
Many diverse examples of invariant manifold construction

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Instructions

- Download and install the computer algebra package *Reduce* via <http://www.reduce-algebra.com>
- Navigate to folder Examples within folder InvariantManifold.
- For each example of interest, start-up *Reduce* and enter the command `in_tex "filename.tex"` where filename is the root name of the example (as listed in the following table of contents).

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1 Six representative examples

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1.1 `simple3d`: Slow manifold of a basic 3D system

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The basic example system to analyse for a slow manifold is

$$\begin{aligned}\dot{u}_1 &= 2u_1 + u_2 + 2u_3 + u_2u_3, \\ \dot{u}_2 &= u_1 - u_2 + u_3 - u_1u_3, \\ \dot{u}_3 &= -3u_1 - u_2 - 3u_3 - u_1u_2,\end{aligned}$$

(Section 1.5 constructs its stable manifold).

Start by loading the procedure.

```
1 in_tex "../invariantManifold.tex"$
```

Execute the construction of the slow manifold for this system.

```
2 invariantmanifold({},  
3      mat(( 2*u1+u2+2*u3+u2*u3,  
4          u1-u2+u3-u1*u3,  
5          -3*u1-u2-3*u3-u1*u2 )),  
6      mat((0)),  
7      mat((1,0,-1)),  
8      mat((4,1,3)),  
9      3 )$  
10 end;
```

The matrix $\begin{bmatrix} 2 & 1 & 2 \\ 1 & -1 & 1 \\ -3 & -1 & -3 \end{bmatrix}$ of the linearisation about the origin has eigenvalues zero and -1 (multiplicity two). We seek the slow manifold so specify the eigenvalue zero in the second parameter to

the procedure. A corresponding eigenvector is $\vec{e} = (1, 0, -1)$, and corresponding left-eigenvector is $\vec{z} = (4, 1, 3)$, as specified above. The last parameter, 3, specifies to construct the slow manifold to errors $\mathcal{O}(\varepsilon^3)$.

The procedure actually analyses the embedding system

$$\begin{aligned}\dot{u}_1 &= 2u_1 + u_2 + 2u_3 + \varepsilon u_2 u_3, \\ \dot{u}_2 &= u_1 - u_2 + u_3 - \varepsilon u_1 u_3, \\ \dot{u}_3 &= -3u_1 - u_2 - 3u_3 - \varepsilon u_1 u_2.\end{aligned}$$

Consequently, here the artificial parameter ε has a physical interpretation in that it counts the nonlinearity: a term in ε^p will be a $(p+1)$ th order term in $\vec{u} = (u_1, u_2, u_3)$. Hence the specified error $\mathcal{O}(\varepsilon^3)$ is here the same as error $\mathcal{O}(|\vec{u}|^4)$ and $\mathcal{O}(|\vec{s}|^4)$.

The slow manifold The constructed slow manifold is, in terms of the parameter s_1 (to error $\mathcal{O}(\varepsilon^2)$, and reverse ordering!),

$$u_1 = -\varepsilon s_1^2 + s_1, \quad u_2 = \varepsilon s_1^2, \quad u_3 = \varepsilon s_1^2 - s_1.$$

Slow manifold ODEs On this slow manifold the evolution is

$$\dot{s}_1 = -9\varepsilon^2 s_1^3 + \varepsilon s_1^2.$$

Here the leading term in s_1^2 establishes the origin is unstable.¹

Normals to isochrons at the slow manifold To project initial conditions onto the slow manifold, or non-autonomous forcing, or modifications of the original system, or to quantify uncertainty ([Roberts 1989, 2000](#)), use the projection defined by the derived vector

$$\vec{z}_1 = \begin{bmatrix} z_{11} \\ z_{12} \end{bmatrix} = \begin{bmatrix} 258\varepsilon^2 s_1^2 - 16\varepsilon s_1 + 4 \\ 93\varepsilon^2 s_1^2 - 9\varepsilon s_1 + 1 \\ 240\varepsilon^2 s_1^2 - 16\varepsilon s_1 + 3 \end{bmatrix}.$$

Evaluate these at $\varepsilon = 1$ to apply to the original specified system, or here just interpret ε as a way to count the order of each term.

1.2 doubleHopfDDE: Double Hopf interaction in a 2D DDE

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[Erneux \(2009\)](#) [§7.2] explored an example of a laser subject to optoelectronic feedback, coded as a delay differential equation. For certain parameter values it has a two frequency Hopf bifurcation.

¹ Then the large negative s_1^3 term suggests the existence of a finite amplitude equilibrium with $s_1 \approx 1/9$ (it is actually closer to $s_1 \approx 0.2$).

Near Erneux's parameters $(\eta, \theta) = (3/5, 2)$, the system may be represented as

$$\begin{aligned}\dot{u}_1 &= -4(1 + \delta)^2 \left[\frac{5}{8}u_2 + \frac{3}{8}u_2(t - \pi) \right] \\ \dot{u}_2 &= u_1(1 + u_2).\end{aligned}$$

for small parameter δ . Due to the delay, $u_2(t - \pi)$, this system is effectively an infinite-dimensional dynamical system. Here we describe the emergent dynamics on its four-dimensional centre manifold.

The linearisation of this system at the origin has modes with frequencies $\omega = 1, 2$, and corresponding eigenvectors $(1, \mp i/\omega)e^{\pm i\omega t}$. Corresponding eigenvectors of the adjoint are $(1, \mp i\omega)e^{\pm i\omega t}$. We model the nonlinear interaction of these four modes over long times.

Start by loading the procedure.

```
11 in_tex ".../invariantManifold.tex"$
```

In the printed output, group terms with like powers of amplitudes s_j , the complex exponential, and the parameter δ .

```
12 factor s,delta,exp;
```

Execute the construction of the slow manifold for this system, where $u_2(\pi)$ denotes the delayed variable $u_2(t - \pi)$, and where `1+small*delta` reflects that we wish to use the 'small' parameter δ to explore regimes where this factor is near the value 1.

```
13 invariantmanifold{},
14     mat(( -4*(1+small*delta)^2*(5/8*u2 +3/8*u2(pi)),
15             +u1*(1+u2) )),
16     mat(( i,-i,2*i,-2*i )),
17     mat( (1,-i), (1,+i), (1,-i/2), (1,+i/2) ),
18     mat( (1,-i), (1,+i), (1,-2*i), (1,+2*i) ),
19     3 )$
```

```
20 end;
```

The code works for errors of order higher than cubic, but is much slower: takes several minutes per iteration.

The procedure actually analyses the embedding system

$$\begin{aligned}\dot{u}_1 &= -4(1 + 2\varepsilon^2\delta + \varepsilon^3\delta^2) \left[\frac{5}{8}u_2 + \frac{3}{8}u_2(t - \pi) \right] \\ \dot{u}_2 &= u_1(1 + \varepsilon u_2).\end{aligned}$$

The centre manifold These give the location of the invariant manifold in terms of parameters s_j . Here, $u_1 \approx s_1 e^{it} + s_2 e^{-it} + s_3 e^{i2t} + s_4 e^{-i2t}$ so that (for real solutions) s_1, s_2 are complex conjugate amplitudes that modulate the oscillations of frequency $\omega = 1$, whereas s_3, s_4 are complex conjugate amplitudes that modulate the

oscillations of frequency $\omega = 2$.

$$\begin{aligned} u_1 &= e^{-it}s_4s_1\varepsilon(0.2309i - 0.04495) + e^{-it}s_2 + 0.1667e^{-4it}s_4^2\varepsilon i + \\ &\quad 0.1875e^{-3it}s_4s_2\varepsilon i + e^{-2it}s_4 + e^{-2it}s_2^2\varepsilon(-0.3953i - 0.1233) + \\ &\quad e^{it}s_3s_2\varepsilon(-0.2309i - 0.04495) + e^{it}s_1 - 0.1667e^{4it}s_3^2\varepsilon i - \\ &\quad 0.1875e^{3it}s_3s_1\varepsilon i + e^{2it}s_3 + e^{2it}s_1^2\varepsilon(0.3953i - 0.1233) \\ u_2 &= e^{-it}s_4s_1\varepsilon(0.04495i + 0.2309) + e^{-it}s_2i - 0.1667e^{-4it}s_4^2\varepsilon - \\ &\quad 0.5625e^{-3it}s_4s_2\varepsilon + 0.5e^{-2it}s_4i + e^{-2it}s_2^2\varepsilon(0.06167i - 0.1977) + \\ &\quad e^{it}s_3s_2\varepsilon(-0.04495i + 0.2309) - e^{it}s_1i - 0.1667e^{4it}s_3^2\varepsilon - \\ &\quad 0.5625e^{3it}s_3s_1\varepsilon - 0.5e^{2it}s_3i + e^{2it}s_1^2\varepsilon(-0.06167i - 0.1977) \end{aligned}$$

Centre manifold ODEs The system evolves on the invariant manifold such that the parameters evolve according to these ODEs that characterise how the modulation of the oscillations evolve due to their nonlinear interaction.

$$\begin{aligned} \dot{s}_1 &= s_4s_3s_1\varepsilon^2(-0.03089i + 0.05032) + s_3s_2\varepsilon(-0.08991i - 0.03816) + \\ &\quad s_2s_1^2\varepsilon^2(-0.01837i - 0.1095) + s_1\delta\varepsilon^2(0.1526i - 0.3596) \\ \dot{s}_2 &= s_4s_3s_2\varepsilon^2(0.03089i + 0.05032) + s_4s_1\varepsilon(0.08991i - 0.03816) + \\ &\quad s_2^2s_1\varepsilon^2(0.01837i - 0.1095) + s_2\delta\varepsilon^2(-0.1526i - 0.3596) \\ \dot{s}_3 &= s_4s_3^2\varepsilon^2(-0.0349i - 0.04111) + s_3s_2s_1\varepsilon^2(-0.2499i - \\ &\quad 0.2153) + s_3\delta\varepsilon^2(0.8376i + 0.9867) + s_1^2\varepsilon(-0.4934i + 0.4188) \\ \dot{s}_4 &= s_4^2s_3\varepsilon^2(0.0349i - 0.04111) + s_4s_2s_1\varepsilon^2(0.2499i - 0.2153) + \\ &\quad s_4\delta\varepsilon^2(-0.8376i + 0.9867) + s_2^2\varepsilon(0.4934i + 0.4188) \end{aligned}$$

1.3 metastable4: Metastability in a four state Markov chain

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Variable ϵ characterises the rate of exchange between metastable states u_1 and u_4 in this system (Roberts 2015, Exercise 5.1):

$$\begin{aligned} \dot{u}_1 &= +u_2 - \epsilon u_1, \\ \dot{u}_2 &= -u_2 + \epsilon(u_3 - u_2 + u_1), \\ \dot{u}_3 &= -u_3 + \epsilon(u_4 - u_3 + u_2), \\ \dot{u}_4 &= +u_3 - \epsilon u_4. \end{aligned}$$

Start by loading the procedure.

```
21 in_tex "../invariantManifold.tex"$
```

Execute the construction of the slow manifold for this system. The explicit parameter `small`, math-name ε , gets replaced by `small^2` in the code, so in effect $\varepsilon^2 = \epsilon$.

```

22 invariantmanifold({},
23      mat(( u2-small*u1,
24          -u2+small*(u1-u2+u3),
25          -u3+small*(u2-u3+u4),
26          u3-small*u4 )),
27      mat((0,0)),
28      mat((1,0,0,0),(0,0,0,1)),
29      mat((1,1,0,0),(0,0,1,1)),
30      6 )$  

31 end;

```

The matrix $\begin{bmatrix} 0 & 1 & 0 & 0 \\ 0 & -1 & 0 & 0 \\ 0 & 0 & -1 & 0 \\ 0 & 0 & 1 & 0 \end{bmatrix}$, of the linearisation about $\varepsilon = 0$, has eigenvalues 0 and -1 (both multiplicity two). We seek the slow manifold so specify the two zero eigenvalues in the second parameter to the procedure. Corresponding eigenvectors are $\vec{e}_1 = (1, 0, 0, 0)$ and $\vec{e}_2 = (0, 0, 0, 1)$. Choosing corresponding left-vector (here not an eigenvector) is $\vec{z}_1 = (1, 1, 0, 0)$ and $\vec{z}_2 = (0, 0, 1, 1)$ means that the slow manifold parameters s_1, s_2 have the physical meaning, respectively, of being the probability that the system is in states $\{1, 2\}$ and $\{3, 4\}$. The last parameter, 6, specifies to construct the slow manifold to errors $\mathcal{O}(\varepsilon^6)$, that is, errors $\mathcal{O}(\varepsilon^3)$.

The slow manifold The constructed slow manifold is, in terms of the lumped-state probability parameters s_1, s_2 (to error $\mathcal{O}(\varepsilon^2)$, and reverse ordering!),

$$\begin{aligned} u_1 &= \varepsilon^4(-s_2 + 2s_1) - \varepsilon^2 s_1 + s_1, & u_3 &= \varepsilon^4(-2s_2 + s_1) + \varepsilon^2 s_2, \\ u_2 &= \varepsilon^4(s_2 - 2s_1) + \varepsilon^2 s_1, & u_4 &= \varepsilon^4(2s_2 - s_1) - \varepsilon^2 s_2 + s_2. \end{aligned}$$

Slow manifold ODEs On this slow manifold the evolution of the lumped-state probabilities is

$$\dot{s}_1 = \varepsilon^4(s_2 - s_1), \quad \dot{s}_2 = \varepsilon^4(-s_2 + s_1).$$

Hence here the long-term evolution is that on a time-scale of $\mathcal{O}(1/\varepsilon^2)$, $\mathcal{O}(1/\varepsilon^4)$, the system equilibrates between the two lumped states, that is, between $\{1, 2\}$ and $\{3, 4\}$.

Normals to isochrons at the slow manifold To project initial conditions onto the slow manifold, or non-autonomous forcing, or modifications of the original system, or to quantify uncertainty (Roberts 1989, 2000), use the projection defined by the derived vector

$$\vec{z}_1 = \begin{bmatrix} z_{11} \\ z_{12} \\ z_{13} \\ z_{14} \end{bmatrix} = \begin{bmatrix} \varepsilon^4 + 1 \\ 4\varepsilon^4 - \varepsilon^2 + 1 \\ -4\varepsilon^4 + \varepsilon^2 \\ -\varepsilon^4 \end{bmatrix}, \quad \vec{z}_2 = \begin{bmatrix} z_{21} \\ z_{22} \\ z_{23} \\ z_{24} \end{bmatrix} = \begin{bmatrix} -\varepsilon^4 \\ -4\varepsilon^4 + \varepsilon^2 \\ 4\varepsilon^4 - \varepsilon^2 + 1 \\ \varepsilon^4 + 1 \end{bmatrix}.$$

Evaluate all these at $\varepsilon^2 = \epsilon$ to apply to the original specified system.

1.4 nonlinNormModes: Interaction of nonlinear normal modes

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Renson et al. (2012) explored finite element construction of the nonlinear normal modes of a pair of coupled oscillators. Defining two new variables one of their example systems is

$$\begin{aligned}\dot{x}_1 &= x_3, & \dot{x}_3 &= -2x_1 + x_2 - \frac{1}{2}x_1^3 + \frac{3}{10}(-x_3 + x_4), \\ \dot{x}_2 &= x_4, & \dot{x}_4 &= x_1 - 2x_2 + \frac{3}{10}(x_3 - 2x_4).\end{aligned}$$

The linearisation of this system at the origin has modes with frequencies $\omega = 1, \sqrt{3}$, corresponding eigenvalues $\lambda = \pm i, \pm i\sqrt{3}$, and corresponding eigenvectors?? $(1, 1, \pm i\omega, \pm i\omega)$. Corresponding eigenvectors of the adjoint are $(1, 1, \pm i, \pm i)$ and $(\mp i\omega, \pm i\omega, 1, -1)$. We model the nonlinear interaction of these four modes over long times.

Here, the analysis constructs a full state space coordinate transformation. We find a mapping from the modulation variables $\vec{s} = (s_1, s_2, s_3, s_4)$ to the original variables $\vec{u} = (u_1, u_2, u_3, u_4)$, and find the corresponding evolution of \vec{s} . The modulation variables \vec{s} are ‘slow’ because the coordinate transform uses time-dependent (rotating) basis vectors that account for the fast oscillation in \vec{u} . Hence the new variables \vec{s} are good variables for making long-term predictions and forming understanding.

