# Aotea Quay (AQ)

Before utilizing the Vs profiles or the experimental dispersion data presented herein, it is strongly recommended that the user read and understand the document titled "Analysis Methodology", particularly the section titled "Limitation of Inversion Derived Vs Profiles", for a short discussion of the relevant limitations of the data presented.



Figure 1: Site plan indicating locations of individual three-component, 20-s seismometers composing the 2D array for Microtremor Array Measurements (MAM) and the linear arrays of 24, 4.5-Hz geophones used for Multichannel Analysis of Surface Waves (MASW) testing. MAM and MASW arrays are denoted in the legend by their largest extent/aperture. Note station 20, located in the southwest corner of the port, is not shown in Figure 1.

Table 1: Latitude and longitude coordinates for MAM seismometer locations.

Station Identifier	Latitude (°)	Longitude (°)
AQ_T11	-41.267877	174.786445
AQ_T12	-41.267823	174.786221
AQ_T14	-41.267883	174.786134
AQ_T15	-41.267968	174.786156
AQ_T16	-41.267767	174.785994
AQ_T17	-41.267940	174.786041
AQ_T18	-41.268116	174.786093
AQ_T19	-41.268643	174.786241
AQ_T20	-41.281759	174.784768

Note: A .kmz with the location of each MAM seismometer is provided.

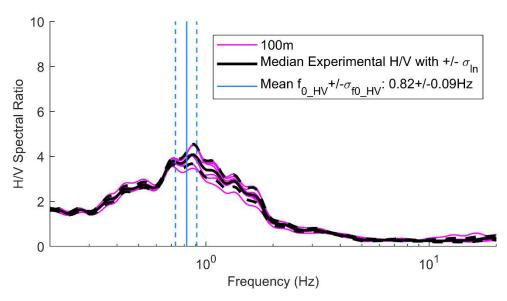


Figure 2: Horizontal-to-Vertical (H/V) Spectral Ratio curves derived from all single station seismometer recordings from the MAM array. The lognormal median experimental H/V curve with +/- one standard deviation curves determined from all single station measurements are shown. The fundamental frequency for the site is represented by the mean fundamental frequency peak ( $f_{0 \text{ H/V}}$ ) calculated from all single station measurements and +/- one standard deviation ( $\sigma_{f0 \text{ H/V}}$ ).

