

# Discrete-Time Signals: Frequency-Domain Representation - II

## CHAPTER 3

These lecture slides are based on "Digital Signal Processing: A Computer-Based Approach, 4th ed." textbook by S.K. Mitra and its instructor materials. U.Sezen

## Contents

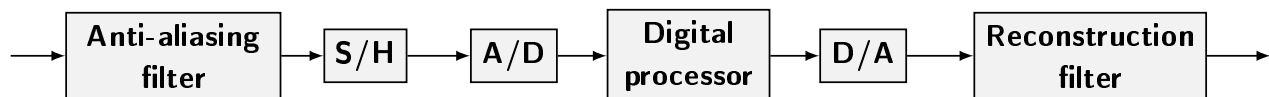
- Digital Processing of Continuous-Time Signals
  - Effect of Sampling in the Frequency Domain
  - Recovery of the Analog Signal
  - Implication of the Sampling Process
  - Sampling of Bandpass Signals

# Digital Processing of Continuous-Time Signals

- ▶ Digital processing of a continuous-time signal involves the following basic steps:
  1. Conversion of the continuous-time signal into a discrete-time signal,
  2. Processing of the discrete-time signal,
  3. Conversion of the processed discrete-time signal back into a continuous-time signal

- ▶ Conversion of a continuous-time signal into digital form is carried out by an **analog-to-digital (A/D) converter**
- ▶ The reverse operation of converting a digital signal into a continuous-time signal is performed by a **digital-to-analog (D/A) converter**
- ▶ Since the A/D conversion takes a finite amount of time, a **sample-and-hold (S/H) circuit** is used to ensure that the analog signal at the input of the A/D converter remains constant in amplitude until the conversion is complete to minimize the error in its representation

- ▶ To prevent aliasing, an analog **anti-aliasing filter** is employed before the S/H circuit
- ▶ To smooth the output signal of the D/A converter, which has a staircase-like waveform, an analog **reconstruction filter** is used
- ▶ Complete block-diagram:



**Note:** Both the anti-aliasing filter and the reconstruction filter are analog lowpass filters

- ▶ As indicated earlier, discrete-time signals in many applications are generated by sampling continuous-time signals
- ▶ We have seen earlier that identical discrete-time signals may result from the sampling of more than one distinct continuous-time function
- ▶ In fact, there exists an infinite number of continuous-time signals, which when sampled lead to the same discrete-time signal

- ▶ However, under certain conditions, it is possible to relate a unique continuous-time signal to a given discrete-time signal
- ▶ If these conditions hold, then it is possible to recover the original continuous-time signal from its sampled values
- ▶ We next develop this correspondence and the associated conditions

## Effect of Sampling in the Frequency Domain

- ▶ Let  $g_a(t)$  be a continuous-time signal that is sampled uniformly at  $t = nT$ , generating the sequence  $g[n]$  where

$$g[n] = g_a(nT), \quad -\infty < n < \infty$$

with  $T$  being the **sampling period**

- ▶ The reciprocal of  $T$  is called the **sampling frequency**  $F_T$ , i.e.,

$$F_T = \frac{1}{T}$$

- Now, the frequency-domain representation of  $g_a(t)$  is given by its continuous-time Fourier transform (**CTFT**):

$$G_a(j\Omega) = \int_{-\infty}^{\infty} g_a(t) e^{-j\Omega t} dt$$

- The frequency-domain representation of  $g[n]$  is given by its discrete-time Fourier transform (**DTFT**):

$$G(e^{j\omega}) = \sum_{n=-\infty}^{\infty} g[n] e^{-j\omega n}$$

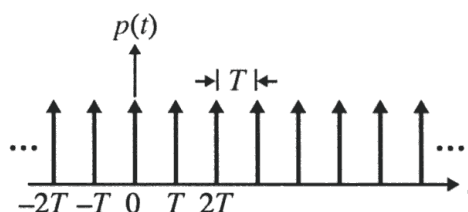
- To establish the relation between  $G_a(j\Omega)$  and  $G(e^{j\omega})$ , we treat the sampling operation mathematically as a modulation of  $g_a(t)$  by a **periodic impulse train**  $p(t)$ :