Start by loading the procedure.

```
32 in_tex "../invariantManifold.tex"$
```

In the printed output, group terms with like powers of amplitudes s_j , and the complex exponential.

```
33 factor small;
```

The following code makes the linear damping to be effectively small (which then makes it `small` squared); consequently, also scale the smallness of the cubic nonlinearity to match.

```
34 invariantmanifold{},
35   mat(( u3,
36     u4,
37     -2*u1 +u2 -small*u1^3/2 +small*3/10*(-u3+u4),
38     u1 -2*u2 +small*3/10*(u3 -2*u4) )),
39   mat(( i,-i,sqrt(3)*i,-sqrt(3)*i )),
40   mat( (1,1,+i,+i), (1,1,-i,-i),
41     (1,-1,i*sqrt(3),-i*sqrt(3)),
42     (1,-1,-i*sqrt(3),i*sqrt(3)) ),
43   mat( (1,1,+i,+i), (1,1,-i,-i),
44     (-i*sqrt(3),+i*sqrt(3),1,-1),
```

```

45      (+i*sqrt(3),-i*sqrt(3),1,-1) ),
46      3 )$ 
47 end;

```

The square root eigenvalues do not cause any trouble (although one may need to reformat the LaTeX of the `exp` operator). In the model, observe that $s_1 = s_2 = 0$ is invariant, as is $s_3 = s_4 = 0$. These are the nonlinear normal modes.

The procedure actually analyses the embedding system

$$\begin{aligned}\dot{u}_1 &= u_3, \quad \dot{u}_3 = \varepsilon^2(-1/2u_1^3 - 3/10u_3 + 3/10u_4) - 2u_1 + u_2, \\ \dot{u}_2 &= u_4, \quad \dot{u}_4 = \varepsilon^2(3/10u_3 - 3/5u_4) + u_1 - 2u_2.\end{aligned}$$

The invariant manifold Here these give the reparametrisation of the state space \vec{u} in terms of parameters s_j , via rotating basis vectors. Here, the coordinate transform is very complicated so I do not give the complexity. The leading approximation is, of course, the linear, errors $\mathcal{O}(\varepsilon^2)$,

$$\begin{aligned}u_1 &= e^{-\sqrt{3}it}s_4 + e^{-it}s_2 + e^{\sqrt{3}it}s_3 + e^{it}s_1 \\ u_2 &= -e^{-\sqrt{3}it}s_4 + e^{-it}s_2 - e^{\sqrt{3}it}s_3 + e^{it}s_1 \\ u_3 &= -\sqrt{3}e^{-\sqrt{3}it}s_4i - e^{-it}s_2i + \sqrt{3}e^{\sqrt{3}it}s_3i + e^{it}s_1i \\ u_4 &= \sqrt{3}e^{-\sqrt{3}it}s_4i - e^{-it}s_2i - \sqrt{3}e^{\sqrt{3}it}s_3i + e^{it}s_1i\end{aligned}$$

Invariant manifold ODEs The system evolves according to these ODEs that characterise how the modulation of the oscillations evolve in state space due to their nonlinear interaction.

$$\begin{aligned}\dot{s}_1 &= 3/4s_4s_3s_1\varepsilon^2i + 3/8s_2s_1^2\varepsilon^2i - 3/40s_1\varepsilon^2 \\ \dot{s}_2 &= -3/4s_4s_3s_2\varepsilon^2i - 3/8s_2^2s_1\varepsilon^2i - 3/40s_2\varepsilon^2 \\ \dot{s}_3 &= 1/8\sqrt{3}s_4s_3^2\varepsilon^2i + 1/4\sqrt{3}s_3s_2s_1\varepsilon^2i - 3/8s_3\varepsilon^2 \\ \dot{s}_4 &= -1/8\sqrt{3}s_4^2s_3\varepsilon^2i - 1/4\sqrt{3}s_4s_2s_1\varepsilon^2i - 3/8s_4\varepsilon^2\end{aligned}$$

Here one can see that each oscillation decays, with a frequency shift due to a combination of nonlinear interaction and nonlinear self-interaction.

1.5 stable3d: Stable manifold of a basic 3D system

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Let's revisit the example of [Section 1.1](#), namely

$$\begin{aligned}\dot{u}_1 &= 2u_1 + u_2 + 2u_3 + u_2u_3, \\ \dot{u}_2 &= u_1 - u_2 + u_3 - u_1u_3,\end{aligned}$$

$$\dot{u}_3 = -3u_1 - u_2 - 3u_3 - u_1u_2,$$

but here construct its 2D stable manifold.

Start by loading the procedure.

```
48 in_tex "../invariantManifold.tex"$
```

Execute the construction of the stable manifold for this system.

```
49 invariantmanifold{},
50     mat(( 2*u1+u2+2*u3+u2*u3,
51             u1-u2+u3-u1*u3,
52             -3*u1-u2-3*u3-u1*u2 )),
53     mat(( -1,-1 )),
54     mat( (1,-1,-1),(0.4,1.4,-1) ),
55     mat( (1,0,1),(1,0,-1) ),
56     3 )$
```

57 end;

The matrix $\begin{bmatrix} 2 & 1 & 2 \\ 1 & -1 & 1 \\ -3 & -1 & -3 \end{bmatrix}$ of the linearisation about the origin has eigenvalues 0 and -1 (multiplicity two). We seek the 2D stable manifold so specify the eigenvalue -1 , twice, in the second parameter to the procedure. A corresponding eigenvector is $\vec{e}_1 = (1, -1, -1)$, and corresponding left-eigenvector is $\vec{z}_2 = (1, 0, 1)$, as specified above. We need two basis eigenvectors, but here there is only one because the other is a generalised eigenvector. We must do more work to find a generalised eigenvector is $\vec{e}_2 = (0.4, 1.4, -1)$, and a generalised left-eigenvector is $\vec{z}_2 = (1, 0, -1)$. The last parameter, 3, specifies to construct the stable manifold to errors $\mathcal{O}(\varepsilon^3)$.

Because of the generalised eigenvector, the procedure modifies the *linear* terms to a more convenient form (not necessary, just *convenient*)—see the warning in its report. So, the procedure actually analyses the embedding system

$$\begin{aligned}\dot{u}_1 &= \varepsilon(-u_1 + u_2u_3 - u_3) + 3u_1 + u_2 + 3u_3, \\ \dot{u}_2 &= \varepsilon(-u_1u_3 + u_1 + u_3) - u_2, \\ \dot{u}_3 &= \varepsilon(-u_1u_2 + u_1 + u_3) - 4u_1 - u_2 - 4u_3.\end{aligned}$$

The stable manifold The constructed stable manifold is, in terms of the parameters s_1, s_2 (to error $\mathcal{O}(\varepsilon^2)$), and reverse ordering!,

$$\begin{aligned}u_1 &= \varepsilon(-51/25 e^{-2t} s_2^2 - 6/5 e^{-2t} s_2 s_1 + 3 e^{-2t} s_1^2) + 2/5 e^{-t} s_2 + e^{-t} s_1, \\ u_2 &= \varepsilon(-2/5 e^{-2t} s_2^2 - 7/5 e^{-2t} s_2 s_1 - e^{-2t} s_1^2) + 7/5 e^{-t} s_2 - e^{-t} s_1, \\ u_3 &= \varepsilon(4 e^{-2t} s_2^2 + 13/5 e^{-2t} s_2 s_1 - 5 e^{-2t} s_1^2) - e^{-t} s_2 - e^{-t} s_1.\end{aligned}$$

Observe the linear terms in \vec{s} all have e^{-t} , and the quadratic terms in \vec{s} all have e^{-2t} . Consequently, we could in principle write the stable manifold in terms of, say, the variables $x_j = s_j e^{-t}$ giving

$$u_1 = \varepsilon(-51/25 x_2^2 - 6/5 x_2 x_1 + 3 x_1^2) + 2/5 x_2 + x_1,$$

$$\begin{aligned} u_2 &= \varepsilon(-2/5x_2^2 - 7/5x_2x_1 - x_1^2) + 7/5x_2 - x_1, \\ u_3 &= \varepsilon(4x_2^2 + 13/5x_2x_1 - 5x_1^2) - x_2 - x_1. \end{aligned}$$

This would be a more usual parametrisation. But here let's remain with \vec{s} and remember to interpret \vec{s} as modifying the exponential decay e^{-t} on this stable manifold.

Stable manifold ODEs On the stable manifold the evolution is

$$\dot{s}_1 = 3/5\varepsilon s_2, \quad \dot{s}_2 = 0.$$

So, s_2 is constant, and hence s_1 increases linearly. But such increase only modifies slightly the robust exponential decay, e^{-t} , on the stable manifold.

In terms of \vec{x} this evolution is $\dot{x}_1 = -x_1 + \frac{3}{5}\varepsilon x_2$, $\dot{x}_2 = -x_2$.

1.6 interpretProjection: Interpret the fast-fibre projection vectors of slow manifolds

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For slow manifolds, this package computes *projection vectors* \vec{z} . This example explores *very simple* cases in order to introduce how one uses these vectors.

1.6.1 Simplest scenario

Construct the slow manifold of the 2-D system

$$\frac{du}{dt} = av, \quad \frac{dv}{dt} = -v,$$

and seek long-time predictions from the initial condition $u(0) = u_0$, $v(0) = v_0$.

Analytically we may solve this system exactly:

$$v = v_0 e^{-t}, \quad u = u_0 + av_0 [1 - e^{-t}].$$

Since $u = u_0 + av_0 + \mathcal{O}(e^{-t})$ we say that $u = u_0 + av_0$ is the long-time behaviour we aim to predict.

Let's make such prediction via the package. Start by loading the procedure.

```
58 in_tex "../invariantManifold.tex"$
```

Construct the slow manifold for this system using $u_1 = u$ and $u_2 = v$:

```

59 invariantmanifold({},
60      mat(( a*u2, -u2 )),
61      mat((0)), mat((1,0)), mat((1,0)), 9)$

```

The output gives the very simple slow manifold is $u = u_1 = s_1$ and $v = u_2 = 0$ in terms of its parameter s_1 , with (non-)evolution $ds_1/dt = 0$, and the projection vector $\vec{z} = (1, a)$.

How do we use this projection vector? Answer: choose initial $s_1(0) = s_0$ such that $\vec{z} \cdot [(u_0, v_0) - \vec{u}(s_0)] = 0$. Here this equation reduces to $(1, a) \cdot (u_0 - s_0, v_0) = 0$. That is, $s_0 := u_0 + av_0$. Solving the slow manifold evolution $ds_1/dt = 0$ then gives the prediction that $u = s_1 = u_0 + av_0$ for all time. This is the correct prediction to the exp-decaying error $\mathcal{O}(e^{-t})$.

1.6.2 Complex valued parameters

For simplicity I code do Reduce treats all parameters and variables as real-valued, *not* complex-valued—with the exception of $i := \sqrt{-1}$.

Thus, for example, let's construct the slow manifold of the 2-D complex-valued system

$$\frac{du}{dt} = (a + i b)v, \quad \frac{dv}{dt} = -v,$$

and seek long-time predictions from the initial condition $u(0) = u_0, v(0) = v_0$. As in the previous subsection, the long-time evolution is simply $v = 0$ and $u = s = u_0 + (a + i b)v_0$ to errors $\mathcal{O}(e^{-t})$.

Construct the slow manifold for this system:

```

62 invariantmanifold({},
63      mat(( (a+i*b)*u2, -u2 )),
64      mat((0)), mat((1,0)), mat((1,0)), 9)$

```

The output gives the very simple slow manifold is $u = u_1 = s_1$ and $v = u_2 = 0$ in terms of its parameter s_1 , with (non-)evolution $ds_1/dt = 0$, and the projection vector $\vec{z} = (1, a - ib)$.

How do we use this projection vector to make the correct initial condition that $s(0) = s_0 = u_0 + (a + ib)v_0$? Answer: instead of using the dot product, we invoke the complex inner product that $\langle \vec{z}, \vec{u} \rangle := \vec{z}^\dagger \vec{u}$ where the dagger denotes the complex-conjugate-transpose. That is, as a, b are both real, here \vec{z}^\dagger is the row vector $[1 \ a + ib]$.

Then the specified equation that we project according to the following, $\langle \vec{z}, (u_0, v_0) - \vec{u}(s_0) \rangle = 0$, becomes $u_0 + (a + ib)v_0 - s_0 = 0$, that is, $s_0 = u_0 + (a + ib)v_0$ as required to match the long-time evolution.

1.6.3 Simplest slow space variation scenario

Construct the slow manifold of the PDE system for two fields $u(x, t)$, $v(x, t)$

$$\frac{\partial u}{\partial t} = a \frac{\partial v}{\partial x}, \quad \frac{\partial v}{\partial t} = -v,$$

and seek long-time predictions from the initial condition $u(x, 0) = u_0(x)$, $v(x, 0) = v_0(x)$.

Analytically, the exactly solution (where dash denotes $\partial/\partial x$) is

$$v = v_0(x) e^{-t}, \quad u = u_0(x) + a v'_0(x) [1 - e^{-t}].$$

Since $u = u_0 + a v'_0 + \mathcal{O}(e^{-t})$ we say that $u = u_0 + a v'_0$ is the long-time behaviour we aim to predict.

Let's make such prediction via the package. Construct the slow manifold for this system using $u_1 = u$ and $u_2 = v$:

```
65 invariantmanifold({x},
66      mat(( a*pdf(u2,x), -u2 )),
67      mat((0)), mat((1,0)), mat((1,0)), 9)$
```

The output gives the very simple slow manifold is $u = u_1 = s_1$ and $v = u_2 = 0$ in terms of its parameter $s_1(x, t)$, with (non-)evolution $\partial s_1/\partial t = 0$, and the projection vector $\vec{z} = (1, a\varepsilon\partial_x)$.

How do we use this projection vector? Answer: first, ε is a book-keeping parameter that counts the order of a term, so ignore ε (or equivalently set $\varepsilon = 1$). Second, choose initial $s_1(x, 0) = s_0(x)$ such that the projection $\langle \vec{z}, (u_0, v_0) - \vec{u}(s_0) \rangle = 0$.

This inner product is *not* any integral over space x ; it is done keeping ' x fixed'. So here the projection equation reduces to $(1, a\partial_x) \cdot (u_0 - s_0, v_0) = 0$. That is, $s_0 := u_0 + a v'_0$. Solving the slow manifold evolution $\partial s_1/\partial t = 0$ then gives the prediction that $u = s_1 = u_0 + a v'_0$ for all time. As before, this is a correct prediction to an exp-decaying error $\mathcal{O}(e^{-t})$.

1.6.4 Nontrivial slow space variation

Construct the slow manifold of the PDE system for two fields $u(x, t)$, $v(x, t)$ where here spatial gradients of u, v feed into the v, u PDEs:

$$\frac{\partial u}{\partial t} = \frac{\partial v}{\partial x}, \quad \frac{\partial v}{\partial t} = -v + \frac{\partial u}{\partial x}.$$

We seek long-time predictions from the initial condition $u(x, 0) = u_0(x)$, $v(x, 0) = v_0(x)$.

Let's predict the long-time evolution via the package. Construct the slow manifold for this system using $u_1 = u$ and $u_2 = v$:

```
68 invariantmanifold({x},
69      mat(( pdf(u2,x), pdf(u1,x)-u2 )),
70      mat((0)), mat((1,0)), mat((1,0)), 4)$
```

The output gives the slow manifold is $u = u_1 = s_1 + \mathcal{O}(\partial_x^3)$ and $v = u_2 = \partial s_1 / \partial x + \mathcal{O}(\partial_x^3)$ in terms of its parameter $s_1(x, t)$. Here the corresponding slow evolution is the non-trivial diffusion PDE $\partial s_1 / \partial t = \partial^2 s_1 / \partial x^2 + \mathcal{O}(\partial_x^4)$.

Lastly, the projection vector (neglecting ε) is $\vec{z} = (1 - \partial_x^2, \partial_x - 2\partial_x^3) + \mathcal{O}(\partial_x^4)$. Hence choose initial $s_1(x, 0) = s_0(x)$ such that the projection $\langle \vec{z}, (u_0, v_0) - \vec{u}(s_0) \rangle = 0$. Here this projection equation reduces to $(1 - \partial_x^2, \partial_x - 2\partial_x^3) \cdot (u_0 - s_0, v_0) = 0$. That is, the initial field $s_0 := u_0 + v'_0 - u''_0 - 2v'''_0 + \mathcal{O}(\partial_x^4)$.

