

Improving the Range of WiFi Backscatter Via a Passive Retro-Reflective Single-Side-Band-Modulating MIMO Array and Non-Absorbing Termination

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Miniature and ubiquitous IoT devices



- Enable new class of applications
- Require miniature size, long lifetime, wireless standard-compliant

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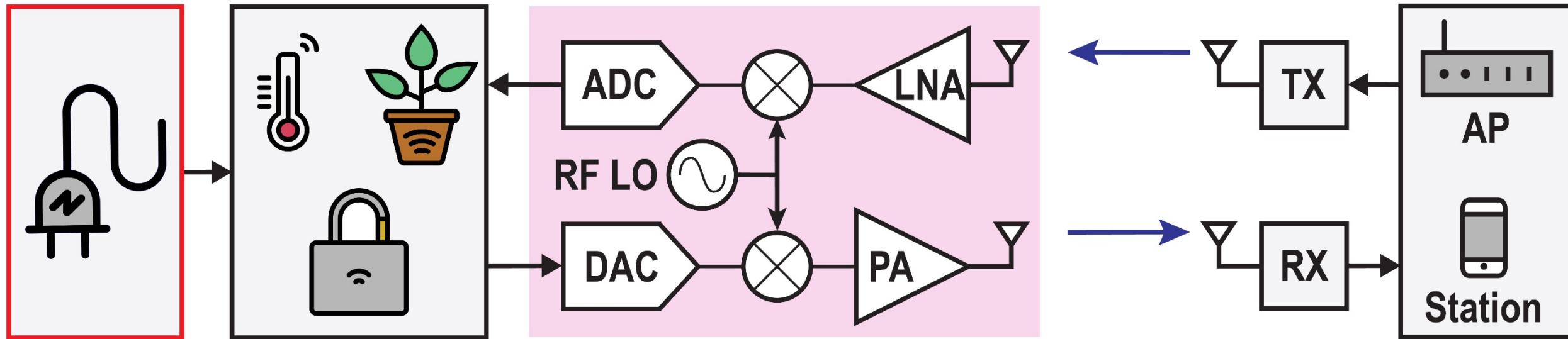
Wireless
interface

Conventional wireless transmission

Wall power /
Large battery

IoT devices

Conventional TRXs

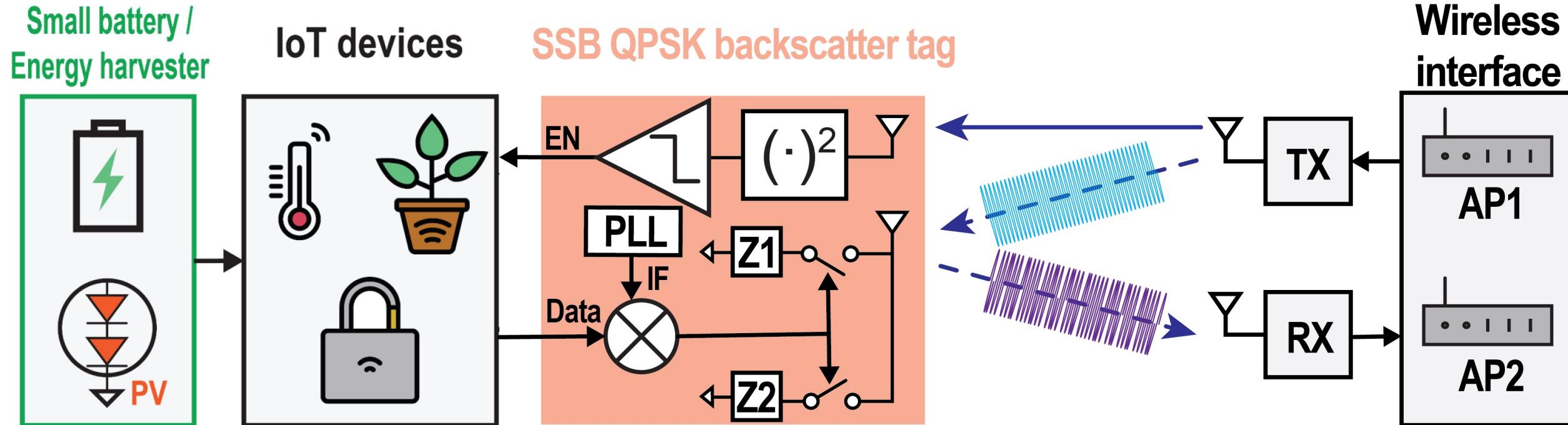


- Conventional WiFi TRXs require 10s~100s mW active power
- Size of IoT devices is limited by power consumption
- Higher order modulation is achievable but trades-off with power

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WiFi compatible backscatter communication

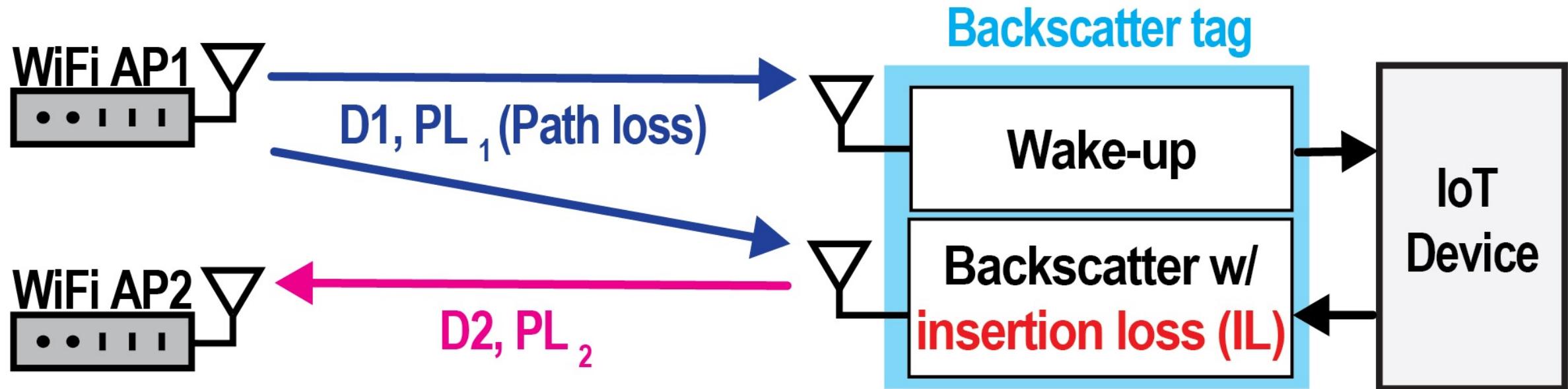


- Elimination of active RF circuit enables low power consumption
- Recent work showed compatibility with existing standards
- Higher order modulation is achievable by implementing IF switches
- Range is limited due to passive nature

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Backscatter - range calculation

$$\text{Downlink: } P_{\text{sens},wu} \leq P_{\text{TX,AP}} - PL_1$$

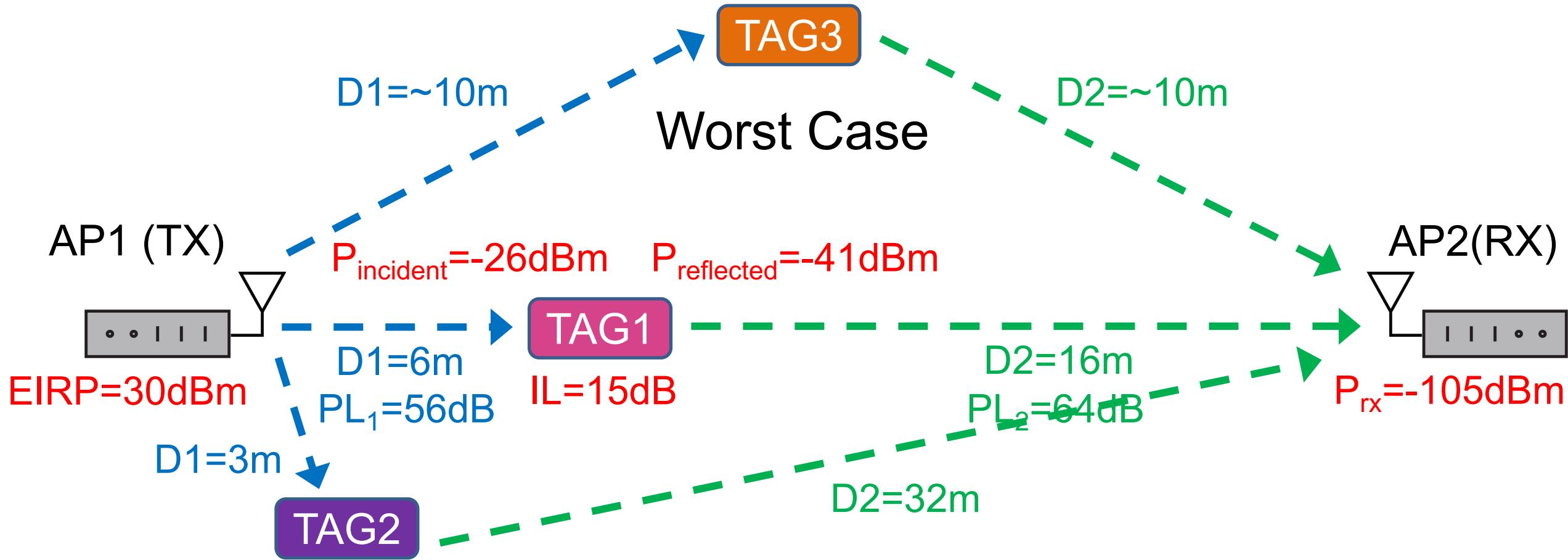


$$\text{Uplink: } P_{\text{sens,AP}} \leq P_{\text{TX,TAP}} - PL_1 - PL_2 - IL_{\text{TAG}}$$

- PL1 and PL2 are determined by D1 and D2
- D1 × D2 is limited by system parameters

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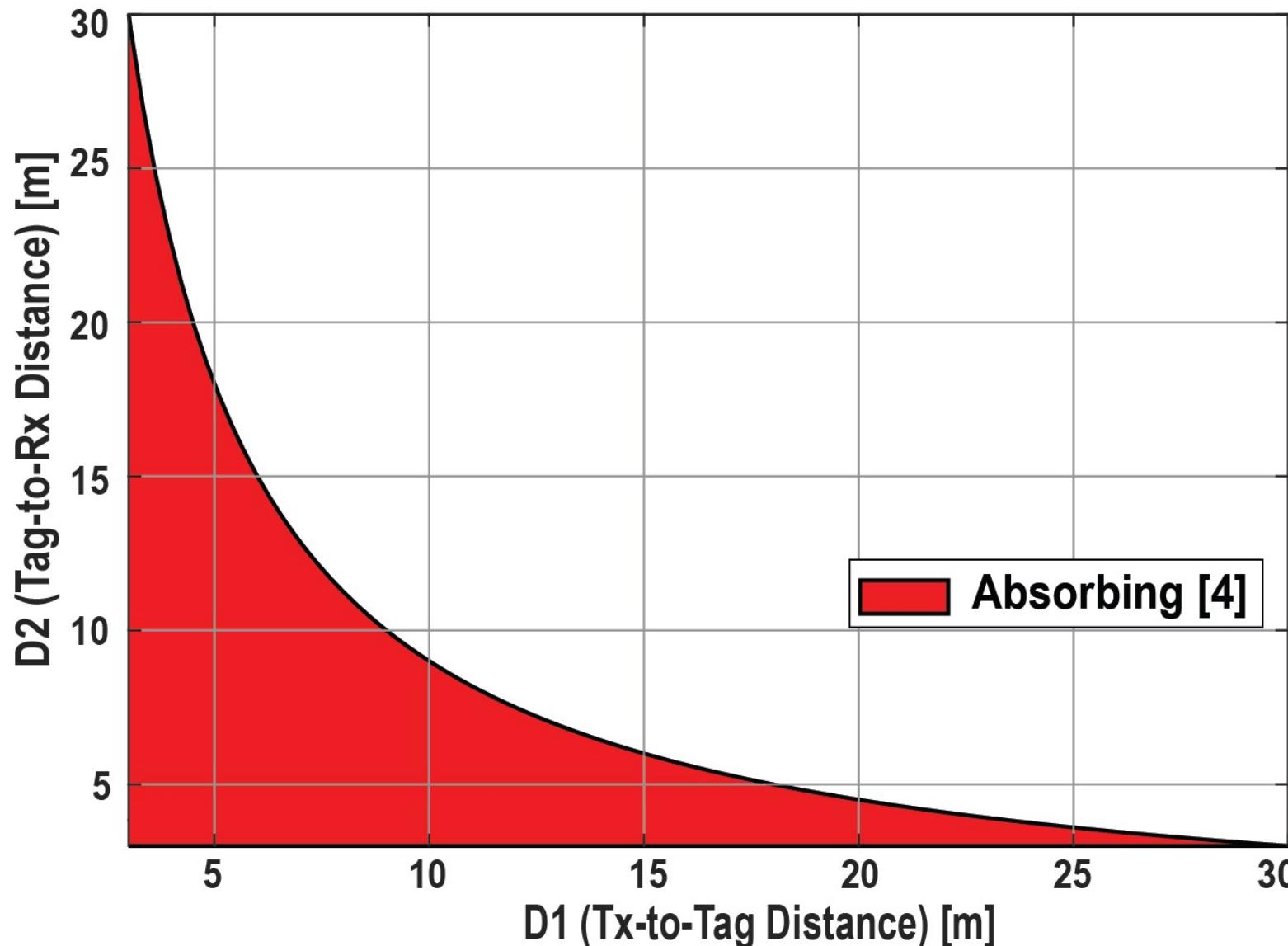
Link budget - Meshed network