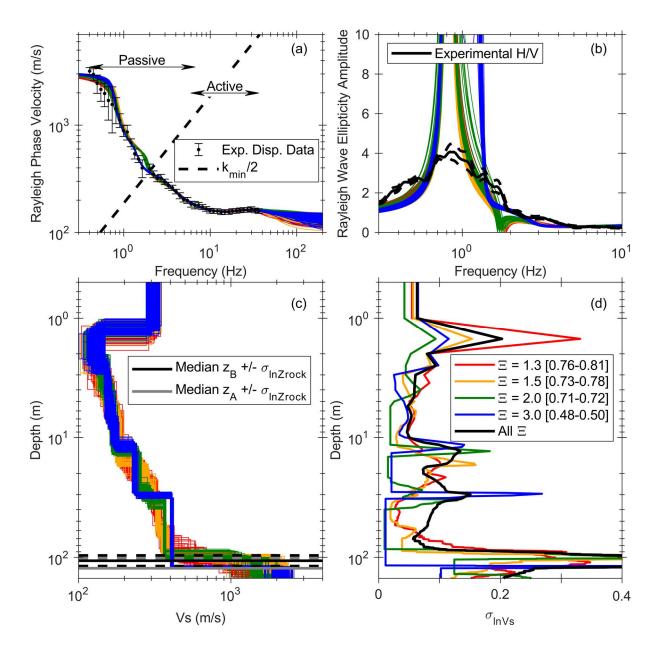


Figure 3: Inversion results. Shown for each layering ratio ( $\Xi$ ) inversion parameterization are the 100 lowest misfit: (a) theoretical fundamental mode Rayleigh wave dispersion curves with the experimental dispersion data; (b) theoretical Rayleigh wave ellipticity with the lognormal median and +/- one standard deviation experimental H/V data; (c) shear wave velocity (Vs) profiles with the lognormal median depth to soft (Vs>760m/s) and hard (Vs>1500m/s) rock; and (d) standard deviation of the natural logarithm of Vs ( $\sigma_{lnVs}$ ). The range of misfit values associated with the 100 lowest misfit velocity profiles for each  $\Xi$  inversion parameterization are shown in brackets in the figure's legend. Note the 1000 lowest misfit and statistical median Vs profiles for each  $\Xi$  inversion parameterization and reference location are provided in text format in the sub-directory Vs Profiles.

Table 2: Resolution depth ( $d_{res}$ ) and maximum depth ( $d_{max}$ ) for the Vs profiles as determined by the array geometry and experimental dispersion data. See document Analysis Methodology for details. Even though the experimental dispersion data for this reference location was combined with data from the BIG array prior to inversion,  $d_{res}$  and  $d_{max}$  have been solely based on the reference location array and data extracted therefrom.

Resolution Depth (dres)	Maximum Depth (d <sub>max</sub> )
94m	150m

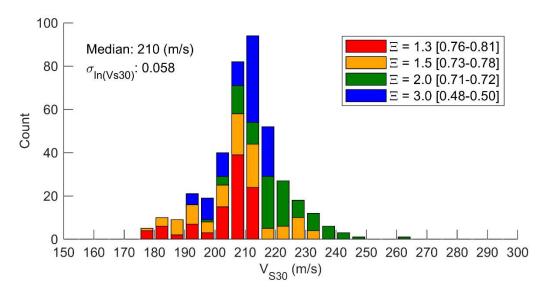


Figure 4: Distribution of the time averaged shear wave velocity in the upper thirty meters (Vs30) for the 100 lowest misfit velocity profiles from each layering ratio ( $\Xi$ ) inversion parameterization. The lognormal median Vs30 value and corresponding standard deviation of the natural logarithm of Vs30 ( $\sigma_{lnVs30}$ ) are provided in the figure.

Table 3: Experimental dispersion data in the form of the mean and standard deviation Rayleigh phase velocity discretized in terms of frequency. The approximate intersection of the theoretical array resolution limit  $(k_{min}/2)$  for the largest MAM array and the fundamental mode Rayleigh experimental dispersion data has been indicated with a dashed line. Dispersion data with frequencies below the dashed line are less certain and should be used with caution. See document Analysis Methodology for more information.

Frequency (Hz)	Rayleigh Phase Velocity (m/s)	Velocity Standard Deviation (m/s)
36	159	8
33	161	8
30	165	8
27	163	8
24	162	8
22	161	8