Finish.

```
71 end;
```

2 Harmonically forced systems

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2.1 `marcusYamabe`: Discover Marcus–Yamabe instability

In nonautonomous systems, such as $\dot{\vec{u}} = L(t)\vec{u}$, just because eigenvalues of $L(t)$ have real-part negative, for all t , does not mean that all solutions $\vec{u}(t)$ decay. Here consider the Marcus–Yamabe system (Chicone 2006, p.197)

$$\frac{d\vec{u}}{dt} = L(t)\vec{u} \quad \text{for } L := \begin{bmatrix} -1 + \frac{3}{2}\varepsilon^2 \cos^2 t & 1 - \frac{3}{2}\varepsilon^2 \sin t \cos t \\ -1 - \frac{3}{2}\varepsilon^2 \sin t \cos t & -1 + \frac{3}{2}\varepsilon^2 \sin^2 t \end{bmatrix}. \quad (1)$$

For example, for $\varepsilon = 1$, the eigenvalues of $L(t)$ are $\frac{1}{4}(-1 \pm \sqrt{7}i)$ (independent of time). Despite the eigenvalues having negative real-part, there are growing solutions $\vec{u} = (-\cos t, \sin t)e^{t/2}$.

Here analyse the system with the late-2022 version of `invariantManifold.tex` that caters for sinusoidal non-autonomous coefficients and forcing.

```
72 in_tex ".../invariantManifold.tex"$
73 factor small;
```

Encode the system with `small = ε`. We find instability predicted when $\frac{3}{2}\varepsilon^2 > 1$; that is, $|\varepsilon| > 0.8165$; for example, $\varepsilon = 1$ as commented above. Then the induced growth of complex amplitudes s_1 and s_2 overcomes the e^{-t} decay that is in $u_1 = e^{(-1+i)t}s_1 + e^{(-1-i)t}s_2$.

```
74 invariantmanifold({},
75   mat((-u1+u2 +small*( 3/2*cos(t)^2*u1 -3/2*cos(t)*sin(t)*u2),
76         -u1-u2 +small*(-3/2*cos(t)*sin(t)*u1 +3/2*sin(t)^2*u2)
77       )),
78   mat((-1+i, -1-i)),
79   mat((1,i), (1,-i)),
80   mat((1,i), (1,-i)),
81   9)$
82 end;
```

The function finds the following exact time-dependent transformation of this linear system. These parameterise state space in terms

of s_j :

$$\begin{aligned} u_1 &= e^{-it-t}s_2 + e^{it-t}s_1 + O(\varepsilon^8) \\ u_2 &= -e^{-it-t}s_2i + e^{it-t}s_1i + O(\varepsilon^8) \end{aligned}$$

Then the system evolves in state space such that the parameters evolve according to these ODEs.

$$\begin{aligned} \dot{s}_1 &= \varepsilon^2(3/4s_2 + 3/4s_1) + O(\varepsilon^9) \\ \dot{s}_2 &= \varepsilon^2(3/4s_2 + 3/4s_1) + O(\varepsilon^9) \end{aligned}$$

The eigenvalues of the above system are $\lambda = 0, \frac{3}{2}\varepsilon^2$. Hence the net growth of \vec{u} is at rate $-1 + \frac{3}{2}\varepsilon^2$; for example, at the unstable rate $+1/2$ when $\varepsilon = 1$.

2.2 forcedNonlinNormMode: harmonically forced nonlinear normal mode

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Renson et al. (2012) explored finite element construction of the nonlinear normal modes of a pair of coupled oscillators. Let's apply periodic forcing to their example, Section 1.4, both direct and parametric. For example, here derive the effect on the mode with frequency one. Defining two new variables one of their example systems is

$$\begin{aligned} \dot{x}_1 &= x_3, \quad \dot{x}_3 = -2x_1 + x_2 - \frac{1}{2}x_1^3 + \frac{3}{10}(-x_3 + x_4) + F_1 \cos t, \\ \dot{x}_2 &= x_4, \quad \dot{x}_4 = x_1 - 2x_2 + \frac{3}{10}(x_3 - 2x_4)F_2 \sin(t/2). \end{aligned}$$

where F_1 is the strength of the direct forcing, and F_2 is the strength of the parametric oscillation in the last ODE. The linearisation of this system at the origin has modes with frequencies $\omega = 1, \sqrt{3}$, corresponding eigenvalues $\lambda = \pm i, \pm i\sqrt{3}$, and corresponding eigenvectors $(1, 1, \pm i\omega, \pm i\omega)$. Corresponding eigenvectors of the adjoint are $(1, 1, \pm i, \pm i)$ and $(\mp i\omega, \pm i\omega, 1, -1)$. We model the nonlinear forced dynamics of the frequency one mode.

Here, the analysis constructs a nonlinear normal mode, time-dependent, coordinate transformation. We find a time-dependent mapping from the modulation variables $\vec{s} = (s_1, s_2)$ to the original variables $\vec{u} = (u_1, u_2, u_3, u_4)$, and find the corresponding evolution of \vec{s} . The modulation variables \vec{s} are ‘slow’ because the coordinate transform uses time-dependent (rotating) basis vectors that account for the fast oscillation in \vec{u} . Hence the new variables \vec{s} are good variables for making long-term predictions and forming understanding.

Start by loading the procedure.

```
83 in_tex ".../invariantManifold.tex"$
```

In the printed output, group terms with like powers of amplitudes s_j , and the complex exponential. I set Reduce to be case sensitive so we can use upper-case forcing, for example.

```
84 factor F_1,F_2,small;
```

The following code makes the linear damping to be effectively small (which then makes it `small` squared); consequently, also scale the smallness of the cubic nonlinearity to match.

```
85 invariantmanifold({},
86     mat(( u3, u4,
87         -2*u1+u2-small*u1^3/2+small*3/10*(-u3+u4)
88         +small*F_1*sin(t),
89         u1-2*u2+small*3/10*(u3-2*u4)*F_2*cos(t/2) )),
90     mat(( i,-i )),
91     mat( (1,1,+i,+i), (1,1,-i,-i) ),
92     mat( (1,1,+i,+i), (1,1,-i,-i) ),
93     5 )$  
94 end;
```

In the derived ODEs for the modulation of the frequency one mode, see that the direct forcing drives effects first seen in terms linear in F_1 . However, the parametric forcing drives effects quadratic in F_2 and so our higher-order, systematic, analysis is required.

The procedure actually analyses the embedding system

$$\begin{aligned}\dot{u}_1 &= u_3, \quad \dot{u}_2 = u_4, \\ \dot{u}_3 &= F_1 \varepsilon^2 \left(\frac{1}{2} e^{-it} i - \frac{1}{2} e^{it} i \right) + \varepsilon^2 \left(-\frac{1}{2} u_1^3 - \frac{3}{10} u_3 + \frac{3}{10} u_4 \right) \\ &\quad - 2u_1 + u_2, \\ \dot{u}_4 &= F_2 \varepsilon^2 \left(\frac{3}{20} e^{-it/2} u_3 - \frac{3}{10} e^{-it/2} u_4 + \frac{3}{20} e^{it/2} u_3 - \frac{3}{10} e^{it/2} u_4 \right) \\ &\quad + u_1 - 2u_2.\end{aligned}$$

The invariant manifold Here these give the reparametrisation of the state space \vec{u} in terms of parameters s_j , via rotating basis vectors. Here, the coordinate transform is very complicated so I do not give the complexity. The leading approximation is, of course, the linear, errors $\mathcal{O}(\varepsilon^2)$,

$$\begin{aligned}u_1 &= +e^{-it}s_2 + e^{it}s_1 + \mathcal{O}(\varepsilon^2) \\ u_2 &= +e^{-it}s_2 + e^{it}s_1 + \mathcal{O}(\varepsilon^2) \\ u_3 &= -e^{-it}s_2i + e^{it}s_1i + \mathcal{O}(\varepsilon^2) \\ u_4 &= -e^{-it}s_2i + e^{it}s_1i + \mathcal{O}(\varepsilon^2)\end{aligned}$$

Invariant manifold ODEs The system evolves according to these ODEs that characterise how the modulation of the oscillations

evolve in state space due to nonlinearity and the forcing.

$$\begin{aligned}\dot{s}_1 &= F_1 \varepsilon^4 \left(\frac{9}{64} s_2 s_1 - \frac{9}{128} s_1^2 + \frac{3}{160} i \right) - \frac{1}{8} F_1 \varepsilon^2 + \frac{93}{5500} F_2^2 \varepsilon^4 s_1 i \\ &\quad + \varepsilon^4 \left(-\frac{155}{256} s_2^2 s_1^3 i + \frac{9}{160} s_2 s_1^2 \right) + \frac{3}{8} \varepsilon^2 s_2 s_1^2 i + O(\varepsilon^5) \\ \dot{s}_2 &= F_1 \varepsilon^4 \left(-\frac{9}{128} s_2^2 + \frac{9}{64} s_2 s_1 - \frac{3}{160} i \right) - \frac{1}{8} F_1 \varepsilon^2 - \frac{93}{5500} F_2^2 \varepsilon^4 s_2 i \\ &\quad + \varepsilon^4 \left(\frac{155}{256} s_2^3 s_1^2 i + \frac{9}{160} s_2^2 s_1 \right) - \frac{3}{8} \varepsilon^2 s_2^2 s_1 i + O(\varepsilon^5)\end{aligned}$$

The second lines of these ODEs are the terms from the nonautonomous part of the system. The first line are the terms induced by the harmonic forcing. The parametric oscillation just induces an $\mathcal{O}(F_2^2)$ frequency shift. The direct harmonic forcing induces a direct $\mathcal{O}(F_1)$ forcing of the amplitudes s_j .

2.3 oscForcedChain: harmonically forced chain of oscillations

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	Finish the script	22

Mingwu Li et al. (2022) discussed the following system of the forcing of a small chain of coupled oscillators. To analyse, first load the function.

```
95 in_tex "../invariantManifold.tex"$
96 factor small,i;
```

Then encode the ODEs

$$\begin{aligned}\ddot{x}_1 + x_1 + C_1 \dot{x}_1 + K(x_1 - x_2)^3 &= F_1 \cos \omega t, \\ \ddot{x}_2 + x_2 + C_2 \dot{x}_2 + K[(x_2 - x_1)^3 + (x_2 - x_3)^3] &= 0, \\ \ddot{x}_3 + x_3 + C_3 \dot{x}_3 + K(x_3 - x_2)^3 &= 0,\end{aligned}$$

as follows with $x_1 = u_1$, $\dot{x}_1 = u_2$, $x_2 = u_3$, $\dot{x}_2 = u_4$, $x_3 = u_5$, $\dot{x}_3 = u_6$,

```
97 odes:=mat((u2, -u1-K*(u1-u3)^3 -C_1*u2+F
98 ,u4, -u3-K*(u3-u1)^3-K*(u3-u5)^3-C_2*u4
99 ,u6, -u5-K*(u5-u3)^3 -C_3*u6
100 ));
```

The procedure introduces the ordering parameter ε to actually analyse the following system:

$$\begin{aligned}\ddot{x}_1 + x_1 + \varepsilon \{C_1 \dot{x}_1 + K(x_1 - x_2)^3 - F_1 \cos \omega t\} &= 0, \\ \ddot{x}_2 + x_2 + \varepsilon \{C_2 \dot{x}_2 + K[(x_2 - x_1)^3 + (x_2 - x_3)^3]\} &= 0, \\ \ddot{x}_3 + x_3 + \varepsilon \{C_3 \dot{x}_3 + K(x_3 - x_2)^3\} &= 0,\end{aligned}$$

Set parameters nearly as in Mingwu Li et al. (2022), but let C_1 remain variable.

```
101 K:=2/10;
102 F:=F_1*cos(w*t);
103 factor F_1;
104 C_2:=2/10; C_3:=3/10; %C_1:=1/10;
Set forcing frequency to one for simplicity;
105 w:=1;
```

2.3.1 Time dependent reparametrisation of entire state space

Each of the three oscillators have identical frequency of one, and the damping is numerically small, so get the procedure to treat as small by giving unperturbed eigenvalues and eigenvectors.

```
106 invariantmanifold({},      odes,
107      mat(( i,-i,i,-i,i,-i)),
108      mat( (1,+i,0,0,0,0), (1,-i,0,0,0,0),
109            (0,0,1,+i,0,0), (0,0,1,-i,0,0),
110            (0,0,0,0,1,+i), (0,0,0,0,1,-i)
111            ),
112      mat( (1,+i,0,0,0,0), (1,-i,0,0,0,0),
113            (0,0,1,+i,0,0), (0,0,1,-i,0,0),
114            (0,0,0,0,1,+i), (0,0,0,0,1,-i)
115            ),
116      2 )$
```

The state space These give the location in state space in terms of parameters s_j .

$$\begin{aligned}u_1 &= e^{-it}s_2 + e^{it}s_1 + O(\varepsilon) \\ u_2 &= i(-e^{-it}s_2 + e^{it}s_1) + O(\varepsilon) \\ u_3 &= e^{-it}s_4 + e^{it}s_3 + O(\varepsilon) \\ u_4 &= i(-e^{-it}s_4 + e^{it}s_3) + O(\varepsilon) \\ u_5 &= e^{-it}s_6 + e^{it}s_5 + O(\varepsilon) \\ u_6 &= i(-e^{-it}s_6 + e^{it}s_5) + O(\varepsilon)\end{aligned}$$

State space ODEs The system evolves such that the parameters evolve according to these ODEs. They show forcing, weak damping,

nonlinear interaction among the modulation of the three modes.

$$\begin{aligned}
\dot{s}_1 &= -\frac{1}{4}F_1 i\varepsilon + i\varepsilon \left(-\frac{3}{10}s_4s_3^2 + \frac{3}{5}s_4s_3s_1 - \frac{3}{10}s_4s_1^2 + \frac{3}{10}s_3^2s_2 \right. \\
&\quad \left. - \frac{3}{5}s_3s_2s_1 + \frac{3}{10}s_2s_1^2 \right) - \frac{1}{2}\varepsilon s_1 C_1 + O(\varepsilon^2) \\
\dot{s}_2 &= \frac{1}{4}F_1 i\varepsilon + i\varepsilon \left(\frac{3}{10}s_4^2s_3 - \frac{3}{10}s_4^2s_1 - \frac{3}{5}s_4s_3s_2 + \frac{3}{5}s_4s_2s_1 \right. \\
&\quad \left. + \frac{3}{10}s_3s_2^2 - \frac{3}{10}s_2^2s_1 \right) - \frac{1}{2}\varepsilon s_2 C_1 + O(\varepsilon^2) \\
\dot{s}_3 &= i\varepsilon \left(-\frac{3}{10}s_6s_5^2 + \frac{3}{5}s_6s_5s_3 - \frac{3}{10}s_6s_3^2 + \frac{3}{10}s_5^2s_4 - \frac{3}{5}s_5s_4s_3 \right. \\
&\quad \left. + \frac{3}{5}s_4s_3^2 - \frac{3}{5}s_4s_3s_1 + \frac{3}{10}s_4s_1^2 - \frac{3}{10}s_3^2s_2 + 3/5s_3s_2s_1 \right. \\
&\quad \left. - \frac{3}{10}s_2s_1^2 \right) - \frac{1}{10}\varepsilon s_3 + O(\varepsilon^2) \\
\dot{s}_4 &= i\varepsilon \left(\frac{3}{10}s_6^2s_5 - \frac{3}{10}s_6^2s_3 - \frac{3}{5}s_6s_5s_4 + \frac{3}{5}s_6s_4s_3 + \frac{3}{10}s_5s_4^2 \right. \\
&\quad \left. - \frac{3}{5}s_4s_3^2 + \frac{3}{10}s_4^2s_1 + \frac{3}{5}s_4s_3s_2 - \frac{3}{5}s_4s_2s_1 - 3/10s_3s_2^2 \right. \\
&\quad \left. + \frac{3}{10}s_2^2s_1 \right) - \frac{1}{10}\varepsilon s_4 + O(\varepsilon^2) \\
\dot{s}_5 &= i\varepsilon \left(\frac{3}{10}s_6s_5^2 - \frac{3}{5}s_6s_5s_3 + \frac{3}{10}s_6s_3^2 - \frac{3}{10}s_5^2s_4 + \frac{3}{5}s_5s_4s_3 \right. \\
&\quad \left. - \frac{3}{10}s_4s_3^2 \right) - \frac{3}{20}\varepsilon s_5 + O(\varepsilon^2) \\
\dot{s}_6 &= i\varepsilon \left(-\frac{3}{10}s_6^2s_5 + \frac{3}{10}s_6^2s_3 + \frac{3}{5}s_6s_5s_4 - \frac{3}{5}s_6s_4s_3 - \frac{3}{10}s_5s_4^2 \right. \\
&\quad \left. + \frac{3}{10}s_4^2s_3 \right) - \frac{3}{20}\varepsilon s_6 + O(\varepsilon^2)
\end{aligned}$$