$$D1 \times D2 = 96 \text{ mm}^2$$

Wang et al., ISSCC20

Tag in meshed network

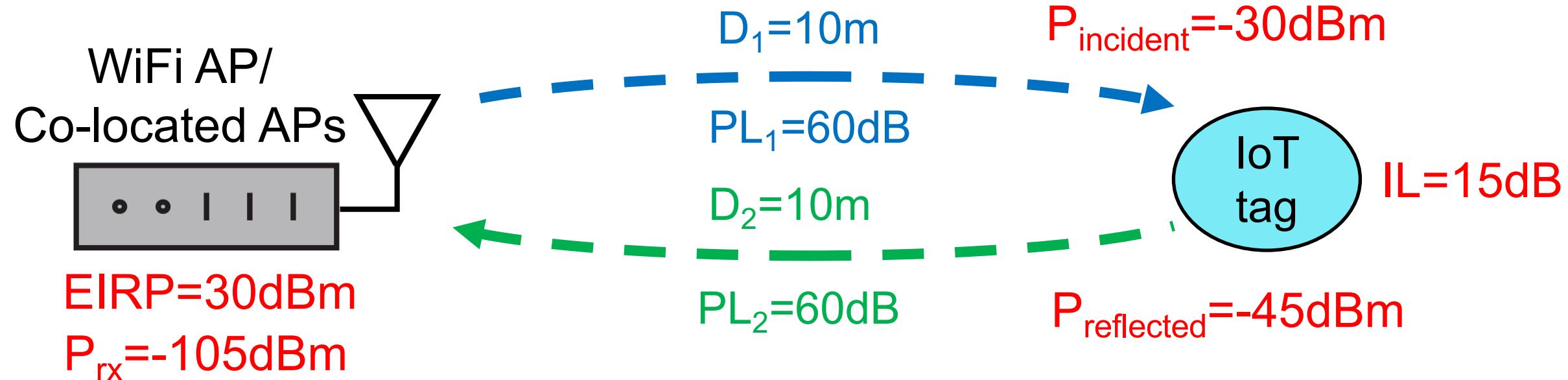


- Tags can work if placed anywhere in the shaded area

Wang et al., ISSCC20

Link budget – single AP or co-located APs

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- Always in the worst-case scenario
- Range improvement is needed for pragmatic adoption in homes and offices with single AP or co-located APs

Range improvement

- TX power: can not be increased, standard in commodity WiFi APs and FDA limits to maximum of 30dBm
- RX Sensitivity: ~-100dBm is the standard for commodity WiFi APs
- D₁xD₂: cannot be improved due to the passive nature of backscatter communication



Improve the insertion loss or apply MIMO gain to improve the covered range

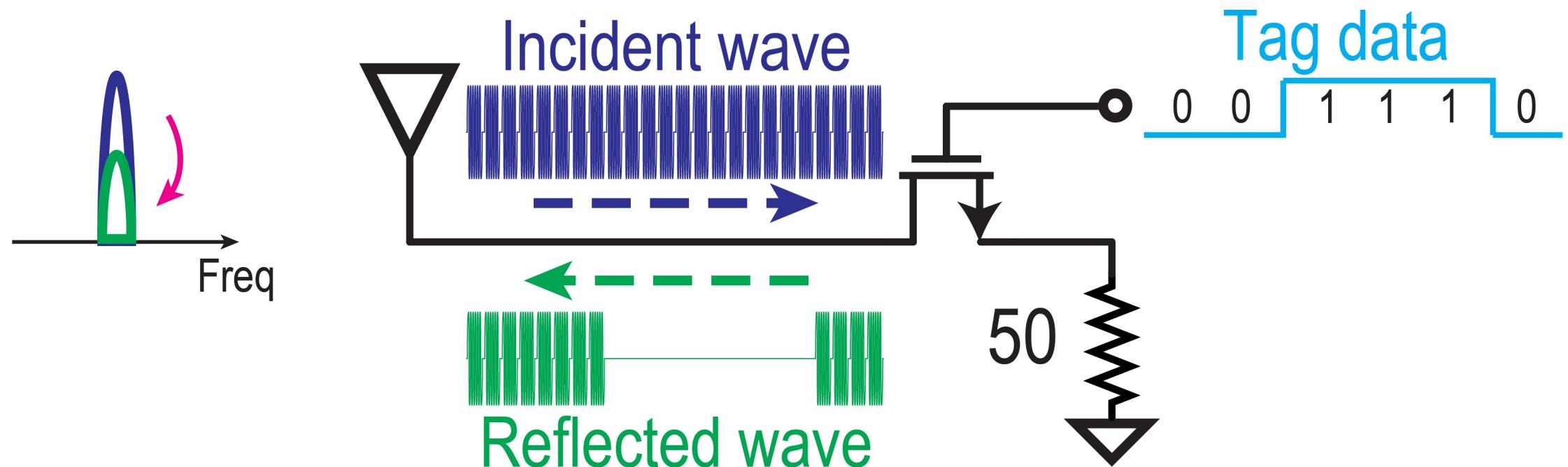
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Outline

- Motivation
- Prior-art and proposed SSB QPSK backscatter with retro-reflective MIMO array and non-absorbing termination
- Proposed fully-WiFi-compliant backscatter
- Circuit implementation
- Measurement results
- Conclusion

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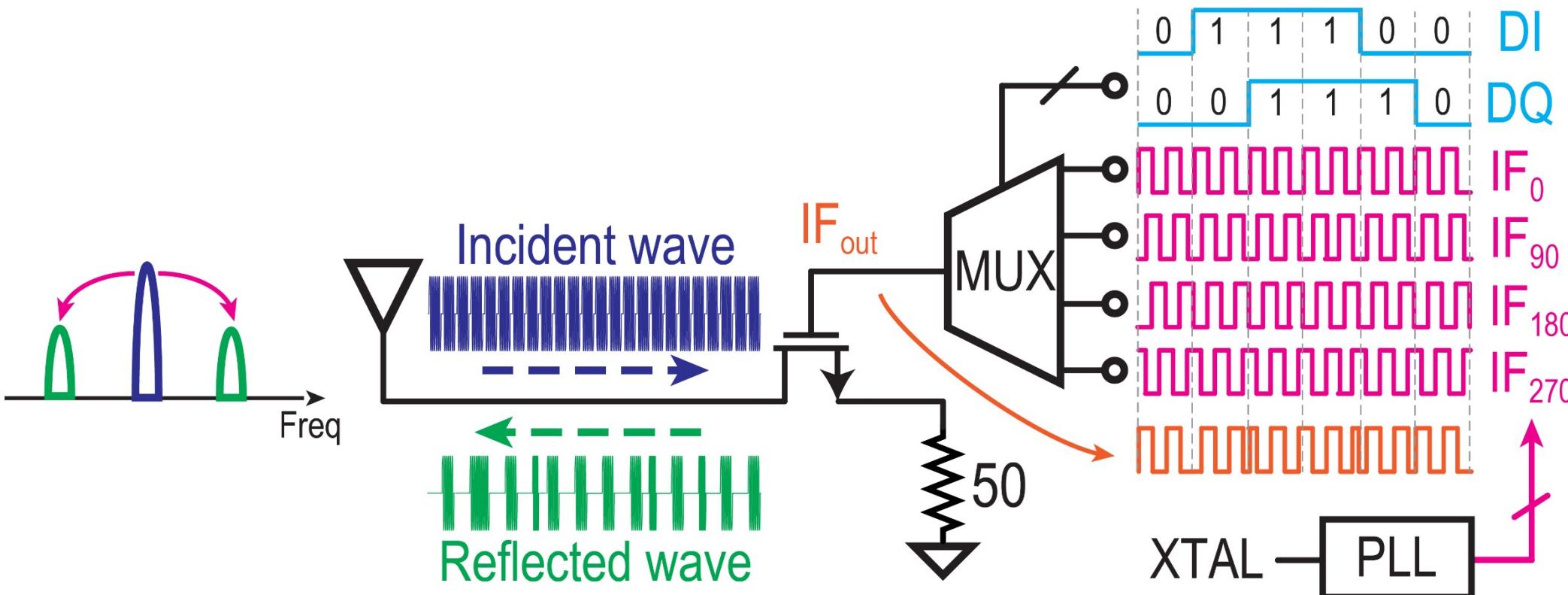
Conventional OOK backscatter



- Tag data modulates the input impedance via a single switch directly
- ✗ OOK modulation only
- ✗ Reflected wave spectrum overlaps with incident wave

QPSK frequency translation backscatter

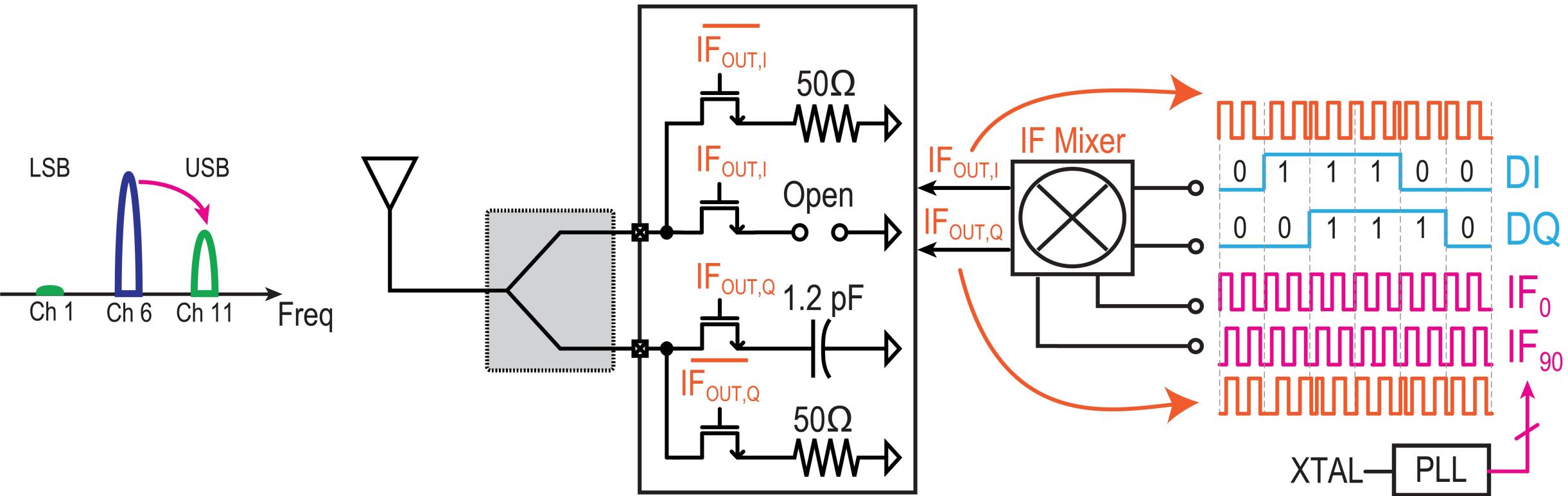
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- 4 phase of IF clock is selected by IQ tag data and mixed with incident signal via a single switch
- QPSK modulation
- Double-side-band modulation occupies 2 adjacent channels

