



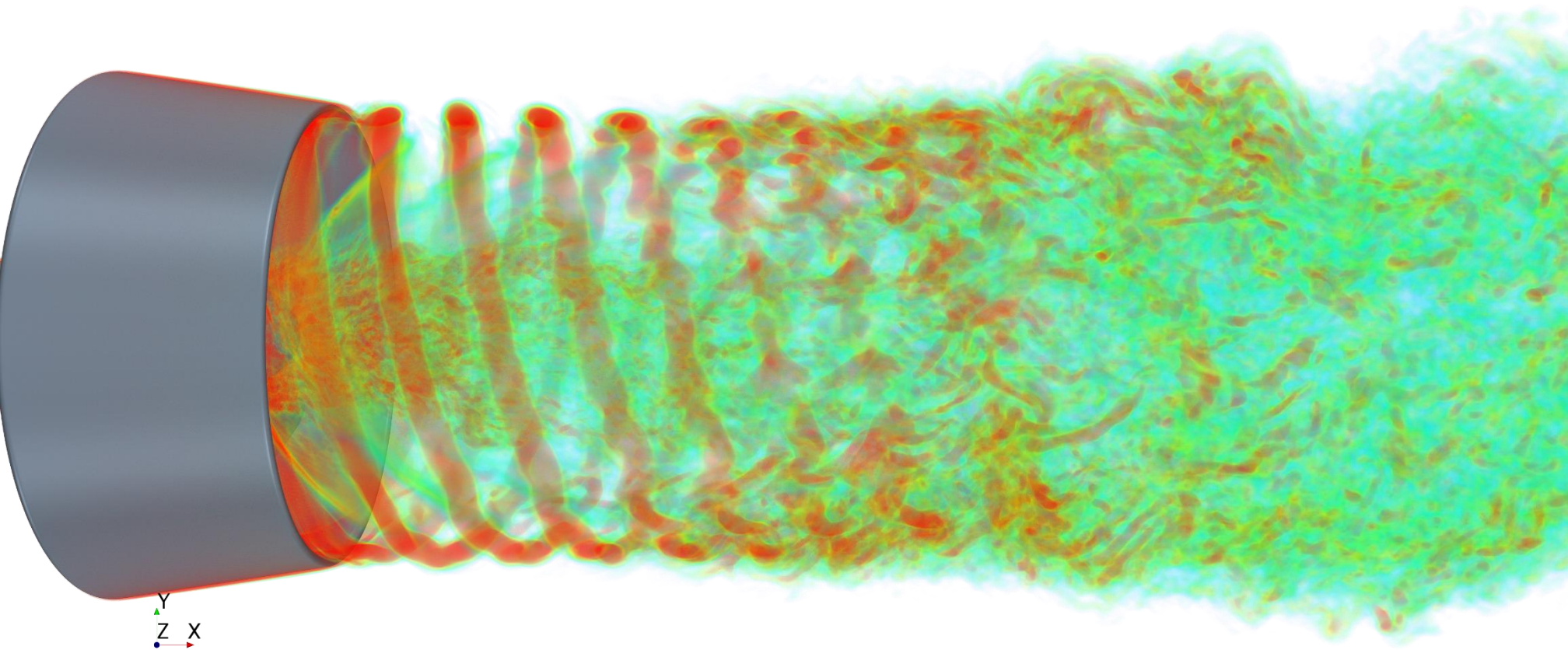
Research on the wake of the ducted propeller with POD and DMD

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The wake of the ducted propeller





- **Modal decomposition methods**
- **Overview of numerical simulation**
- **Data preprocessing**
- **Modes and reconstruction results display**