$$g_p(t) = g_a(t) p(t)$$


where

$$p(t) = \sum_{n=-\infty}^{\infty} \delta(t - nT).$$

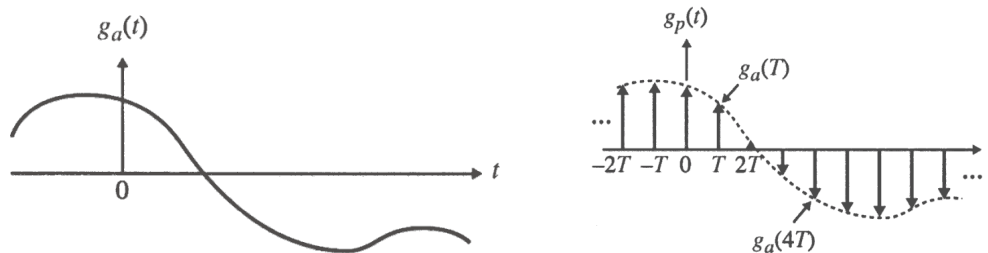
Here,  $p(t)$  consists of a train of ideal impulses with a period  $T$  as shown below



- The modulation operation yields an impulse train:

$$\begin{aligned} g_p(t) &= g_a(t) p(t) \\ &= \sum_{n=-\infty}^{\infty} g_a(nT) \delta(t - nT) \end{aligned}$$

- Here,  $g_p(t)$  is a continuous-time signal consisting of a train of uniformly spaced impulses with the impulse at  $t = nT$  weighted by the sampled value  $g_a(nT)$  of  $g_a(t)$  at that instant



- There are two different forms of  $G_p(j\Omega)$ :
  - One form is given by the weighted sum of the CTFTs of  $\delta(t - nT)$

$$G_p(j\Omega) = \sum_{n=-\infty}^{\infty} g_a(nT) e^{-j\Omega nT}$$

- To derive the second form, we make use of the **Poisson's formula**:

$$\sum_{n=-\infty}^{\infty} \phi(t + nT) = \frac{1}{T} \sum_{k=-\infty}^{\infty} \Phi(jk\Omega_T) e^{jk\Omega_T t}$$

where  $\Omega_T = \frac{2\pi}{T}$  and  $\Phi(j\Omega)$  is the CTFT of  $\phi(t)$

For  $t = 0$ , equation given on the previous slide reduces to

$$\sum_{n=-\infty}^{\infty} \phi(nT) = \frac{1}{T} \sum_{k=-\infty}^{\infty} \Phi(jk\Omega_T)$$

Now, from the frequency shifting property of the CTFT, the CTFT of  $g_a(t)e^{-j\Psi t}$  is given by  $G_a(j(\Omega + \Psi))$

Substituting  $\phi(t) = g_a(t)e^{-j\Psi t}$  in the equation above, we arrive at

$$\sum_{n=-\infty}^{\infty} g_a(nT)e^{-j\Psi nT} = \frac{1}{T} \sum_{k=-\infty}^{\infty} G_a(j(k\Omega_T + \Psi))$$

By replacing  $\Psi$  with  $\Omega$  in the above equation we arrive at the alternative form of the CTFT  $G_p(j\Omega)$  of  $g_p(t)$

The alternative form of the CTFT of  $g_p(t)$  is given by

$$G_p(j\Omega) = \frac{1}{T} \sum_{k=-\infty}^{\infty} G_a(j(\Omega + k\Omega_T))$$

Therefore,  $G_p(j\Omega)$  is a periodic function of  $\Omega$  consisting of a sum of shifted and scaled replicas of  $G_a(j\Omega)$ , shifted by integer multiples of  $\Omega_T$  and scaled by  $\frac{1}{T}$

- ▶ The term on the right hand side (RHS) of the previous equation for  $k = 0$  is the **baseband** portion of  $G_p(j\Omega)$ , and each of the remaining terms are the frequency translated portions of  $G_p(j\Omega)$
- ▶ The frequency range

$$-\frac{\Omega_T}{2} \leq \Omega \leq \frac{\Omega_T}{2}$$

is called the **baseband** or **Nyquist band**

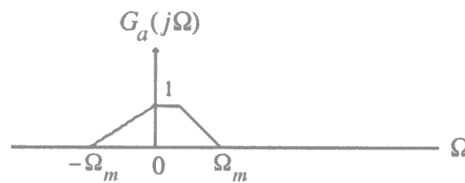
- ▶ The term on the right hand side (RHS) of the previous equation for  $k = 0$  is the **baseband** portion of  $G_p(j\Omega)$ , and each of the remaining terms are the frequency translated portions of  $G_p(j\Omega)$
- ▶ The frequency range