SSB QPSK backscatter

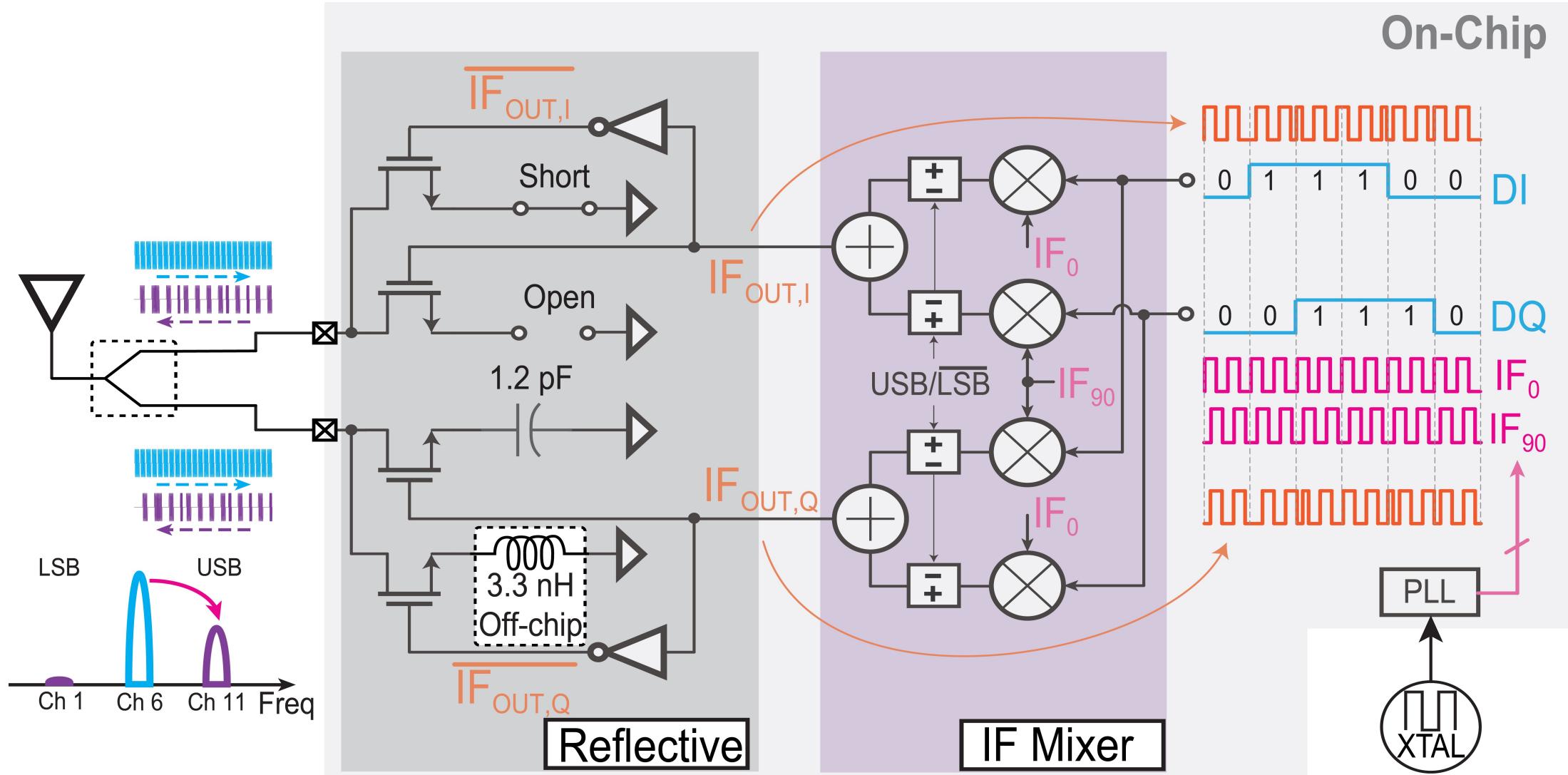
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- QPSK modulation
- Single-side-band modulation occupies only one adjacent channel
- Range is limited to 10m with co-located APs

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Proposed fully-reflective SSB QPSK backscatter

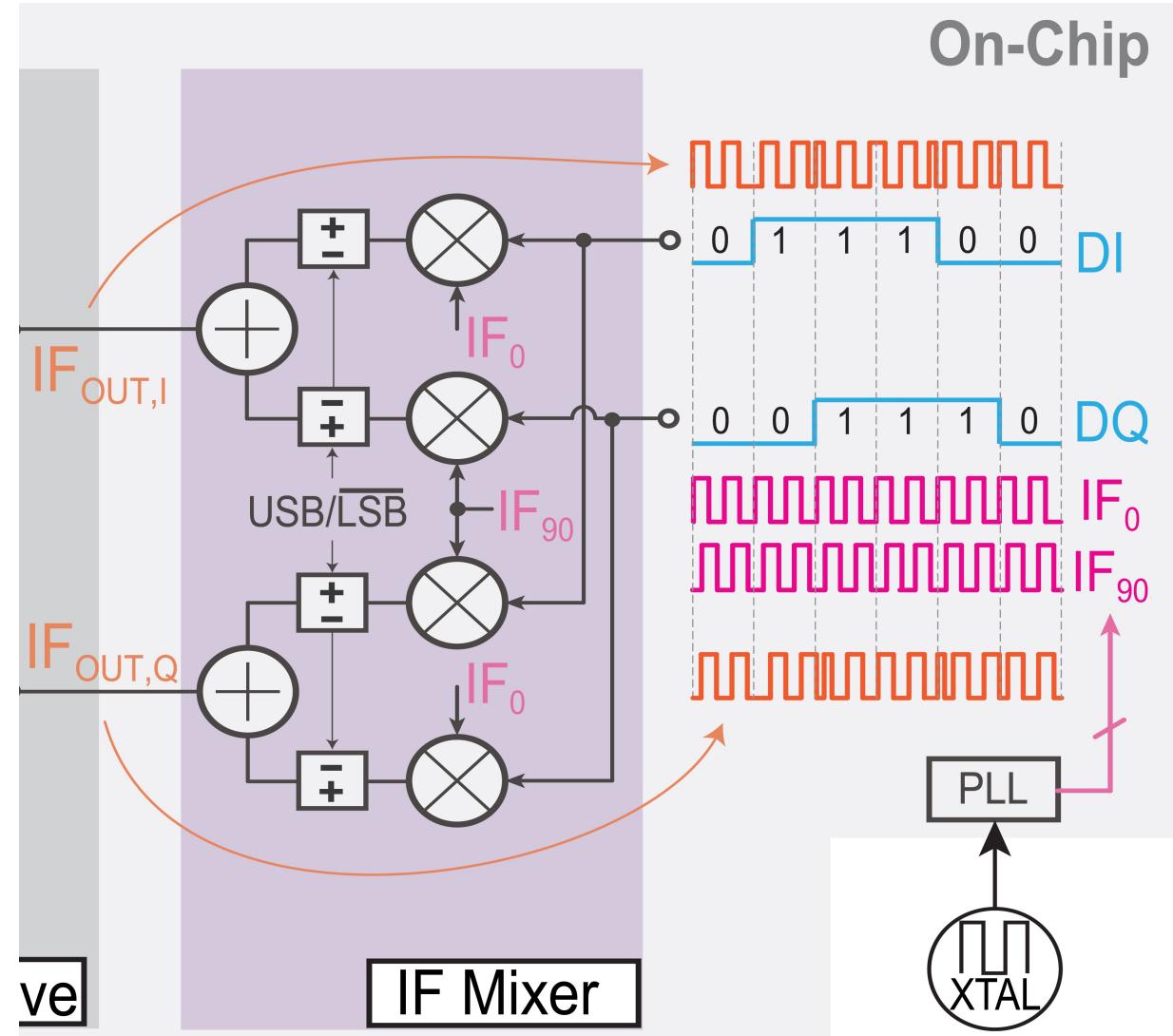


12.2: Improving the Range of WiFi Backscatter Via a Passive Retro-Reflective Single-Side-Band-Modulating MIMO Array and Non-Absorbing Termination

Proposed fully-reflective SSB QPSK backscatter

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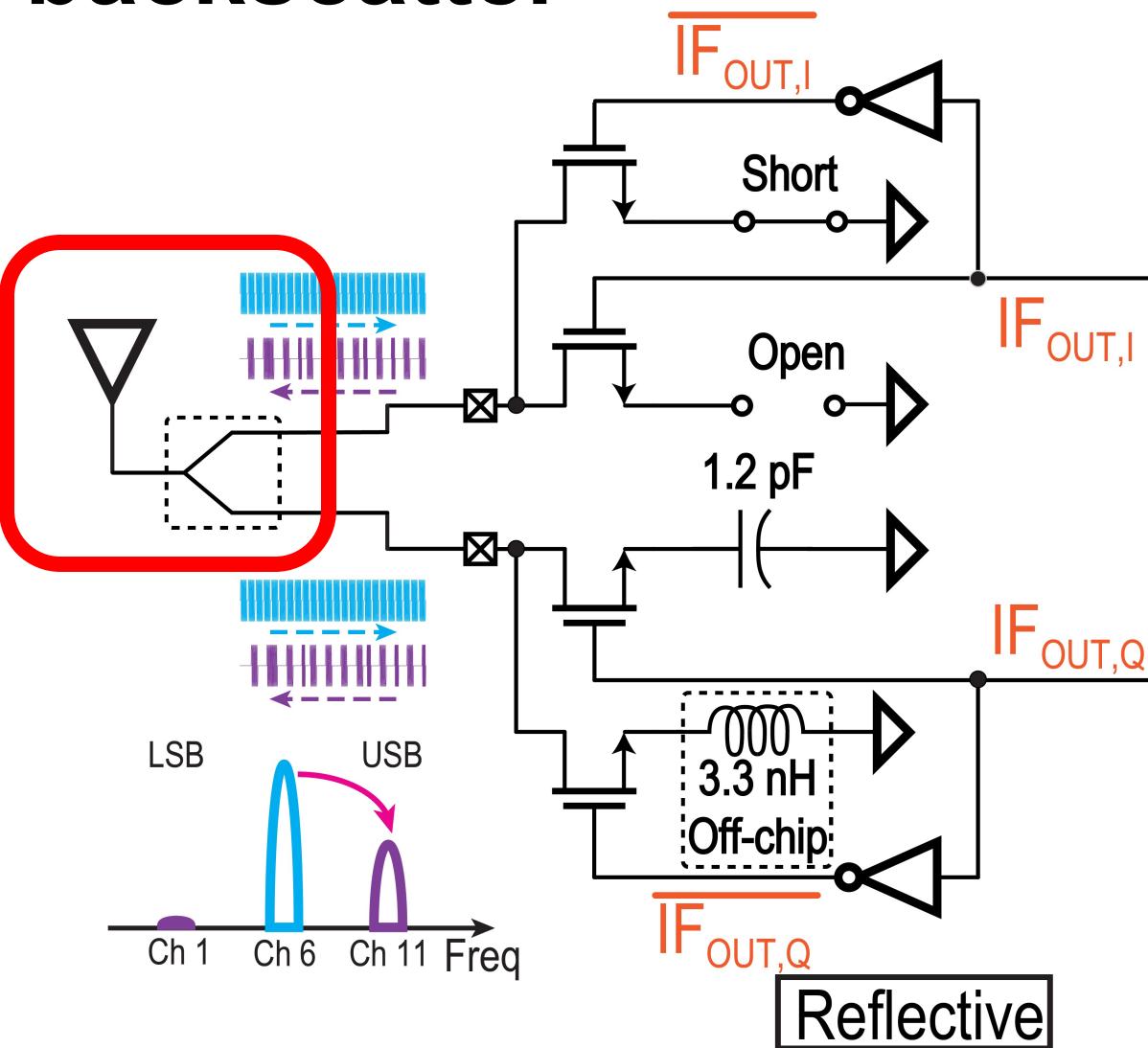
- IQ tag data is first upconverted to IF via a SSB digital mixer



12.2: Improving the Range of WiFi Backscatter Via a Passive Retro-Reflective Single-Side-Band-Modulating MIMO Array and Non-Absorbing Termination

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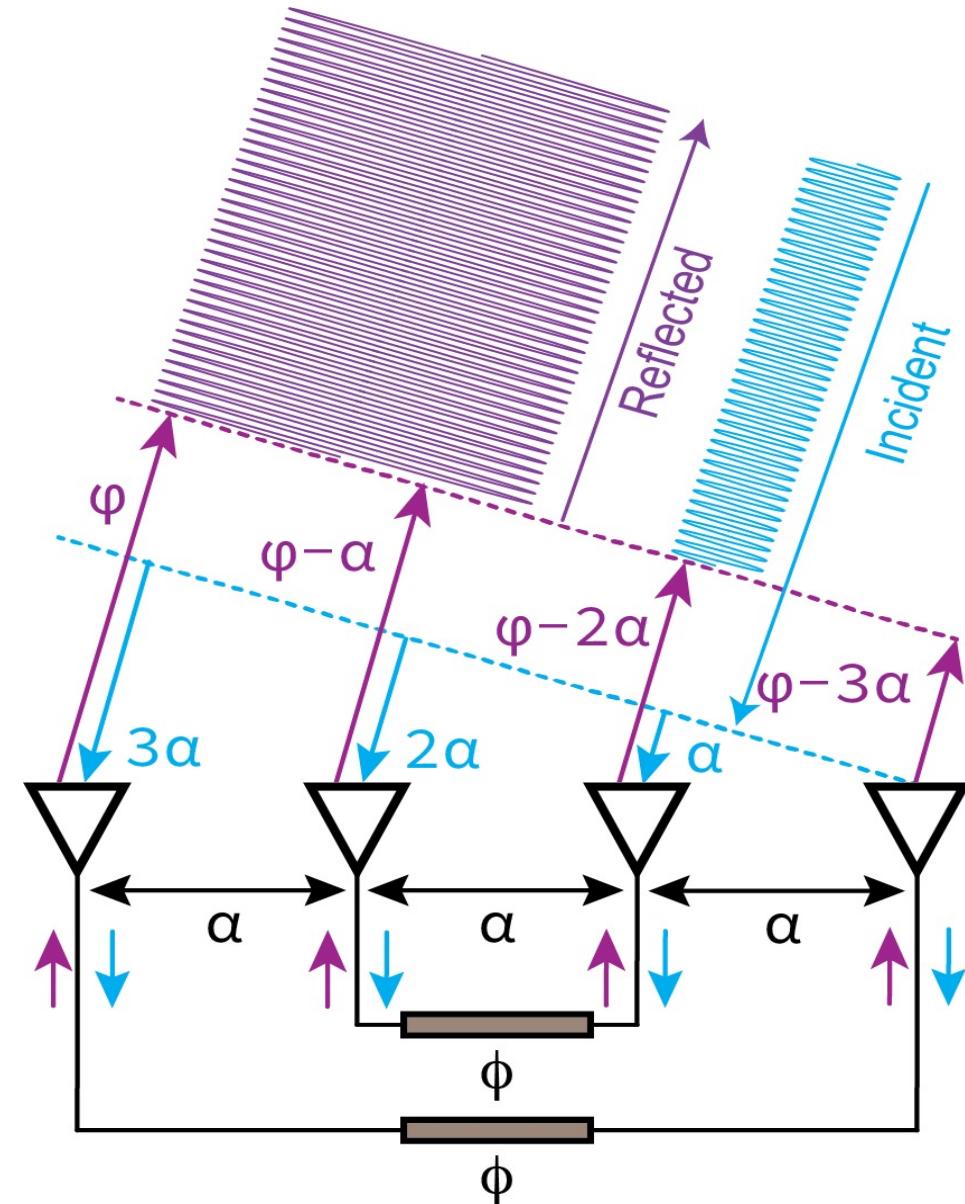
Proposed fully-reflective SSB QPSK backscatter