The snapshot matrix

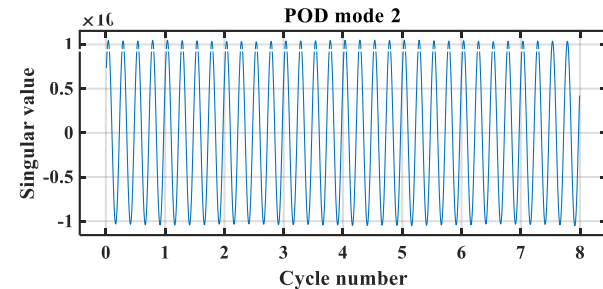
Singular value matrix

$$X = U \Sigma V^T$$

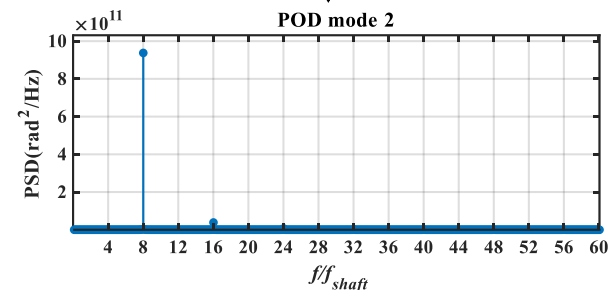
Right singular matrix

POD mode matrix

$$a_i(t) = \sigma_i v_i^T$$



FFT



Power spectral density
(PSD)



$$Y = AX$$

$$\Rightarrow A = YX^\dagger$$

$$\text{SVD: } X = U\Sigma V^T$$

$$\Rightarrow A' = U_r^T A U_r$$

EVD

$$\Rightarrow A' w_i = w_i \lambda_i$$

Dimensionality
reduction
projection

$$g_i = \text{real}(\ln(\lambda_i)) / \Delta t$$

$$\phi_i = U_r w_i$$

$$f_i = \text{imag}(\ln(\lambda_i)) / 2\pi \Delta t$$

$$\alpha_i = \phi_i^\dagger x_0$$

Creat two matrices:

```
X=matrix(:,1:end-1);
```

```
Y=matrix(:,2:end);
```

Compute the economy SVD of X:

```
[U,S,V] = svd(X, 'econ')
```

Compute the approximate matrix:

