

**EEC 134 A&B**

# **Design of RF & Microwave Systems**

## **Lecture 4: Building Blocks of RF Systems – Oscillators and Synthesizers**

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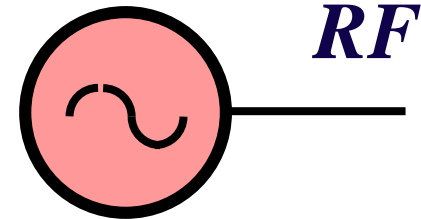
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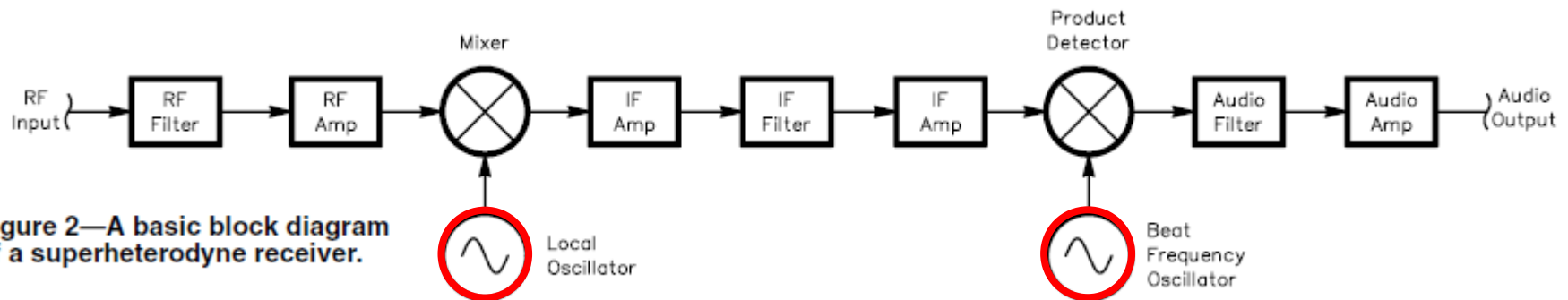
# RF Oscillator

## ❖ Oscillator

- RF signal source
- Converts dc energy into RF



## ❖ Oscillator in an RF system



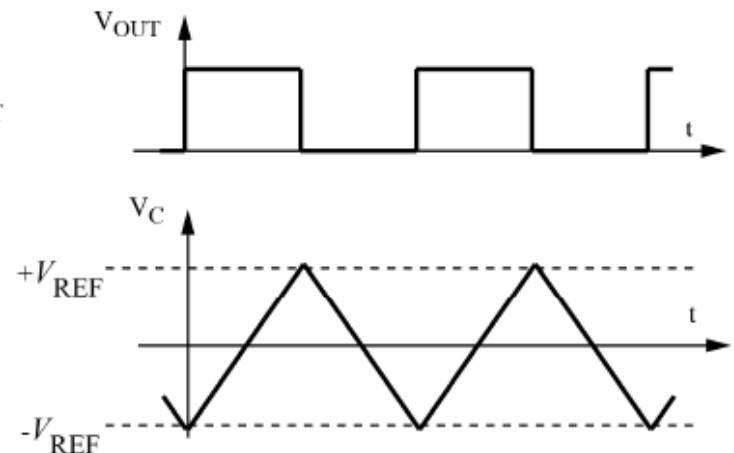
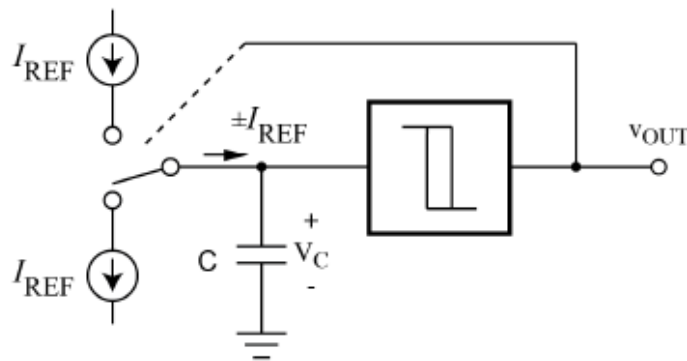
# Types of Oscillator Design

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- ❖ Multi-vibrator
- ❖ Ring
- ❖ Feedback
- ❖ Negative Resistance

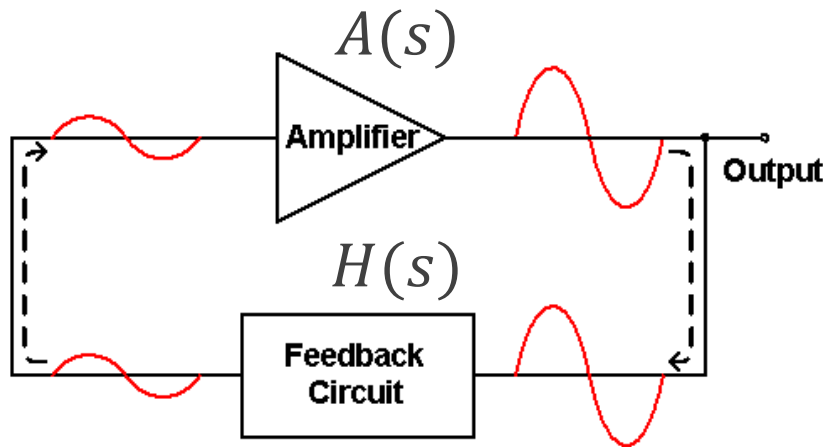
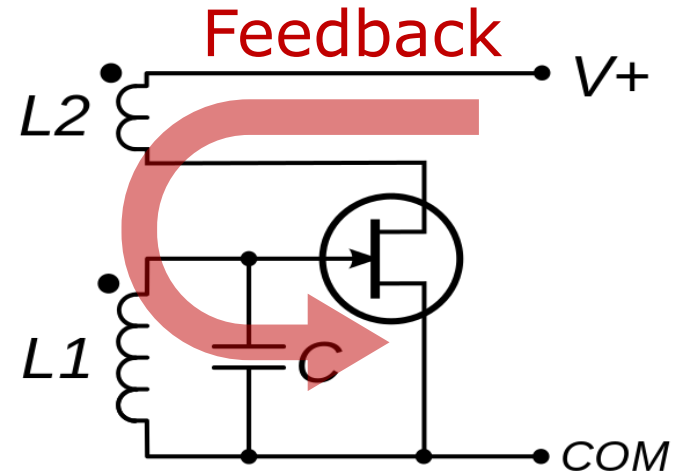
# Multi-vibrator Oscillator

- ❖ One or more current sources charge and discharge an energy storage element whose voltages flips a comparator (usually with hysteresis) to disconnect or connect the current source(s)
- ❖ Also called astable or relaxation oscillator
- ❖ Amplitude is controlled by the thresholds
- ❖ Start-up is guaranteed (will always oscillate)
- ❖ Usually used for low frequency (up to a few MHz)



# Feedback Oscillator

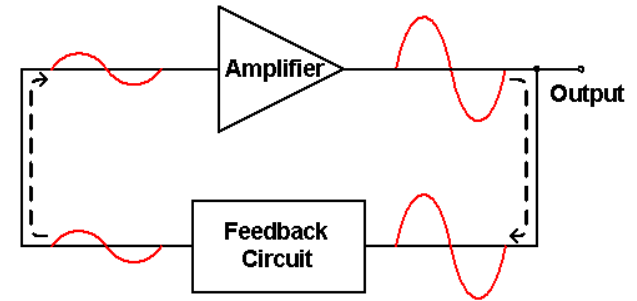
- ❖ While in college, Edwin H. Armstrong observed high frequency oscillation if the output signal of a vacuum tube amplifier is fed back to its input; thus inventing an oscillator which could be used to generate strong signals for radio transmitters
- ❖ Oscillation can be created by introducing positive feedback



$$\frac{S_o}{S_i}(s) = \frac{A(s)}{1 - A(s)H(s)}$$

# Barkhausen Criteria

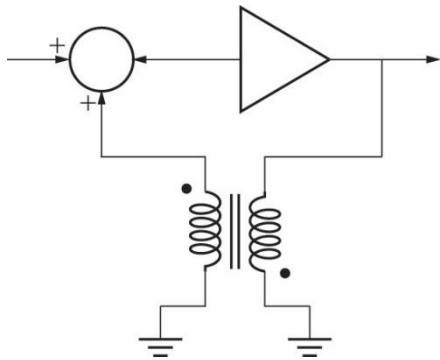
- ❖ It states that if  $A(s)$  is the gain of the amplifying element in the circuit and  $H(s)$  is the transfer function of the feedback path, so  $HA$  is the loop gain around the feedback loop of the circuit, the circuit will sustain steady-state oscillations only at frequencies for which:
  - The loop gain is equal to unity in absolute magnitude, that is,  $\beta A = 1$ , and
  - The phase shift around the loop is zero or an integer multiple of  $2\pi$ :  $\angle HA = 2n\pi, n = 0, 1, 2, \dots$
- ❖ In an actual oscillator, the  $HA$  product will **initially exceed 1** to start the oscillation; As the oscillation grows, the gain compresses to reach the  $HA = 1$  steady state.



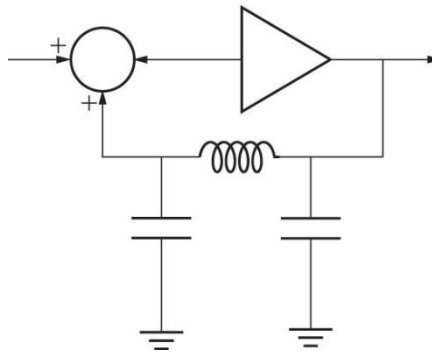
$$\frac{S_o}{S_i}(s) = \frac{A(s)}{1 - A(s)H(s)}$$

# Realization of the Feedback Oscillator

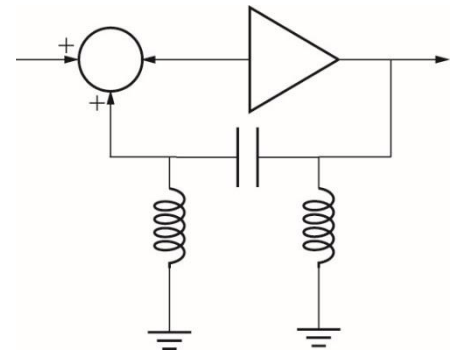
- ❖ A frequency selective network is usually used as the feedback network
- ❖ Most oscillator designs are based on a few classic structures (templates)