- Two 90° separated loads provide 90° rotated reflection coefficients
 - $Z_{L,0} = \text{open}; \Gamma_{L,0} = 1 = e^{j \times 0^\circ}$
 - $Z_{L,180} = \text{short}; \Gamma_{L,180} = -1 = e^{-j \times 180^\circ}$
 - $Z_{L,90} = j \times 50 = 3.3\text{nH}@2.4\text{GHz}; \Gamma_{L,90} = -j = e^{j \times 90^\circ}$
 - Quadrature IF signal modulates quadrature RF loading => SSB backscattering
 - ☒ Power splitter => Insertion loss
 - ☒ Single antenna => No gain
- Improve insertion loss by 6dB without power cost!**

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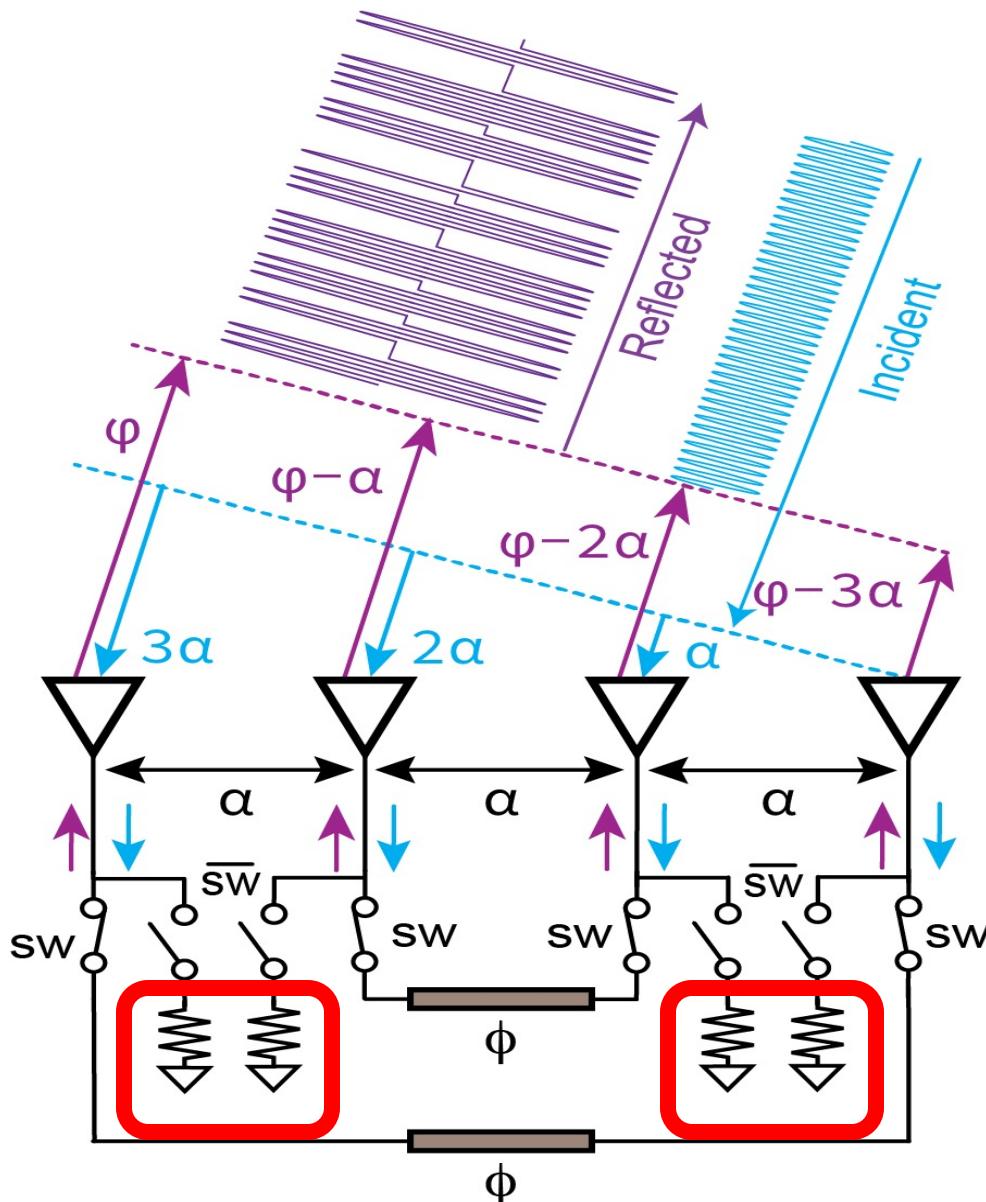
Passive MIMO – Van Atta antenna array



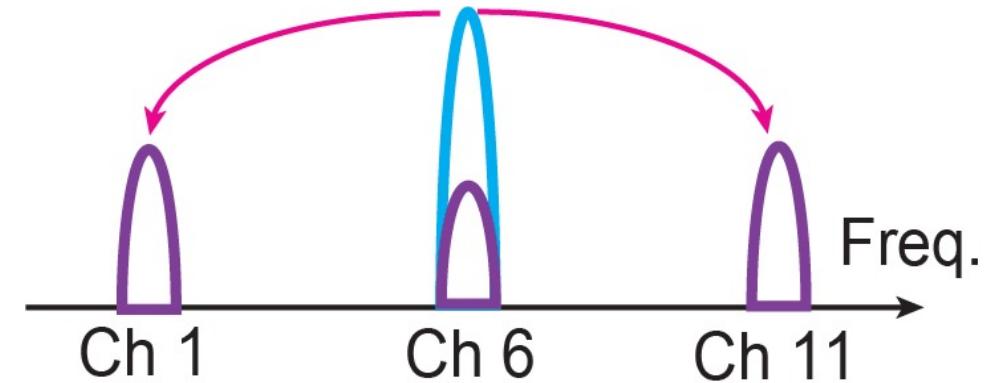
- Passively steers an incident beam back to its source with MIMO gain
- Reflected signal power is increased
- No data can be modulated onto reflected signal

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Passive MIMO: one possible implementation



- Modulated data is reflected with increased signal power
- Absorbing termination decreases signal power
- Double-side-band modulation occupies 2 adjacent channels

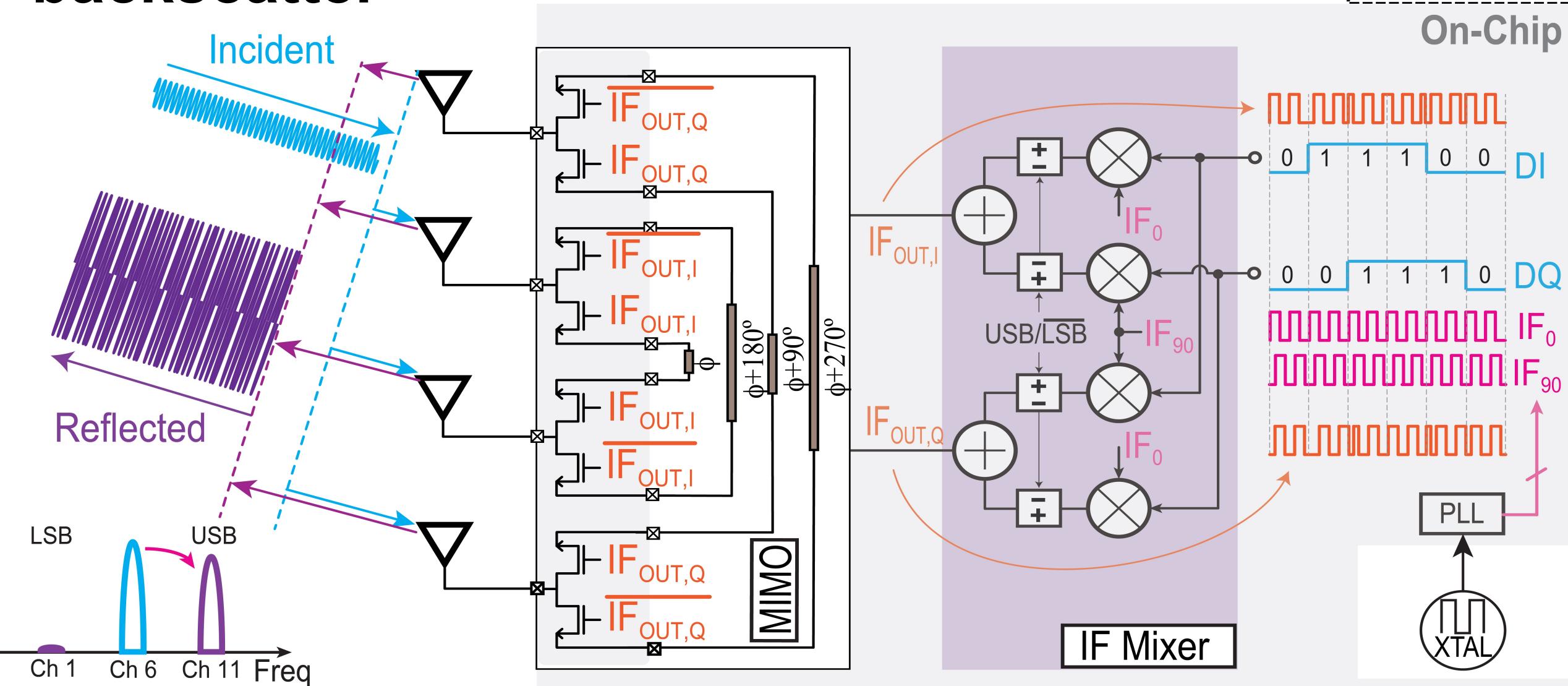


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Proposed retro-reflective SSB MIMO QPSK backscatter

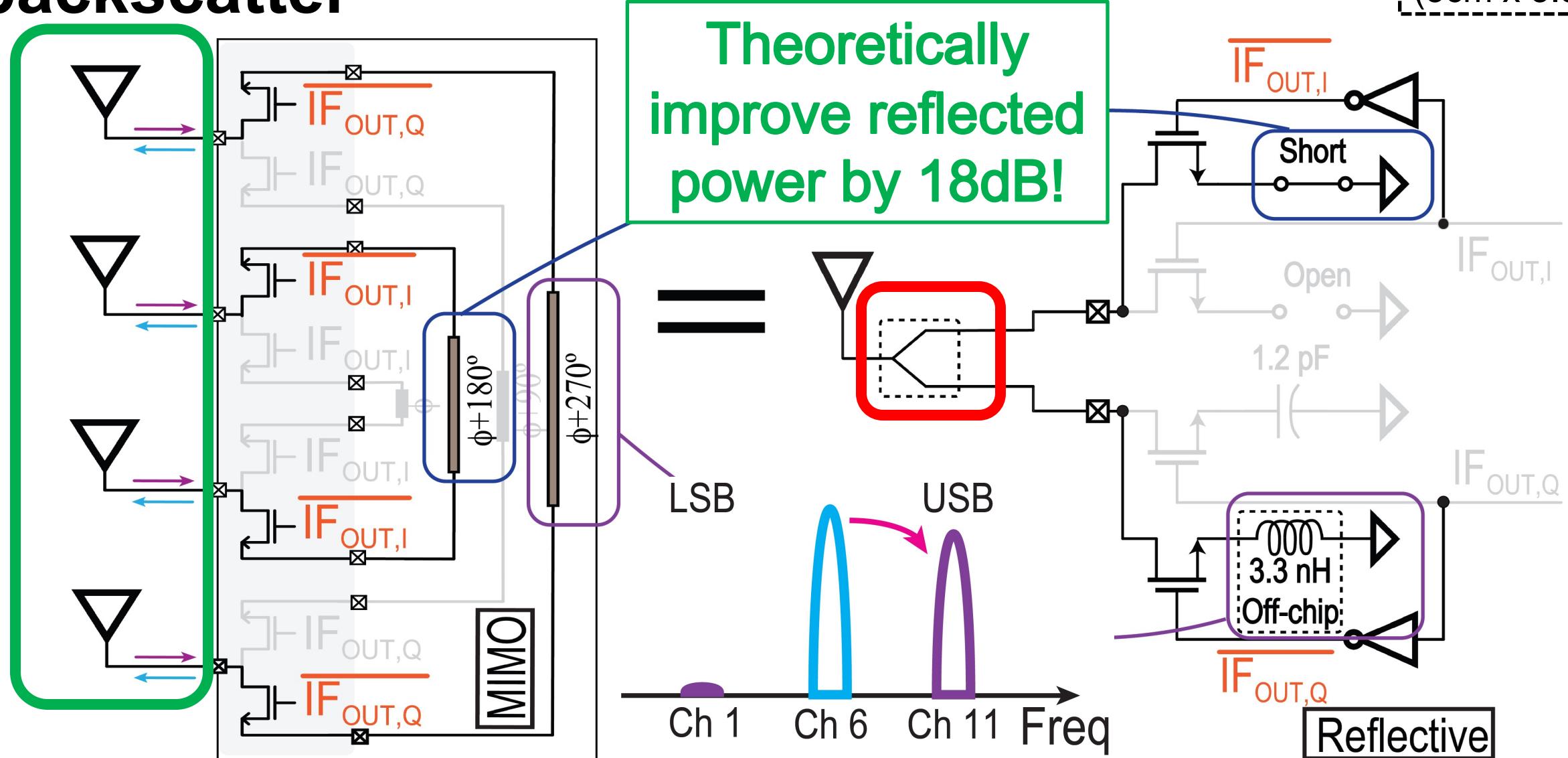
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On-Chip