2.3.2 Emergent mode at general frequency

Here suppose damping C_1 is significantly smaller than the other damping. Hence here consider the first oscillator as dominantly the ‘master’ mode. First, analyse for general frequency ω by ‘clearing’ w.

```

117 clear w;
118 invariantmanifold({},      odes,
119      mat(( i,-i)),
120      mat( (1,+i,0,0,0,0), (1,-i,0,0,0,0)
121      ),
122      mat( (1,+i,0,0,0,0), (1,-i,0,0,0,0)
123      ),
124      2 )$ % use 3 to get these reported results

```

The invariant manifold These give the location of the invariant manifold in terms of parameters s_j . There are divisions by $(1 - \omega^2)$ flagging resonance when the forcing is at the resonant frequency.

$$\begin{aligned}
u_1 &= F_1 \varepsilon \left(-\frac{1}{2}e^{-itw} - \frac{1}{2}e^{itw} \right) / (w^2 - 1) + i\varepsilon \left(\frac{1}{4}e^{-it}s_2C_1 - 1/4e^{it}s_1C_1 \right) \\
&\quad + \varepsilon \left(-\frac{3}{20}e^{-it}s_2^2s_1 + \frac{1}{40}e^{-3it}s_2^3 - \frac{3}{20}e^{it}s_2s_1^2 + \frac{1}{40}e^{3it}s_1^3 \right) \\
&\quad + e^{-it}s_2 + e^{it}s_1 + O(\varepsilon^2) \\
u_2 &= F_1 i\varepsilon \left(\frac{1}{2}e^{-itw}w - \frac{1}{2}e^{itw}w \right) / (w^2 - 1) + i\varepsilon \left(-\frac{3}{20}e^{-it}s_2^2s_1 \right. \\
&\quad \left. - \frac{3}{40}e^{-3it}s_2^3 + \frac{3}{20}e^{it}s_2s_1^2 + \frac{3}{40}e^{3it}s_1^3 \right) + i \left(-e^{-it}s_2 + e^{it}s_1 \right) \\
&\quad + \varepsilon \left(-\frac{1}{4}e^{-it}s_2C_1 - \frac{1}{4}e^{it}s_1C_1 \right) + O(\varepsilon^2) \\
u_3 &= i\varepsilon \left(3e^{-it}s_2^2s_1 + \frac{3}{1609}e^{-3it}s_2^3 - 3e^{it}s_2s_1^2 - \frac{3}{1609}e^{3it}s_1^3 \right) \\
&\quad + \varepsilon \left(-\frac{40}{1609}e^{-3it}s_2^3 - \frac{40}{1609}e^{3it}s_1^3 \right) + O(\varepsilon^2)
\end{aligned}$$

$$\begin{aligned}
u_4 &= i\varepsilon \left(\frac{120}{1609} e^{-3it} s_2^3 - \frac{120}{1609} e^{3it} s_1^3 \right) \\
&\quad + \varepsilon \left(3e^{-it} s_2^2 s_1 + \frac{9}{1609} e^{-3it} s_2^3 + 3e^{it} s_2 s_1^2 + \frac{9}{1609} e^{3it} s_1^3 \right) + O(\varepsilon^2) \\
u_5 &= O(\varepsilon^2) \\
u_6 &= O(\varepsilon^2)
\end{aligned}$$

Invariant manifold ODEs The system evolves on the invariant manifold such that the parameters evolve according to these ODEs. With general forcing frequency the algorithm does not detect resonance here, it only shows up as above divisions by $(1 - \omega^2)$. These evolution equations only show nonlinear frequency modification and the damping at rate $C_1/2$.

$$\begin{aligned}
\dot{s}_1 &= i\varepsilon^2 \left(-\frac{77259}{643600} s_2^2 s_1^3 - \frac{1}{8} s_1 C_1^2 \right) + \frac{3}{10} i\varepsilon s_2 s_1^2 - \frac{1449}{1609} \varepsilon^2 s_2^2 s_1^3 - \\
&\quad \frac{1}{2} \varepsilon s_1 C_1 + O(\varepsilon^3) \\
\dot{s}_2 &= i\varepsilon^2 \left(\frac{77259}{643600} s_2^3 s_1^2 + \frac{1}{8} s_2 C_1^2 \right) - \frac{3}{10} i\varepsilon s_2^2 s_1 - \frac{1449}{1609} \varepsilon^2 s_2^3 s_1^2 - \frac{1}{2} \varepsilon s_2 C_1 + \\
&\quad O(\varepsilon^3)
\end{aligned}$$

2.3.3 Emergent mode exactly at frequency one

So here, set forcing frequency back to one and re-analyse.

```

125 w:=1;
126 invariantmanifold({},      odes,
127      mat(( i,-i)),
128      mat( (1,+i,0,0,0,0), (1,-i,0,0,0,0)
129      ),
130      mat( (1,+i,0,0,0,0), (1,-i,0,0,0,0)
131      ),
132      2 )$
```

Invariant manifold ODEs The system evolves on the invariant manifold such that the parameters evolve according to these ODEs. They show the forcing directly pumps the mode.

$$\begin{aligned}
\dot{s}_1 &= -\frac{1}{4} F_1 i\varepsilon + \frac{3}{10} i\varepsilon s_2 s_1^2 - \frac{1}{2} \varepsilon s_1 C_1 + O(\varepsilon^2) \\
\dot{s}_2 &= \frac{1}{4} F_1 i\varepsilon - \frac{3}{10} i\varepsilon s_2^2 s_1 - \frac{1}{2} \varepsilon s_2 C_1 + O(\varepsilon^2)
\end{aligned}$$

2.3.4 Emergent mode near frequency one

For forcing $F \propto \cos[(1 + \omega')t]$ for small ω' we write $F := a \cos t - b \sin t$ where $a = F_1 \cos \omega' t$ and $b = F_1 \sin \omega' t$. Then $da/dt = -\omega' b$ and $db/dt = +\omega' a$ so code these relations, and truncate independently in small ω' .

```

133 F:=a*cos(t)-b*sin(t);
134 depend a,t; depend b,t;
135 let { df(a,t)=>-wd*b, df(b,t)=>wd*a, wd^3>0 };
```

Construct the invariant manifold for detuned forcing and find little difference, just a slowly modulating forcing through $a(t), b(t)$.

```

136 invariantmanifold( {},      odes,
137      mat(( i,-i)),
138      mat( (1,+i,0,0,0,0), (1,-i,0,0,0,0)
139          ),
140      mat( (1,+i,0,0,0,0), (1,-i,0,0,0,0)
141          ),
142      2 )$
```

Invariant manifold ODEs The system evolves on the invariant manifold such that the parameters evolve according to these ODEs.

$$\begin{aligned}\dot{s}_1 &= i\varepsilon\left(\frac{3}{10}s_2s_1^2 - \frac{1}{4}a\right) + \varepsilon\left(-\frac{1}{2}s_1C_1 + \frac{1}{4}b\right) + O(\varepsilon^2, \omega'^3) \\ \dot{s}_2 &= i\varepsilon\left(-\frac{3}{10}s_2^2s_1 + \frac{1}{4}a\right) + \varepsilon\left(-\frac{1}{2}s_2C_1 + \frac{1}{4}b\right) + O(\varepsilon^2, \omega'^3)\end{aligned}$$

Finish the script

```
143 end;
```

3 Slow invariant manifolds

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3.2	<code>lorenz86sm</code> : Slow manifold of the Lorenz 1986 atmosphere model	24
3.3	<code>majdaTriad2010</code> : project stochastic forcing in Majda's triad model	26

Also see Sections 1.1, 1.3 and 1.6.

3.1 `simple2d`: Slow manifold of a simple 2D system

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Slow manifold ODEs	24
Normals to isochrons at the slow manifold	24

The example system to analyse is specified to be

$$\dot{u}_1 = -u_1 + u_2 - u_1^2, \quad \dot{u}_2 = u_1 - u_2 + u_2^2.$$

Start by loading the procedure.

```
144 in_tex ".../invariantManifold.tex" $
```

Execute the construction of the slow manifold for this system.

```
145 invariantmanifold({},  
146     mat((-u1+u2-u1^2,u1-u2+u2^2)),  
147     mat((0)),  
148     mat((1,1)),  
149     mat((1,1)),  
150     5)$  
151 end;
```

We seek the slow manifold so specify the eigenvalue zero. From the linearisation matrix $\begin{bmatrix} -1 & 1 \\ 1 & -1 \end{bmatrix}$ a corresponding eigenvector is $\vec{e} = (1, 1)$, and corresponding left-eigenvector is $\vec{z} = \vec{e} = (1, 1)$, as specified. The last parameter specifies to construct the slow manifold to errors $\mathcal{O}(\varepsilon^5)$.

The procedure actually analyses the embedding system

$$\dot{u}_1 = -u_1 + u_2 - \varepsilon u_1^2, \quad \dot{u}_2 = u_1 - u_2 + \varepsilon u_2^2.$$

So here the artificial parameter ε has a physical interpretation in that it counts the nonlinearity: a term in ε^p will be a $(p+1)$ th order term in $\vec{u} = (u_1, u_2)$. Hence the specified error $\mathcal{O}(\varepsilon^5)$ is here the same as error $\mathcal{O}(|\vec{u}|^6)$.

The slow manifold The constructed slow manifold is, in terms of the parameter s_1 (and reverse ordering!),

$$\begin{aligned} u_1 &= 3/8\varepsilon^3 s_1^4 - 1/2\varepsilon s_1^2 + s_1, \\ u_2 &= -3/8\varepsilon^3 s_1^4 + 1/2\varepsilon s_1^2 + s_1. \end{aligned}$$

Slow manifold ODEs On this slow manifold the evolution is

$$\dot{s}_1 = -3/4\varepsilon^4 s_1^5 + \varepsilon^2 s_1^3 :$$

here the leading term in s_1^3 indicates the origin is unstable.

Normals to isochrons at the slow manifold To project initial conditions onto the slow manifold, or non-autonomous forcing, or modifications of the original system, or to quantify uncertainty, use the projection defined by the derived vector

$$\vec{z}_1 = \begin{bmatrix} z_{11} \\ z_{12} \end{bmatrix} = \begin{bmatrix} 3/2\varepsilon^4 s_1^4 + 3/4\varepsilon^3 s_1^3 - 1/2\varepsilon^2 s_1^2 - 1/2\varepsilon s_1 + 1/2 \\ 3/2\varepsilon^4 s_1^4 - 3/4\varepsilon^3 s_1^3 - 1/2\varepsilon^2 s_1^2 + 1/2\varepsilon s_1 + 1/2 \end{bmatrix}.$$

Evaluate these at $\varepsilon = 1$ to apply to the original specified system, or here just interpret ε as a way to count the order of each term.

3.2 lorenz86sm: Slow manifold of the Lorenz 1986 atmosphere model

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In this case we construct the slow sub-centre manifold, analogous to quasi-geostrophy, in order to disentangle the slow dynamics from fast oscillations, analogous to gravity waves, in the [Lorenz \(1986\)](#) model. The normals to the isochrons determine ‘balancing’ onto the slow manifold.

$$\begin{aligned} \dot{u}_1 &= bu_2u_5 - u_2u_3, \\ \dot{u}_2 &= -bu_1u_5 + u_1u_3, \\ \dot{u}_3 &= -u_1u_2, \\ \dot{u}_4 &= -u_5, \\ \dot{u}_5 &= bu_1u_2 + u_4. \end{aligned}$$

The parameter b controls the interaction between slow and fast waves. [Section 4.3](#) constructs its full state space normal form in order to determine the forcing of the slow modes by the mean fast waves.

Start by loading the procedure.

```
152 in_tex "../invariantManifold.tex"$
```

Group output expressions on b .

```
153 factor b;
```

Execute the construction of the slow manifold for this system.

```
154 invariantmanifold({},
155      mat(( -u2*u3+b*u2*u5,
156          u1*u3-b*u1*u5,
157          -u1*u2,
158          -u5,
159          +u4+b*u1*u2 )),
160      mat(( 0,0,0 )),
161      mat( (1,0,0,0,0),(0,1,0,0,0),(0,0,1,0,0) ),
162      mat( (1,0,0,0,0),(0,1,0,0,0),(0,0,1,0,0) ),
163      4 )$  

164 end;
```

The matrix of the linearisation about the origin has eigenvalues zero (multiplicity three) and $\pm i$. We seek the slow manifold so specify the eigenvalue zero (thrice) in the second parameter to the procedure. Since the system is already in linearly separated form, the slow eigenvectors are simply the three given unit vectors. The last parameter, 4, specifies to construct the slow manifold to errors $\mathcal{O}(\varepsilon^4)$, that is, to errors $\mathcal{O}(|\vec{s}|^5)$.

The procedure actually analyses the embedding system

$$\begin{aligned}\dot{u}_1 &= b\varepsilon u_2 u_5 - \varepsilon u_2 u_3, \\ \dot{u}_2 &= -b\varepsilon u_1 u_5 + \varepsilon u_1 u_3, \\ \dot{u}_3 &= -\varepsilon u_1 u_2, \\ \dot{u}_4 &= -u_5, \\ \dot{u}_5 &= b\varepsilon u_1 u_2 + u_4.\end{aligned}$$

Consequently, here the artificial parameter ε has a physical interpretation in that it counts the nonlinearity: a term in ε^p will be a $(p+1)$ th order term in \vec{s} .

The slow manifold The constructed slow manifold is, in terms of the parameters \vec{s} (to errors $\mathcal{O}(\varepsilon^3)$, and reverse ordering!),

$$\begin{aligned}u_1 &= s_1, \\ u_2 &= s_2, \\ u_3 &= s_3, \\ u_4 &= -b\varepsilon s_2 s_1, \\ u_5 &= b\varepsilon^2 (-s_3 s_2^2 + s_3 s_1^2).\end{aligned}$$

Slow manifold ODEs On this slow manifold the evolution is

$$\dot{s}_1 = b^2 \varepsilon^3 (-s_3 s_2^3 + s_3 s_2 s_1^2) - \varepsilon s_3 s_2,$$

$$\begin{aligned}\dot{s}_2 &= b^2 \varepsilon^3 (s_3 s_2^2 s_1 - s_3 s_1^3) + \varepsilon s_3 s_1, \\ \dot{s}_3 &= -\varepsilon s_2 s_1.\end{aligned}$$

Here the quadratic terms in s_1, s_2, s_3 is that of nonlinear slow wave oscillations. The b -terms modify these slow waves, reflecting the influence of the fast dynamics (as distinct from the effects of fast waves—these effects are quantified by [Section 4.3](#)).

Normals to isochrons at the slow manifold To project initial conditions onto the slow manifold, or non-autonomous forcing, or modifications of the original system, or to quantify uncertainty ([Roberts 1989, 2000](#)), use the projection defined by the derived vectors

$$\begin{aligned}\vec{z}_1 &= \begin{bmatrix} b^2 \varepsilon^2 s_2^2 + 1 \\ b^2 \varepsilon^2 s_2 s_1 \\ 0 \\ b^3 \varepsilon^3 (s_2^3 - s_2 s_1^2) + b \varepsilon^3 (-s_2^3 + s_2 s_1^2) + b \varepsilon s_2 \\ 0 \end{bmatrix}, \\ \vec{z}_2 &= \begin{bmatrix} -b^2 \varepsilon^2 s_2 s_1 \\ -b^2 \varepsilon^2 s_1^2 + 1 \\ 0 \\ b^3 \varepsilon^3 (-s_2^2 s_1 + s_1^3) + b \varepsilon^3 (s_2^2 s_1 - s_1^3) - b \varepsilon s_1 \\ 0 \end{bmatrix}, \\ \vec{z}_3 &= \begin{bmatrix} 0 \\ 0 \\ 1 \\ -4b \varepsilon^3 s_3 s_2 s_1 \\ b \varepsilon^2 (-s_2^2 + s_1^2) \end{bmatrix}.\end{aligned}$$

Evaluate these at $\varepsilon = 1$ to apply to the original specified system, or here just interpret ε as a way to count the order of each term.

