ze^{-x}) dx = 1$$

At  $x = 1, z = 0$

$$\int_0^1 (e^{-z} - xe^{-y}) dy = \frac{1}{e}$$

At  $x = y = 1,$

$$\int_0^1 (e^{-x} - ye^{-z}) dz = -1 + \frac{2}{e}$$

So the line integral is the sum of these three results,  $3/e$ .

## Problem 10

(III-22) (a) Apply the divergence theorem to the function

$$\mathbf{G}(x, y) = \mathbf{i}G_x(x, y) + \mathbf{j}G_y(x, y)$$

... (problem omitted)

### Solution

(a) There is no  $z$  component, so

$$\nabla \cdot \mathbf{G} = \frac{\partial G_x}{\partial x} + \frac{\partial G_y}{\partial y}$$

Therefore

$$\iiint_V \nabla \cdot \mathbf{G} dV = \iiint_V \left( \frac{\partial G_x}{\partial x} + \frac{\partial G_y}{\partial y} \right) dV = h \iint_R \left( \frac{\partial G_x}{\partial x} + \frac{\partial G_y}{\partial y} \right) dx dy$$

On the other hand, the top and bottom has no contribution to the surface integral. The surface integral does not change through the  $h$ , so

$$\begin{aligned} \iint_S \mathbf{G} \cdot \hat{\mathbf{n}} dS &= h \oint_C \mathbf{G} \cdot \hat{\mathbf{n}} dx dy \\ &= h \oint_C \left( \frac{\partial G}{\partial x} - \frac{\partial G}{\partial y} \right) dx dy \\ &= h \oint_C \left( \frac{G_x}{dx} - \frac{G_y}{dy} \right) dx dy \\ &= h \oint_C (G_x dy - G_y dx) \end{aligned}$$

So

$$\iint_R \left( \frac{\partial G_x}{\partial x} + \frac{\partial G_y}{\partial y} \right) dx dy = \oint_C (G_x dy - G_y dx)$$

(b)

$$\nabla \times \mathbf{F} = \frac{\partial F_y}{\partial x} - \frac{\partial F_x}{\partial y}$$

So

$$\iint_R \nabla \times \mathbf{F} \cdot d\mathbf{S} = \iint_R \left( \frac{\partial F_y}{\partial x} - \frac{\partial F_x}{\partial y} \right) dx dy$$

And

$$\oint_C \mathbf{F} \cdot d\mathbf{r} = \oint_C (F_x dx + F_y dy)$$

So

$$\oint_C (F_x dx + F_y dy) = \iint_R \left( \frac{\partial F_y}{\partial x} - \frac{\partial F_x}{\partial y} \right) dx dy$$

(c) With the result from the two problems above, just let  $G_x = F_y$ , and  $G_y = -F_x$ .