Proposed retro-reflective SSB MIMO QPSK backscatter

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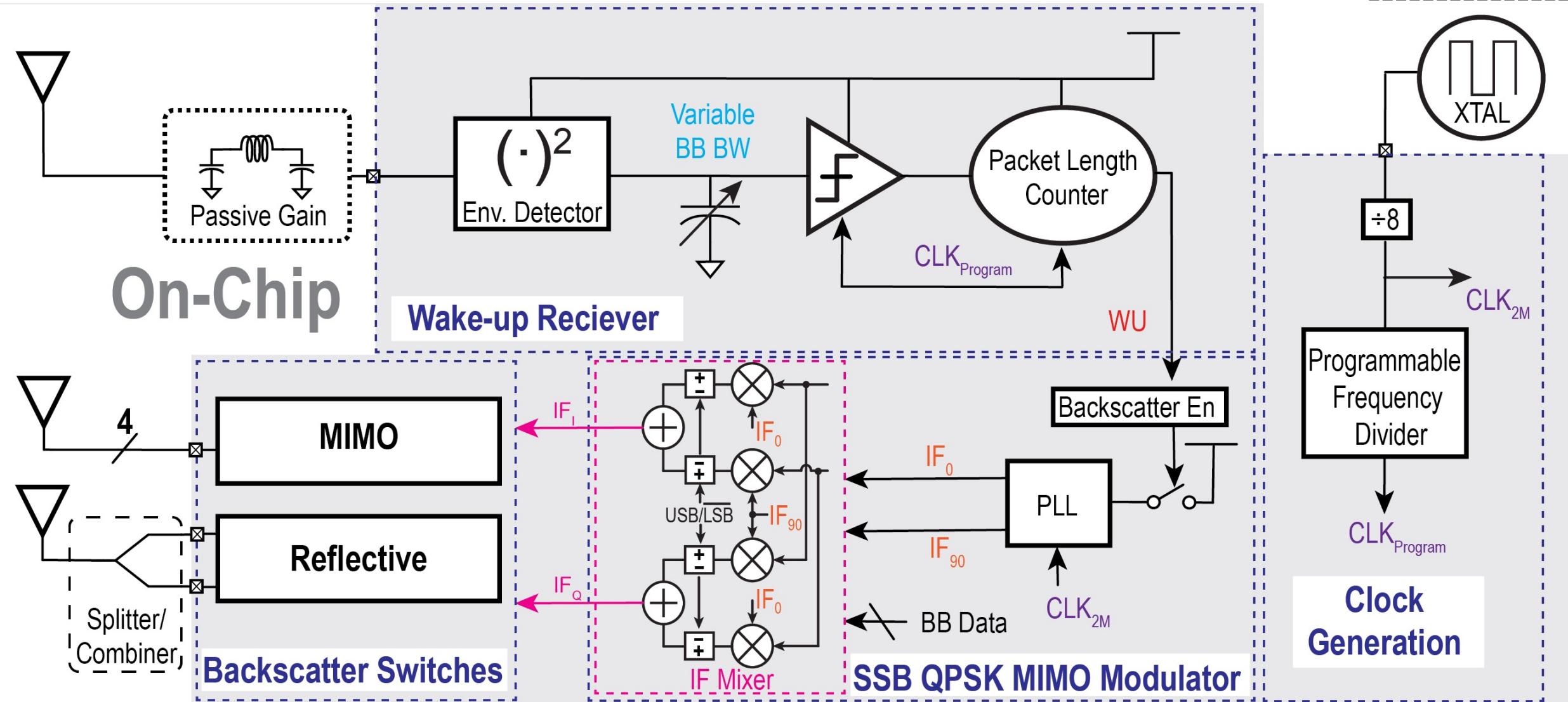
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- **Proposed fully-WiFi-compliant backscatter**
- Circuit implementation
- Measurement results
- Conclusion

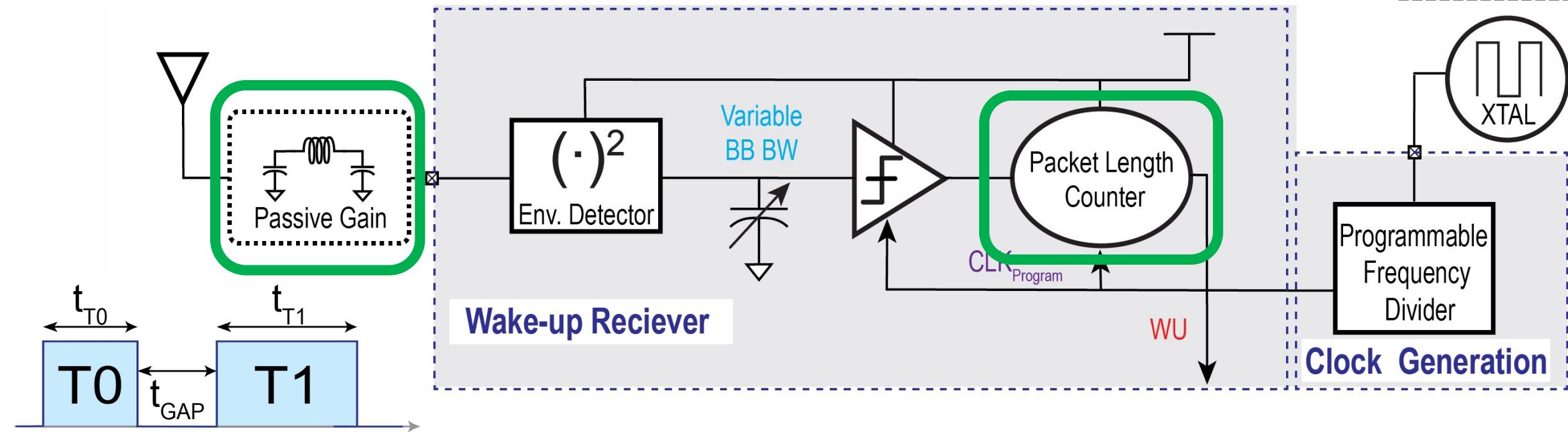
Block diagram of proposed IoT tag

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Block diagram of downlink

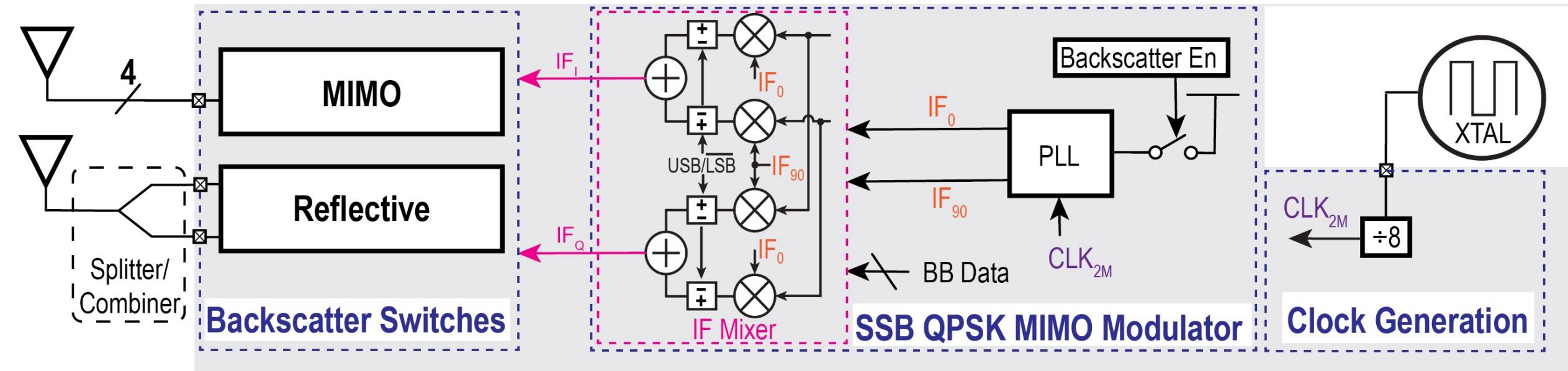
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- Direct envelope detection architecture for low standby power
- 8dB passive voltage gain from input matching network
- WiFi packets counter supports robust WiFi compatible wake-up and multi-tag wake-up regardless of the length of inter-packet gaps

Block diagram of uplink

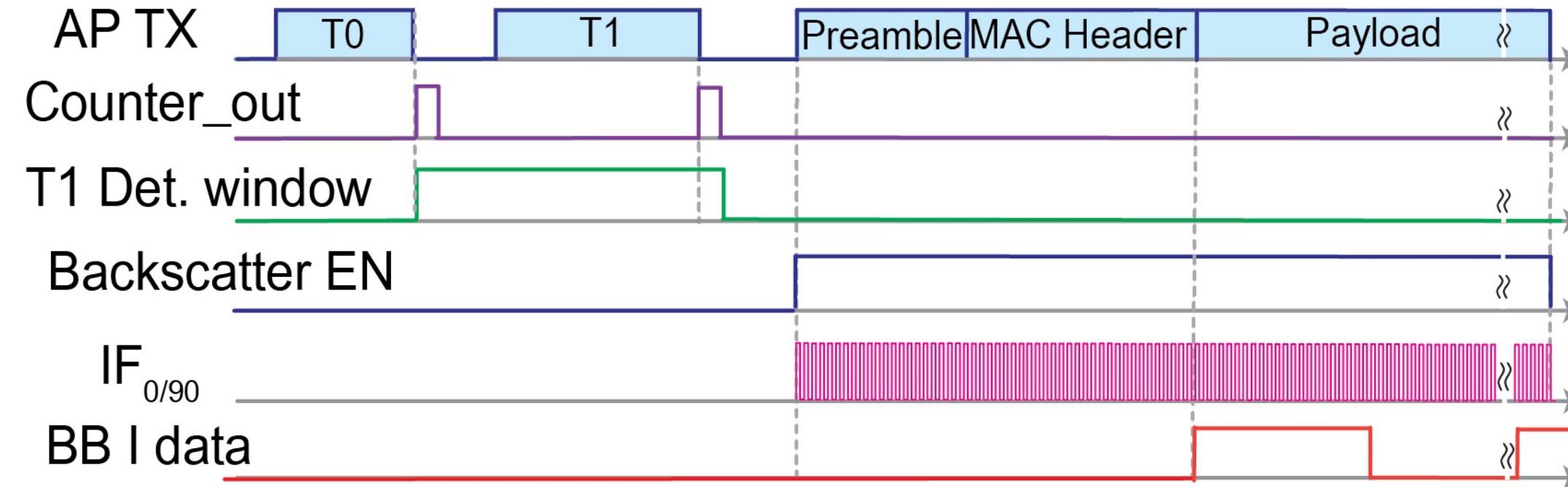
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- A PLL based backscatter modulator enabled by wake-up signal
- PLL provides 25/50MHz frequency translation for backscatter
- IF mixer controls impedance loading for tag data modulation

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Wake up and backscatter timing



- Robust WiFi-compatible wake-up regardless of the length of gaps between T0 and T1
- A PLL based backscatter modulator enabled by wake-up signal
- PLL provides 25/50MHz frequency translation for backscatter
- IF mixer controls impedance loading for tag data modulation