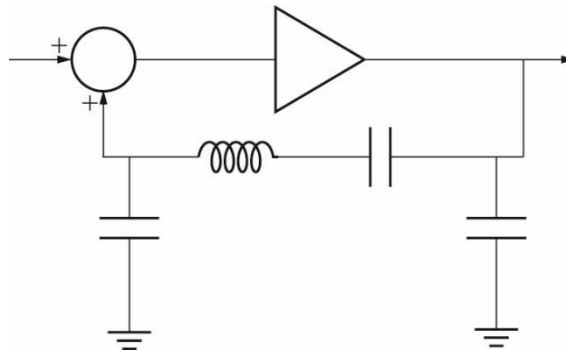
Armstrong oscillator



Colpitts Oscillator



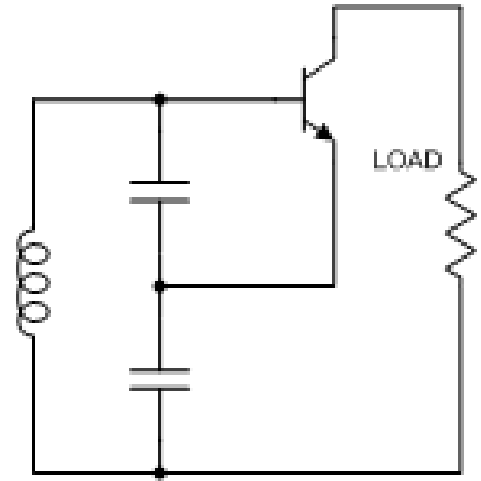
Hartley Oscillator



Clapp Oscillator

# Frequency Selective Network

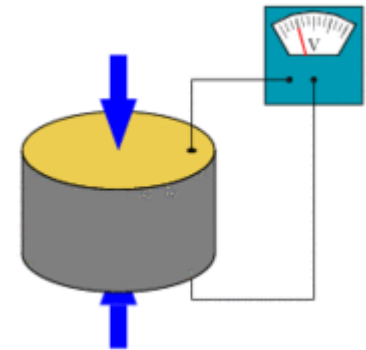
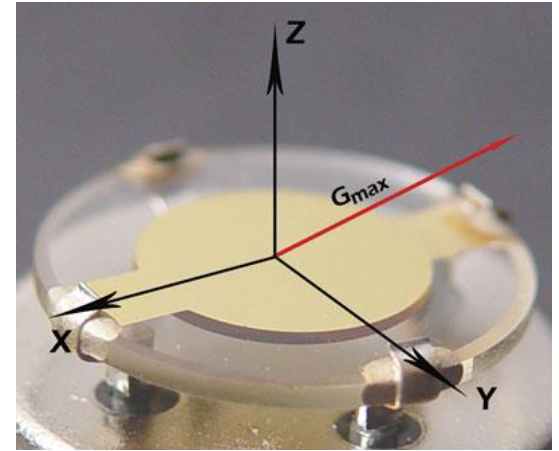
- ❖ The frequency selective (feedback) network is usually a bandpass network whose center frequency set the correct frequency
- ❖ In general, the higher the  $Q$  of the frequency selective network, the more stable the oscillation is.
- ❖ The frequency selective network can be made of a variety of resonator structures
  - Simple L-C resonator ( $Q$  of 5 ~ 100)
  - Transmission line resonator ( $Q$  of 30 ~ 250)
  - Waveguide/Cavity resonator ( $Q$  of 300 ~ 5000)
  - Dielectric resonator ( $Q$  of 3000 ~ 6000)
  - Crystal resonator ( $Q$  of 10,000 ~ 200,000!)





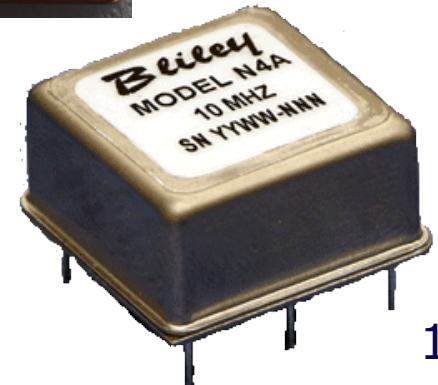
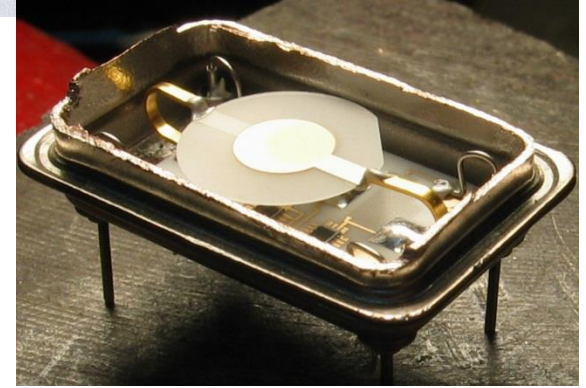
# Crystal Oscillators

- ❖ The “crystal” is a piece of well shaped single crystal piezoelectric material (most commonly quartz) sandwiched between two metal electrodes.
- ❖ The piezoelectric effect is a property that some materials exhibit: external applied mechanical stress can induce a voltage potential and vice versa.
- ❖ Quartz is a natural piezoelectric material.
- ❖ The piezoelectric effect serves as a transduction mechanism, converting electric signals into mechanical vibration and back to electric signal again
- ❖ The transduction is the strongest when the crystal oscillates at its natural frequency which is determined by the shape of the crystal



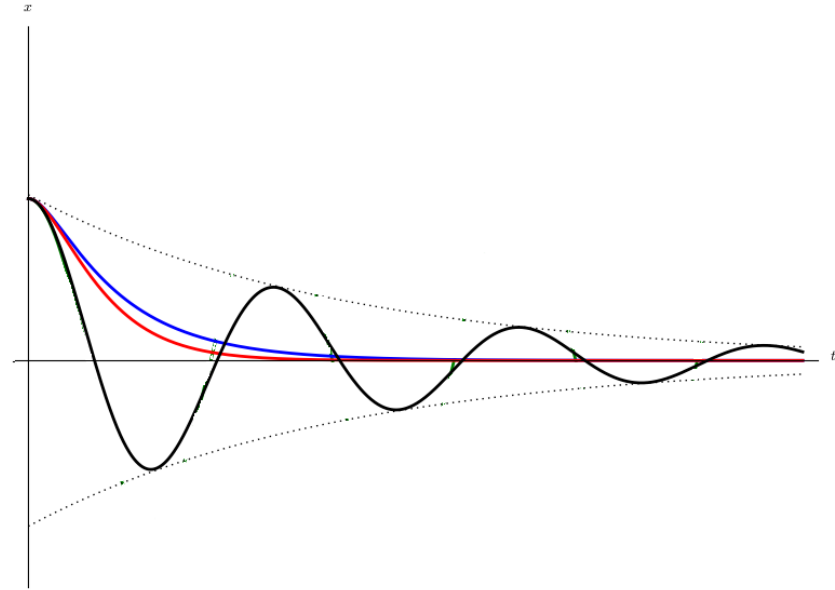
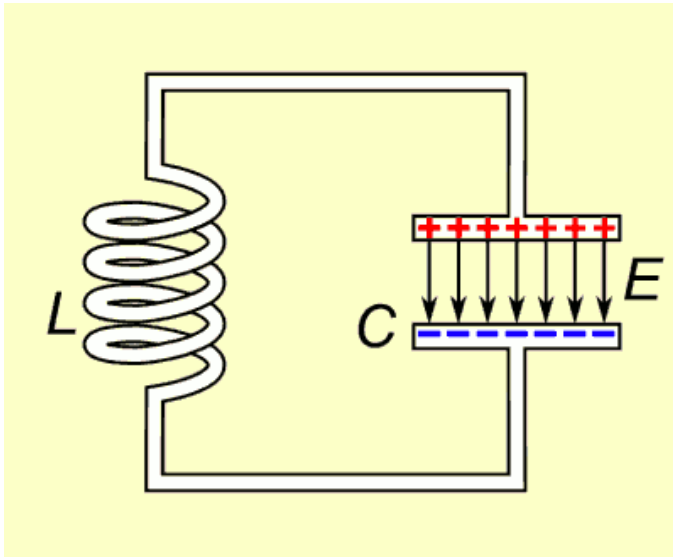
# Crystal Oscillators (cont.)

- ❖ Because of the extremely high  $Q$ , crystal oscillators are often used as very stable frequency sources.
- ❖ The frequency of crystal oscillators are in the range of  $\sim 10$  kHz to  $\sim 100$  MHz.
  - The frequency is primarily determined by the size and shape of the crystal. The lower frequency is usually bound by the crystal size; the higher end bound by the precision of machining the crystal.
- ❖ The frequency of a crystal oscillator (XO) is temperature dependent, which is an undesirable effect.
  - *Temperature compensated crystal oscillator (TCXO)* are designed carefully to reduce the temperature dependence
  - *Oven controlled crystal oscillator (OCXO)* uses active temperature control to maintain a stable temperature around the crystal for the best stability. Downside is that it burns power and needs start-up (warm-up) time.



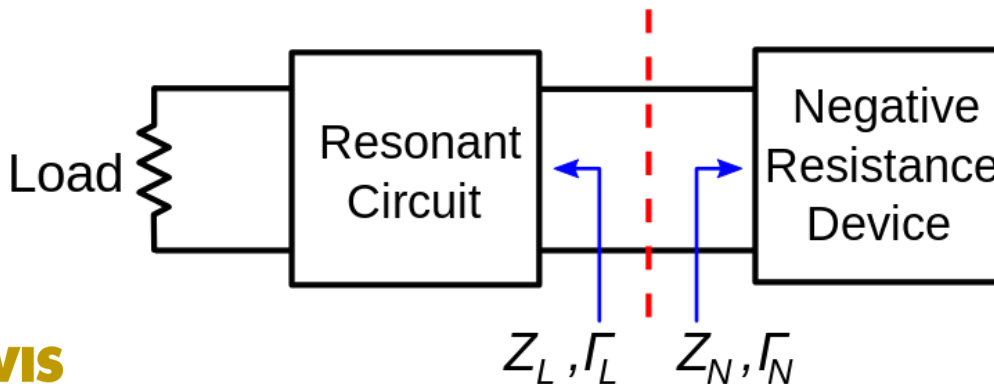
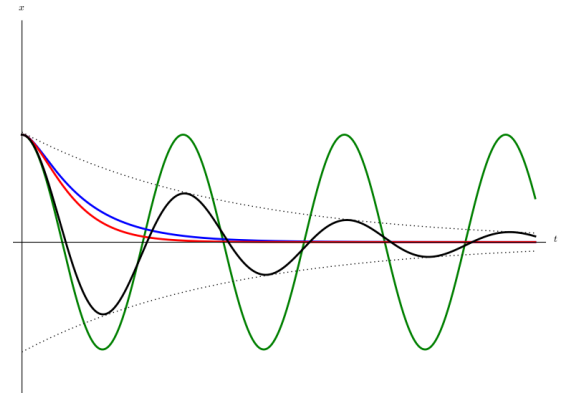
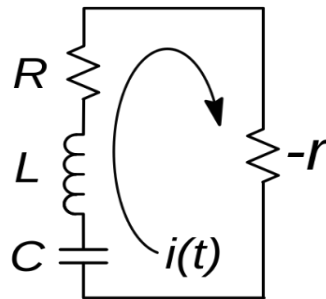
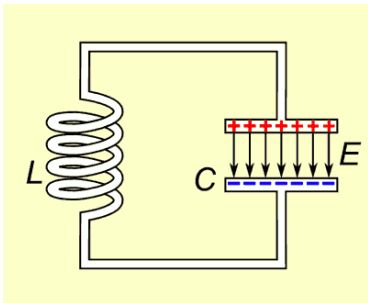
# Another Oscillator Design Perspective

- ❖ Let's look at oscillation of voltage/current in a resonant circuit
- ❖ The quality factor ( $Q$ ) determines the damping (loss) of the system
  - The higher the  $Q$ , the lower the damping, the longer the oscillation lasts
  - In all practical systems, the oscillation eventually dies down