20     159     8       18     159     8       16     155     8       15     155     8       13     154     8       12     158     8       11     158     8       9.9     160     8       9.0     166     8       8.1     173     9       7.3     180     10       6.6     180     14       6.0     184     12       5.4     199     13       4.9     202     10       4.5     220     14       4.0     241     12       3.6     261     14       3.3     276     18       3.0     296     18       2.7     322     26       2.4     319     22       2.2     349     25       2.0     391     43       1.6     399     75       1.5
16     155     8       15     155     8       13     154     8       12     158     8       11     158     8       9.9     160     8       9.0     166     8       8.1     173     9       7.3     180     10       6.6     180     14       6.0     184     12       5.4     199     13       4.9     202     10       4.5     220     14       4.0     241     12       3.6     261     14       3.3     276     18       3.0     296     18       2.7     322     26       2.4     319     22       2.2     349     25       2.0     391     43       1.6     399     75       1.5     484     36       1.3     542     58       1.1
16     155     8       15     155     8       13     154     8       12     158     8       11     158     8       9.9     160     8       9.0     166     8       8.1     173     9       7.3     180     10       6.6     180     14       6.0     184     12       5.4     199     13       4.9     202     10       4.5     220     14       4.0     241     12       3.6     261     14       3.3     276     18       3.0     296     18       2.7     322     26       2.4     319     22       2.2     349     25       2.0     391     43       1.6     399     75       1.5     484     36       1.3     542     58       1.1
13     154     8       12     158     8       11     158     8       9.9     160     8       9.0     166     8       8.1     173     9       7.3     180     10       6.6     180     14       6.0     184     12       5.4     199     13       4.9     202     10       4.5     220     14       4.0     241     12       3.6     261     14       3.3     276     18       3.0     296     18       2.7     322     26       2.4     319     22       2.2     349     25       2.0     391     43       1.6     399     75       1.5     484     36       1.3     542     58       1.1     864     136       1.0     889     104       0.90<
13     154     8       12     158     8       11     158     8       9.9     160     8       9.0     166     8       8.1     173     9       7.3     180     10       6.6     180     14       6.0     184     12       5.4     199     13       4.9     202     10       4.5     220     14       4.0     241     12       3.6     261     14       3.3     276     18       3.0     296     18       2.7     322     26       2.4     319     22       2.2     349     25       2.0     391     43       1.6     399     75       1.5     484     36       1.3     542     58       1.1     864     136       1.0     889     104       0.90<
11     158     8       9.9     160     8       9.0     166     8       8.1     173     9       7.3     180     10       6.6     180     14       6.0     184     12       5.4     199     13       4.9     202     10       4.5     220     14       4.0     241     12       3.6     261     14       3.3     276     18       3.0     296     18       2.7     322     26       2.4     319     22       2.2     349     25       2.0     391     43       1.6     399     75       1.5     484     36       1.3     542     58       1.1     864     136       1.0     889     104       0.90     1114     163       0.73     1559     713
11     158     8       9.9     160     8       9.0     166     8       8.1     173     9       7.3     180     10       6.6     180     14       6.0     184     12       5.4     199     13       4.9     202     10       4.5     220     14       4.0     241     12       3.6     261     14       3.3     276     18       3.0     296     18       2.7     322     26       2.4     319     22       2.2     349     25       2.0     391     43       1.6     399     75       1.5     484     36       1.3     542     58       1.1     864     136       1.0     889     104       0.90     1114     163       0.73     1559     713