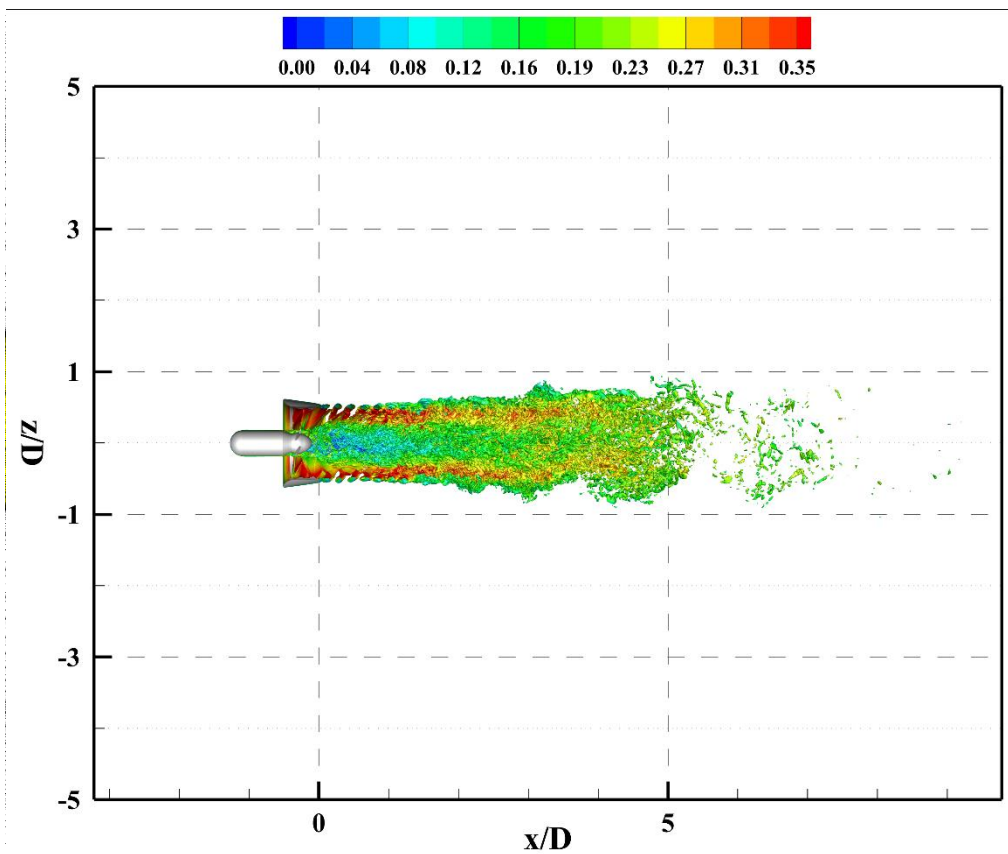
```
Atilde = U'*Y*V/S
```

Decompose:

```
[W, D] = eig(Atilde)
```

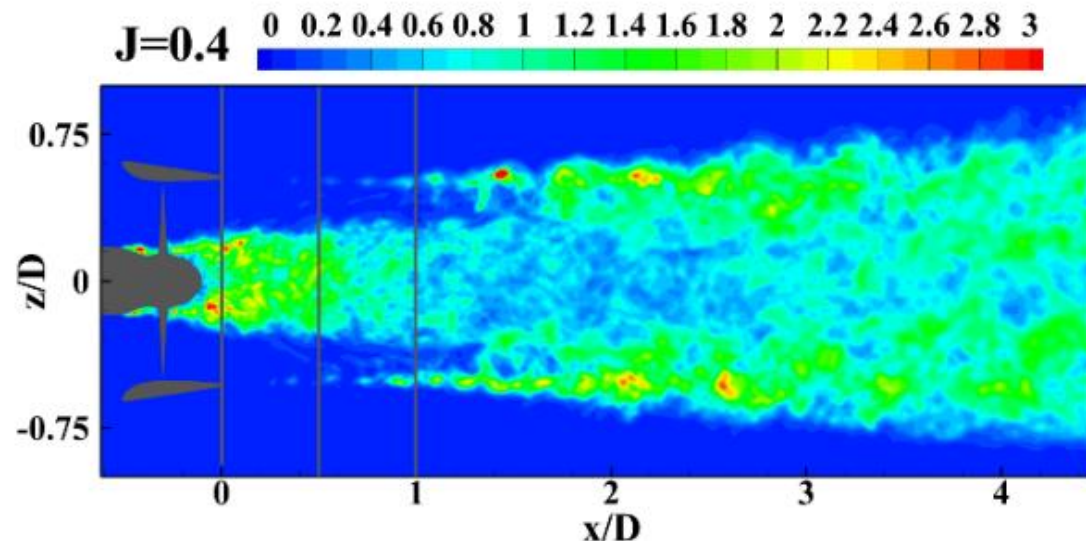
DMD mode:

```
Phi = U*W
```



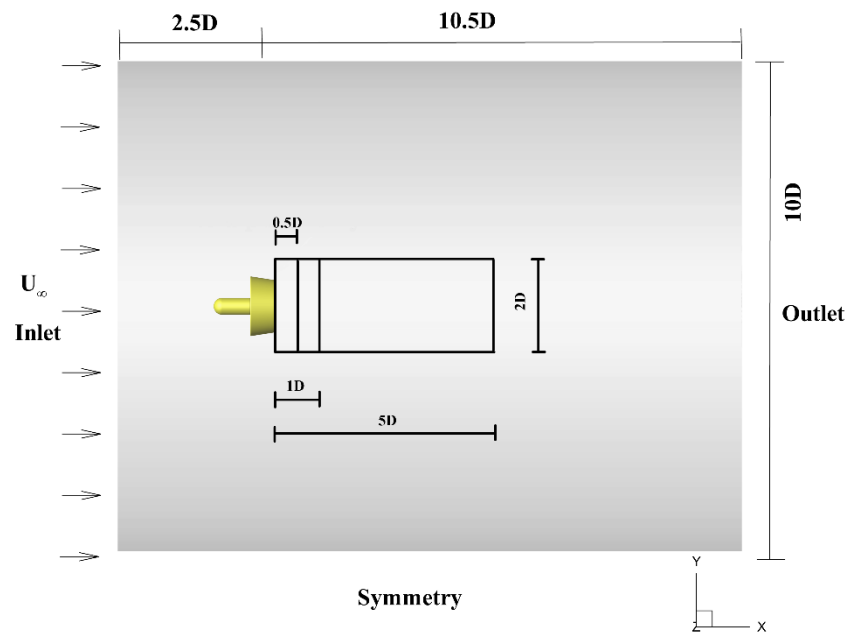
Parameters	Unit	Value
Propeller diameter D	m	0.10
Number of blades Z	-	4
Pitch P/D	-	1.00
Rotation rate n	rps	17.65
Advance coefficient J	-	0.4
Length	m	13D
Diameter	m	10D
Total computational cells	-	33×10^6
Re_n	-	1.765×10^5
Output interval dt	s	0.0001575