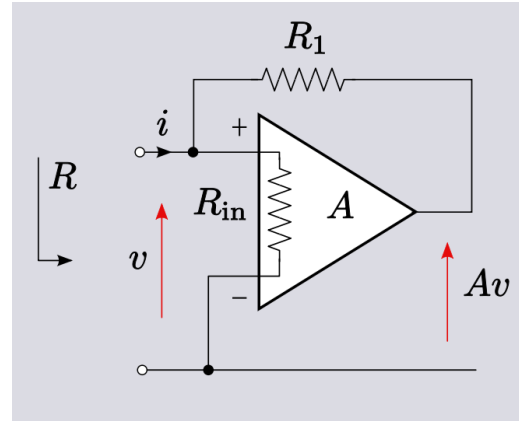
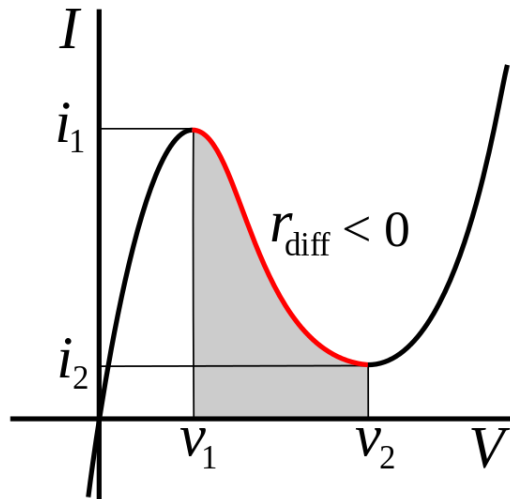
# Sustaining the Oscillation – Negative Resistance

- ❖ If we can replenish the dissipated energy in a resonator, we could possibly sustain the oscillation
- ❖ Adding a “negative resistance” device will do the trick
  - A positive resistance dissipates energy; a negative resistance generates energy



# Creating Negative Resistance

- ❖ How do we realize negative resistance?
  - I-V curves with negative slope
  - Positive feedback provides effective negative resistance; the idea of a negative resistance oscillator is unified with a feedback oscillator

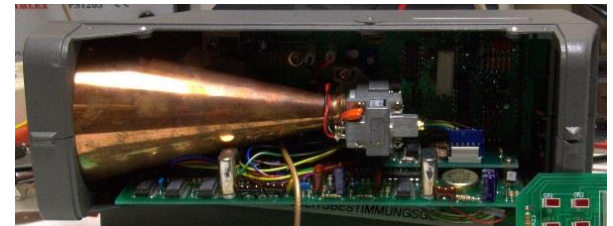
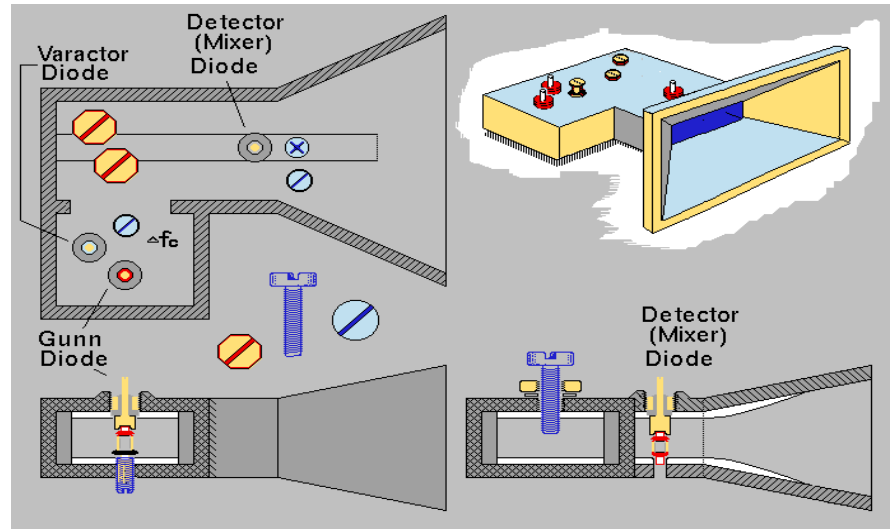
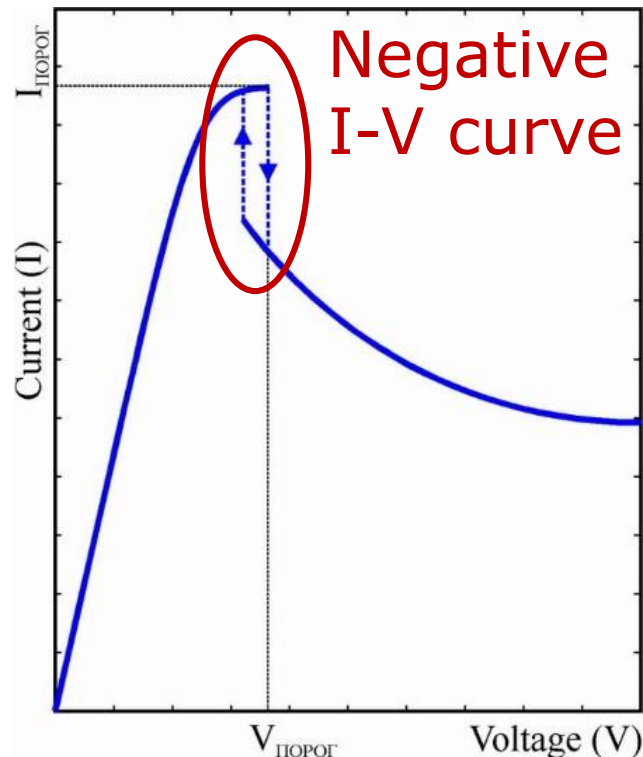


$$i = \frac{v - Av}{R_1} + \frac{v}{R_{\text{in}}}$$

$$R = \frac{v}{i} = \frac{R_1}{1 + R_1/R_{\text{in}} - A}$$

# Creating Negative Resistance

- ❖ How do we create negative resistance?
  - Some semiconductor devices exhibit negative resistance naturally; the mechanism cannot be described clearly with positive feedback
  - The microwave Gunn diode is a great example
  - Can be placed into a high-Q cavity resonator to generate oscillation

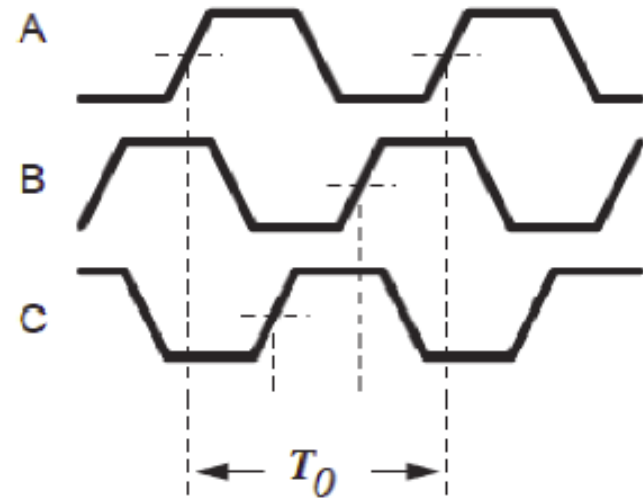
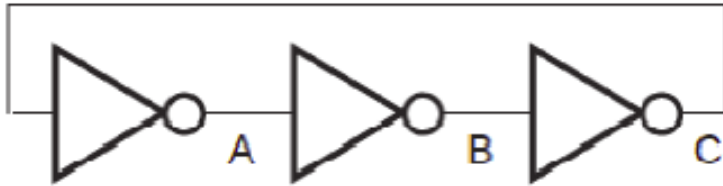


# Ring Oscillator

- ❖ Frequency is determined by the delay of amplifiers (inverters)

$$f = \frac{1}{N\tau_d}$$

- ❖ Guaranteed start up.



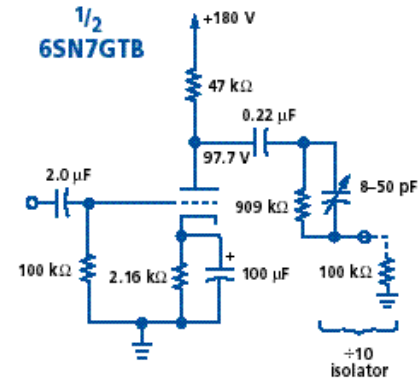
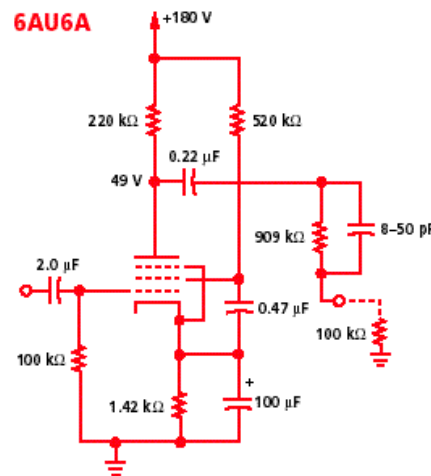
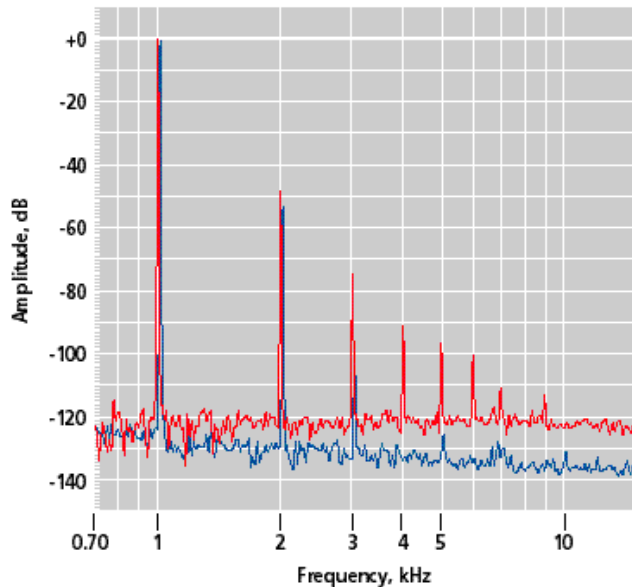
# Oscillator Specifications

## ❖ Output power

- Some oscillators have built in buffer/driver amplifiers to improve the output power, obviously at the penalty of high dc power consumption

## ❖ Harmonics

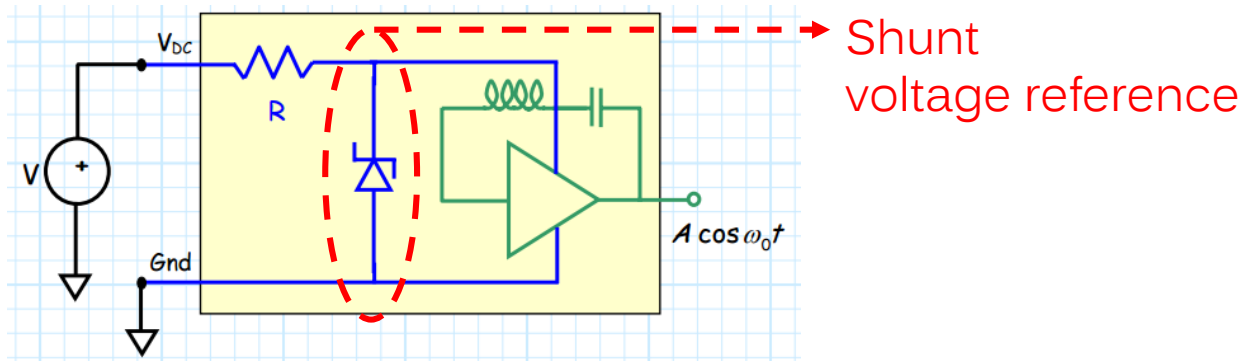
- In reality, the voltage/current waveform in an oscillator is not purely sinusoidal. Some distortion is usually present, resulting in harmonic content in the output spectrum.