3.3 majdaTriad2010: project stochastic forcing in Majda's triad model

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Normals to isochrons at the slow manifold . . .	28
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[Falasca \(2025\)](#) investigated averaging in the 3D SDE system of [Majda et al. \(2010\)](#). Let's see how the deterministic slow manifold projection matches their heuristic stochastic normal form: (B2) by [Falasca \(2025\)](#) and/or (47) by [Majda et al. \(2010\)](#).

Start by loading the procedure.

```
165 in_tex ".../invariantManifold.tex"$
```

The system uses parameters L_{1j} and γ_j so define the following: **clear gamma** because by default it is the gamma function.

```
166 off raise,lower;
167 operator L; defindex L(down);
168 clear gamma;
169 operator gamma; defindex gamma(down);
```

The additive triad model of [Falasca \(2025\)](#), [Majda et al. \(2010\)](#) consists of three modes, x_1 , x_2 and x_3 , evolving in time according to the stochastic ODES

$$\begin{aligned}\frac{dx_1}{dt'} &= L_1 x_1 + L_2 x_2 + L_3 x_3 + I x_2 x_3, \\ \frac{dx_2}{dt'} &= -\gamma_2 \epsilon^{-1} x_2 - L_2 x_1 - I x_1^2 + \sigma_2 \epsilon^{-1/2} \dot{W}_2, \\ \frac{dx_3}{dt'} &= -\gamma_3 \epsilon^{-1} x_3 - L_3 x_1 + \sigma_3 \epsilon^{-1/2} \dot{W}_3,\end{aligned}$$

where L_j and σ_j are some constants, and there is independent stochastic forcing of the second and third modes.

With its divisions by ϵ , the system is written in singular perturbation form. Unfortunately, singular perturbations often ‘sweep-under-the-carpet’ key physics that occur at finite ϵ . So first rescale time to the fast time $t = t'/\epsilon$ and define **small** = $\epsilon := \sqrt{\epsilon}$ for convenience. In terms of new dependent variables $u_j := x_j$ the above triad system becomes

$$\begin{aligned}\frac{du_1}{dt} &= \epsilon^2 (L_1 u_1 + L_2 u_2 + L_3 u_3 + I u_2 u_3), \\ \frac{du_2}{dt} &= -\gamma_2 u_2 + \epsilon^2 (-L_2 u_1 - I u_1^2) + \sigma_2 \dot{W}_2, \\ \frac{du_3}{dt} &= -\gamma_3 u_3 - \epsilon^2 L_3 u_1 + \sigma_3 \dot{W}_3,\end{aligned}$$

Because of their decay rates γ_2, γ_3 , over long time scales we expect the second and third modes to be essentially negligible and the system to be modelled by the relatively slow evolution of the first mode. However, the stochastic forcing excites these modes and we turn to the projection vectors to determine how they then affect the slow manifold model.

The procedure **invariantmanifold** is previously loaded. Write a message saying we are now analysing the next system.

```
170 write "**** Additive Triad system of Majda (2010) ****";
```

Construct a slow manifold for the deterministic system (no stochastic noise): terms in **small** = ϵ get multiplied by another factor of **small** = ϵ before analysis, so these explicit **small** factors become equivalent to ϵ factors;

```
171 factor small;
```

```

172 invariantmanifold( {},
173   mat( ( small*( L(1)*u1+L(2)*u2+L(3)*u3 +I*u1*u2 ),
174     -gamma(2)*u2 +small*( -L(2)*u1-I*u1^2 ),
175     -gamma(3)*u3 -small*L(3)*u1 ) ),
176   mat( ( 0 ) ),
177   mat( ( 1,0,0 ) ),
178   mat( ( 1,0,0 ) ),
179   6 )$)
180 end;

```

The procedure reports that it analyses the following family

$$\begin{aligned}\dot{u}_1 &= \varepsilon^2(L_3u_3 + L_2u_2 + L_1u_1 + Iu_1u_2) \\ \dot{u}_2 &= \varepsilon^2(-L_2u_1 - Iu_1^2) - \gamma_2u_2 \\ \dot{u}_3 &= -\varepsilon^2L_3u_1 - \gamma_3u_3\end{aligned}$$

Here, ε^2 counts the order of perturbation in ϵ .

The invariant manifold These give the location of the invariant manifold in terms of parameters s_1 and $\epsilon = \varepsilon^2$.

$$\begin{aligned}u_1 &= s_1 + O(\varepsilon^5) \\ u_2 &= \varepsilon^2(-L_2\gamma_2^{-1}s_1 - \gamma_2^{-1}s_1^2I) + \varepsilon^4(L_2L_1\gamma_2^{-2}s_1 + 2L_1\gamma_2^{-2}s_1^2I) + O(\varepsilon^5) \\ u_3 &= -\varepsilon^2L_3\gamma_3^{-1}s_1 + \varepsilon^4L_3L_1\gamma_3^{-2}s_1 + O(\varepsilon^5)\end{aligned}$$

Invariant manifold ODEs The system evolves on the invariant manifold such that the parameters evolve according to this ODE.

$$\dot{s}_1 = \varepsilon^2L_1s_1 + \varepsilon^4(-L_3^2\gamma_3^{-1}s_1 - L_2^2\gamma_2^{-1}s_1 - 2L_2\gamma_2^{-1}s_1^2I - \gamma_2^{-1}s_1^3I^2) + O(\varepsilon^6)$$

These match the deterministic part of [Falasca \(2025\)](#)'s (B2) and [Majda et al. \(2010\)](#)'s (47)—except of course for the quadratic noise-noise induced drifts in his Itô form.

The stochastic parts of (B2) and/or (47) now come from the projection of forcing onto the above deterministic slow manifold.

Normals to isochrons at the slow manifold Use these vectors: to project initial conditions onto the slow manifold; to project non-autonomous forcing onto the slow evolution; to predict the consequences of modifying the original system; in uncertainty quantification to quantify effects on the model of uncertainties in the original system. The normal vector

$$\vec{z} := \begin{bmatrix} 1 + \varepsilon^4(L_3^2\gamma_3^{-2} + L_2^2\gamma_2^{-2} + 3L_2\gamma_2^{-2}s_1I + 2\gamma_2^{-2}s_1^2I^2) + O(\varepsilon^6) \\ + \varepsilon^2(L_2\gamma_2^{-1} + \gamma_2^{-1}s_1I) - \varepsilon^4L_2L_1\gamma_2^{-2} + O(\varepsilon^6) \\ + \varepsilon^2L_3\gamma_3^{-1} - \varepsilon^4L_3L_1\gamma_3^{-2} + O(\varepsilon^6) \end{bmatrix}$$

$$= \begin{bmatrix} 1 + O(\varepsilon^4) \\ +\varepsilon^2(L_2\gamma_2^{-1} + \gamma_2^{-1}s_1I) + O(\varepsilon^4) \\ +\varepsilon^2L_3\gamma_3^{-1} + O(\varepsilon^4) \end{bmatrix}.$$

Consequently, the leading effect of the stochastic forcing $\vec{f} := (0, \sigma_2 \dot{W}_2, \sigma_3 \dot{W}_3)$ is to add the following stochastic terms to the s_1 ODE: namely, and agreeing with [Falasca \(2025\)](#)'s (B2),

$$+\varepsilon^2(L_2\gamma_2^{-1} + \gamma_2^{-1}s_1I)\sigma_2 \dot{W}_2 + \varepsilon^2L_3\gamma_3^{-1}\sigma_3 \dot{W}_3.$$

Summary The derived projection vectors also determine how stochastic forcing effects are mapped onto a slow manifold, to linear effects in the noise.

4 Oscillation in a centre manifold

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Also see Sections 1.4 and 2.2.

4.1 `simpleosc`: Oscillatory centre manifold—separated form

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Let's try complex eigenvectors. Adjoint eigenvectors \mathbf{zz}_- must be the eigenvectors of the complex conjugate transpose matrix.

$$\begin{aligned}\dot{u}_1 &= u_2 \\ \dot{u}_2 &= -\varepsilon u_3 u_1 - u_1 \\ \dot{u}_3 &= 5\varepsilon u_1^2 - u_3\end{aligned}$$

Start by loading the procedure.

```
181 in_tex "../invariantManifold.tex"$
```

In the printed output, group terms with like powers of amplitudes s_j and the complex exponential

```
182 factor s,exp;
```

Execute the construction of the centre manifold for this system.

```
183 invariantmanifold({},  
184     mat((u2,-u1-u1*u3,-u3+5*u1^2)),  
185     mat((i,-i)),  
186     mat((1,+i,0),(1,-i,0)),  
187     mat((1,+i,0),(1,-i,0)),  
188     3)$  
189 end;
```

The centre manifold These give the location of the invariant manifold in terms of parameters s_j .

$$\begin{aligned} u_1 &= e^{-it}s_2 + e^{it}s_1 \\ u_2 &= -e^{-it}s_2i + e^{it}s_1i \\ u_3 &= e^{-2it}s_2^2\varepsilon(2i+1) + e^{2it}s_1^2\varepsilon(-2i+1) + 10s_2s_1\varepsilon \end{aligned}$$

Centre manifold ODEs The system evolves on the invariant manifold such that the parameters evolve according to these ODEs.

$$\begin{aligned} \dot{s}_1 &= s_2s_1^2\varepsilon^2(11/2i+1) \\ \dot{s}_2 &= s_2^2s_1\varepsilon^2(-11/2i+1) \end{aligned}$$

4.2 quasidde: Quasi-delay DE with Hopf bifurcation

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Centre manifold ODEs	32

Shows Hopf bifurcation as parameter α crosses 0 to oscillations with base frequency two.

$$\begin{aligned} \dot{u}_1 &= -\alpha\varepsilon^2u_3 - \varepsilon^2u_1^3 - 2\varepsilon u_1^2 - 4u_3 \\ \dot{u}_2 &= 2u_1 - 2u_2 \\ \dot{u}_3 &= 2u_2 - 2u_3 \end{aligned}$$

for small parameter α . We code the parameter α as ‘small’, and observe it is consequently considered as ‘small squared’ because all nonlinear terms and already ‘small’ terms, are multiplied by another `small`.

Start by loading the procedure.

```
190 in_tex ".../invariantManifold.tex"$
```

In the printed output, group terms with like powers of amplitudes s_j , the complex exponential, and the parameter α .

```
191 factor s,exp,alpha;
```

Execute the construction of the slow manifold for this system (ignore the warning messages about `u1` declared, and then already defined, as an operator).

```
192 invariantmanifold{},
193      mat((-4*u3-small*alpha*u3-2*u1^2-small*u1^3,
194           2*u1-2*u2,
195           2*u2-2*u3)),
196      mat((2*i,-2*i)),
197      mat((1,1/2-i/2,-i/2),(1,1/2+i/2,+i/2)),
198      mat((1,-i,-1-i),(1,+i,-1+i)),
199      3)$
200 end;
```

The centre manifold These give the location of the invariant manifold in terms of parameters s_1, s_2 (complex conjugate for real solutions).

$$\begin{aligned} u_1 &= e^{-4it}s_2^2\varepsilon(-7/12i + 1/12) + e^{-2it}s_2 + e^{4it}s_1^2\varepsilon(7/12i + 1/12) + e^{2it}s_1 - s_2s_1\varepsilon \\ u_2 &= e^{-4it}s_2^2\varepsilon(-1/12i + 1/4) + e^{-2it}s_2(1/2i + 1/2) + e^{4it}s_1^2\varepsilon(1/12i + 1/4) + e^{2it}s_1(-1/2i + 1/2) - s_2s_1\varepsilon \\ u_3 &= e^{-4it}s_2^2\varepsilon(1/12i + 1/12) + 1/2e^{-2it}s_2i + e^{4it}s_1^2\varepsilon(-1/12i + 1/12) - 1/2e^{2it}s_1i - s_2s_1\varepsilon \end{aligned}$$

Centre manifold ODEs The system evolves on the invariant manifold such that the parameters evolve according to these ODEs.

$$\begin{aligned} \dot{s}_1 &= s_2s_1^2\varepsilon^2(-16/15i - 1/5) + s_1\alpha\varepsilon^2(1/5i + 1/10) \\ \dot{s}_2 &= s_2^2s_1\varepsilon^2(16/15i - 1/5) + s_2\alpha\varepsilon^2(-1/5i + 1/10) \end{aligned}$$

Hence there is a supercritical Hopf bifurcation as parameter α increases through zero.

4.3 lorenz86nf: Paradoxically justify a slow manifold despite being proven to not exist

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Lorenz (1986) proposed the following simple system in order to understand aspects of the quasi-geostrophic approximation in atmospheric dynamics.

$$\begin{aligned} \dot{u}_1 &= bu_2u_5 - u_2u_3, \\ \dot{u}_2 &= -bu_1u_5 + u_1u_3, \\ \dot{u}_3 &= -u_1u_2, \\ \dot{u}_4 &= -u_5, \\ \dot{u}_5 &= bu_1u_2 + u_4. \end{aligned}$$

The parameter b controls the interaction between slow and fast dynamics. As in Section 3.2, it appears that a slow manifold of quasi-geostrophy exists and is constructible. Nonetheless, Lorenz & Krishnamurthy (1987) proved that a slow manifold cannot exist for this system!

A resolution of this apparent paradox comes via backwards theory (Roberts 2022, §2.5). There are systems exponentially close to the above Lorenz86 system (that is, asymptotically the same to all orders in $|\vec{u}|$) which do possess a slow manifold. Hence the properties that cause the non-existence are exponentially small, they

are beyond all orders, and so are likely to be physically irrelevant—they are likely to be smaller than the mathematical modelling errors of the original system.

Let's see this resolution by constructing, to any specified order, a system that has a slow manifold and is close to the Lorenz86 system. We do this by constructing a coordinate transform of the 5D state space. Start by loading the procedure.

```
201 in_tex "../invariantManifold.tex"$
```

Group output expressions on b .

```
202 factor b;
203 %b:=1; factor small;% or otherwise
```

Execute the construction of the coordinate transform for this system.

```
204 invariantmanifold({},
205     mat((-u2*u3+b*u2*u5,
206         u1*u3-b*u1*u5,
207         -u1*u2,
208         -u5,
209         +u4+b*u1*u2 )),
210     mat((0,0,0,i,-i)),
211     mat((1,0,0,0,0),(0,1,0,0,0),(0,0,1,0,0),
212         (0,0,0,1,-i), (0,0,0,1,+i)),
213     mat((1,0,0,0,0),(0,1,0,0,0),(0,0,1,0,0),
214         (0,0,0,1,-i), (0,0,0,1,+i)),
215     4 )$)
216 end;
```

The matrix of the linearisation about the origin has eigenvalues zero (multiplicity three) and $\pm i$, as specified for the eigenvalues in the second parameter to the procedure. Corresponding eigenvectors are simply the three unit vectors and the two complex eigenvectors of the fast waves. The last parameter, 4, specifies to construct the slow manifold to errors $\mathcal{O}(\varepsilon^4)$, that is, to errors $\mathcal{O}(|\vec{s}|^5)$.