Analysis variable: **magnitude vorticity**
calculated by the **vorticity** function object
of **OpenFOAM-v3.0+**



Phase-averaged turbulence kinetic energy field

The bird order of the cylindrical computational subdomain are obtained through the **topoSet** function in OpenFOAM.



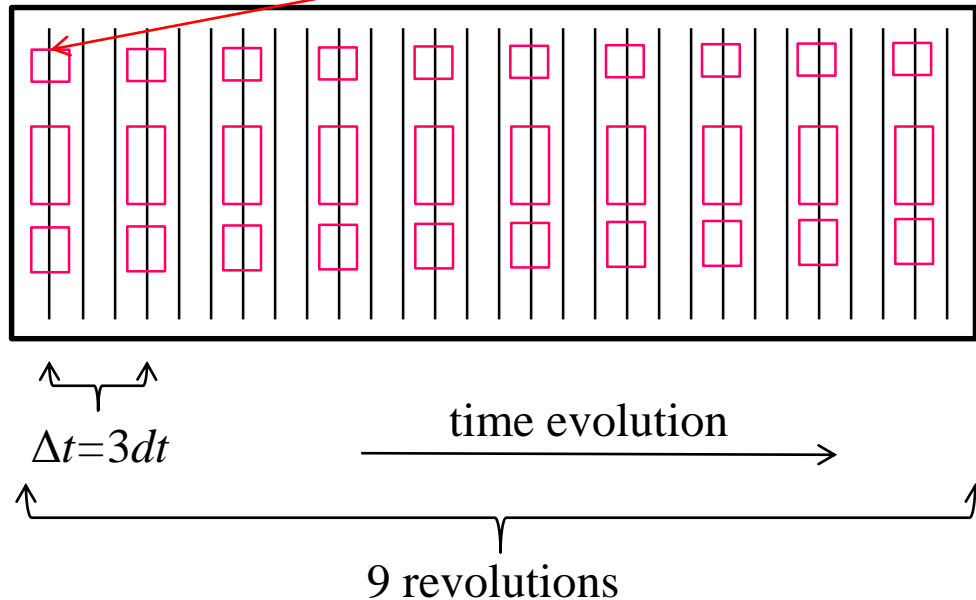
Computational subdomain of the ducted propeller