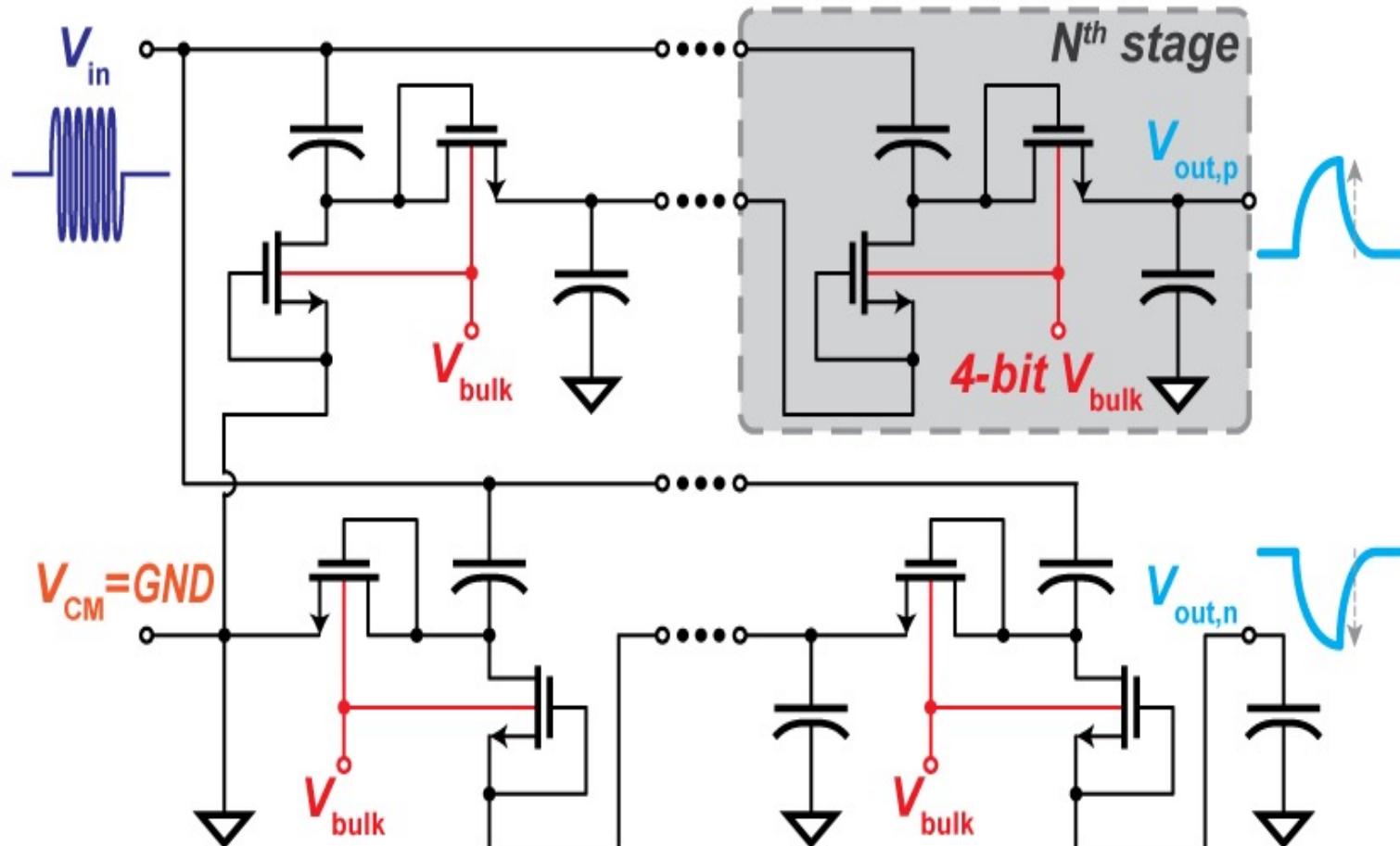
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Passive pseudo-balun envelop detector

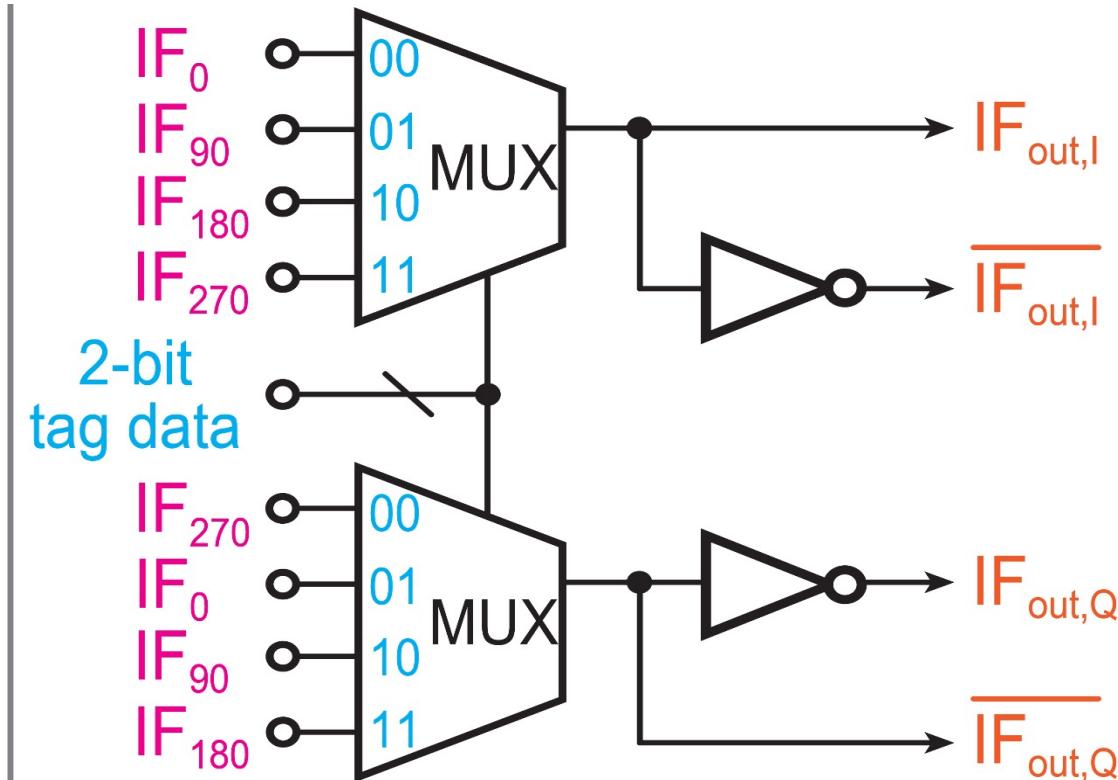
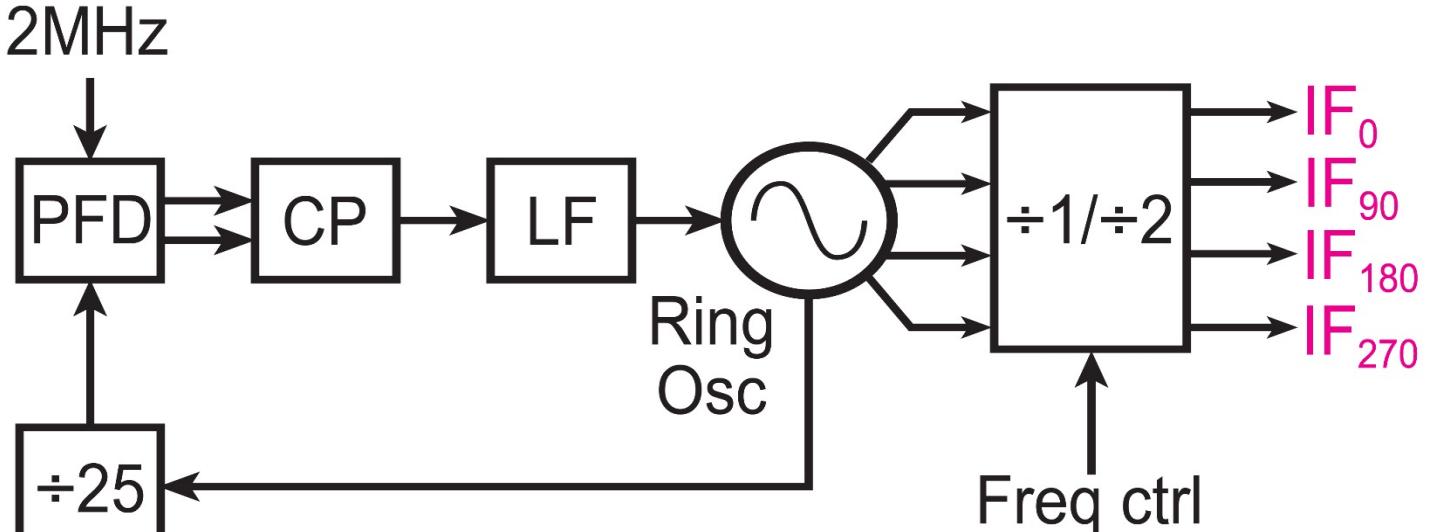


- Single-ended input RF to differential output BB signal
- 2× conversion gain w/o output BW penalty
- 1.5dB sensitivity improvement
- Tunable V_{th} via DNW device bulk control for PVT

Wang et al., SSCL'18

PLL and digital SSB IF mixer

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- Ring oscillator based integer- N PLL: 4-phase of output
- Digital SSB IF mixer

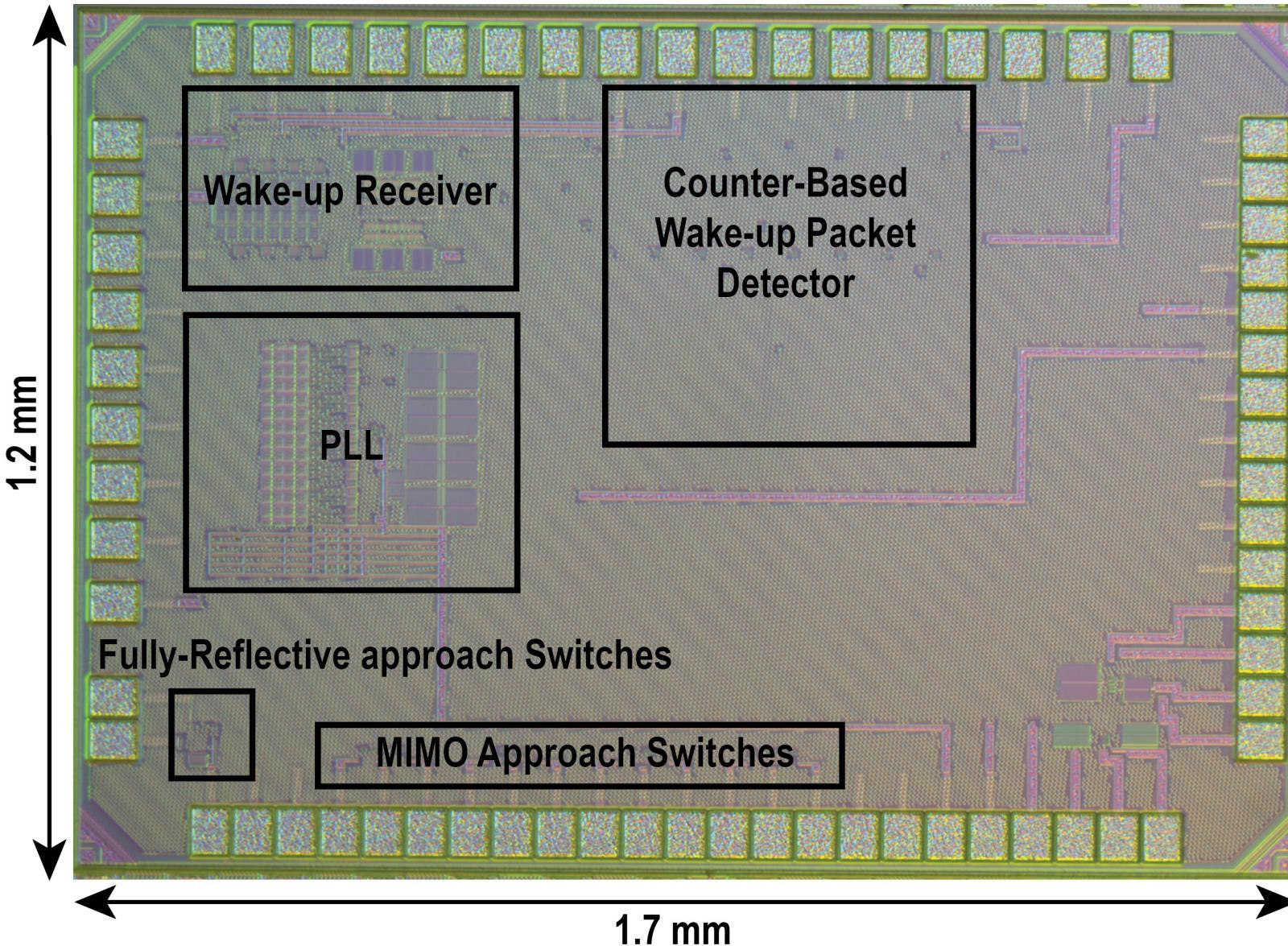
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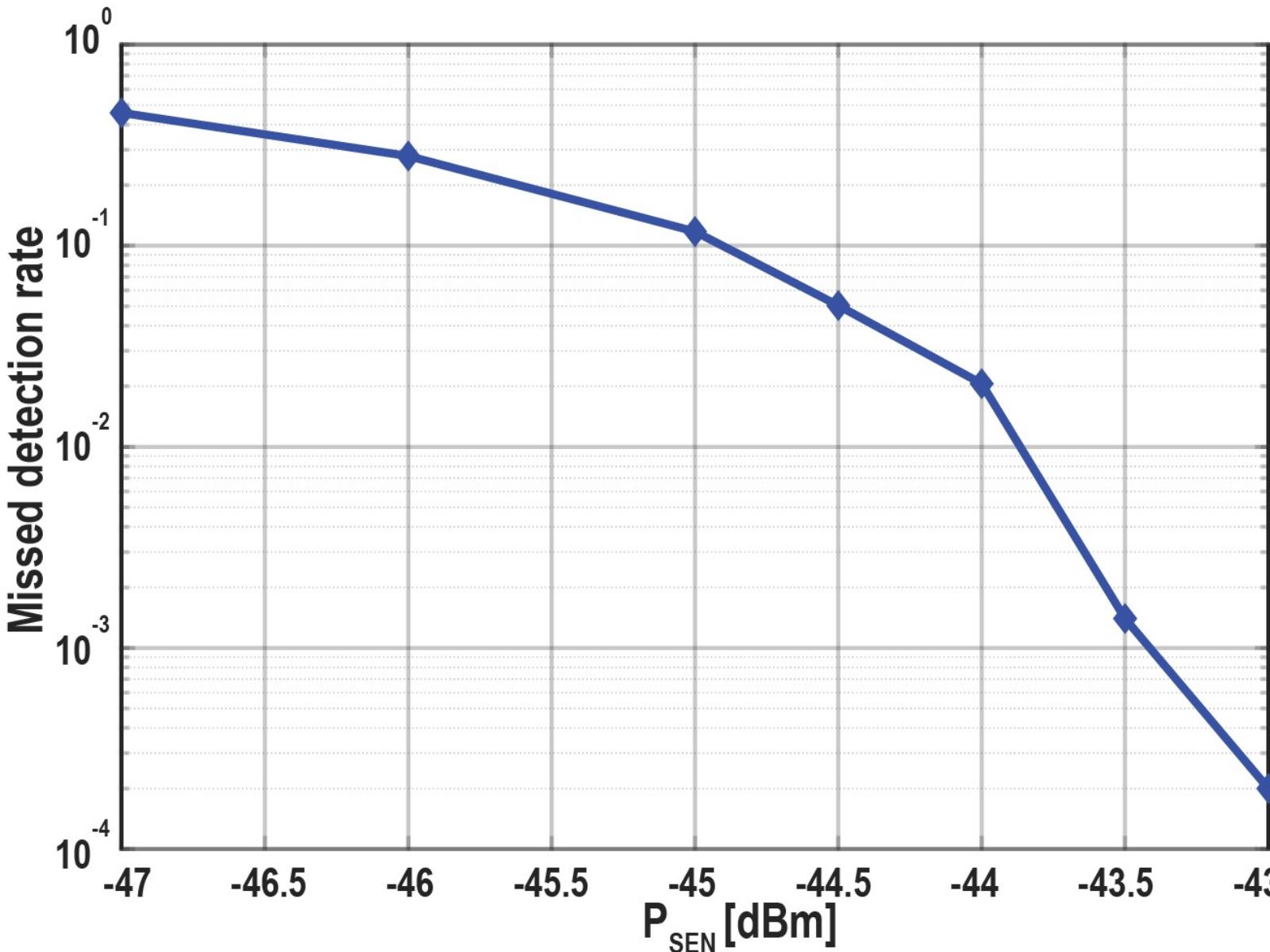
Die micrograph