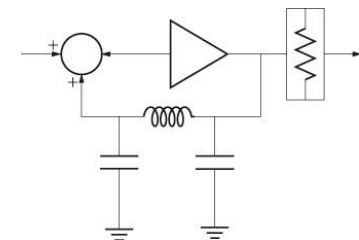
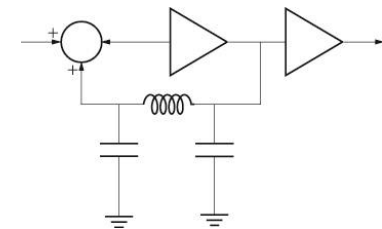
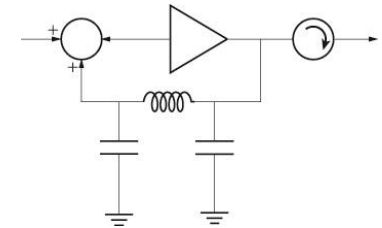
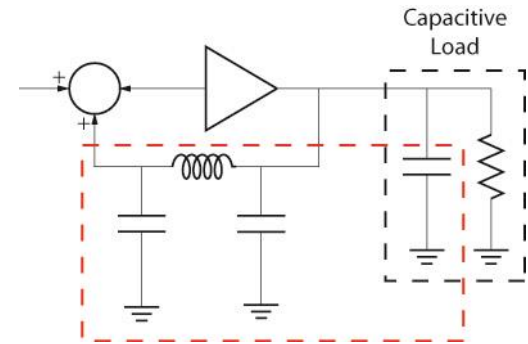
# Oscillator Specifications – Pushing

- ❖ In practical oscillators, the active circuit characteristics will be influenced by the supply voltage
  - e.g. recall that a transistor's IV characteristics are functions of both gate (base) and drain (collector) voltages
  - Fluctuation in the supply voltages can result in fluctuation in the oscillator output frequency and power
- ❖ Oscillator **frequency pulling** is specified as the frequency shift per volt change in the supply voltage: **Hz/V**, or Hz/mV, kHz/mV, MHz/V, or any other variants
- ❖ To counteract pushing, some oscillators integrate a voltage regulator/reference



# Oscillator Specifications – Pulling

- ❖ The load impedance of an oscillator can also affect the oscillator output performance
  - e.g. consider a conceptual Collpitts oscillator shown in the left: the capacitance in the load becomes part of the frequency selective network, which may shift the resonant frequency and the output power of the oscillator. The pulling characteristics in a real oscillator may be much more complex.
  - Because impedance is a complex number, there is not a single quantity to quantify pulling, a typical specification could read “less than 2 MHz at VSWR = 3”; this is usually the worst-case specification.
- ❖ To counteract pulling of an oscillator, the output is usually isolated from the load by an isolator/circulator, amplifier, or simply an attenuator.

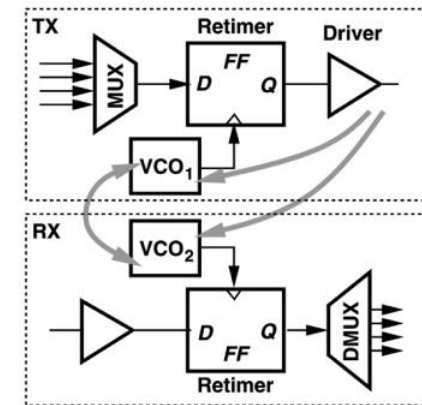


# Oscillator Characteristics – Locking

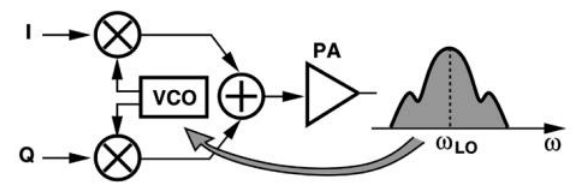
- ❖ When oscillators are coupled with each other, they tend to synchronize in phase and frequency
  - Watch a video on mechanical oscillators synchronizing in phase
  - Same phenomena can be observed in electronic oscillators – we call it *injection locking or pulling* (when the initial frequency or phase difference is too great to achieve total synchronization)
- ❖ Locking can be used to our advantage
  - E.g. clock distribution – locking many oscillators to the same frequency reference
- ❖ Unwanted locking can also be detrimental to an RF system



Synchronization of mechanical oscillators



(a)

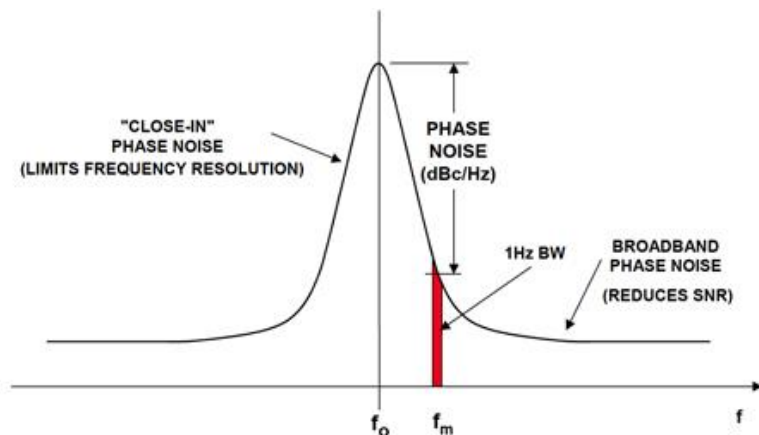
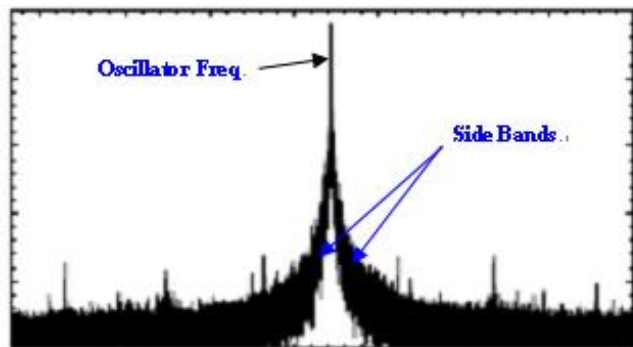


(b)

Undesirable Effects of Injection Pulling

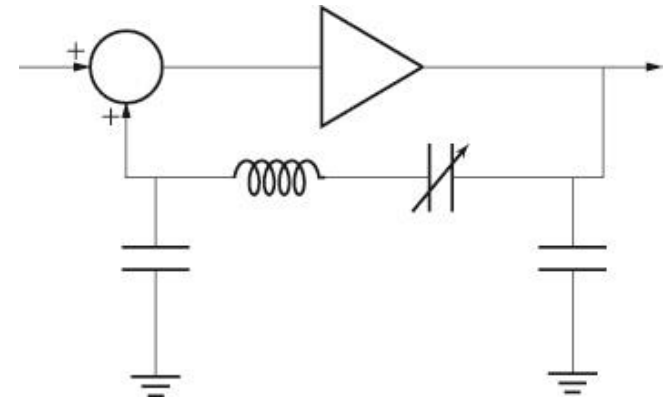
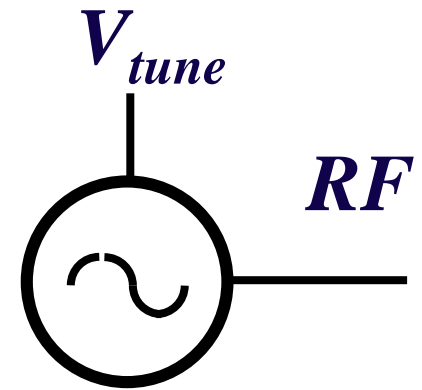
# Phase Noise

- ❖ Phase noise is a very important system parameter and is worth learning a little more about
- ❖ Phase noise results from
  - imperfect frequency selectivity of the feedback network
  - noise sources that modulates the high frequency current/voltage that passes through the active (gain) part of an oscillator
  - Noise (mostly thermal) from loss components in the passive part of the circuit
- ❖ Phase noise is usually specified with respect to the carrier power: dBc, in which “c” means carrier. Also, because phase noise shows itself as a continuous spectrum, its power is measured within a certain bandwidth, hence the unit of “dBc/Hz”



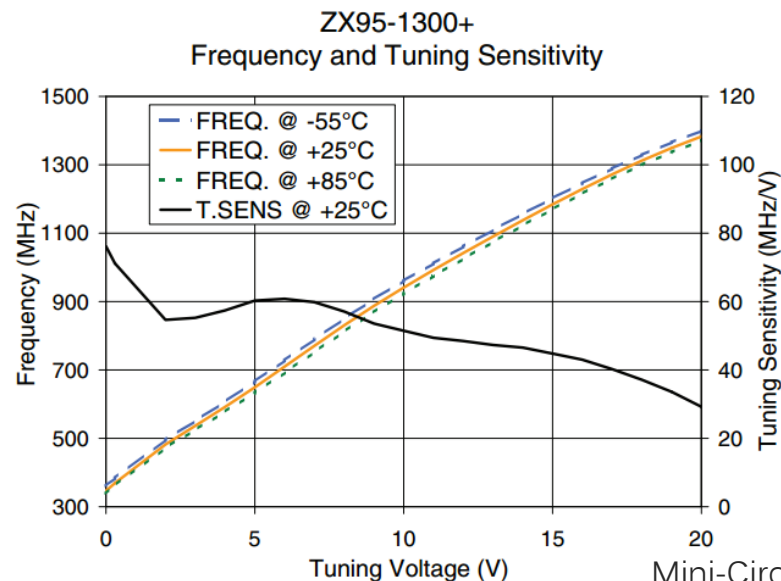
# Voltage Controlled Oscillator (VCO)

- ❖ An oscillator whose output frequency can be controlled by a voltage signal
- ❖ Usually implemented by tuning the feedback network by a variable capacitor
- ❖ Very useful component in any system whose operating frequency needs to change
  - FM radio
  - Frequency sweeping radars
  - Frequency synthesizers
  - Spectrum analyzers
  - Network analyzers



# VCO Specifications

- ❖ All the specifications for fixed oscillators are still applicable
- ❖ Tuning sensitivity: frequency change per volt of tuning voltage change
  - Sometimes referred to as “VCO gain”
  - Specified in Hz/V, or MHz/V
  - A higher sensitivity means that you can cover a large frequency range with small tuning voltage; it also means that the output frequency is more sensitive to the noise in the tuning voltage
- ❖ In some applications, particularly frequency modulation (FM) systems, tuning linearity is of particular concern
  - Good linearity ensures good modulation fidelity



# Example VCO Datasheet

## ❖ Mini-Circuits ZX95-1300+

Coaxial

## Voltage Controlled Oscillator

**ZX95-1300+**

Wide Band 400 to 1300 MHz

### Features

- very wide band frequency
- linear tuning characteristics
- low phase noise
- low pushing
- protected by US patent 6,790,049

### Applications

- r & d
- lab
- instrumentation
- wireless communications
- industrial communications
- test equipment



CASE STYLE: GB956

Connectors	Model	Price	Qty.
<b>SMA</b>	ZX95-1300-S+	\$49.95 ea.	(1-9)

### +RoHS Compliant

The +Suffix identifies RoHS Compliance. See our web site for RoHS Compliance methodologies and qualifications