$$-\frac{\Omega_T}{2} \leq \Omega \leq \frac{\Omega_T}{2}$$

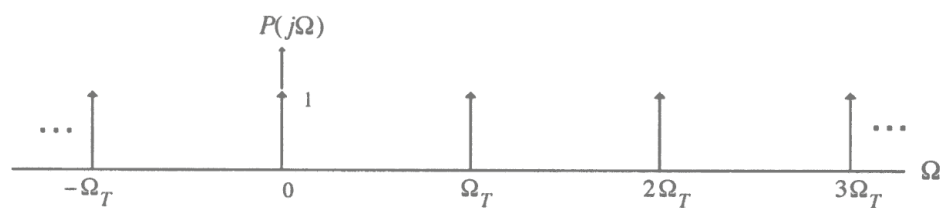
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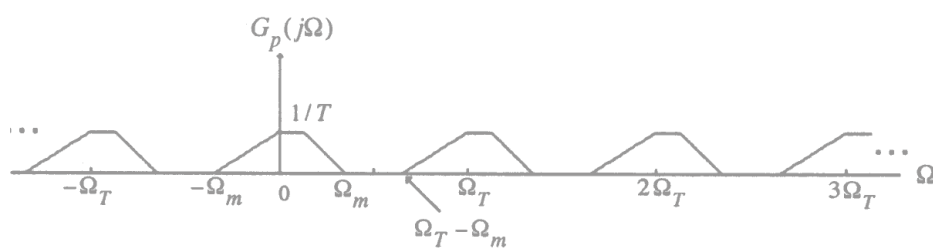
- Assume is a band-limited signal  $g_a(t)$  with a CTFT  $G_a(j\Omega)$  as shown below



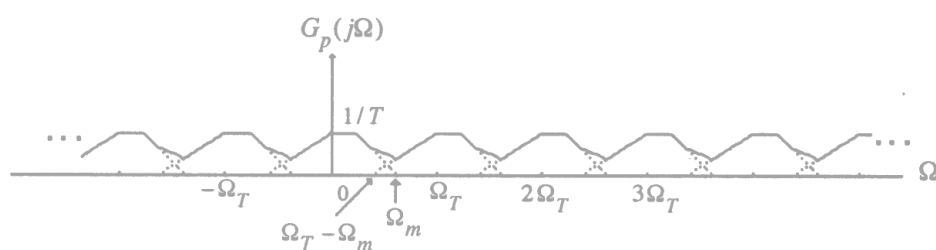
- The spectrum  $P(j\Omega)$  of  $p(t)$  having a sampling period  $T = \frac{2\pi}{\Omega_T}$  is indicated below