- 65nm CMOS
- 0.44mm^2 active area

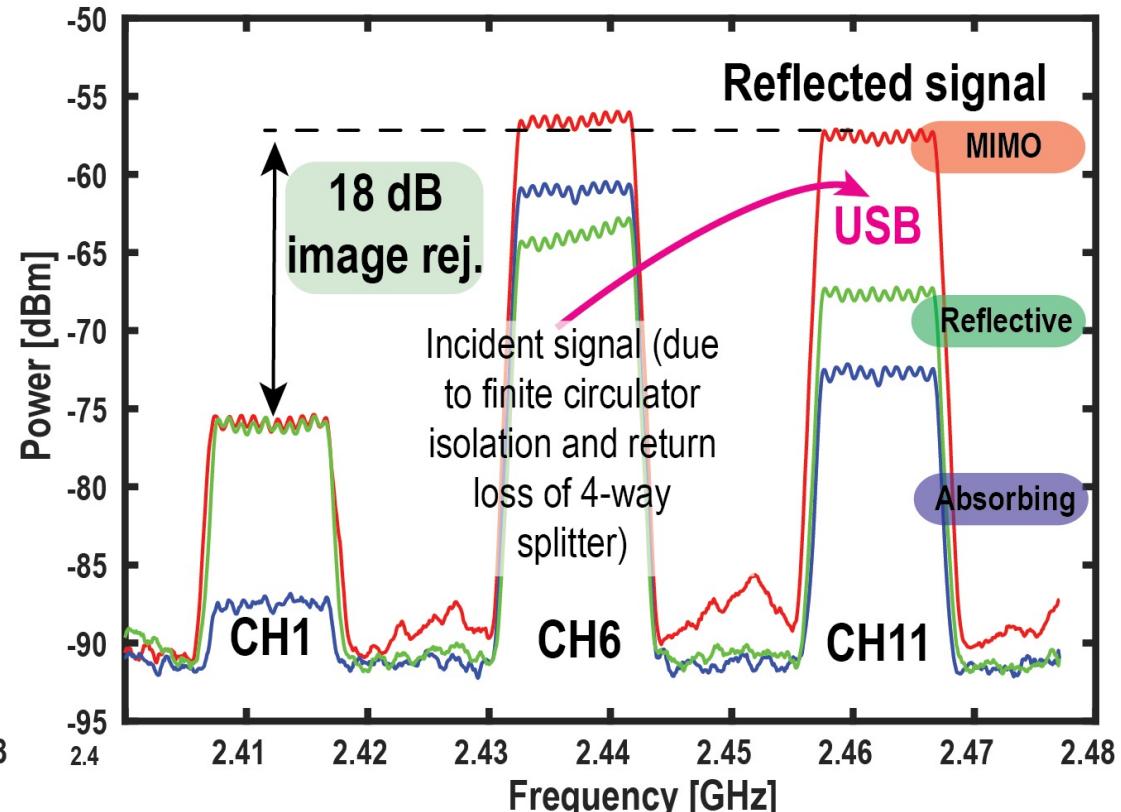
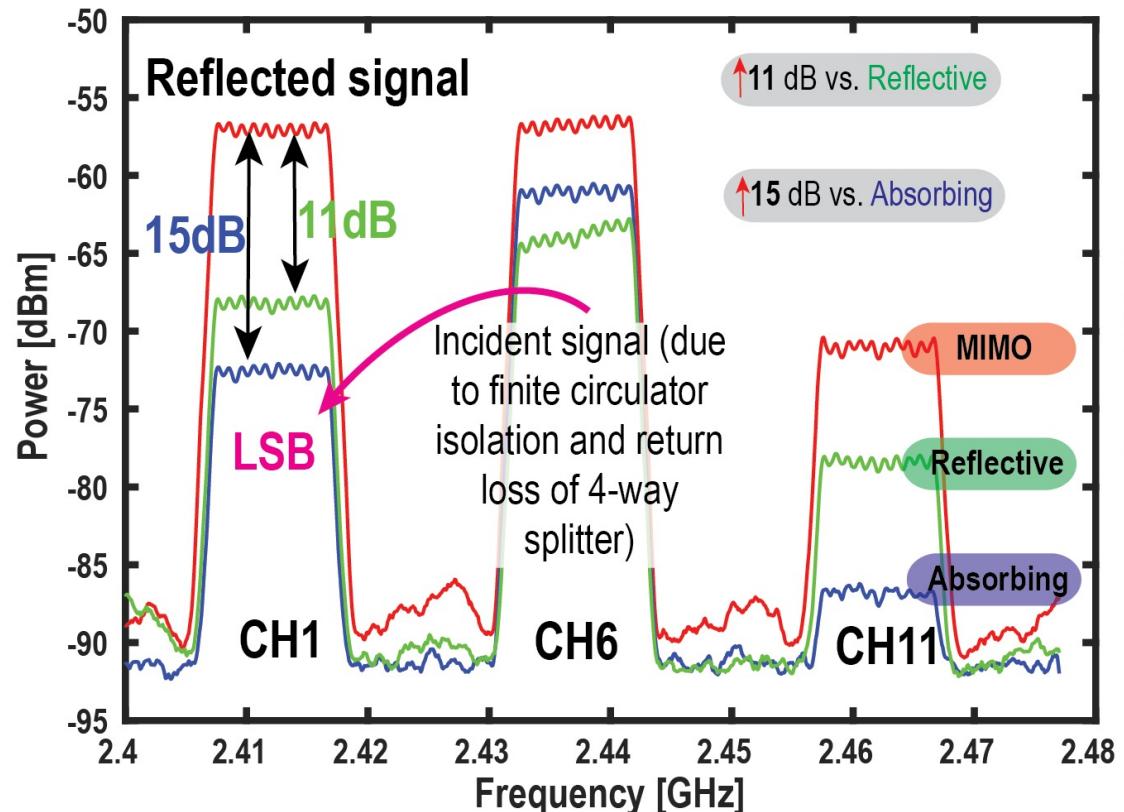
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Downlink sensitivity



- -43.4dBm downlink sensitivity for 1e-3 wake-up event missed detection rate
- > 30m wake-up range

SSB frequency translation



- Incident signal at CH6 reflected to either CH1 or CH11 based on logic setting with up to 18dB image rejection
- 11dB improvement of passive MIMO compared to reflective method and 15dB improvement over absorbing method

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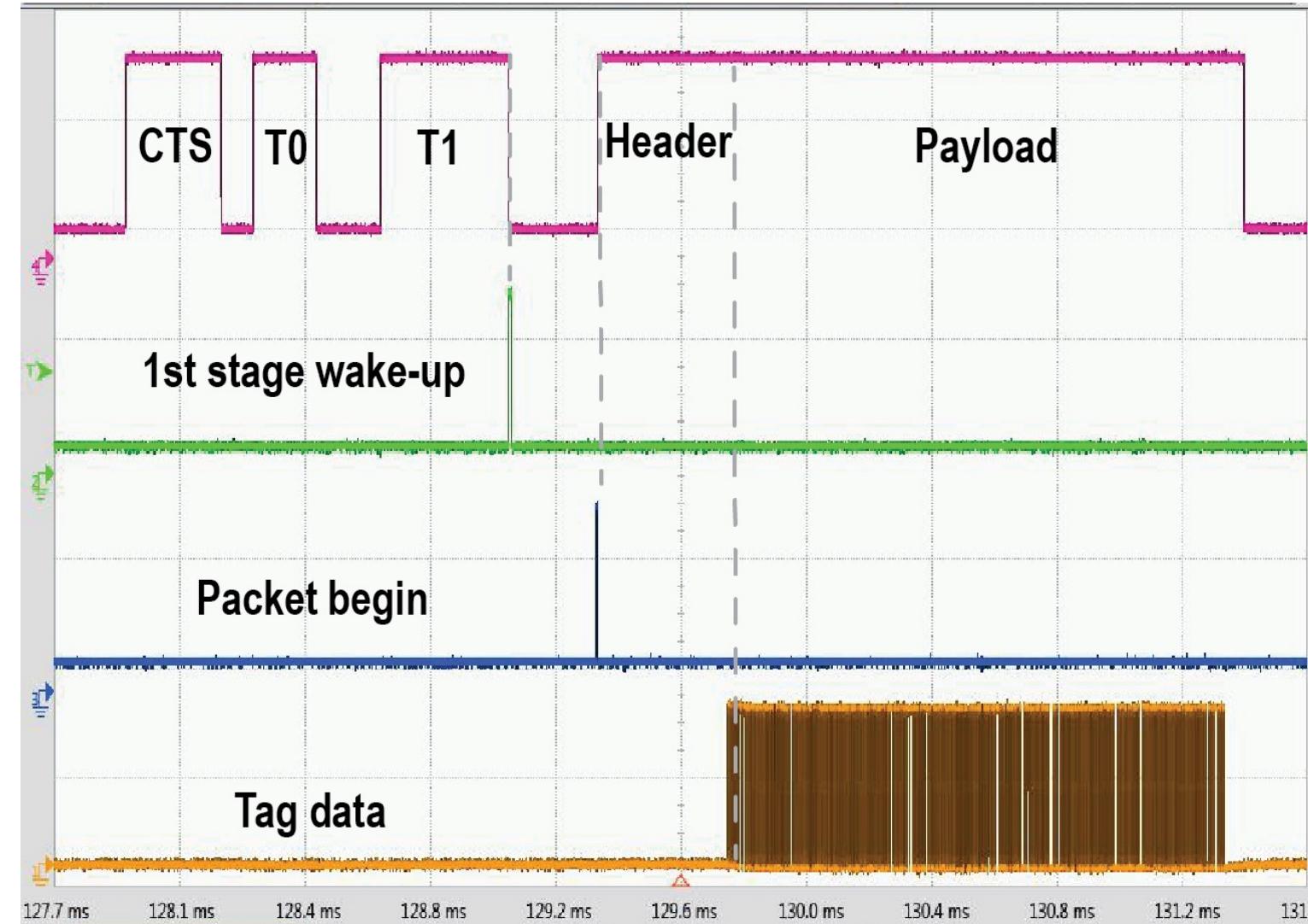
Wake-up and backscatter transient measurement