### Electrical Specifications

MODEL NO.	FREQ. (MHz)		POWER OUTPUT (dBm)	PHASE NOISE dBc/Hz SSB at offset frequencies,kHz				TUNING					NON HARMONIC SPURIOUS (dBc)	HARMONICS (dBc)		PULLING pk-pk @12 dB (MHz)	PUSHING (MHz/V)	DC OPERATING POWER				
	Min.	Max.		Typ.				VOLTAGE RANGE (V)		SENSI- TIVITY (MHz/V)	PORT CAP (pF)	3 dB MODULATION BANDWIDTH (MHz)		Typ.	Typ.			Max.	Typ.	Typ.	Vcc (volts)	Current (mA)
				1	10	100	1000	Min.	Max.	Typ.	Typ.	Typ.										
ZX95-1300+	400	1300	+8	-65	-91	-120	-141	0.3	20	40	- 60	100	30	-90	-12	-	3.5	1.5	5	40		



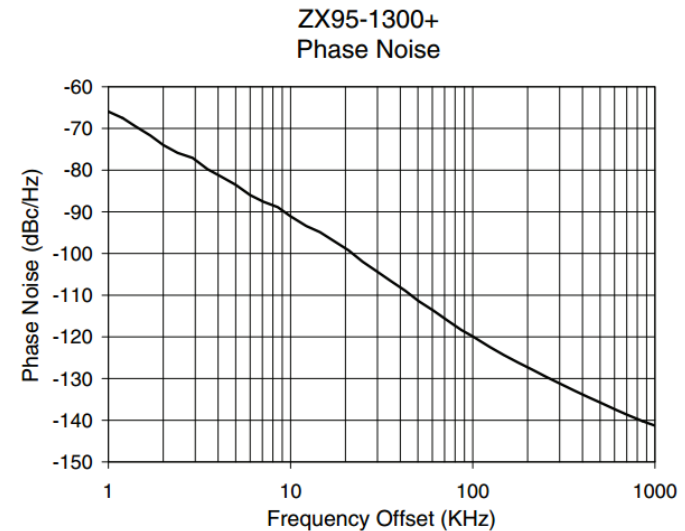
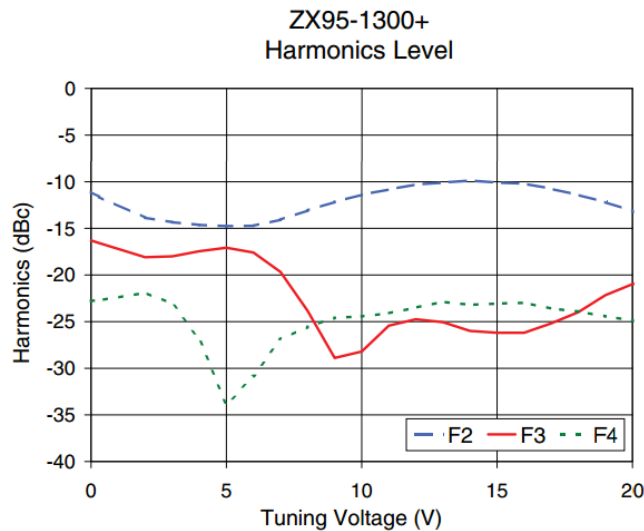
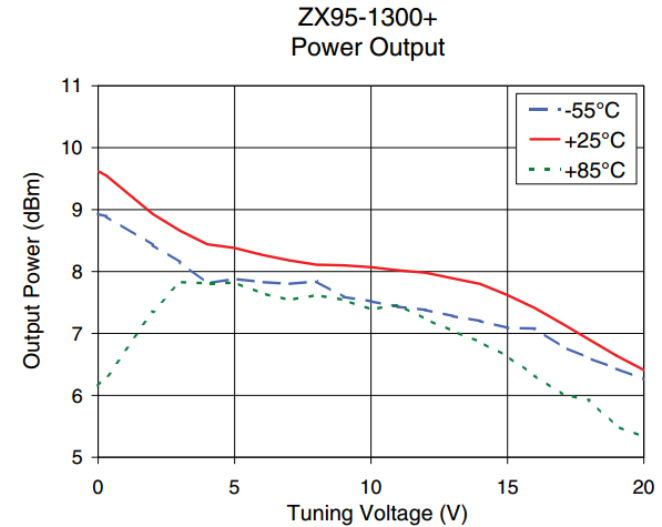
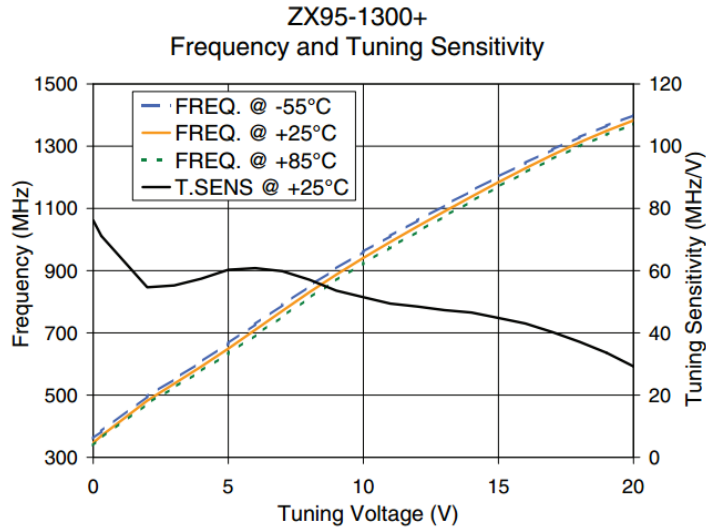
# Example VCO Datasheet (cont.)

V TUNE	TUNE SENS (MHz/V)	FREQUENCY (MHz)			POWER OUTPUT (dBm)			Icc (mA)	HARMONICS (dBc)			FREQ. PUSH (MHz/V)	FREQ. PULL (MHz)	PHASE NOISE (dBc/Hz) at offsets				FREQ OFFSET (KHz)	PHASE NOISE at 850 MHz (dBc/Hz)
		-55°C	+25°C	+85°C	-55°C	+25°C	+85°C		F2	F3	F4			1kHz	10kHz	100kHz	1MHz		
0.00	76.16	361.3	346.5	339.1	8.93	9.62	6.16	29.90	-11.1	-16.3	-22.8	2.56	0.80	-63.1	-88.0	-118.0	-139.8	1.0	-65.96
0.30	71.15	383.9	369.3	361.9	8.89	9.55	6.29	30.05	-11.6	-16.6	-22.7	2.29	1.02	-63.7	-88.8	-118.3	-139.9	2.0	-73.98
2.00	54.66	496.1	482.1	472.6	8.43	8.93	7.35	30.89	-13.9	-18.1	-21.9	1.28	1.74	-67.4	-92.1	-120.2	-140.9	3.5	-79.77
3.00	55.23	551.2	536.8	524.9	8.15	8.66	7.83	31.31	-14.3	-18.0	-23.1	0.90	1.55	-68.4	-94.0	-120.9	-141.7	6.0	-85.98
4.00	57.41	607.4	592.0	578.0	7.81	8.44	7.81	31.68	-14.6	-17.5	-26.9	0.64	2.24	-68.6	-94.0	-121.4	-142.3	8.5	-88.86
5.00	60.29	666.6	649.4	633.6	7.88	8.38	7.82	31.93	-14.8	-17.1	-33.9	0.90	4.21	-69.8	-92.6	-121.1	-142.2	10.0	-91.08
6.00	60.80	728.1	709.7	692.4	7.83	8.27	7.65	32.09	-14.7	-17.6	-30.8	1.28	4.31	-66.2	-92.8	-120.2	-141.6	20.8	-99.24
7.00	59.84	789.8	770.5	752.5	7.80	8.18	7.54	32.16	-14.1	-19.7	-26.9	1.54	4.21	-64.1	-91.2	-119.8	-141.2	35.5	-106.61
8.00	57.09	849.9	830.3	812.2	7.84	8.11	7.62	32.23	-13.1	-23.8	-25.6	1.66	3.95	-66.2	-91.4	-120.0	-141.4	60.7	-113.68
9.00	53.57	907.2	887.4	869.2	7.59	8.10	7.54	32.30	-12.2	-28.9	-24.6	1.79	2.62	-66.2	-91.2	-120.2	-141.5	86.7	-118.37
10.00	51.46	960.8	941.0	923.3	7.52	8.07	7.39	32.25	-11.4	-28.2	-24.4	1.66	3.67	-65.2	-91.1	-120.0	-141.7	100.0	-119.89
11.00	49.41	1011.6	992.4	975.2	7.43	8.02	7.46	32.19	-10.8	-25.4	-24.1	1.28	4.21	-64.4	-91.6	-120.4	-142.1	148.1	-124.35
12.00	48.45	1061.1	1041.9	1025.2	7.38	7.98	7.23	32.03	-10.3	-24.7	-23.5	1.15	4.22	-66.0	-92.0	-121.0	-142.5	177.0	-126.14
13.00	47.30	1109.2	1090.3	1074.6	7.28	7.89	7.04	31.87	-10.1	-25.1	-22.9	1.15	4.35	-68.2	-92.5	-121.4	-142.8	211.6	-127.85
14.00	46.53	1156.4	1137.6	1122.7	7.20	7.80	6.86	31.69	-9.9	-26.0	-23.2	1.41	3.41	-68.2	-92.6	-122.0	-143.1	302.4	-131.25
15.00	44.80	1202.2	1184.1	1170.0	7.09	7.62	6.63	31.54	-10.1	-26.2	-23.1	1.41	3.85	-66.9	-93.2	-122.5	-143.8	361.5	-132.89
16.00	43.01	1246.3	1228.9	1215.6	7.08	7.41	6.32	31.41	-10.2	-26.2	-23.0	1.54	3.96	-66.7	-94.4	-123.0	-144.4	507.5	-135.86
17.00	40.26	1289.0	1271.9	1258.9	6.79	7.16	6.02	31.34	-10.8	-25.2	-23.6	1.79	2.22	-66.8	-95.2	-123.4	-144.3	606.7	-137.44
18.00	37.12	1328.7	1312.2	1299.6	6.60	6.90	5.92	31.31	-11.4	-24.0	-23.9	1.66	3.77	-69.7	-95.3	-123.8	-144.6	851.6	-140.19
20.00	29.25	1399.2	1382.9	1370.3	6.26	6.41	5.33	31.30	-13.1	-21.0	-24.9	1.54	3.89	-71.6	-96.7	-123.4	-144.3	1000.0	-141.30

\*at 25°C unless mentioned otherwise



# Example VCO Datasheet (cont.)



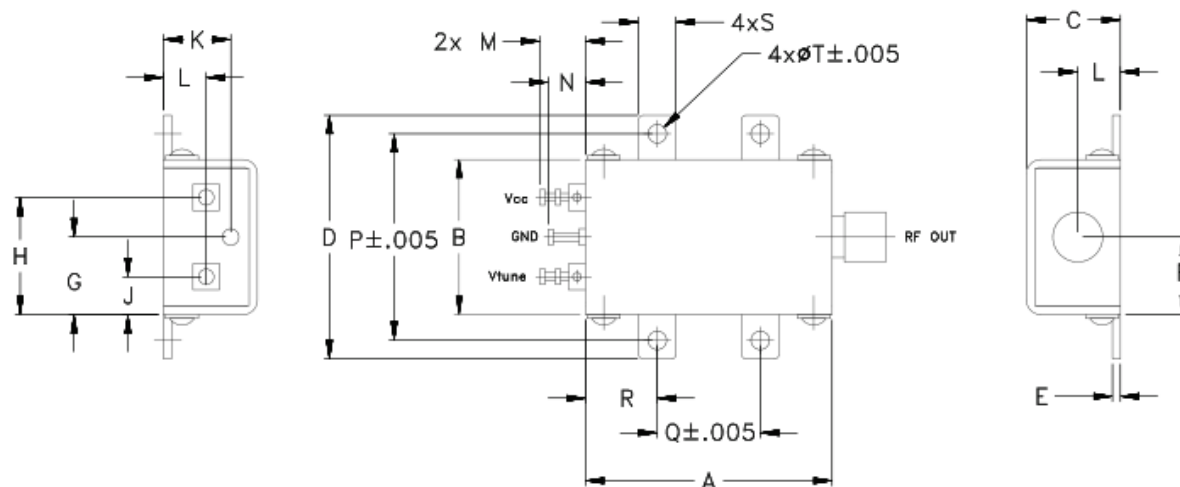
# Example VCO Datasheet (cont.)