The procedure actually analyses the embedding system

$$\begin{aligned}\dot{u}_1 &= b\varepsilon u_2 u_5 - \varepsilon u_2 u_3, \\ \dot{u}_2 &= -b\varepsilon u_1 u_5 + \varepsilon u_1 u_3, \\ \dot{u}_3 &= -\varepsilon u_1 u_2, \\ \dot{u}_4 &= -u_5, \\ \dot{u}_5 &= b\varepsilon u_1 u_2 + u_4.\end{aligned}$$

The coordinate transform The constructed coordinate transform is, in terms of the slow variables \vec{s} and a time-dependent basis (to errors $\mathcal{O}(\varepsilon^3)$, and reverse ordering!),

$$u_1 = b^2 \varepsilon^2 (-1/2 e^{-2it} s_5^2 s_1 - 1/2 e^{2it} s_4^2 s_1) + b\varepsilon (-e^{-it} s_5 s_2 - e^{it} s_4 s_2) + s_1,$$

$$\begin{aligned}
u_2 &= b^2 \varepsilon^2 (-1/2 e^{-2it} s_5^2 s_2 - 1/2 e^{2it} s_4^2 s_2) + b \varepsilon (e^{-it} s_5 s_1 + e^{it} s_4 s_1) + s_2, \\
u_3 &= b \varepsilon^2 (e^{-it} s_5 s_2^2 i - e^{-it} s_5 s_1^2 i - e^{it} s_4 s_2^2 i + e^{it} s_4 s_1^2 i) + s_3, \\
u_4 &= b^2 \varepsilon^2 (1/4 e^{-it} s_5 s_2^2 - 1/4 e^{-it} s_5 s_1^2 + 1/4 e^{it} s_4 s_2^2 - 1/4 e^{it} s_4 s_1^2) - b \varepsilon s_2 s_1 + e^{-it} s_5 + e^{it} s_4, \\
u_5 &= b^2 \varepsilon^2 (-1/4 e^{-it} s_5 s_2^2 i + 1/4 e^{-it} s_5 s_1^2 i + 1/4 e^{it} s_4 s_2^2 i - 1/4 e^{it} s_4 s_1^2 i) + b \varepsilon^2 (-s_3 s_2^2 + s_3 s_1^2) + e^{-it} s_5 i - e^{it} s_4 i.
\end{aligned}$$

Transformed ODEs In the variables \vec{s} the evolution is

$$\begin{aligned}
\dot{s}_1 &= b^2 \varepsilon^3 (-s_3 s_2^3 + s_3 s_2 s_1^2) - \varepsilon s_3 s_2, \\
\dot{s}_2 &= b^2 \varepsilon^3 (s_3 s_2^2 s_1 - s_3 s_1^3) + \varepsilon s_3 s_1, \\
\dot{s}_3 &= \color{red}{2b^2 \varepsilon^3 s_5 s_4 s_2 s_1} - \varepsilon s_2 s_1, \\
\dot{s}_4 &= b^2 \varepsilon^2 (-1/2 s_4 s_2^2 i + 1/2 s_4 s_1^2 i), \\
\dot{s}_5 &= b^2 \varepsilon^2 (1/2 s_5 s_2^2 i - 1/2 s_5 s_1^2 i).
\end{aligned}$$

When $s_4 = s_5 = 0$ we recover precisely the same slow manifold as constructed by [Section 3.2](#). Hence the above system of $\vec{u} = \dots$ and $\dot{\vec{s}} = \dots$ together both has a slow manifold, and is $\mathcal{O}(|\vec{s}|^5)$ close to the original Lorenz86 system. Such construction can proceed to any order, and so the above closeness of a system with a slow manifold holds to all orders in $|\vec{s}|$.

Also of interest is the red term in the \dot{s}_3 ODE: it shows that the evolution of the slow variables, s_1, s_2, s_3 , is affected by the presence of fast waves, s_4, s_5 non-zero. That is, the evolution on and off the slow manifold differ by this term (and similar higher-order terms). Users of slow models among fast waves need to be aware of this physical feature.

4.4 stoleriu2: Oscillatory centre manifold among stable and unstable modes

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Consider the case [Stoleriu \(2012\)](#) calls $(3\pi/4, k^2/2)$.

$$\begin{aligned}
\dot{u}_1 &= u_2, \\
\dot{u}_2 &= -\sigma u_3 + 1 - \cos u_1, \\
\dot{u}_3 &= u_4, \\
\dot{u}_4 &= (u_3 + \frac{1}{\sigma}) \sin u_1
\end{aligned}$$

Eigenvalues are ± 1 and $\pm i$, so we find the centre manifold among stable and unstable modes.

Start by loading the procedure.

```
217 in_tex ".../invariantManifold.tex" $
```

In the printed output, group terms with like powers of amplitudes s_j and the complex exponential

```
218 factor s,exp;
```

Execute the construction of the centre manifold for Stoleriu's system. But use Taylor expansions for trigonometric functions in the ODES, and multiply higher-orders of nonlinearity by `small` to better (not best) count and manage nonlinearities.

```
219 invariantmanifold( {},  
220      mat(( u2,  
221          sigma*u3+u1^2/2-small*u1^4/24,  
222          u4,  
223          (u3+1/sigma)*(u1-small*u1^3/6)  
224          ),  
225          mat(( i,-i )),  
226          mat( (sigma,i*sigma,-1,-i),(sigma,-i*sigma,-1,+i) ),  
227          mat( (+i,-1,-i*sigma,sigma),(-i,-1,+i*sigma,sigma) ),  
228          3)$  
229 end;
```

Code adjoint eigenvectors `zz_` that are eigenvectors of the complex conjugate transpose matrix of the linear matrix $\begin{bmatrix} 0 & 1 & 0 & 0 \\ 0 & 0 & \sigma & 0 \\ 0 & 0 & 0 & 1 \\ 1/\sigma & 0 & 0 & 0 \end{bmatrix}$. Here analyse to errors $\mathcal{O}(\varepsilon^3)$.

The procedure analyses the embedding system

$$\begin{aligned}\dot{u}_1 &= u_2, \\ \dot{u}_2 &= -1/24\varepsilon^2 u_1^4 + 1/2\varepsilon u_1^2 + \sigma u_3, \\ \dot{u}_3 &= u_4, \\ \dot{u}_4 &= \varepsilon^2 (-1/6\sigma^{-1}u_1^3 - 1/6u_1^3 u_3) + \varepsilon u_1 u_3 + \sigma^{-1} u_1\end{aligned}$$

The centre manifold These give the location of the invariant manifold in terms of (complex conjugate) parameters s_1, s_2 .

$$\begin{aligned}u_1 &= e^{-it}s_2\sigma - 1/5e^{-2it}s_2^2\varepsilon\sigma^2 + e^{it}s_1\sigma - 1/5e^{2it}s_1^2\varepsilon\sigma^2 + 2s_2s_1\varepsilon\sigma^2 \\ u_2 &= -e^{-it}s_2i\sigma + 2/5e^{-2it}s_2^2\varepsilon i\sigma^2 + e^{it}s_1i\sigma - 2/5e^{2it}s_1^2\varepsilon i\sigma^2 \\ u_3 &= -e^{-it}s_2 + 3/10e^{-2it}s_2^2\varepsilon\sigma - e^{it}s_1 + 3/10e^{2it}s_1^2\varepsilon\sigma - s_2s_1\varepsilon\sigma \\ u_4 &= e^{-it}s_2i - 3/5e^{-2it}s_2^2\varepsilon i\sigma - e^{it}s_1i + 3/5e^{2it}s_1^2\varepsilon i\sigma\end{aligned}$$

Centre manifold ODEs The system evolves on the centre manifold such that the parameters evolve according to these ODEs.

$$\begin{aligned}\dot{s}_1 &= -6/5s_2s_1^2\varepsilon^2i\sigma^2 \\ \dot{s}_2 &= 6/5s_2^2s_1\varepsilon^2i\sigma^2\end{aligned}$$

These establish that the leading effect of the nonlinearities is to cause a frequency down-shift in the oscillations on the centre manifold. Higher-order analysis indicates the only effect is a frequency shift of the nonlinear oscillations.

4.5 bauer2021: Rephrase phase-averaging as nonlinear normal modes

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Bauer et al. (2021) introduced a *higher order phase averaging method* for nonlinear oscillatory systems. Here we construct cognate high-order approximations by constructing the modulation of the nonlinear normal modes in the system. Their example system (3.2) may be rewritten in variables $\vec{u}(t)$ as

$$\begin{aligned}\dot{u}_1 &= \omega_R u_2, & \dot{u}_2 &= -\omega_R u_1 + \frac{\lambda}{\omega_R} u_1 u_5, \\ \dot{u}_3 &= \omega_R u_4, & \dot{u}_4 &= -\omega_R u_3 + \frac{\lambda}{\omega_R} u_3 u_5, \\ \dot{u}_5 &= \omega_Z u_6, & \dot{u}_6 &= -\omega_Z u_5 + \frac{\lambda}{\omega_z} (u_1^2 + u_3^2).\end{aligned}$$

Bauer et al. (2021), their §4, chose base frequencies $\omega_R = \pi$ and $\omega_Z = 2\pi$ so we do so also.

The linearisation at the origin then has the following modes:

- eigenvalues $\pm i\pi$ with corresponding eigenvectors proportional to $(1, \pm i, 0, 0, 0, 0)$ and $(0, 0, 1, \pm i, 0, 0)$;
- eigenvalues $\pm 2i\pi$ with corresponding eigenvector proportional to $(0, 0, 0, 0, 1, \pm i)$.

We model the nonlinear interaction of these six modes over long times—these are the nonlinear normal modes. The analysis constructs a full state space coordinate transformation mapping from the complex-valued modulation variables $\vec{s} = (s_1, \dots, s_6)$ to the original variables $\vec{u} = (u_1, \dots, u_6)$, and find the corresponding evolution of \vec{s} . The modulation variables \vec{s} are ‘slow’ because the coordinate transform uses time-dependent (rotating) basis vectors that account for the fast oscillation in \vec{u} . Hence the new variables \vec{s} are good variables for making long-term predictions and forming understanding.

Start by loading the procedure.

```
230 in_tex "../invariantManifold.tex"$
```

In the printed output, group terms depending upon real or imaginary coefficient, and factor out π .

```
231 factor pi,i;
```

The following procedure call constructs the time-dependent coordinate transform for this system.

```
232 invariantmanifold({},  
233      mat((pi*u2,-pi*u1+u1*u5/pi
```

```

234      ,pi*u4,-pi*u3+u3*u5/pi
235      ,2*pi*u6,-2*pi*u5+(u1^2+u3^2)/pi/2 )),
236      mat((pi*i,-pi*i,pi*i,-pi*i,2*pi*i,-2*pi*i)),
237      mat((1,+i,0,0,0,0),(1,-i,0,0,0,0)
238      ,(0,0,1,+i,0,0),(0,0,1,-i,0,0)
239      ,(0,0,0,0,1,+i),(0,0,0,0,1,-i)),
240      mat((1,+i,0,0,0,0),(1,-i,0,0,0,0)
241      ,(0,0,1,+i,0,0),(0,0,1,-i,0,0)
242      ,(0,0,0,0,1,+i),(0,0,0,0,1,-i)),
243      3 )$  

244 end;

```

The procedure then actually analyses the embedding system

$$\begin{aligned}\dot{u}_1 &= \pi u_2 & \dot{u}_2 &= -\pi u_1 + \pi^{-1} \varepsilon u_1 u_5 \\ \dot{u}_3 &= \pi u_4 & \dot{u}_4 &= -\pi u_3 + \pi^{-1} \varepsilon u_3 u_5 \\ \dot{u}_5 &= 2\pi u_6 & \dot{u}_6 &= -2\pi u_5 + \pi^{-1} \varepsilon (1/2u_1^2 + 1/2u_3^2)\end{aligned}$$

Hence the procedure's artificial parameter ε is precisely the physical parameter λ of [Bauer et al. \(2021\)](#). As specified, the construction is here done to errors $\mathcal{O}(\varepsilon^3)$.

The invariant manifold Here these give the reparametrisation of the state space \vec{u} in terms of modulation variables s_j , via rotating basis vectors.

$$\begin{aligned}u_1 &= e^{-i\pi t} s_2 + e^{i\pi t} s_1 + \pi^{-2} \varepsilon (1/4 e^{-i\pi t} s_6 s_1 - 1/8 e^{-3i\pi t} s_6 s_2 + \\ &\quad 1/4 e^{i\pi t} s_5 s_2 - 1/8 e^{3i\pi t} s_5 s_1) \\ u_2 &= i(-e^{-i\pi t} s_2 + e^{i\pi t} s_1) + \pi^{-2} i \varepsilon (1/4 e^{-i\pi t} s_6 s_1 + \\ &\quad 3/8 e^{-3i\pi t} s_6 s_2 - 1/4 e^{i\pi t} s_5 s_2 - 3/8 e^{3i\pi t} s_5 s_1) \\ u_3 &= e^{-i\pi t} s_4 + e^{i\pi t} s_3 + \pi^{-2} \varepsilon (1/4 e^{-i\pi t} s_6 s_3 - 1/8 e^{-3i\pi t} s_6 s_4 + \\ &\quad 1/4 e^{i\pi t} s_5 s_4 - 1/8 e^{3i\pi t} s_5 s_3) \\ u_4 &= i(-e^{-i\pi t} s_4 + e^{i\pi t} s_3) + \pi^{-2} i \varepsilon (1/4 e^{-i\pi t} s_6 s_3 + \\ &\quad 3/8 e^{-3i\pi t} s_6 s_4 - 1/4 e^{i\pi t} s_5 s_4 - 3/8 e^{3i\pi t} s_5 s_3) \\ u_5 &= e^{-2i\pi t} s_6 + e^{2i\pi t} s_5 + \pi^{-2} \varepsilon (1/16 e^{-2i\pi t} s_4^2 + 1/16 e^{-2i\pi t} s_2^2 + \\ &\quad 1/16 e^{2i\pi t} s_3^2 + 1/16 e^{2i\pi t} s_1^2 + 1/2 s_4 s_3 + 1/2 s_2 s_1) \\ u_6 &= i(-e^{-2i\pi t} s_6 + e^{2i\pi t} s_5) + \pi^{-2} i \varepsilon (1/16 e^{-2i\pi t} s_4^2 + \\ &\quad 1/16 e^{-2i\pi t} s_2^2 - 1/16 e^{2i\pi t} s_3^2 - 1/16 e^{2i\pi t} s_1^2)\end{aligned}$$

Invariant manifold ODEs The system evolves according to these ODEs that characterise how the modulation of the oscillations evolve in state space due to their nonlinear interaction.

$$\begin{aligned}\dot{s}_1 &= -1/2\pi^{-1} i \varepsilon s_5 s_2 + \pi^{-3} i \varepsilon^2 (-1/16 s_6 s_5 s_1 - 1/4 s_4 s_3 s_1 - \\ &\quad 1/32 s_3^2 s_2 - 9/32 s_2 s_1^2) \\ \dot{s}_2 &= 1/2\pi^{-1} i \varepsilon s_6 s_1 + \pi^{-3} i \varepsilon^2 (1/16 s_6 s_5 s_2 + 1/32 s_4^2 s_1 + 1/4 s_4 s_3 s_2 + \\ &\quad 9/32 s_2^2 s_1)\end{aligned}$$

$$\begin{aligned}\dot{s}_3 &= -1/2\pi^{-1}i\varepsilon s_5 s_4 + \pi^{-3}i\varepsilon^2(-1/16s_6 s_5 s_3 - 9/32s_4 s_3^2 - \\ &\quad 1/32s_4 s_1^2 - 1/4s_3 s_2 s_1) \\ \dot{s}_4 &= 1/2\pi^{-1}i\varepsilon s_6 s_3 + \pi^{-3}i\varepsilon^2(1/16s_6 s_5 s_4 + 9/32s_4^2 s_3 + 1/4s_4 s_2 s_1 + \\ &\quad 1/32s_3 s_2^2) \\ \dot{s}_5 &= \pi^{-1}i\varepsilon(-1/4s_3^2 - 1/4s_1^2) + \pi^{-3}i\varepsilon^2(-1/16s_5 s_4 s_3 - 1/16s_5 s_2 s_1) \\ \dot{s}_6 &= \pi^{-1}i\varepsilon(1/4s_4^2 + 1/4s_2^2) + \pi^{-3}i\varepsilon^2(1/16s_6 s_4 s_3 + 1/16s_6 s_2 s_1)\end{aligned}$$

These all preserve complex conjugation, and so preserve reality. All coefficients are pure imaginary, so the dominant effect of the modulation is to modify the frequency of the oscillations. Amplitude modifications arise due to the phase relationship between the modes.

4.6 timeVaryingForcing: slowly varying in time forcing of a spectral sub-centre manifold

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[Section 2.2](#) constructed a spectral submanifold of a system forced by sinusoidal factors $\cos t$ and $\sin(t/2)$. Our modelling code can also model arbitrary forcing provided the forcing is varying slowly enough in time.