- Two possible spectra of  $G_p(j\Omega)$  are shown below



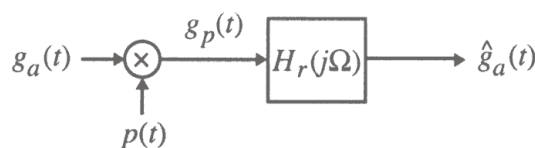
Sampling without aliasing



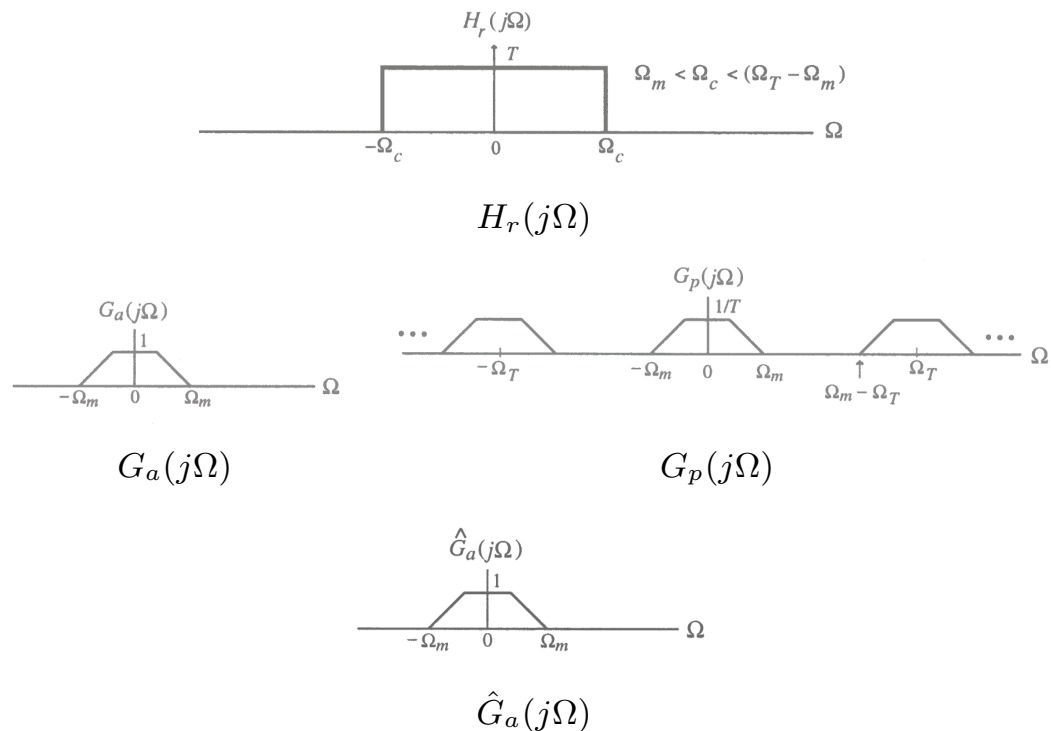
Sampling with aliasing

- It is evident from the top figure on the previous slide that if  $\Omega_T > \Omega_m$ , there is no overlap between the shifted replicas of  $G_a(j\Omega)$  generating  $G_p(j\Omega)$
- On the other hand, as indicated by the figure on the bottom, if  $\Omega_T < \Omega_m$ , there is an overlap of the spectra of the shifted replicas of  $G_a(j\Omega)$  generating  $G_p(j\Omega)$

- If  $\Omega_T > \Omega_m$ ,  $g_a(t)$  can be recovered exactly from  $g_p(t)$  by passing it through an **ideal lowpass filter**  $H_r(j\Omega)$  with a gain  $T$  and a cutoff frequency  $\Omega_c$  greater than  $\Omega_m$  and less than  $\Omega_T - \Omega_m$  as shown below
- On the other hand, as indicated by the figure below, if  $\Omega_T < \Omega_m$ , there is an overlap of the spectra of the shifted replicas of  $G_a(j\Omega)$  generating  $G_p(j\Omega)$



- The spectra of the filter and pertinent signals are shown below



- On the other hand, if  $\Omega_T < 2\Omega_m$ , due to the overlap of the shifted replicas of  $G_a(j\Omega)$ , the spectrum  $G_a(j\Omega)$  cannot be separated by filtering to recover  $G_a(j\Omega)$  because of the distortion caused by a part of the replicas immediately outside the baseband folded back or **aliased** into the baseband

- **Sampling theorem:** Let  $g_a(t)$  be a bandlimited signal with CTFT  $G_a(j\Omega) = 0$  for  $|\Omega| > \Omega_m$

- Then  $g_a(t)$  is uniquely determined by its samples  $g_a(nT)$ ,  $-\infty \leq n \leq \infty$  if

$$\Omega_T \geq 2\Omega_m$$

where  $\Omega_T = \frac{2\pi}{T}$

- The condition  $\Omega_T \geq 2\Omega_m$  is often referred to as the **Nyquist condition**
- The frequency  $\frac{\Omega_T}{2}$  is usually referred to as the **folding frequency**

- Given  $\{g_a(nT)\}$ , we can recover exactly  $g_a(t)$  by generating an impulse train

$$g_p(t) = \sum_{n=-\infty}^{\infty} g_a(nT)\delta(t - nT)$$

and then passing it through an ideal lowpass filter  $H_r(j\Omega)$  with a gain  $T$  and a cutoff frequency  $\Omega_c$  satisfying

$$\Omega_m < \Omega_c < (\Omega_T - \Omega_m)$$

- The highest frequency  $\Omega_m$  contained in  $g_a(t)$  is usually called the **Nyquist frequency** since it determines the minimum sampling frequency  $\Omega_T = 2\Omega_m$  that must be used to fully recover  $g_a(t)$  from its sampled version
- The condition  $\Omega_T \geq 2\Omega_m$  is often referred to as the **Nyquist condition**
- The frequency  $2\Omega_m$  is called the **Nyquist rate**

- ▶ **Oversampling:** The sampling frequency is higher than the Nyquist rate
- ▶ **Undersampling:** The sampling frequency is lower than the Nyquist rate
- ▶ **Critical sampling:** The sampling frequency is equal to the Nyquist rate

**Note:** A pure sinusoid may not be recoverable from its critically sampled version

- ▶ In digital telephony, a **3.4 kHz** signal bandwidth is acceptable for telephone conversation

Here, a sampling rate of **8 kHz**, which is greater than twice the signal bandwidth, is used

- ▶ In high-quality analog music signal processing, a bandwidth of **20 kHz** has been determined to preserve the fidelity

Hence, in compact disc (CD) music systems, a sampling rate of **44.1 kHz**, which is slightly higher than twice the signal bandwidth, is used