## Maximum Ratings

Operating Temperature	-55°C to 85°C
Storage Temperature	-55°C to 100°C
Absolute Max. Supply Voltage (Vcc)	6V
Absolute Max. Tuning Voltage (Vtune)	22V
All specifications	50 ohm system

Permanent damage may occur if any of these limits are exceeded.

## Outline Drawing



## Outline Dimensions (inch mm)

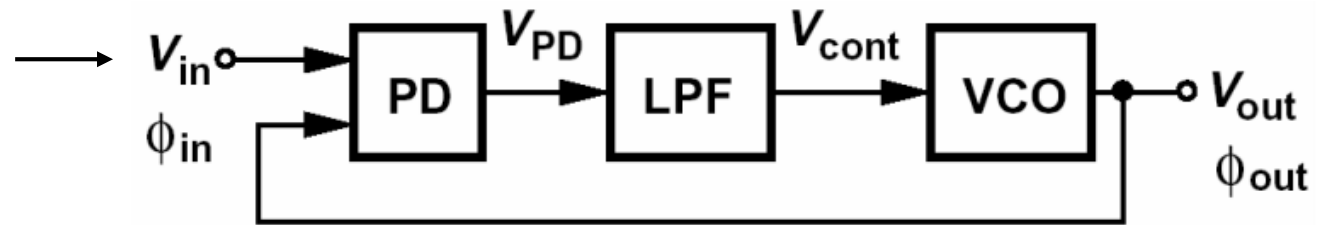
A	B	C	D	E	F	G	H	J	K	L	M	N	P	Q	R	S	T	wt.
1.20	.75	.46	1.18	.04	.38	.38	.57	.18	.33	.21	.22	.18	1.00	.50	.35	.18	.106	grams
30.48	19.05	11.68	29.97	1.02	9.65	9.65	14.48	4.57	8.38	5.33	5.59	4.57	25.40	12.70	8.89	4.57	2.69	35.0

# Phase-Locked-Loop (PLL)

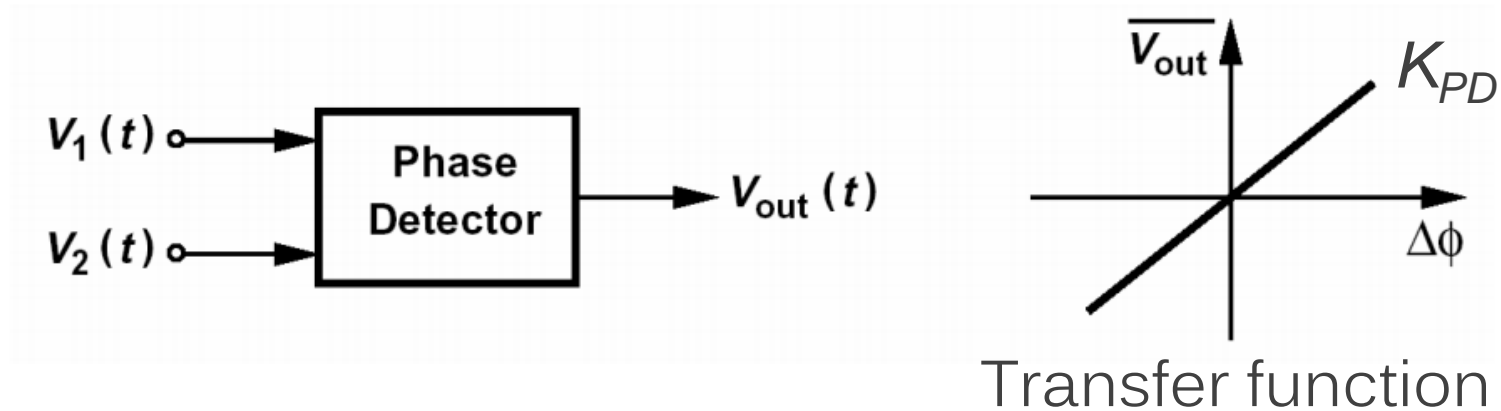
- ❖ A feedback loop to achieve very high frequency stability and low phase noise
- ❖ Also a very useful technique to accurately track the frequency and phase of the input signal



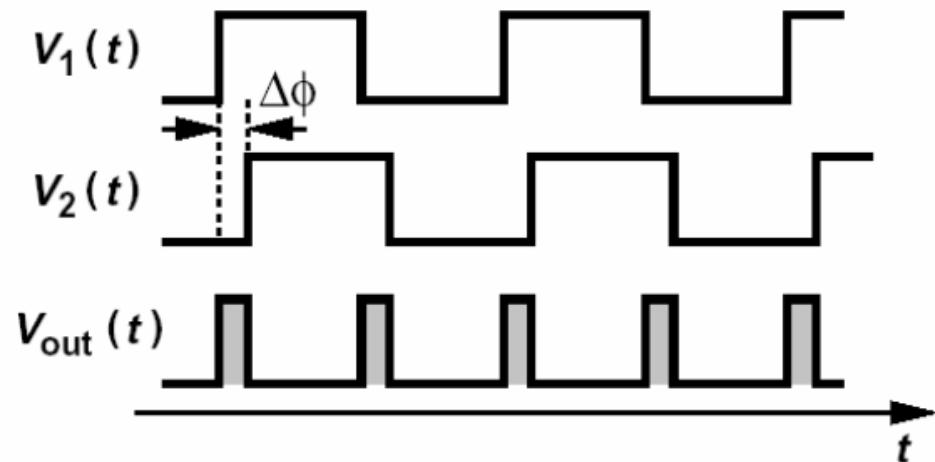
Crystal frequency reference



# Phase Detector

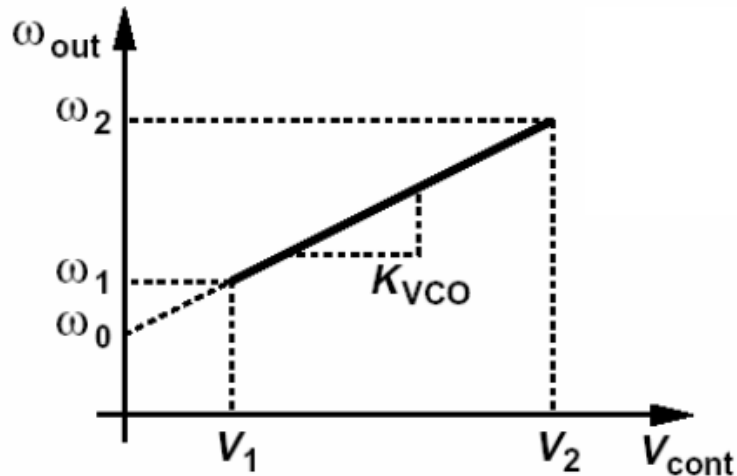


XOR as a simple implementation



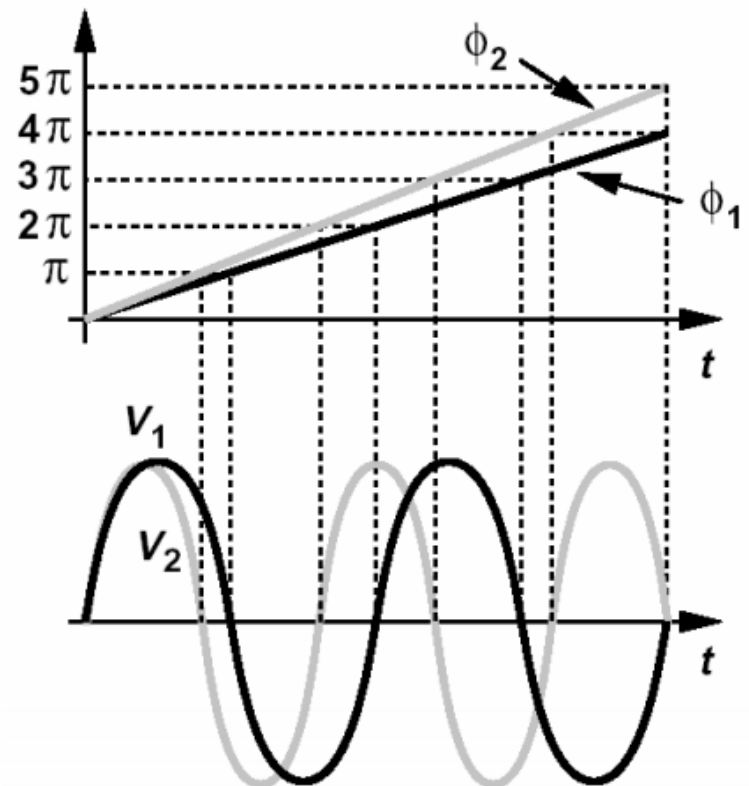
# Modeling the VCO

- ❖ Assuming that the VCO has a linear tuning characteristics and its sensitivity/gain is  $K_{VCO}$



$$\omega_{out} = \omega_0 + K_{VCO} V_{TUNE}$$

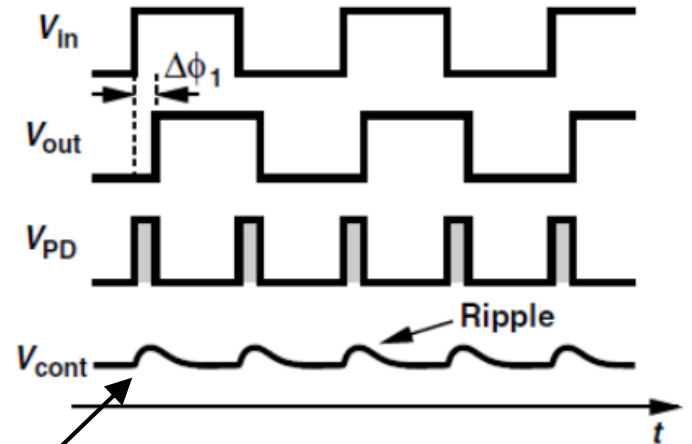
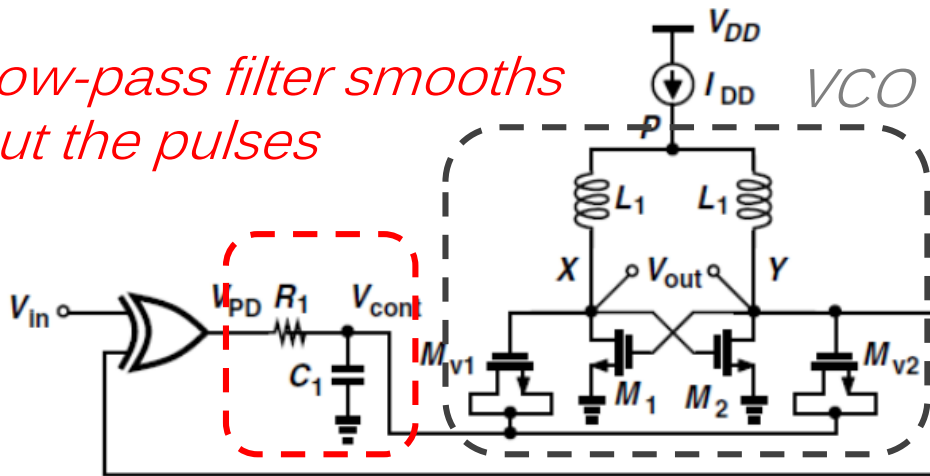
A higher frequency means faster phase progression