Packet envelope

Wake-up signal

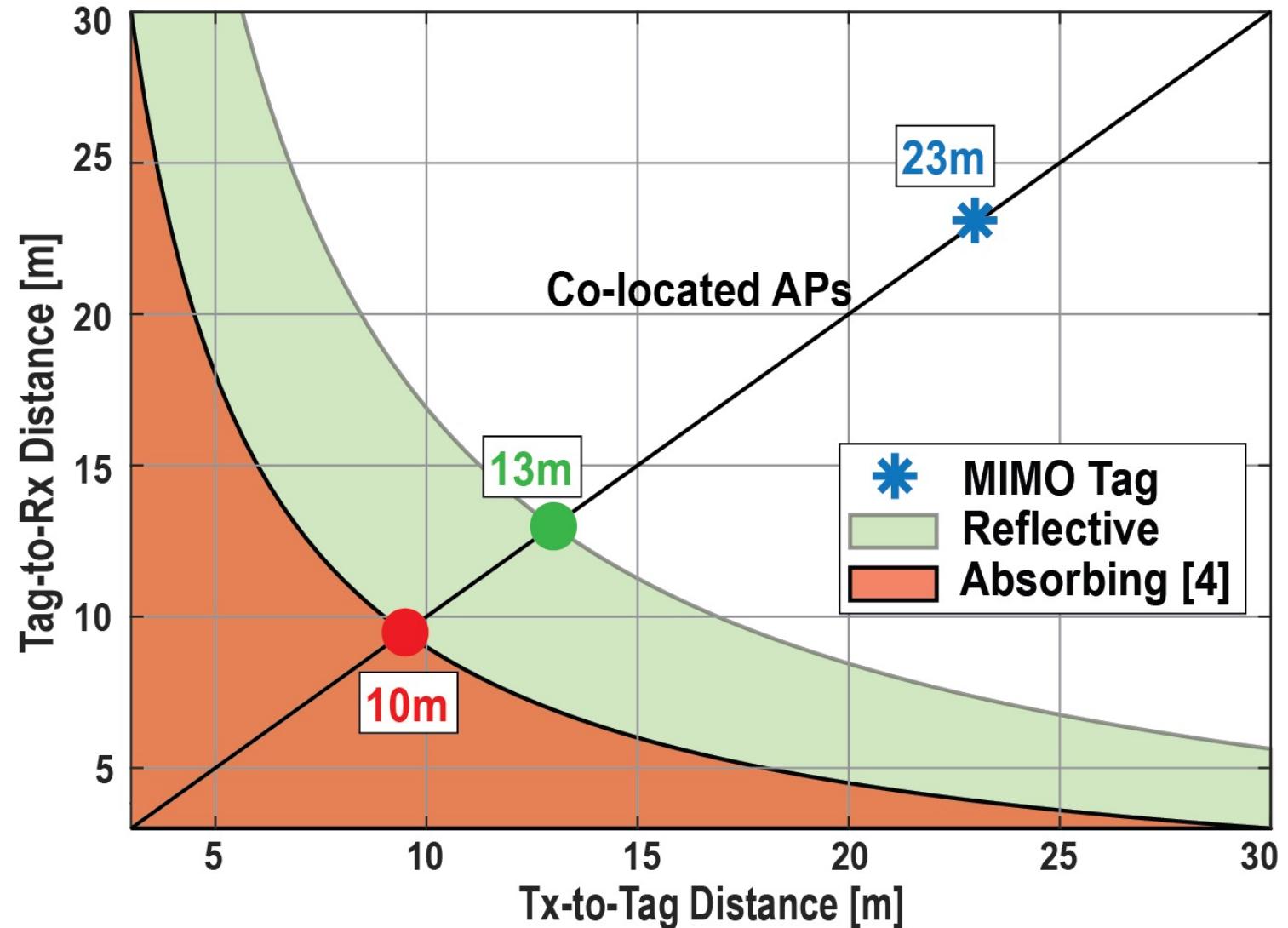
Backscatter En

Tag data



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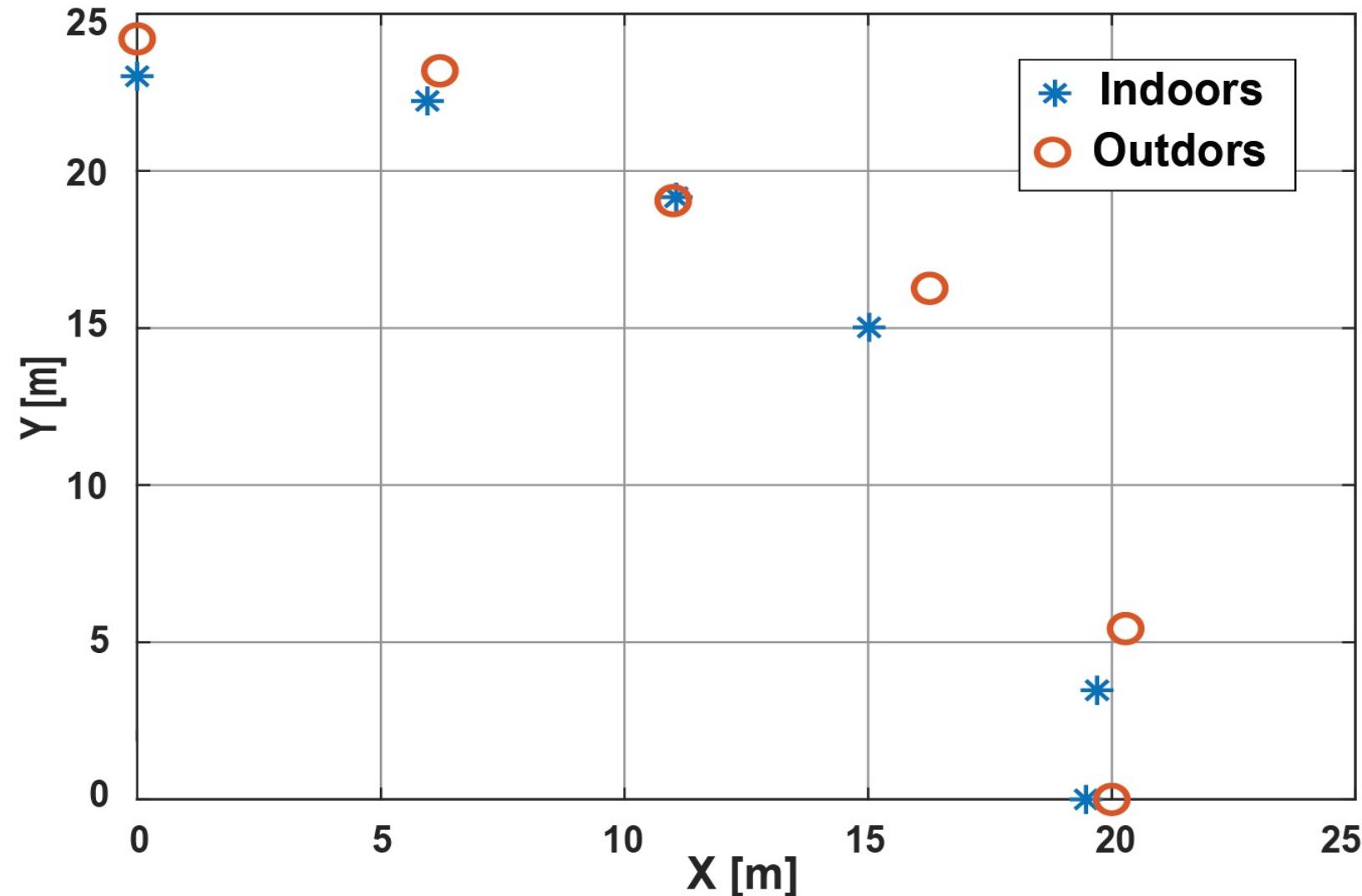
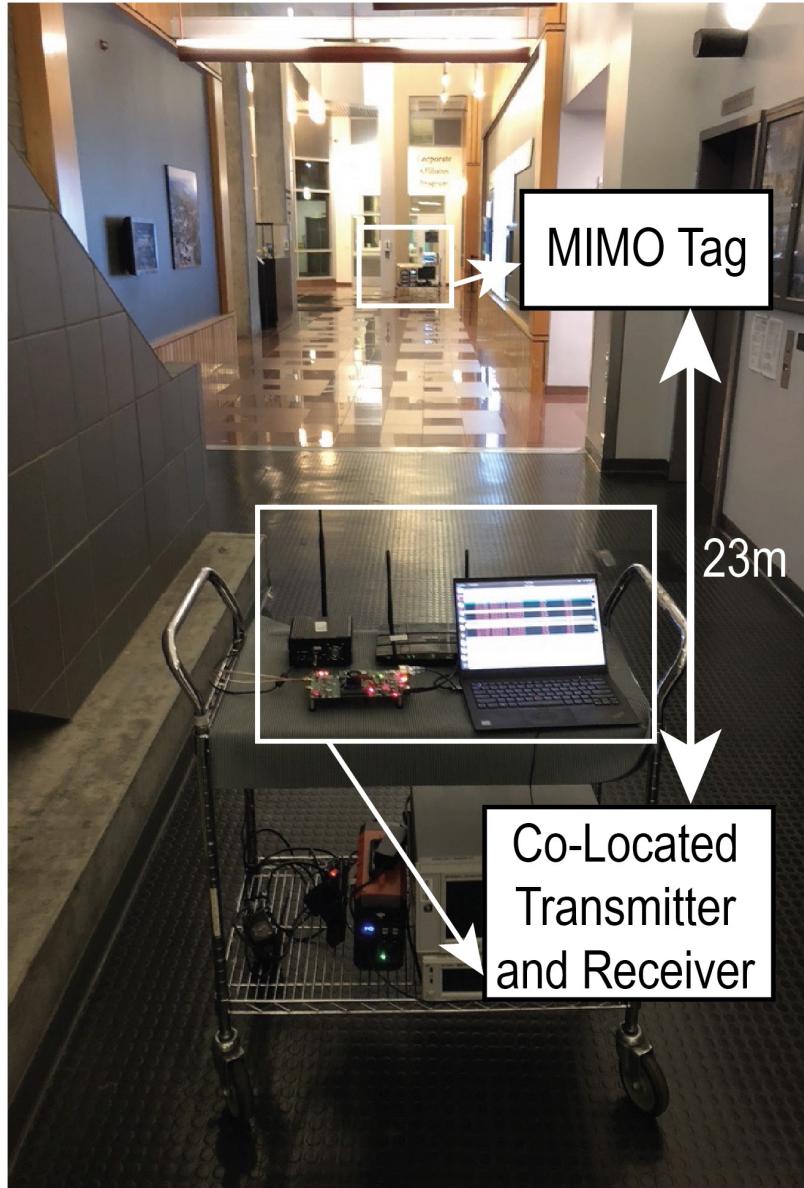
Wireless experiment - range



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Wireless experiment - angle

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Comparison to prior art

	[1]	[2]	[3]	[4]	This work	
					Fully-Reflective	MIMO
Technology (nm)	65	NA	NA	65	65	
Scheme	Backscatter	Backscatter	SSB WiFi Backscatter	SSB Partially Absorbing WiFi Backscatter	SSB Fully Reflective WiFi Backscatter	SSB Passive Retro-Reflective MIMO WiFi Backscatter
Frequency (GHz)	5.8	2.4	2.4	2.4	2.4	
Incident signal source	Tone Transmitter	Tone Transmitter	WiFi	WiFi	WiFi	WiFi
Wake-up power (μW)	8.2	18 (COTS)	NA	2.8	4.5	
Backscatter communication power (μW)	113	59.2**	33**	28	32	38
Range: equidistance TX and RX (m)	0.1	4.6	6	10.5	13	>23

*Simulated

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Conclusion

- The first IC demonstrating WiFi-compatible passive MIMO backscatter communication to cover $>1600\text{ m}^2$ area towards pragmatic adoption in home and office environment
- A fully-reflective backscatter communication with $\sim 13\text{ m}$ communication range for device-area-restricted applications
- Low power: A $4.5\mu\text{W}$ standby power, $32\mu\text{W}$ for fully reflective and $38\mu\text{W}$ for passive MIMO
- Acknowledgement: This work was supported in part by the National Science Foundation (NSF) under Grant No. 1923902.