- **Example:** Consider the three continuous-time sinusoidal signals:

$$g_1(t) = \cos(6\pi t)$$

$$g_2(t) = \cos(14\pi t)$$

$$g_3(t) = \cos(26\pi t)$$

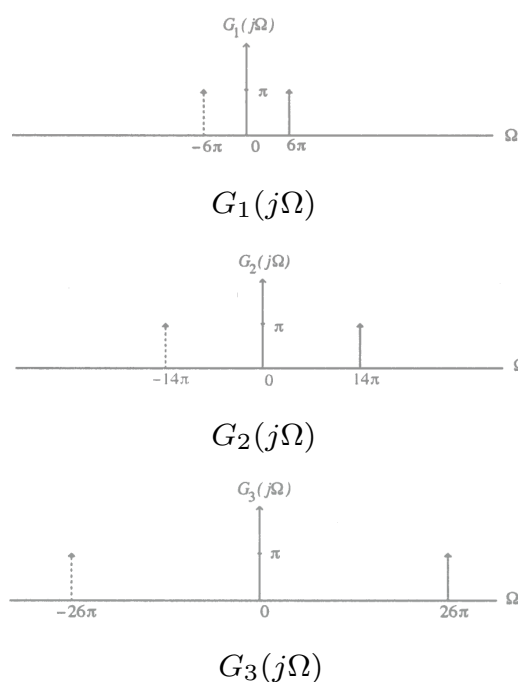
Their corresponding CTFTs are:

$$G_1(j\Omega) = \pi[\delta(\Omega - 6\pi) + \delta(\Omega + 6\pi)]$$

$$G_2(j\Omega) = \pi[\delta(\Omega - 14\pi) + \delta(\Omega + 14\pi)]$$

$$G_3(j\Omega) = \pi[\delta(\Omega - 26\pi) + \delta(\Omega + 26\pi)]$$

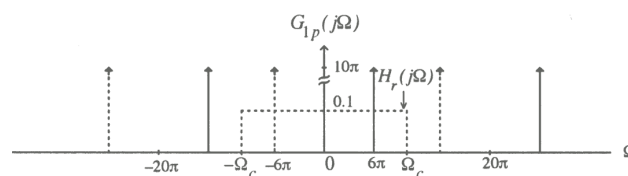
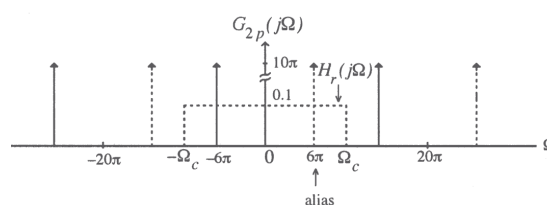
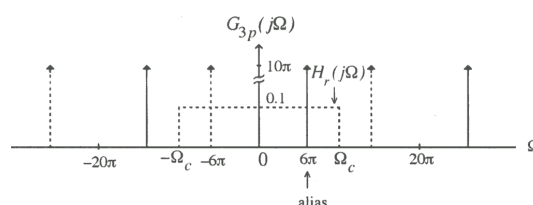
- These three transforms are plotted below



- These continuous-time signals sampled at a rate of  $T = 0.1$  sec, i.e., with a sampling frequency  $\Omega_T = 20\pi$  rad/sec
- The sampling process generates the continuous-time impulse trains,  $q_{1p}(t)$ ,  $q_{2p}(t)$ , and  $q_{3p}(t)$
- Their corresponding CTFTs are given by

$$G_{\ell p}(j\Omega) = 10 \sum_{k=-\infty}^{\infty} G_{\ell}(j(\Omega - k\Omega_T)), \quad 1 \leq \ell \leq 3$$

- Plots of the 3 CTFTs are shown below

 $G_{1p}(j\Omega)$  $G_{2p}(j\Omega)$  $G_{3p}(j\Omega)$

- ▶ These figures also indicate by dotted lines the frequency response of an ideal lowpass filter with a cutoff at  $\Omega_c = \frac{\Omega_T}{2} = 10\pi$  and a gain  $T = 0.1$
- ▶ The CTFTs of the lowpass filter output are also shown in these three figures
- ▶ In the case of  $g_1(t)$ , the sampling rate satisfies the Nyquist condition, hence no aliasing
- ▶ Moreover, the reconstructed output is precisely the original continuous-time signal
- ▶ In the other two cases, the sampling rate does not satisfy the Nyquist condition, resulting in aliasing and the filter outputs are all equal to  $\cos(6\pi t)$