# Example

- ❖ The PFD allows the use of charge-pump circuits to create the control signal for the VCO

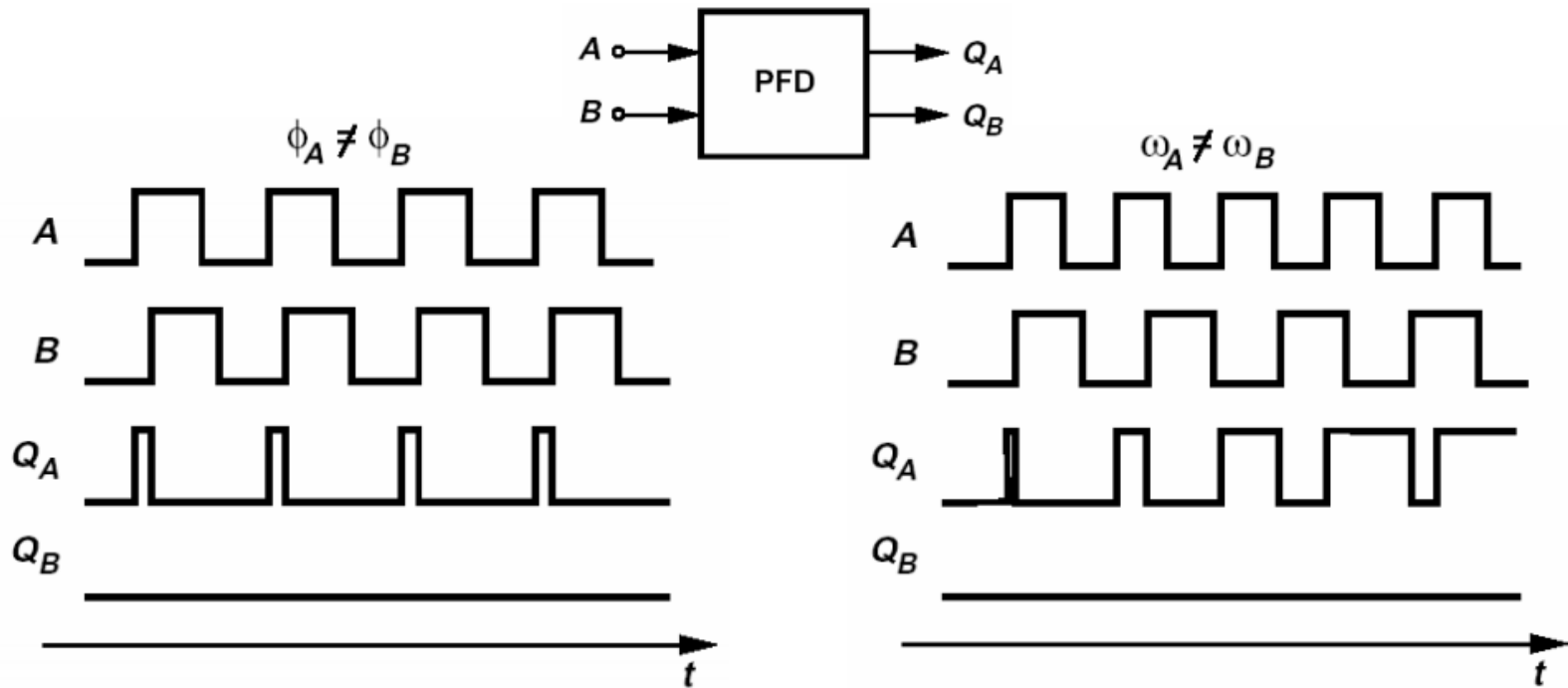
*Low-pass filter smooths out the pulses*



*Increase in  $V_{cont}$  ( $V_{TUNE}$ ) bumps up the frequency and therefore the phase progression so that the VCO output phase can catch up with the  $V_{in}$  ( $V_{ref}$ ) phase*

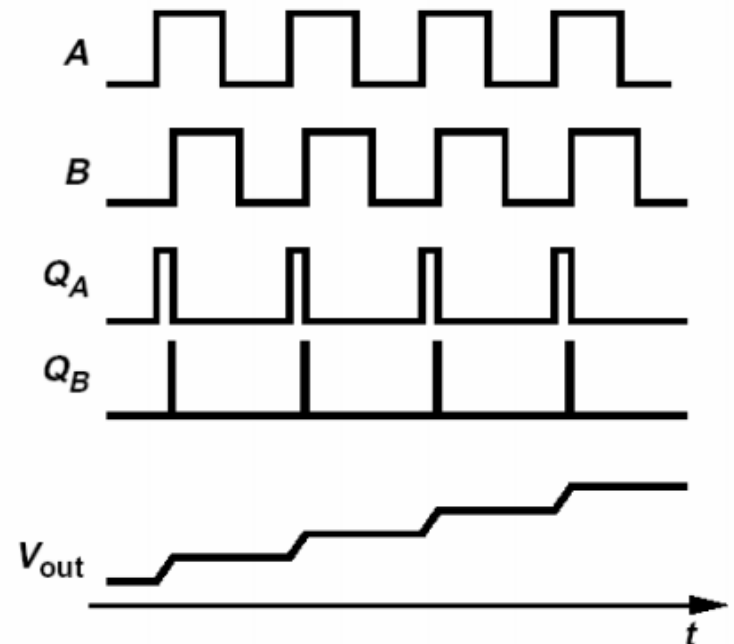
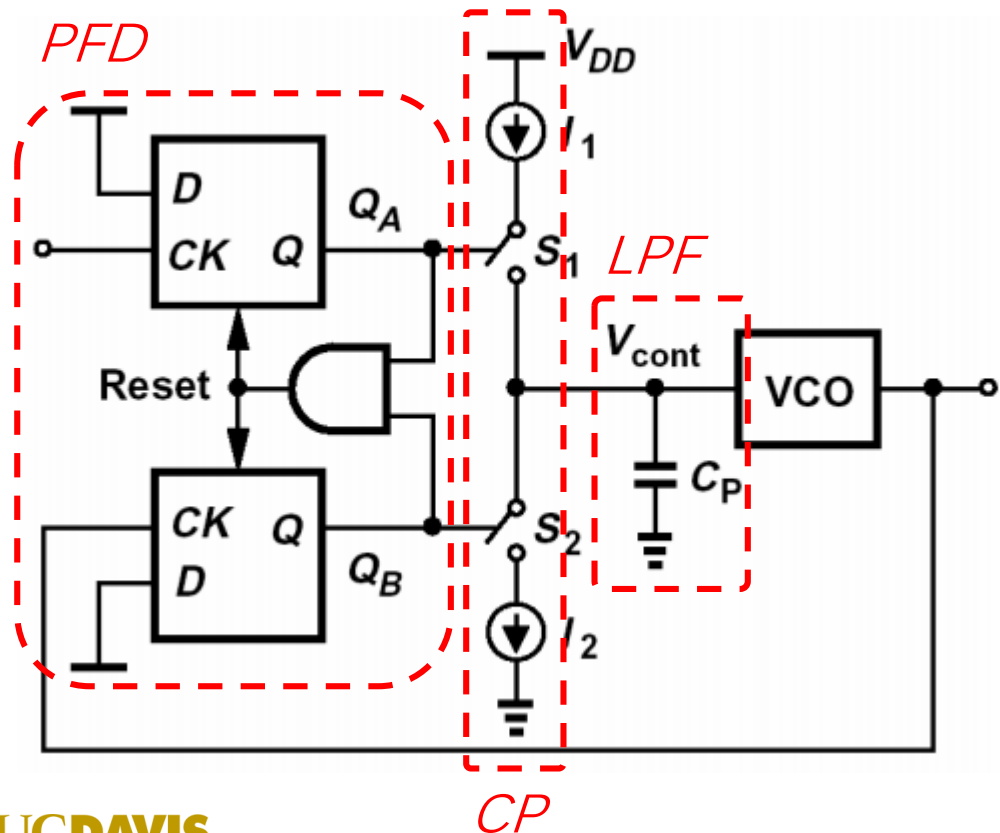
# Phase/Frequency Detector

- ❖ The phase/frequency detector (PFD) provides the correct output even when the frequencies of the two inputs are different



# PFD+ Charge Pump (CP) in PLL

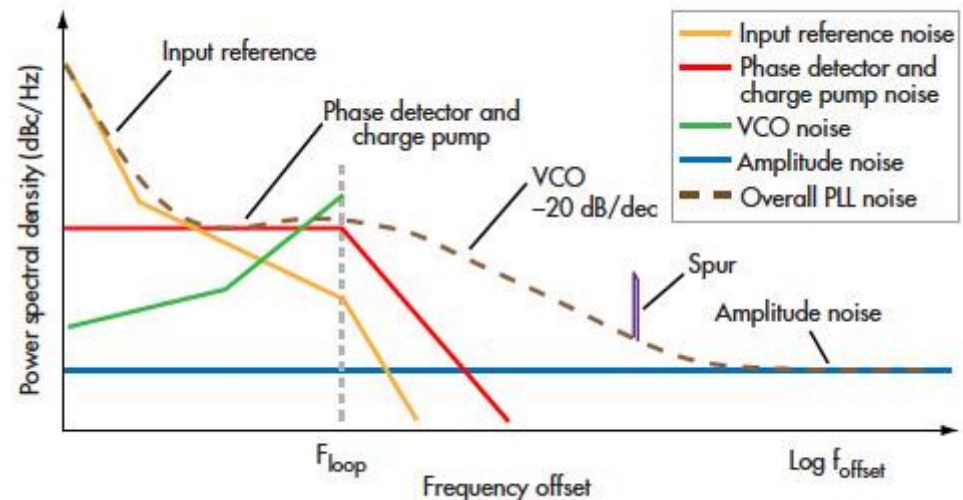
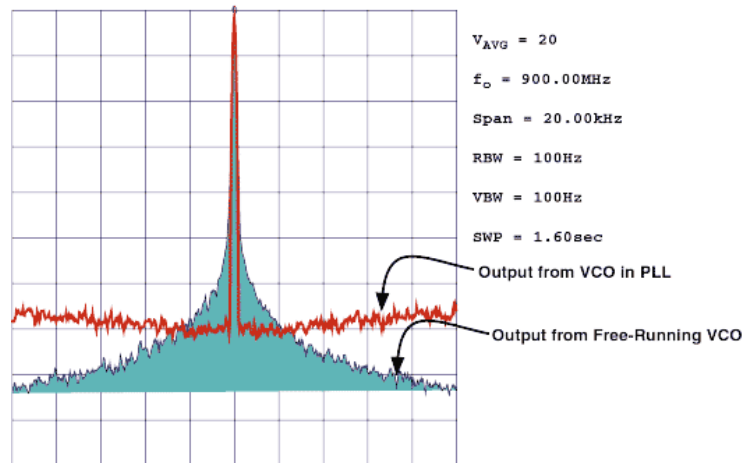
- ❖ The charge pump provides the current to drive the subsequent stage in the PLL
- ❖ The PLL locks the output signals phase and frequency to the reference: we can now replicate the stability and low phase noise of the reference!





