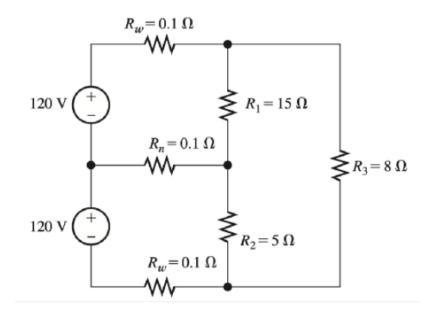
- 5. (35 points) The circuit shown in Figure 4.1 is the dc equivalent of a simple residential power distribution system. Each of the resistances labeled R<sub>1</sub> and R<sub>2</sub> represents various parallel-connected loads, such as lights or devices plugged into outlets that nominally operate at 120 V, while R<sub>3</sub> represents a load, such as the heating element in an oven that nominally operates at 240 V. The resistances labeled R<sub>W</sub> represent the resistances of wires. R<sub>R</sub> represents the "neutral" wire.
- a) Use mesh-current analysis to determine the voltage magnitude for  $R_n$  (10pts). Write the equations in matrix form (5pts). Use Matlab (or any other software) to solve the equations (5 pts).
- b) Now suppose that due to a fault in the wiring at the distribution panel, the neutral wire becomes an open circuit. Again compute the voltages across the loads (10pts) and comment on the probable outcome for a sensitive device such as a computer or plasma television that is part of the 15Ω load (5pts).



## Circuit labeling (so our equations match)

- Top "hot" node on the right: A
- Middle node on the right (where the neutral wire connects): B
- Bottom "hot" node on the right: C

## Components:

- Wire resistances  $R_w=0.1~\Omega$  on the top and bottom rails
- Neutral wire  $R_n=0.1~\Omega$
- Loads:  $R_1=15~\Omega$  (between A and B),  $R_2=5~\Omega$  (between B and C),  $R_3=8~\Omega$  (between A and C
- Two 120-V sources in series on the left (split-phase DC model), so top-left node is at 240 V, middle-left at 120 V, bottom-left at 0 V.

# (a) Mesh analysis to get the neutral voltage $V_n$

## Choose clockwise mesh currents

- $i_1$ : top-left rectangular loop (through top  $R_w$ ,  $R_1$ ,  $R_n$ , and the upper 120-V source)
- $i_2$ : bottom-left rectangular loop (through bottom  $R_w$ ,  $R_2$ ,  $R_n$ , and the lower 120-V source)
- $i_3$ : right rectangular loop (through  $R_1, R_2, R_3$ )

#### KVL for each mesh

(Shared elements appear with opposite signs; the source term is +120 for both left meshes because, traversed clockwise, each source is crossed from - to +.)

$$( ext{Top mesh}) \quad (R_w + R_1 + R_n)i_1 - R_ni_2 - R_1i_3 = +120$$
 $( ext{Bottom mesh}) \quad -R_ni_1 + (R_w + R_2 + R_n)i_2 - R_2i_3 = +120$ 
 $( ext{Right mesh}) \quad -R_1i_1 - R_2i_2 + (R_1 + R_2 + R_3)i_3 = 0$ 

#### Matrix form

$$\underbrace{\begin{bmatrix} R_w + R_1 + R_n & -R_n & -R_1 \\ -R_n & R_w + R_2 + R_n & -R_2 \\ -R_1 & -R_2 & R_1 + R_2 + R_3 \end{bmatrix}}_{\mathbf{A}} \begin{bmatrix} i_1 \\ i_2 \\ i_3 \end{bmatrix} = \underbrace{\begin{bmatrix} 120 \\ 120 \\ 0 \end{bmatrix}}_{\mathbf{b}}$$

Plugging  $R_w=R_n=0.1\,\Omega$ ,  $R_1=15\,\Omega$ ,  $R_2=5\,\Omega$ ,  $R_3=8\,\Omega$  and solving  ${\bf Ai}={\bf b}$  gives

$$oxed{i_1 = 36.75 ext{ A}}, \quad oxed{i_2 = 51.56 ext{ A}}, \quad oxed{i_3 = 28.89 ext{ A}}$$

These are the currents circulating in the three meshes; note that  $i_1$  equals the current in the **top**  $R_w$ ,  $i_2$  equals the (left-to-right reference) current in the **bottom**  $R_w$ , and  $i_3$  equals the current in  $R_3$ .

### Neutral voltage.

The current through the neutral resistor is the difference of the two left meshes across the shared  $R_n$ :  $i_n = i_2 - i_1$ .

Therefore

$$oxed{V_n = R_n(i_2 - i_1) = 0.1(51.56 - 36.75) = 1.48 ~
m V}$$

(magnitude). This matches the key.

## Sanity check via node voltages (optional but reassuring):

$$V_A = 240 - i_1 R_w = 236.33 \text{ V}, \quad V_B = 120 - V_n = 118.52 \text{ V}, \quad V_C = i_2 R_w = 5.157 \text{ V}.$$

## (b) Open neutral (fault): compute voltages across the loads

With  $R_n$  open, node B floats;  $R_1$  and  $R_2$  become a series string between A and C. Solve by nodal KCL at A, B, C:

$$\begin{split} \frac{V_A - 240}{R_w} + \frac{V_A - V_B}{R_1} + \frac{V_A - V_C}{R_3} &= 0\\ \frac{V_B - V_A}{R_1} + \frac{V_B - V_C}{R_2} &= 0\\ \frac{V_C - 0}{R_w} + \frac{V_C - V_B}{R_2} + \frac{V_C - V_A}{R_3} &= 0 \end{split}$$

Solving gives

$$V_A = 235.942 \text{ V}, \qquad V_B = 62.029 \text{ V}, \qquad V_C = 4.058 \text{ V}.$$

Hence the load voltages are

$$oxed{V_{R_3} = V_A - V_C = 231.884 \, ext{V}}, \qquad oxed{V_{R_1} = V_A - V_B = 173.913 \, ext{V}}, \qquad oxed{V_{R_2} = V_B - V_C = 57.971 \, ext{V}},$$

exactly as in the key.

#### What this means physically.

With the neutral open, the 120-V loads  $R_1$  and  $R_2$  no longer sit with respect to a stiff 120-V reference. They form a divider across the hot-to-hot potential, so the mid-node B "floats" to a value set by the ratio  $R_1:R_2=3:1$ . That puts ~174 V across the 15- $\Omega$  branch and only ~58 V across the 5- $\Omega$  branch.

Power comparison (to see the danger):

$$P_{R_1} = rac{V_{R_1}^2}{R_1} pprox rac{(173.9)^2}{15} pprox 2.02 \ {
m kW} \quad {
m vs.} \quad rac{120^2}{15} = 0.96 \ {
m kW} \ ({
m normal}).$$

So the "120-V" devices on the  $15\,\Omega$  branch are severely **over-volted** (~45% high) and can fail catastrophically. The  $5\,\Omega$  branch is in brownout (~58 V), so devices there likely shut down or behave erratically.  $R_3$  (the 240-V load) remains close to nominal voltage, aside from small drops in the hot conductors.