- ▶ **Note:** In the figure at the bottom, the impulse appearing at  $\Omega = 6\pi$  in the positive frequency passband of the filter results from the aliasing of the impulse in  $G_2(j\Omega)$  at  $\Omega = -14\pi$

Likewise, the impulse appearing at  $\Omega = 6\pi$  in the positive frequency passband of the filter results from the aliasing of the impulse in  $G_3(j\Omega)$  at  $\Omega = 26\pi$



- We now derive the relation between the DTFT of  $g[n]$  and the CTFT of  $g_p(t)$

To this end we compare

$$G(e^{j\omega}) = \sum_{n=-\infty}^{\infty} g[n]e^{-j\omega n}$$

with

$$G_p(j\Omega) = \sum_{n=-\infty}^{\infty} g_a(nT)e^{-j\Omega nT}$$

and make use of

$$g[n] = g_a(nT), \quad -\infty < n < \infty$$

- **Observation:** We have

$$G(e^{j\omega}) = G_p(j\Omega)|_{\Omega=\omega/T}$$

or, equivalently,

$$G_p(j\Omega) = G(e^{j\omega})|_{\omega=\Omega T}$$

From the above observation and

$$G_p(j\Omega) = \frac{1}{T} \sum_{k=-\infty}^{\infty} G_a(j(\Omega + k\Omega_T))$$

we arrive at the desired result given by

$$\begin{aligned}
 G(e^{j\omega}) &= \frac{1}{T} \sum_{k=-\infty}^{\infty} G_a(j(\Omega + k\Omega_T)) \Big|_{\Omega=\omega/T} \\
 &= \frac{1}{T} \sum_{k=-\infty}^{\infty} G_a\left(j\frac{\omega}{T} + jk\Omega_T\right) \\
 &= \frac{1}{T} \sum_{k=-\infty}^{\infty} G_a\left(j\frac{\omega}{T} + j\frac{2\pi k}{T}\right)
 \end{aligned}$$

- This relation can be alternately expressed as

$$G(e^{j\Omega T}) = \frac{1}{T} \sum_{k=-\infty}^{\infty} G_a(j(\Omega + k\Omega_T))$$

- From

$$G(e^{j\omega}) = G_p(j\Omega) \Big|_{\Omega=\omega/T}$$

or from

$$G_p(j\Omega) = G(e^{j\omega}) \Big|_{\omega=\Omega T}$$

it follows that  $G(e^{j\omega})$  is obtained from  $G_p(j\Omega)$  by applying the mapping  $\Omega = \frac{\omega}{T}$

- Now, the CTFT  $G_p(j\Omega)$  is a periodic function of  $\Omega$  with a period  $\Omega_T = \frac{2\pi}{T}$
- Because of the mapping, the DTFT  $G(e^{j\omega})$  is a periodic function of  $\omega$  with a period of  $2\pi$

- We now derive the expression for the output  $\hat{g}_a(t)$  of the ideal lowpass reconstruction filter  $H_r(j\Omega)$  as a function of the samples  $g[n]$
- The impulse response  $h_r(t)$  of the lowpass reconstruction filter is obtained by taking the inverse CTFT of  $H_r(j\Omega)$ :

$$H_r(j\Omega) = \begin{cases} T, & |\Omega| \leq \Omega_c \\ 0, & |\Omega| > \Omega_c \end{cases}$$

- Thus, the impulse response is given by

$$\begin{aligned} h_r(t) &= \frac{1}{2\pi} \int_{-\infty}^{\infty} H_r(j\Omega) e^{j\Omega t} d\Omega \\ &= \frac{T}{2\pi} \int_{-\Omega_c}^{\Omega_c} e^{j\Omega t} d\Omega \\ &= \frac{\sin(\Omega_c t)}{\Omega_c t/2}, \quad -\infty \leq t \leq \infty \end{aligned}$$

- The input to the lowpass filter is the impulse train  $g_p(t)$ :

$$g_p(t) = \sum_{n=-\infty}^{\infty} g[n] \delta(t - nT)$$

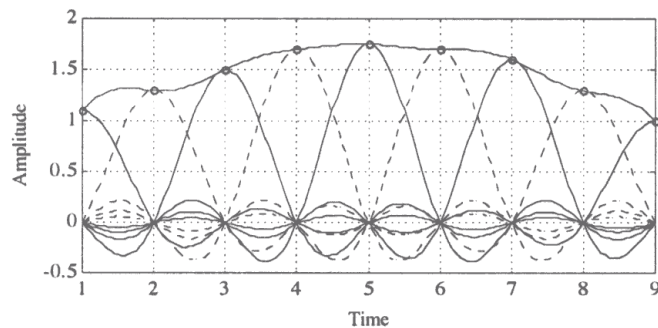
- Therefore, the output  $\hat{g}_a(t)$  of the ideal lowpass filter is given by:

$$\hat{g}_a(t) = h_r(t) \circledast g_p(t) = \sum_{n=-\infty}^{\infty} g[n] h_r(t - nT)$$