Thus let's modify the system of [Section 2.2](#) to

$$\begin{aligned}\dot{x}_1 &= x_3, \quad \dot{x}_3 = -2x_1 + x_2 - \frac{1}{2}x_1^3 + \frac{3}{10}(-x_3 + x_4) + F_1(t), \\ \dot{x}_2 &= x_4, \quad \dot{x}_4 = x_1 - 2x_2 + \frac{3}{10}(x_3 - 2x_4)F_2(t).\end{aligned}$$

where $F_1(t)$ is the strength of a direct forcing, and $F_2(t)$ is the strength of a parametric variation. A linearisation of this system at the origin has modes with frequencies $\omega = 1, \sqrt{3}$, corresponding eigenvalues $\lambda = \pm i, \pm i\sqrt{3}$, and corresponding eigenvectors $(1, 1, \pm i\omega, \pm i\omega)$. Corresponding eigenvectors of the adjoint are $(1, 1, \pm i, \pm i)$ and $(\mp i\omega, \pm i\omega, 1, -1)$. We construct the spectral sub-centre manifold (e.g., [Sijbrand 1985](#), §7) of the nonlinear forced dynamics of the frequency one mode.

Start by loading the procedure.

```
245 in_tex ".../invariantManifold.tex"$
```

In the printed output, group terms with like powers of amplitudes s_j , and with like effects in the forcing and its time-derivatives.

```
246 factor df,F_1,F_2,small;
247 depend F_1,t; depend F_2,t;
```

To encode that the time-variation of the forcing is somehow slow, we need to truncate the analysis to some order of time-derivatives

of the forcing F_j . Here choose to truncate by neglecting third and higher order derivatives.

```
248 let { df(F_1,t,3)>0, df(F_2,t,3)>0 };
```

These are truncations additional to that of the procedure call that specifies also truncating to errors $\mathcal{O}(\varepsilon^5)$.

The following code makes the linear damping to be effectively small (which then makes it `small` squared); consequently, also scale the smallness of the cubic nonlinearity to match.

```
249 invariantmanifold{},
250   mat(( u3, u4,
251     -2*u1+u2-small*u1^3/2+small*3/10*(-u3+u4)+small*F_1,
252     u1-2*u2+small*3/10*(u3-2*u4)*F_2 ),
253   mat(( i,-i )),
254   mat( (1,1,+i,+i), (1,1,-i,-i) ),
255   mat( (1,1,+i,+i), (1,1,-i,-i) ),
256   5 )$  
257 end;
```

The procedure reports that it actually analyses the embedding system

$$\begin{aligned}\dot{u}_1 &= u_3, & \dot{u}_2 &= u_4, \\ \dot{u}_3 &= F_1\varepsilon^2 + \varepsilon^2(-1/2u_1^3 - 3/10u_3 + 3/10u_4) - 2u_1 + u_2, \\ \dot{u}_4 &= F_2\varepsilon^2(3/10u_3 - 3/5u_4) + u_1 - 2u_2.\end{aligned}$$

The invariant manifold Here these give the reparametrisation of the state space \vec{u} in terms of parameters s_1, s_2 , via rotating basis vectors. Here, the coordinate transform is complicated. Interesting effects are the those on the shape of the spectral sub-centre manifold of the forcings F_j and their ‘slow’ time-derivatives. Quadratic effects would be seen here at order ε^4 .

$$\begin{aligned}u_1 &= -5/9 \frac{\partial^2 F_1}{\partial t^2} \varepsilon^2 + \frac{\partial^2 F_2}{\partial t^2} \varepsilon^2 (33/320 e^{-it} s_2 i - 33/320 e^{it} s_1 i) + \\ &\quad \frac{\partial F_2}{\partial t} \varepsilon^2 (3/32 e^{-it} s_2 + 3/32 e^{it} s_1) + 2/3 F_1 \varepsilon^2 + F_2 \varepsilon^2 (- \\ &\quad 3/80 e^{-it} s_2 i + 3/80 e^{it} s_1 i) + \varepsilon^2 (-9/16 e^{-it} s_2^2 s_1 + 7/96 e^{-3it} s_2^3 - \\ &\quad 9/16 e^{it} s_2 s_1^2 + 7/96 e^{3it} s_1^3) + e^{-it} s_2 + e^{it} s_1 + O(\varepsilon^4) \\ u_2 &= -4/9 \frac{\partial^2 F_1}{\partial t^2} \varepsilon^2 + \frac{\partial^2 F_2}{\partial t^2} \varepsilon^2 (-39/320 e^{-it} s_2 i + 39/320 e^{it} s_1 i) + \\ &\quad \frac{\partial F_2}{\partial t} \varepsilon^2 (-9/160 e^{-it} s_2 - 9/160 e^{it} s_1) + 1/3 F_1 \varepsilon^2 + \\ &\quad F_2 \varepsilon^2 (9/80 e^{-it} s_2 i - 9/80 e^{it} s_1 i) + \varepsilon^2 (3/16 e^{-it} s_2^2 s_1 - \\ &\quad 1/96 e^{-3it} s_2^3 + 3/16 e^{it} s_2 s_1^2 - 1/96 e^{3it} s_1^3) + e^{-it} s_2 + e^{it} s_1 + \\ &\quad O(\varepsilon^4) \\ u_3 &= 2/3 \frac{\partial F_1}{\partial t} \varepsilon^2 + \frac{\partial^2 F_2}{\partial t^2} \varepsilon^2 (63/320 e^{-it} s_2 + 63/320 e^{it} s_1) + \frac{\partial F_2}{\partial t} \varepsilon^2 (- \\ &\quad 21/160 e^{-it} s_2 i + 21/160 e^{it} s_1 i) + F_2 \varepsilon^2 (-9/80 e^{-it} s_2 - \\ &\quad 9/80 e^{it} s_1) + \varepsilon^2 (3/16 e^{-it} s_2^2 s_1 i - 7/32 e^{-3it} s_2^3 i - \\ &\quad 3/16 e^{it} s_2 s_1^2 i + 7/32 e^{3it} s_1^3 i) - e^{-it} s_2 i + e^{it} s_1 i + O(\varepsilon^4)\end{aligned}$$

$$u_4 = 1/3 \frac{\partial F_1}{\partial t} \varepsilon^2 + \frac{\partial^2 F_2}{\partial t^2} \varepsilon^2 (-57/320 e^{-it} s_2 - 57/320 e^{it} s_1) + \\ \frac{\partial F_2}{\partial t} \varepsilon^2 (27/160 e^{-it} s_2 i - 27/160 e^{it} s_1 i) + F_2 \varepsilon^2 (3/80 e^{-it} s_2 + \\ 3/80 e^{it} s_1) + \varepsilon^2 (-9/16 e^{-it} s_2^2 s_1 i + 1/32 e^{-3it} s_2^3 i + \\ 9/16 e^{it} s_2 s_1^2 i - 1/32 e^{3it} s_1^3 i) - e^{-it} s_2 i + e^{it} s_1 i + O(\varepsilon^4)$$

Invariant manifold ODEs The system evolves according to these ODEs that characterise how the modulation of the oscillations evolve in state space due to nonlinearity and the forcing. Both linear and quadratic effects in the forcing and their time-derivatives are found.

$$\dot{s}_1 = -531/12800 \frac{\partial^2 F_2}{\partial t^2} F_2 \varepsilon^4 s_1 i + \frac{\partial^2 F_2}{\partial t^2} \varepsilon^4 (99/2560 s_2 s_1^2 + 9/320 s_1 i) + \\ 9/256 \frac{\partial F_2}{\partial t} F_2 \varepsilon^4 s_1 + \frac{\partial F_2}{\partial t} \varepsilon^4 (27/256 s_2 s_1^2 i - 9/400 s_1) + \\ 9/640 F_2^2 \varepsilon^4 s_1 i + F_2 \varepsilon^4 (-9/80 s_2 s_1^2 - 9/800 s_1 i) - 3/40 F_2 \varepsilon^2 s_1 + \\ \varepsilon^4 (-155/256 s_2 s_1^3 i + 9/160 s_2 s_1^2) + 3/8 \varepsilon^2 s_2 s_1^2 i + O(\varepsilon^5)$$

$$\dot{s}_2 = 531/12800 \frac{\partial^2 F_2}{\partial t^2} F_2 \varepsilon^4 s_2 i + \frac{\partial^2 F_2}{\partial t^2} \varepsilon^4 (99/2560 s_2^2 s_1 - 9/320 s_2 i) + \\ 9/256 \frac{\partial F_2}{\partial t} F_2 \varepsilon^4 s_2 + \frac{\partial F_2}{\partial t} \varepsilon^4 (-27/256 s_2^2 s_1 i - 9/400 s_2) - \\ 9/640 F_2^2 \varepsilon^4 s_2 i + F_2 \varepsilon^4 (-9/80 s_2^2 s_1 + 9/800 s_2 i) - 3/40 F_2 \varepsilon^2 s_2 + \\ \varepsilon^4 (155/256 s_2^3 s_1 i + 9/160 s_2^2 s_1) - 3/8 \varepsilon^2 s_2^2 s_1 i + O(\varepsilon^5)$$

5 Stable invariant manifolds

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Also see [Section 1.5](#).

5.1 stable2d: Stable manifold of a 2D system

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Let's construct the 1D stable manifold of the system, for small bifurcation parameter ϵ ,

$$\begin{aligned}\dot{u}_1 &= -\frac{1}{2}u_1 - u_2 - u_1^2u_2, \\ \dot{u}_2 &= -u_1 - 2u_2 + \epsilon u_2 - u_2^2.\end{aligned}$$

Start by loading the procedure.

```
258 in_tex "../invariantManifold.tex"$
```

Execute the construction of the stable manifold for this system.

```
259 invariantmanifold({},  
260     mat((-u1/2-u2-small*u1^2*u2,  
261         -u1-2*u2+small*epsilon*u2-u2^2)),  
262     mat((-5/2)),  
263     mat((1,2)),  
264     mat((1,2)),  
265     5 )$  
266 end;
```

The matrix $\begin{bmatrix} -\frac{1}{2} & -1 \\ -1 & -2 \end{bmatrix}$ of the linearisation about the origin has eigenvalues 0 and $-5/2$. We seek the 1D stable manifold so specify the eigenvalue $-5/2$ in the second parameter to the procedure. Due to symmetry, corresponding eigenvectors are $\vec{e}_1 = \vec{z}_1 = (1, 2)$ in the third and fourth parameter. The last parameter, 5, specifies to construct the stable manifold to errors $\mathcal{O}(\epsilon^5)$.

To consistently count the orders of the nonlinearities we multiply the cubic term by `small`. To treat parameter ϵ as small, we also multiply it by `small` so it becomes effectively a second-order order-parameter (useful for pitchfork bifurcations). So, the procedure actually analyses the embedding system

$$\begin{aligned}\dot{u}_1 &= -\epsilon^2 u_1^2 u_2 - 1/2 u_1 - u_2, \\ \dot{u}_2 &= \epsilon^2 \epsilon u_2 - \epsilon u_2^2 - u_1 - 2u_2.\end{aligned}$$

The stable manifold The constructed stable manifold is, in terms of the parameter s_1 (to error $\mathcal{O}(\varepsilon^4)$, and reverse ordering!), and in terms of the ugly $e^{(-5t/2)} = e^{-5t/2}$ which needs fixing sometime!),

$$\begin{aligned} u_1 &= \varepsilon^3 (53152/140625 e^{-10t} s_1^4 + 88/625 e^{-5t} s_1^2 \epsilon) + \\ &\quad \varepsilon^2 (838/1875 e^{(-15t/2)} s_1^3 + 8/25 e^{(-5t/2)} s_1 \epsilon) + \\ &\quad 8/25 \varepsilon e^{-5t} s_1^2 + e^{(-5t/2)} s_1, \\ u_2 &= \varepsilon^3 (122444/140625 e^{-10t} s_1^4 + 76/625 e^{-5t} s_1^2 \epsilon) + \\ &\quad \varepsilon^2 (2116/1875 e^{(-15t/2)} s_1^3 - 4/25 e^{(-5t/2)} s_1 \epsilon) + \\ &\quad 36/25 \varepsilon e^{-5t} s_1^2 + 2 e^{(-5t/2)} s_1. \end{aligned}$$

Observe the linear terms in s_1 all have $e^{-5t/2}$, and the quadratic terms in s_1 all have e^{-5t} , and so on. Consequently, we could in principle write the stable manifold in terms of, say, the variables $x_1 = s_1 e^{-5t/2}$ giving

$$\begin{aligned} u_1 &= \varepsilon^3 (53152/140625 x_1^4 + 88/625 x_1^2 \epsilon) + \varepsilon^2 (838/1875 x_1^3 + \\ &\quad 8/25 x_1 \epsilon) + 8/25 \varepsilon x_1^2 + x_1, \\ u_2 &= \varepsilon^3 (122444/140625 x_1^4 + 76/625 x_1^2 \epsilon) + \varepsilon^2 (2116/1875 x_1^3 - \\ &\quad 4/25 x_1 \epsilon) + 36/25 \varepsilon x_1^2 + 2 x_1. \end{aligned}$$

This would be a more usual parametrisation. But here let's remain with s_1 and remember to interpret s_1 as modifying the exponential decay $e^{-5t/2}$ on this stable manifold.

Stable manifold ODEs On the stable manifold the evolution is

$$\dot{s}_1 = -8/125 \varepsilon^4 s_1 \epsilon^2 + 4/5 \varepsilon^2 s_1 \epsilon.$$

That the ODE for s_1 is linear is a consequence of the Hartmann-Grobman Theorem. It just reflects that the decay-rate of the stable mode varies with parameter ϵ : evidently, the decay rate is approximately $-\frac{5}{2} + \frac{4}{5}\epsilon - \frac{8}{125}\epsilon^2$.

6 Invariant manifolds in delay DEs

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Also see [Section 1.2](#)

6.1 `simple1dde`: Simple DDE with a Hopf bifurcation

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Model a delayed ‘logistic’ system in one variable with

$$\frac{du}{dt} = -(1+a)[1+u(t)]u(t-\pi/2),$$

for small parameter a . We code the parameter a as ‘small’, and observe it is consequently considered as ‘small squared’ because all nonlinear terms and already ‘small’ terms are multiplied by `small`.

Start by loading the procedure.

```
267 in_tex "../invariantManifold.tex"$
```

In the printed output, group terms with like powers of amplitudes s_j , the complex exponential, and the parameter a .

```
268 factor s,exp,a;
```

Execute the construction of the slow manifold for this system (ignore the warning messages about `u1` declared, and then already defined, as an operator).

```
269 invariantmanifold({},  
270      mat((-1+small*a)*(1+u1)*u1(pi/2) ),  
271      mat((i,-i)),  
272      mat((1),(1)),  
273      mat((1),(1)),  
274      3)$  
275 end;
```

The marginal modes are $e^{\pm it}$ so nominate the frequencies ± 1 . The eigenvectors are just $1 \cdot e^{\pm it}$. Because for delay differential equations the time dependence $e^{\pm i\omega t}$ is an integral part of the definition of the eigenvector; hence the coded eigenvectors can be the same, as here, because they are differentiated through the time dependence $e^{\pm i\omega t}$.

The code works for orders higher than cubic, but is slow: takes about a minute per iteration.

The procedure actually analyses the embedding system

$$\frac{du}{dt} = -[1 + \varepsilon u(t)]u(t - \pi/2) - \varepsilon^2 a[1 + u(t)]u(t - \pi/2).$$

The centre manifold These give the location of the invariant manifold in terms of parameters s_j .

$$u_1 = e^{-it}s_2 + e^{-2it}s_2^2\varepsilon(1/5i + 2/5) + e^{it}s_1 + e^{2it}s_1^2\varepsilon(-1/5i + 2/5)$$

Centre manifold ODEs The system evolves on the invariant manifold such that the parameters evolve according to these ODEs.

$$\begin{aligned}\dot{s}_1 &= s_2 s_1^2 \varepsilon^2 (-2/5i\pi - 12/5i - 6/5\pi + 4/5)/(\pi^2 + 4) + \\ &\quad s_1 a \varepsilon^2 (4i + 2\pi)/(\pi^2 + 4) \\ \dot{s}_2 &= s_2^2 s_1 \varepsilon^2 (2/5i\pi + 12/5i - 6/5\pi + 4/5)/(\pi^2 + 4) + s_2 a \varepsilon^2 (- \\ &\quad 4i + 2\pi)/(\pi^2 + 4)\end{aligned}$$

6.2 logistic1dde: Logistic DDE displays a Hopf bifurcation

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Form a centre manifold for the delayed ‘logistic’ system in one variable, for delay $\tau = 3\pi/4$, with

$$\frac{du}{dt} = -u(t) - (\sqrt{2} + a)u(t - \tau) + \mu u(t - \tau)^2 + \nu u(t - \tau)^3,$$

for and nonlinearity parameters μ and ν , and small parameter a . Numerical computation of the spectrum indicates that the system has a Hopf bifurcation as parameter a crosses zero.