$$1.9 \times 10^6, 3.55 \times 10^6, 1.17 \times 10^7$$

Data preprocessing

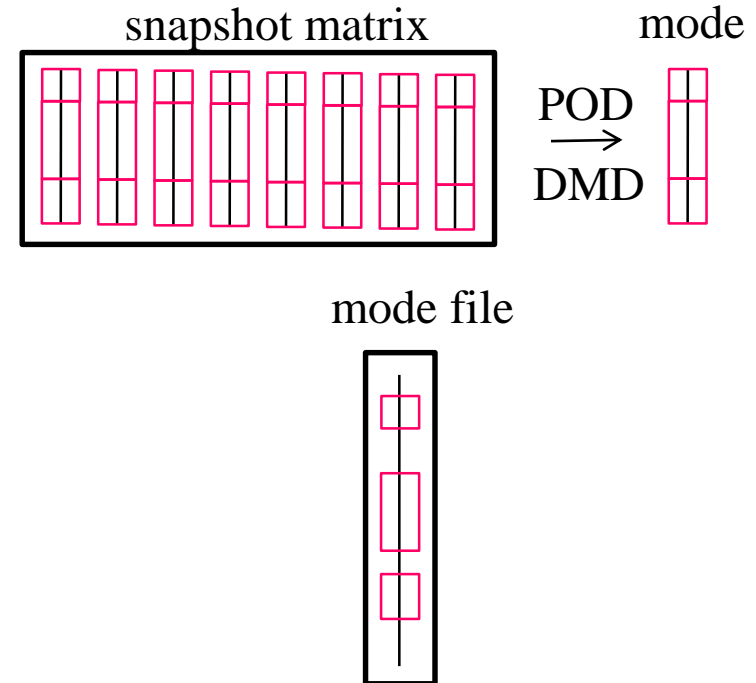
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data of the computational subdomain



Speed up reading data:

```
Memmapfile('file path')
```



The snapshot sampling interval

According to the **Nyquist-Shannon criterion**, the minimum sampling frequency f_{samp} should be two times of the blade passage frequency (BPF) f_{blade} :

$$f_{samp} = 1/\Delta t > 2f_{blade}$$

Parameters	Unit	Value
original output frequency f_{max}	Hz	6349
BPF f_{blade}	Hz	141

The sampling interval $\Delta t = 3dt, 4dt, 5dt, 6dt, 9dt$



According to the research of K. K. Chen, J. H. Tu, and C. W. Rowley (2012), **DMD is not sensitive to whether the analysis data cover integer number of periods, while POD may generate unexpected results when analyzing the data with non-integer multiple periods.**

Parameters	Unit	Value
Diameter	m	2D
Length	<i>m</i>	0.5D, 1D, 5D (1.9×10^6 , 3.55×10^6 , 1.17×10^7)
The snapshot sampling intervals	s	$3dt, 4dt, 5dt, 6dt, 9dt$ ($3^\circ, 4^\circ, 5^\circ, 6^\circ, 9^\circ$)
The data coverage revolutions	-	2-9 (0.1134-0.6237)