- Substituting  $h_r(t) = \frac{\sin(\Omega_c t)}{\Omega_c t/2}$  in the above and assuming for simplicity  $\Omega_c = \frac{\Omega_T}{2} = \frac{\pi}{T}$ , we get

$$\hat{g}_a(t) = \sum_{n=-\infty}^{\infty} g[n] \frac{\sin(\pi(t - nT)/T)}{\pi(t - nT)/T}$$

- The ideal bandlimited interpolation process is illustrated below



- It can be shown that when  $\Omega_c = \frac{\Omega_T}{2}$  in

$$h_r(t) = \frac{\sin(\Omega_c t)}{\Omega_T t/2}$$

$h_r(0)$  and for  $h_r(nT) = 0$  for  $n \neq 0$

- As a result, from

$$\hat{g}_a(t) = \sum_{n=-\infty}^{\infty} g[n] \frac{\sin(\pi(t - nT)/T)}{\pi(t - nT)/T}$$

we observe

$$\hat{g}_a(rT) = g[r] = g_a(rT)$$

for all integer values of  $r$  in the range  $-\infty < r < \infty$

- The relation

$$\hat{g}_a(rT) = g[r] = g_a(rT)$$

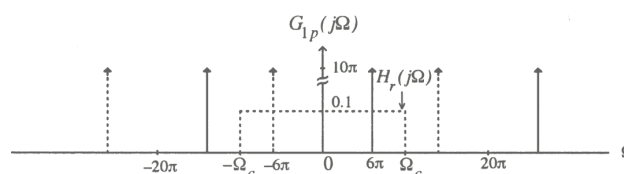
holds for all values of  $n$  whether or not the condition of the sampling theorem is satisfied

- However,  $\hat{g}_a(t) = g_a(t)$  for all values of  $t$  only if the sampling frequency  $\Omega_T$  satisfies the condition of the sampling theorem

## Implication of the Sampling Process

- Consider again the three continuous-time signals:  $g_1(t) = \cos(6\pi t)$ ,  $g_2(t) = \cos(14\pi t)$ , and  $g_3(t) = \cos(26\pi t)$

The plot of the CTFT  $G_{1p}(j\Omega)$  of the sampled version  $g_{1p}(t)$  of  $g_1(t)$  is shown below



- From the plot, it is apparent that we can recover any of its frequency-translated versions  $\cos[(20k \pm 6)\pi t]$  outside the baseband by passing  $g_{1p}(t)$  through an ideal analog bandpass filter with a passband centered at  $\Omega = (20k \pm 6)\pi$

- For example, to recover the signal  $\cos(34\pi t)$ , it will be necessary to employ a bandpass filter with a frequency response

$$H_r(j\Omega) = \begin{cases} 0.1, & (34 - \Delta)\pi \leq |\Omega| \leq (34 + \Delta)\pi \\ 0, & \text{otherwise} \end{cases}$$

where  $\Delta$  is a small number

- Likewise, we can recover the aliased baseband component  $\cos(6\pi t)$ , from the sampled version of either  $g_{2p}(t)$  or  $g_{3p}(t)$  by passing it through an ideal lowpass filter with a frequency response:

$$H_r(j\Omega) = \begin{cases} 0.1, & (6 - \Delta)\pi \leq |\Omega| \leq (6 + \Delta)\pi \\ 0, & \text{otherwise} \end{cases}$$

- There is no aliasing distortion unless the original continuous-time signal also contains the component  $\cos(6\pi t)$
- Similarly, from either  $g_{2p}(t)$  or  $g_{3p}(t)$  we can recover any one of the frequency-translated versions, including the parent continuous-time signal  $g_2(t)$  or  $g_3(t)$  as the case may be, by employing suitable filters

# Sampling of Bandpass Signals

- ▶ The conditions developed earlier for the unique representation of a continuous-time signal by the discrete-time signal obtained by uniform sampling assumed that the continuous-time signal is bandlimited in the frequency range from DC to some frequency  $\Omega_m$
- ▶ Such a continuous-time signal is commonly referred to as a **lowpass signal**
- ▶ There are applications where the continuous-time signal is bandlimited to a higher frequency range  $\Omega_L \leq |\Omega| \leq \Omega_H$  with  $\Omega_L > 0$
- ▶ Such a signal is usually referred to as the **bandpass signal**