9.9     160     8       9.0     166     8       8.1     173     9       7.3     180     10       6.6     180     14       6.0     184     12       5.4     199     13       4.9     202     10       4.5     220     14       4.0     241     12       3.6     261     14       3.3     276     18       3.0     296     18       2.7     322     26       2.4     319     22       2.2     349     25       2.0     391     43       1.6     399     75       1.5     484     36       1.3     542     58       1.1     864     136       1.0     889     104       0.90     1114     163       0.73     1559     713
9.0 166 8   8.1 173 9   7.3 180 10   6.6 180 14   6.0 184 12   5.4 199 13   4.9 202 10   4.5 220 14   4.0 241 12   3.6 261 14   3.3 276 18   3.0 296 18   2.7 322 26   2.4 319 22   2.2 349 25   2.0 391 43   1.6 399 75   1.5 484 36   1.3 542 58   1.1 864 136   1.0 889 104   0.90 1114 163   0.81 1417 386   0.73 1559 713
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6.6   180   14     6.0   184   12     5.4   199   13     4.9   202   10     4.5   220   14     4.0   241   12     3.6   261   14     3.3   276   18     3.0   296   18     2.7   322   26     2.4   319   22     2.2   349   25     2.0   391   43     1.6   399   75     1.5   484   36     1.3   542   58     1.2   687   58     1.1   864   136     1.0   889   104     0.90   1114   163     0.81   1417   386     0.73   1559   713
6.6   180   14     6.0   184   12     5.4   199   13     4.9   202   10     4.5   220   14     4.0   241   12     3.6   261   14     3.3   276   18     3.0   296   18     2.7   322   26     2.4   319   22     2.2   349   25     2.0   391   43     1.6   399   75     1.5   484   36     1.3   542   58     1.2   687   58     1.1   864   136     1.0   889   104     0.90   1114   163     0.81   1417   386     0.73   1559   713
5.4   199   13     4.9   202   10     4.5   220   14     4.0   241   12     3.6   261   14     3.3   276   18     3.0   296   18     2.7   322   26     2.4   319   22     2.2   349   25     2.0   391   43     1.6   399   75     1.5   484   36     1.3   542   58     1.1   864   136     1.0   889   104     0.90   1114   163     0.81   1417   386     0.73   1559   713
5.4   199   13     4.9   202   10     4.5   220   14     4.0   241   12     3.6   261   14     3.3   276   18     3.0   296   18     2.7   322   26     2.4   319   22     2.2   349   25     2.0   391   43     1.6   399   75     1.5   484   36     1.3   542   58     1.1   864   136     1.0   889   104     0.90   1114   163     0.81   1417   386     0.73   1559   713
4.9 202 10   4.5 220 14   4.0 241 12   3.6 261 14   3.3 276 18   3.0 296 18   2.7 322 26   2.4 319 22   2.2 349 25   2.0 391 43   1.6 399 75   1.5 484 36   1.3 542 58   1.1 864 136   1.0 889 104   0.90 1114 163   0.81 1417 386   0.73 1559 713
4.5 220 14   4.0 241 12   3.6 261 14   3.3 276 18   3.0 296 18   2.7 322 26   2.4 319 22   2.2 349 25   2.0 391 43   1.6 399 75   1.5 484 36   1.3 542 58   1.1 864 136   1.0 889 104   0.90 1114 163   0.81 1417 386   0.73 1559 713
3.6 261 14   3.3 276 18   3.0 296 18   2.7 322 26   2.4 319 22   2.2 349 25   2.0 391 43   1.6 399 75   1.5 484 36   1.3 542 58   1.2 687 58   1.1 864 136   1.0 889 104   0.90 1114 163   0.81 1417 386   0.73 1559 713
3.3 276 18   3.0 296 18   2.7 322 26   2.4 319 22   2.2 349 25   2.0 391 43   1.6 399 75   1.5 484 36   1.3 542 58   1.2 687 58   1.1 864 136   1.0 889 104   0.90 1114 163   0.81 1417 386   0.73 1559 713
3.0 296 18   2.7 322 26   2.4 319 22   2.2 349 25   2.0 391 43   1.6 399 75   1.5 484 36   1.3 542 58   1.2 687 58   1.1 864 136   1.0 889 104   0.90 1114 163   0.81 1417 386   0.73 1559 713
2.7 322 26   2.4 319 22   2.2 349 25   2.0 391 43   1.6 399 75   1.5 484 36   1.3 542 58   1.2 687 58   1.1 864 136   1.0 889 104   0.90 1114 163   0.81 1417 386   0.73 1559 713
2.4 319 22   2.2 349 25   2.0 391 43   1.6 399 75   1.5 484 36   1.3 542 58   1.2 687 58   1.1 864 136   1.0 889 104   0.90 1114 163   0.81 1417 386   0.73 1559 713
2.2 349 25   2.0 391 43   1.6 399 75   1.5 484 36   1.3 542 58   1.2 687 58   1.1 864 136   1.0 889 104   0.90 1114 163   0.81 1417 386   0.73 1559 713
2.0 391 43   1.6 399 75   1.5 484 36   1.3 542 58   1.2 687 58   1.1 864 136   1.0 889 104   0.90 1114 163   0.81 1417 386   0.73 1559 713
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1.0 889 104   0.90 1114 163   0.81 1417 386   0.73 1559 713
0.90 1114 163   0.81 1417 386   0.73 1559 713
0.81 1417 386   0.73 1559 713
0.73 1559 713
0.66
0.66 1699 585
0.60 1975 488
0.54 2156 489
0.49 2454 475
0.47 2434 475
0.45 2971 379

Table 4: Lognormal median depth to the National Earthquake Hazards Reduction Program (NEHRP) Site Class B ("soft rock" = 760 m/s) and Site Class A ("hard rock" = 1500 m/s) boundaries determined from surface wave inversion Vs profiles.

	Lognormal Median	Lognormal Standard Deviation
	(m)	(#)
BC Boundary	107	0.10
AB Boundary	124	0.20