Interval:3

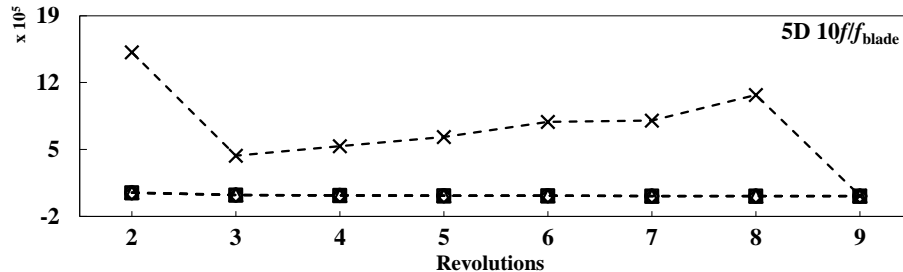
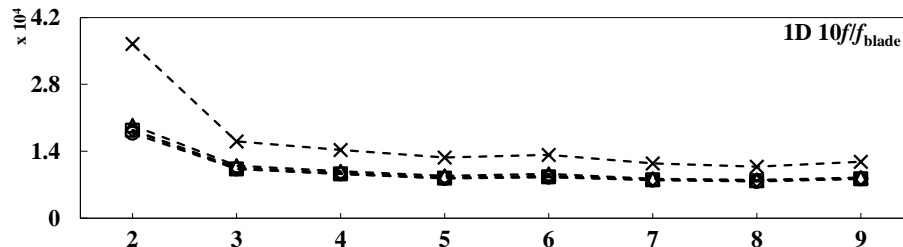
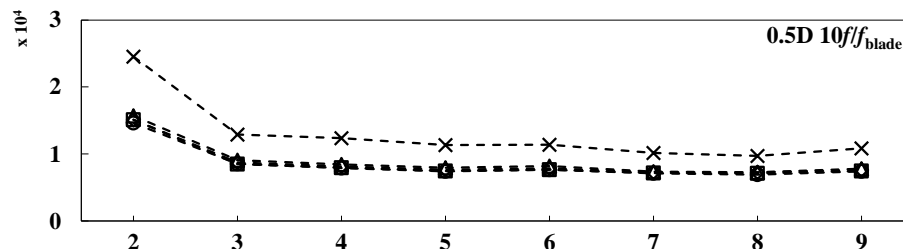
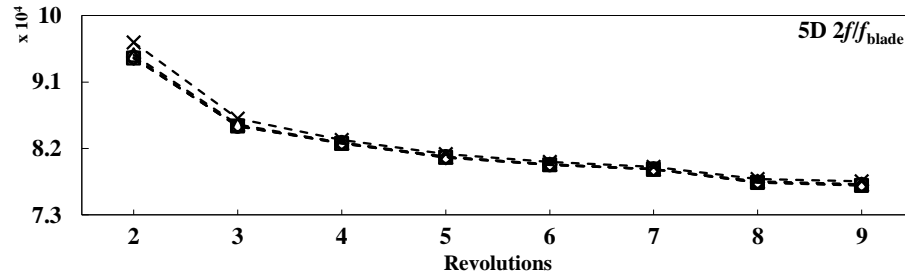
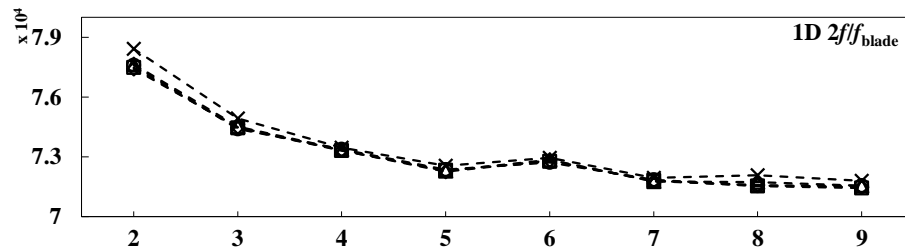
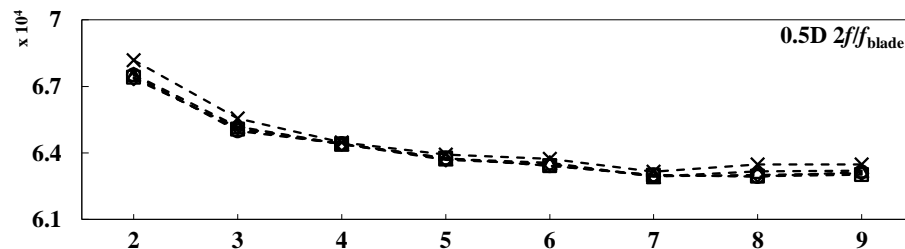
Interval:4