- ▶ To prevent aliasing a bandpass signal can of course be sampled at a rate greater than twice the highest frequency, i.e. by ensuring

$$\Omega_T \geq 2\Omega_H$$

- ▶ However, due to the bandpass spectrum of the continuous-time signal, the spectrum of the discrete-time signal obtained by sampling will have spectral gaps with no signal components present in these gaps
- ▶ Moreover, if  $\Omega_H$  is very large, the sampling rate also has to be very large which may not be practical in some situations

- ▶ A more practical approach is to use **undersampling**
- ▶ Let  $\Delta\Omega = \Omega_H - \Omega_L$  define the bandwidth of the bandpass signal
- ▶ Assume first that the highest frequency contained in the signal is an integer multiple of the bandwidth, i.e.,

$$\Omega_H = M \Delta\Omega$$

- ▶ We choose the sampling frequency  $\Omega_T$  to satisfy the condition

$$\Omega_T = 2 \Delta\Omega = \frac{2\Omega_H}{M}$$

which is smaller than  $2\Omega_H$ , the Nyquist rate

- ▶ Substitute the above expression for  $\Omega_T$  in

$$G_p(j\Omega) = \frac{1}{T} \sum_{k=-\infty}^{\infty} G_a(j(\Omega + k\Omega_T))$$

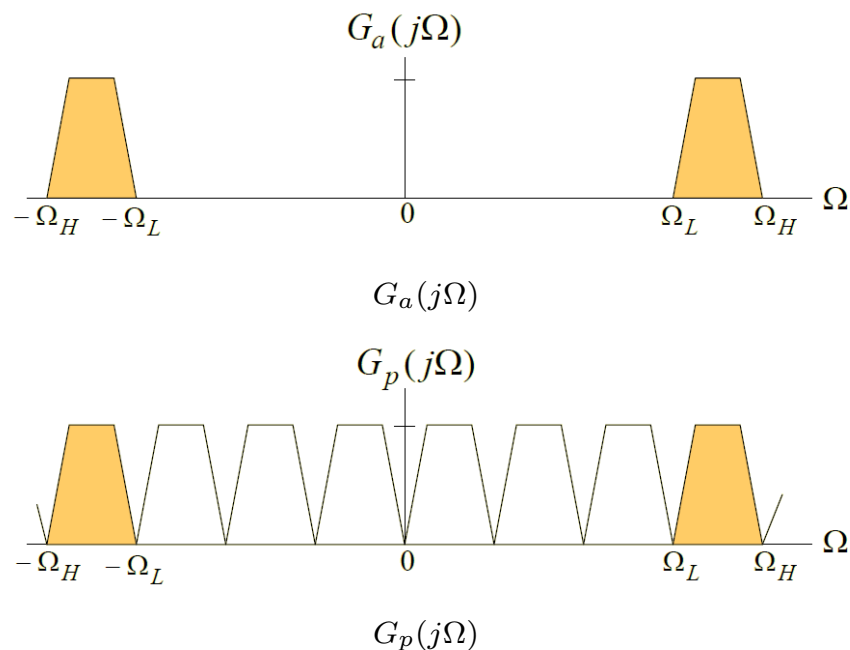
- ▶ This leads to

$$G_p(j\Omega) = \frac{1}{T} \sum_{k=-\infty}^{\infty} G_a(j(\Omega + 2k\Delta\Omega))$$

- ▶ As before,  $G_p(j\Omega)$  consists of a sum of  $G_a(j\Omega)$  and replicas of  $G_a(j\Omega)$  shifted by integer multiples of twice the bandwidth  $\Delta\Omega$  and scaled by  $1/T$
- ▶ The amount of shift for each value of  $k$  ensures that there will be no overlap between all shifted replicas, i.e., **no aliasing**



- Figures below illustrate the idea behind



- As can be seen,  $g_a(t)$  can be recovered from  $g_p(t)$  by passing it through an ideal bandpass filter with a passband given by  $\Omega_L \leq |\Omega| \leq \Omega_H$  and a gain of  $T$
- **Note:** Any of the replicas in the lower frequency bands can be retained by passing  $g_p(t)$  through bandpass filters with passbands

$$\Omega_L - k \Delta\Omega \leq |\Omega| \leq \Omega_H - k \Delta\Omega, \quad 1 \leq k \leq M - 1$$

providing a translation to lower frequency ranges