# Phase Noise in a PLL

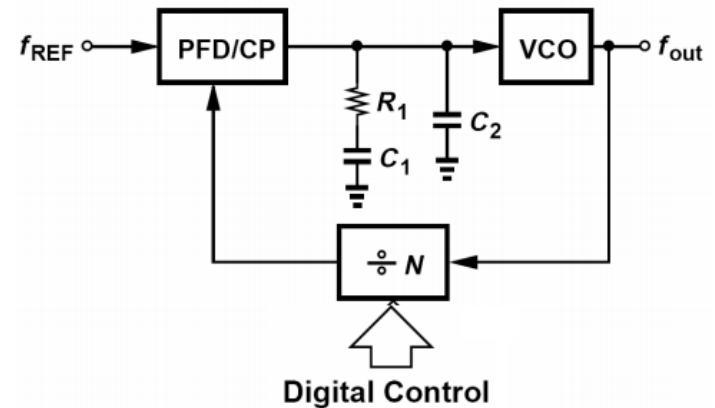
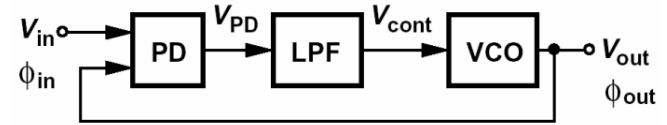
- ❖ A PLL is basically a negative feedback loop that stabilizes the output signal to the reference.
- ❖ The stabilization only takes effect within the loop bandwidth—effectively the bandwidth of the low-pass filter.





# Frequency Synthesis – Integer-N Synthesizer

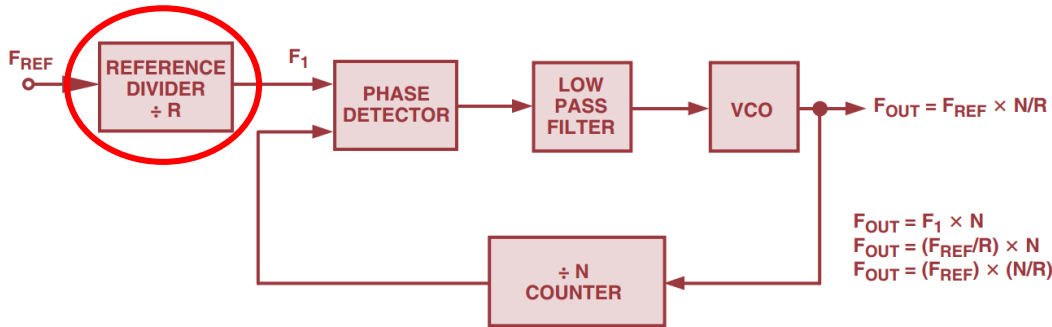
- ❖ The basic PLL studied above isn't very useful for frequency synthesis; the output signal frequency is the same as the reference!
- ❖ Adding a divide by N block:
  - Output frequency now a multiple of the reference frequency
  - By digitally controlling the divider ratio N we can generate different frequencies
  - Drawback: Output frequency resolution is determined by the reference frequency
  - One penalty paid is the phase noise: **Phase noise grows 6 dB per multiple by 2, or 20 dB per multiple by 10, in frequency**



$$f_{out} = N \times f_{REF}$$

# Integer-N Synthesizer – Adding a Reference Counter

- ❖ A reference counter can improve frequency resolution

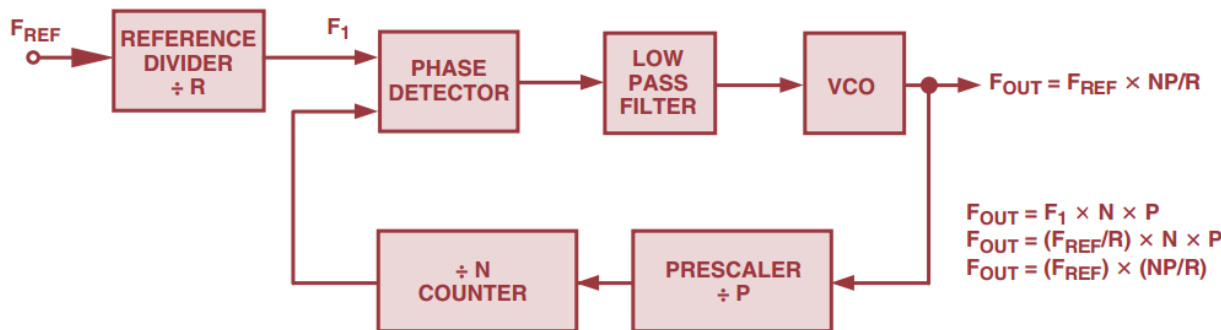


$$f_{out} = \frac{N \times f_{REF}}{R}$$

- ❖ Drawback: the reference counter  $R$  makes the feedback counter very large!
- ❖ Example:
  - Using a 10 MHz reference clock and a reference counter of 1,000, we can achieve frequency resolution of 10 kHz
  - To get an output frequency around 900 MHz, we'd need a  $N$  value of 90,000 -> equivalent of a 17-bit counter, difficult to make it working right at high frequency

# Integer-N Synthesizer – Prescalar

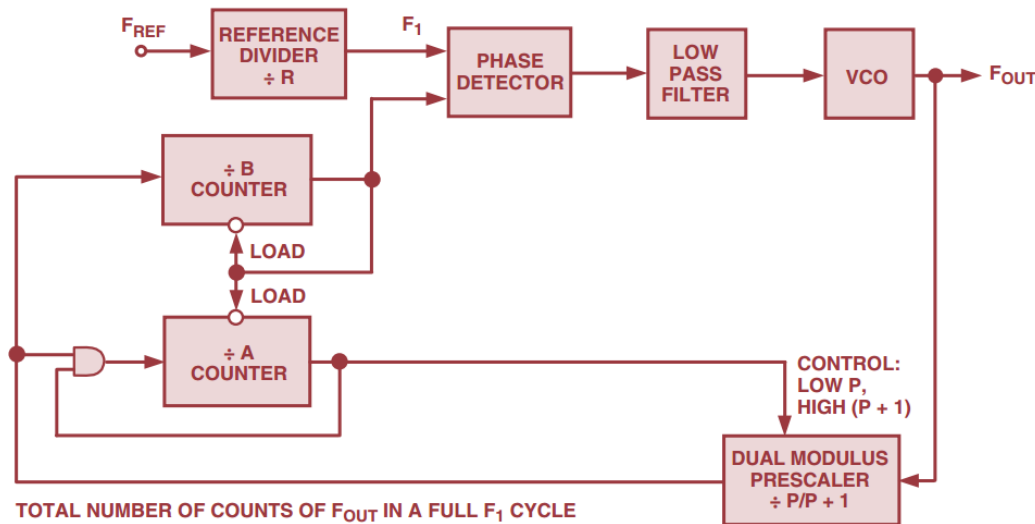
- ❖ Adding a pre-scalar to alleviate the issue: the division is now done in two steps
  - The pre-scalar is a high-frequency component that divide the feedback signal by a **fixed** ratio, e.g. /2, /4, /8, /32, etc
  - Because  $P$  is fixed, the frequency resolution degrades by  $P$ ! Now we seem be going in circles!
    - Fortunately  $P$  is usually much smaller than  $R$ , so we still get a net gain
    - And another clever solution exists to solve this issue



$$f_{out} = \frac{PN \times f_{REF}}{R}$$

# Integer-N Synthesizer – Dual Modulus Prescaler

- ❖ Counter A and counter B time-outs sequentially to toggle the prescaler value by 1
  - Both A and B can be digitally controlled



$$f_{out} = \frac{(BP + A) \times f_{REF}}{R}$$

TOTAL NUMBER OF COUNTS OF  $F_{OUT}$  IN A FULL  $F_1$  CYCLE

$$A \times (P + 1) + (B - A)P$$

$$AP + A + BP - AP$$

$$BP + A$$

$$F_{OUT} = F_1 \times (BP + A)$$

$$F_{OUT} = (F_{REF}/R) \times (BP + A)$$

# Fractional-N Synthesizer

- ❖ Fractional-N synthesizer shifts the modulus of the divider randomly to achieve lower phase noise
- ❖ It also achieves greater frequency resolution and faster switching time
- ❖ And it's too complicated for this class, so we won't discuss it further.

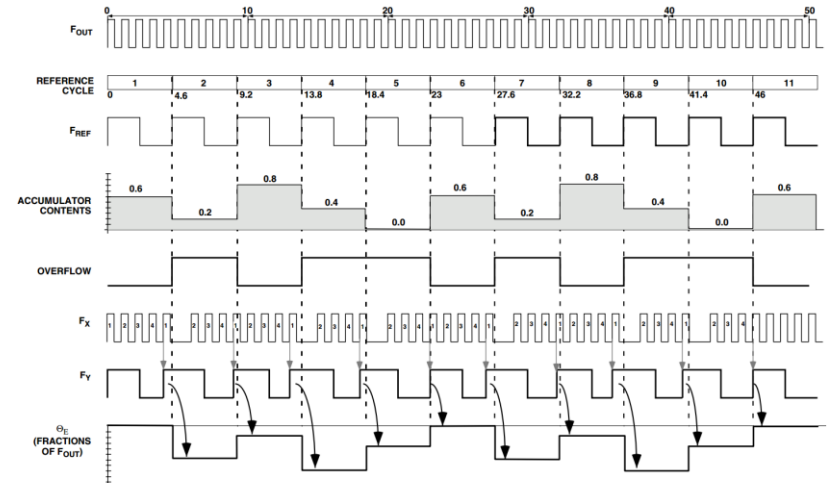
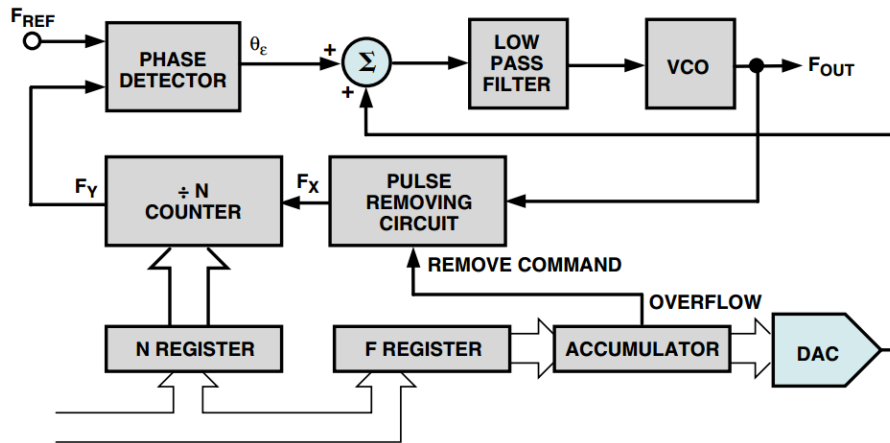


Figure 9. Fractional-N timing.