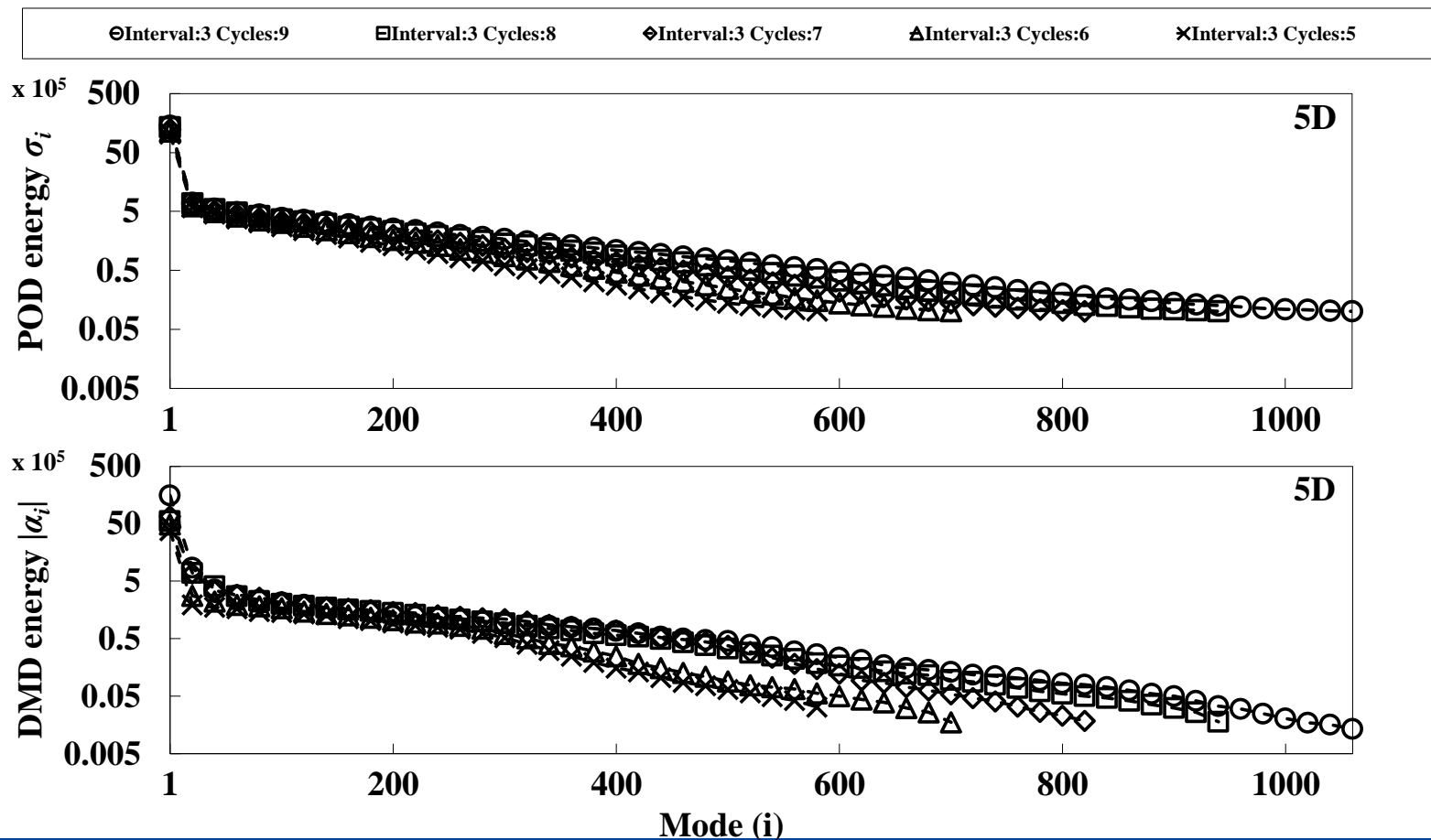
Interval:5

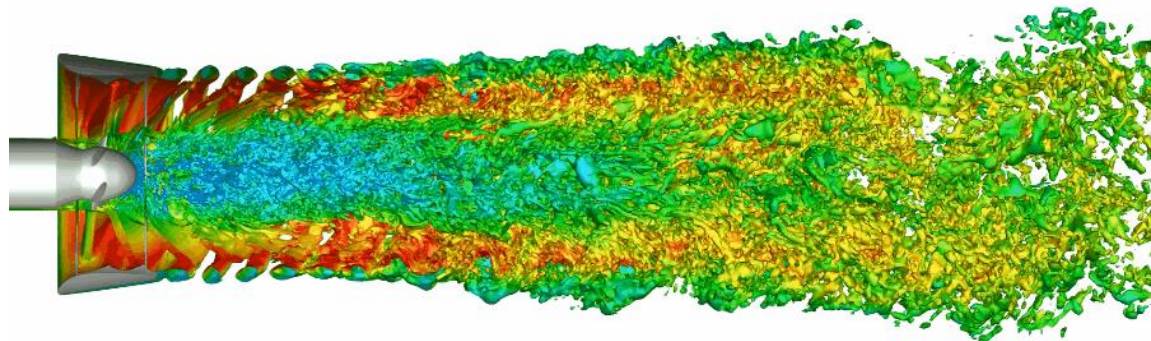
Interval:6

Interval:9

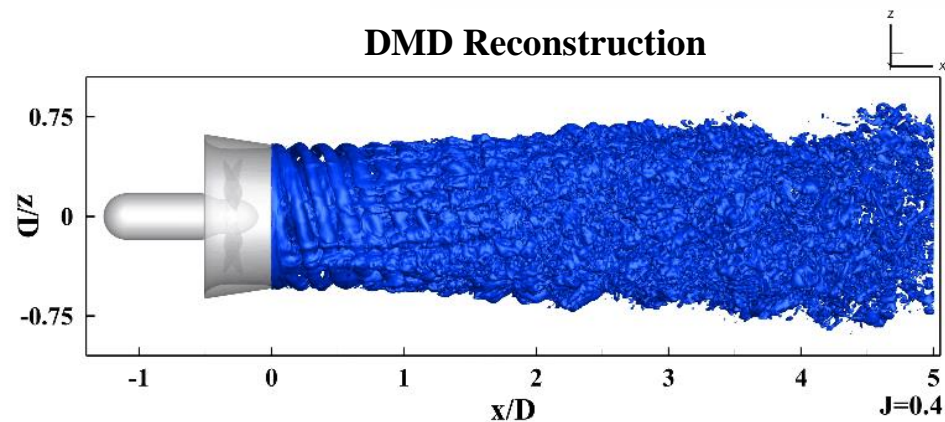
Amplitude $|\alpha_i|$





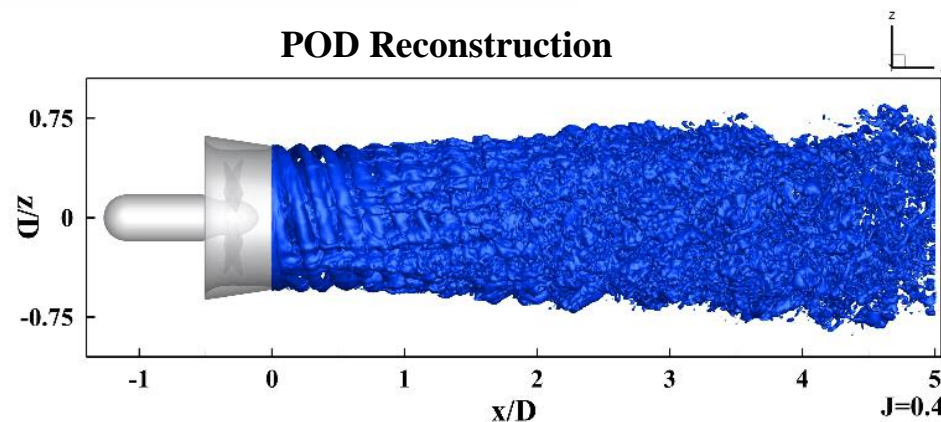


DMD Reconstruction



DMD reconstruction error: $\|X' - AX\|_F = 6.39 \times 10^{-5}$

POD Reconstruction



POD reconstruction error: $\|X - \sum_{i=1}^{960} \mathbf{u}_i a_i(t)\|_F = 5.67 \times 10^{-8}$



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- POD modes are independent in **space**, while DMD modes are in **frequency**.
- When **the sampling interval** reaches a certain level, it only affects the frequency range of the modes captured by POD and DMD, and **has little influence on the modal convergence**.
- The key factor affecting the modal convergence is **the data coverage revolutions**, which determines the frequency interval between two captured modes. A larger subdomain requires more revolutions.



- Future work will focus on the relationship between modes and **physical phenomena** under different operating conditions



- **Thanks!**