We code the parameter a as ‘small’, and observe it is consequently considered as ‘small squared’ because all nonlinear terms, and already ‘small’ terms, are multiplied by ε (`small`).

Start by loading the procedure.

```
276 in_tex ".../invariantManifold.tex"$
```

In the printed output, group terms with like powers of amplitudes s_j , the complex exponential, and the parameters.

```
277 factor s,exp,a,mu,nu;
```

Execute the construction of the slow manifold for this system (ignore the warning messages about `u1` declared, and then already defined, as an operator).

```
278 invariantmanifold({},
279      mat((-u1-(sqrt(2)+small*a)*u1(3*pi/4)
280           +mu*u1(3*pi/4)^2 +small*nu*u1(3*pi/4)^3)),
```

```

281      mat((i,-i)),
282      mat((1),(1)),
283      mat((1),(1)),
284      3)$
285 end;

```

The marginal modes are $e^{\pm it}$ so nominate the frequencies ± 1 . The eigenvectors are just $1 \cdot e^{\pm it}$. Because for delay differential equations the time dependence $e^{\pm i\omega t}$ is an integral part of the definition of the eigenvector; hence the coded eigenvectors can be the same, as here, because they are differentiated through the time dependence $e^{\pm i\omega t}$.

The procedure actually analyses the embedding system, for delay $\tau = 3\pi/4$,

$$\dot{u}_1 = -a\varepsilon^2 u_1(t-\tau) + \mu\varepsilon u_1(t-\tau)^2 + \nu\varepsilon^2 u_1(t-\tau)^3 - \sqrt{2}u_1(t-\tau) - u_1.$$

The centre manifold These give the location of the invariant manifold in terms of parameters s_j .

$$u_1 = e^{-it}s_2 + e^{-2it}s_2^2\mu\varepsilon(-0.07901i + 0.2698) + e^{it}s_1 + e^{2it}s_1^2\mu\varepsilon(0.07901i + 0.2698) + 0.8284s_2s_1\mu\varepsilon$$

Centre manifold ODEs The system evolves on the invariant manifold such that the parameters evolve according to these ODEs.

$$\begin{aligned}\dot{s}_1 &= s_2s_1^2\mu^2\varepsilon^2(-0.1303i - 0.5209) + s_2s_1^2\nu\varepsilon^2(-0.1262i - 0.7206) + s_1a\varepsilon^2(0.04205i + 0.2402) \\ \dot{s}_2 &= s_2^2s_1\mu^2\varepsilon^2(0.1303i - 0.5209) + s_2^2s_1\nu\varepsilon^2(0.1262i - 0.7206) + s_2a\varepsilon^2(-0.04205i + 0.2402)\end{aligned}$$

Hence the centre manifold model predicts a supercritical Hopf bifurcation as parameter a increases through zero.

7 Slow manifolds of spatiotemporal systems

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Also see [Section 1.6](#).

7.1 `heatX`: spatial diffusion in simple heat exchanger

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A heat exchanger is simply two pipes with ‘fluid’ flowing in opposite directions, and exchanging heat between them. Let $u_1(x, t), u_2(x, t)$ be the temperatures in the two pipes as a function of space-time. Advecting at the same but opposite velocities, non-dimensional PDEs are

$$\frac{\partial u_1}{\partial t} = -\frac{\partial u_1}{\partial x} + u_2 - u_1, \quad \frac{\partial u_2}{\partial t} = +\frac{\partial u_1}{\partial x} + u_1 - u_2.$$

The linearisation for *gradual* variations in space is to then neglect the spatial derivatives: $\partial u_1 / \partial t = u_2 - u_1$, $\partial u_2 / \partial t = u_1 - u_2$. This has eigenvalues $\lambda = 0, -2$ with respective eigenvectors $(1, 1), (1, -1)$. We model effective dispersion of heat in these two pipes in space-time over long times and large space scales.

Start by loading the procedure.

```
286 in_tex "../invariantManifold.tex"$
```

In the printed output, group terms depending upon order of spatial derivatives (which are assumed ‘small’).

```
287 factor small;
```

The following procedure call constructs the slow manifold for this system to errors $\mathcal{O}(\partial_x^5)$.

```
288 invariantmanifold( {x},  
289     mat((-pdf(u1,x)+(u2-u1)  
290         ,+pdf(u2,x)+(u1-u2))),  
291     mat(( 0 )),  
292     mat( (1/2,1/2) ),
```

```

293      mat( (1,1) ),
294      5 )$  

295 end;
```

The procedure then actually analyses the parametrised system

$$\frac{\partial u_1}{\partial t} = -\varepsilon \frac{\partial u_1}{\partial x} - u_1 + u_2, \quad \frac{\partial u_2}{\partial t} = \varepsilon \frac{\partial u_2}{\partial x} + u_1 - u_2.$$

Consequently the procedure's artificial parameter ε counts the number of spatial derivatives in each term.

The invariant manifold The slow manifold is expressed in terms of a series in space derivatives.

$$\begin{aligned} u_1 &= 1/16\varepsilon^3 \frac{\partial^3 s_1}{\partial x^3} - 1/4\varepsilon \frac{\partial s_1}{\partial x} + O(\varepsilon^4) + 1/2s_1 \\ u_2 &= -1/16\varepsilon^3 \frac{\partial^3 s_1}{\partial x^3} + 1/4\varepsilon \frac{\partial s_1}{\partial x} + O(\varepsilon^4) + 1/2s_1 \end{aligned}$$

Invariant manifold PDEs The system evolves according to this PDE that describes the effective dispersion of heat in the pipes: a simple diffusion albeit with higher-order improvements:

$$\frac{\partial s_1}{\partial t} = -1/8\varepsilon^4 \frac{\partial^4 s_1}{\partial x^4} + 1/2\varepsilon^2 \frac{\partial^2 s_1}{\partial x^2} + O(\varepsilon^5)$$

Project initial conditions et al. To project initial conditions onto the slow manifold, or non-autonomous forcing, or modifications of the original system, or to quantify uncertainty ([Roberts 1989, 2000, 2015](#), Ch.12), use the projection defined by the following derived vector.

$$\begin{aligned} \vec{z}_1 &= [z_{11} \ z_{12}]^T \\ &= \begin{bmatrix} 3/16\varepsilon^4 \partial_x^4 + 1/4\varepsilon^3 \partial_x^3 - 1/4\varepsilon^2 \partial_x^2 - 1/2\varepsilon \partial_x + O(\varepsilon^5) + 1 \\ 3/16\varepsilon^4 \partial_x^4 - 1/4\varepsilon^3 \partial_x^3 - 1/4\varepsilon^2 \partial_x^2 + 1/2\varepsilon \partial_x + O(\varepsilon^5) + 1 \end{bmatrix}. \end{aligned}$$

7.2 randWalkIn2D: advection-diffusion of random walk in 2D

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A ‘drunk’ walker stumbles around in a 2D meadow. Let position of the walker at any time t be (x_1, x_2) . The walker:

- sometimes heads North-East, direction $(1, 1)$, but may decide to turn West;
- sometimes West, direction $(-1, 0)$, but may turn to the North-East or South-East; and

- sometimes South-East, direction $(1, -1)$, but may turn back to the West.

Where can we expect the drunk walker to be as time varies?

Let $u_j(x_1, x_2, t)$ be the probability of the walker being at position (x_1, x_2) and walking in the j th of the mentioned directions. Then the non-dimensional PDEs for these probabilities may be

$$\begin{aligned}\frac{\partial u_1}{\partial t} &= -\frac{\partial u_1}{\partial x_1} - \frac{\partial u_1}{\partial x_2} - u_1 + u_2, \\ \frac{\partial u_2}{\partial t} &= +\frac{\partial u_2}{\partial x_1} + u_1 - 2u_2 + u_3, \\ \frac{\partial u_3}{\partial t} &= -\frac{\partial u_3}{\partial x_1} + \frac{\partial u_3}{\partial x_2} + u_2 - u_3.\end{aligned}$$

The linearisation for *gradual* variations in space is to then neglect the spatial derivatives: $\partial u_1 / \partial t = -u_1 + u_2$, $\partial u_2 / \partial t = +u_1 - 2u_2 + u_3$, $\partial u_3 / \partial t = u_2 - u_3$. This has eigenvalues $\lambda = 0, -1, -3$ with respective eigenvectors $(1, 1, 1)$, $(1, 0, -1)$, $(1, -2, 1)$. We use this information to model the probability distribution of the dispersion of the drunk walker in space-time over long times and large space scales.

Start by loading the procedure.

```
296 in_tex ".../invariantManifold.tex"$
```

In the printed output, group terms depending upon order of spatial derivatives (which are assumed ‘small’).

```
297 factor small;
```

The following procedure call constructs the slow manifold for this system to errors $\mathcal{O}(\vec{\nabla}^5)$.

```
298 invariantmanifold( {x_1,x_2},
299      mat((-pdf(u1,x_1)-pdf(u1,x_2)+(u2-u1)
300          ,+pdf(u2,x_1)           +(u1-2*u2+u3)
301          ,-pdf(u3,x_1)+pdf(u3,x_2)+(u2-u3)
302          )),
303      mat(( 0 )),
304      mat( (1/3,1/3,1/3) ),
305      mat( (1,1,1) ),
306      4 )$
307 end;
```

The procedure then actually analyses the parametrised system

$$\begin{aligned}\frac{\partial u_1}{\partial t} &= \varepsilon \left(-\frac{\partial u_1}{\partial x_1} - \frac{\partial u_1}{\partial x_2} \right) - u_1 + u_2, \\ \frac{\partial u_2}{\partial t} &= \varepsilon \frac{\partial u_2}{\partial x_1} + u_1 - 2u_2 + u_3.\end{aligned}$$

$$\frac{\partial u_3}{\partial t} = \varepsilon \left(-\frac{\partial u_3}{\partial x_1} + \frac{\partial u_3}{\partial x_2} \right) + u_2 - u_3.$$

Consequently the procedure's artificial parameter ε counts the number of spatial derivatives in each term.

The invariant manifold Five iterations constructs the slow manifold model. The slow manifold is expressed in terms of a series in space derivatives.

$$\begin{aligned} u_1 &= \varepsilon^2 \left(8/27 \frac{\partial^2 s_1}{\partial x_1 \partial x_2} - 4/243 \frac{\partial^2 s_1}{\partial x_1^2} + 1/27 \frac{\partial^2 s_1}{\partial x_2^2} \right) + \varepsilon \left(-2/27 \frac{\partial s_1}{\partial x_1} - \right. \\ &\quad \left. 1/3 \frac{\partial s_1}{\partial x_2} \right) + O(\varepsilon^3) + 1/3s_1 \\ u_2 &= \varepsilon^2 \left(8/243 \frac{\partial^2 s_1}{\partial x_1^2} - 2/27 \frac{\partial^2 s_1}{\partial x_2^2} \right) + 4/27 \varepsilon \frac{\partial s_1}{\partial x_1} + O(\varepsilon^3) + 1/3s_1 \\ u_3 &= \varepsilon^2 \left(-8/27 \frac{\partial^2 s_1}{\partial x_1 \partial x_2} - 4/243 \frac{\partial^2 s_1}{\partial x_1^2} + 1/27 \frac{\partial^2 s_1}{\partial x_2^2} \right) + \varepsilon \left(-2/27 \frac{\partial s_1}{\partial x_1} + \right. \\ &\quad \left. 1/3 \frac{\partial s_1}{\partial x_2} \right) + O(\varepsilon^3) + 1/3s_1 \end{aligned}$$

Invariant manifold PDEs The system evolves according to this PDE that describes the effective movement of the random walker: an advection-diffusion PDE, with anisotropic diffusion, and third-order dispersive effects included:

$$\frac{\partial s_1}{\partial t} = \varepsilon^3 \left(-20/27 \frac{\partial^3 s_1}{\partial x_1 \partial x_2^2} + 16/243 \frac{\partial^3 s_1}{\partial x_1^3} \right) + \varepsilon^2 \left(8/27 \frac{\partial^2 s_1}{\partial x_1^2} + \right. \\ \left. 2/3 \frac{\partial^2 s_1}{\partial x_2^2} \right) - 1/3 \varepsilon \frac{\partial s_1}{\partial x_1} + O(\varepsilon^4)$$

So, on average, the walker will drift in the $+x_1$ -direction, but with significant and growing spread in the $x_1 x_2$ -meadow.

Project initial conditions et al. To project initial conditions onto the slow manifold, or non-autonomous forcing, or modifications of the original system, or to quantify uncertainty (Roberts 1989, 2000, 2015, Ch.12), use the projection defined by the following derived vector.

$$\begin{aligned} \vec{z}_1 &= [z_{11} \ z_{12} \ z_{13}]^T \\ &= \begin{bmatrix} \varepsilon^3 (-8/729 \partial_{x_1}^3 - 4/27 \partial_{x_1}^2 \partial_{x_2} + 38/27 \partial_{x_1} \partial_{x_2}^2 + 11/9 \partial_{x_2}^3) + \varepsilon^2 (- \\ 4/27 \partial_{x_1}^2 + 8/9 \partial_{x_1} \partial_{x_2} - 5/9 \partial_{x_2}^2) + \varepsilon (-2/9 \partial_{x_1} - \partial_{x_2}) + O(\varepsilon^4) + 1 \\ \varepsilon^3 (-80/729 \partial_{x_1}^3 + 28/27 \partial_{x_1} \partial_{x_2}^2) - 8/9 \varepsilon^2 \partial_{x_2}^2 + 4/9 \varepsilon \partial_{x_1} + \\ O(\varepsilon^4) + 1 \\ \varepsilon^3 (-8/729 \partial_{x_1}^3 + 4/27 \partial_{x_1}^2 \partial_{x_2} + 38/27 \partial_{x_1} \partial_{x_2}^2 - 11/9 \partial_{x_2}^3) + \varepsilon^2 (- \\ 4/27 \partial_{x_1}^2 - 8/9 \partial_{x_1} \partial_{x_2} - 5/9 \partial_{x_2}^2) + \varepsilon (-2/9 \partial_{x_1} + \partial_{x_2}) + O(\varepsilon^4) + 1 \end{bmatrix}. \end{aligned}$$

7.3 gradsSystem: spatiotemporal long-waves in Grad's system

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This is Example B from ‘‘Dynamically Optimal Projection onto Slow Spectral Manifolds for Linear Systems’’ by Kogelbauer and Karlin (2025). The PDEs are apparently a classical system in kinetic theory. Variables are the pressure u_1 , velocity u_2 , and stress u_3 . What are the PDEs for the long-wave pressure-velocity waves?

$$\begin{aligned}\frac{\partial u_1}{\partial t} &= -\frac{5}{3} \frac{\partial u_1}{\partial x}, \\ \frac{\partial u_2}{\partial t} &= -\frac{\partial u_1}{\partial x} - \frac{\partial u_3}{\partial x}, \\ \frac{\partial u_3}{\partial t} &= -\frac{4}{3} \frac{\partial u_2}{\partial x} - u_3/\epsilon.\end{aligned}$$

The linearisation for *gradual* variations in space is to then neglect the spatial derivatives: $\partial u_1/\partial t = \partial u_2/\partial t = 0$ and $\partial u_3/\partial t = -u_3/\epsilon$ which decays to quasi-equilibria quite ‘rapidly’. Simply, the pressure and velocity are slow variables.

Start by loading the procedure.

```
308 in_tex ".../invariantManifold.tex"$
```

In the printed output, group terms depending upon order of spatial derivatives (which are assumed ‘small’).

```
309 factor small;
```

The following procedure call constructs the slow manifold for this system to errors $\mathcal{O}(\partial_x^5)$.

```
310 invariantmanifold( {x},
311     mat((-5/3*pdf(u2,x)
312         ,-pdf(u1,x)-pdf(u3,x)
313         ,-4/3*pdf(u2,x)-u3/epsilon
314         )),
315     mat(( 0,0 )),
316     mat( (1,0,0),(0,1,0) ),
317     mat( (1,0,0),(0,1,0) ,
318     5 )$
319 end;
```

The procedure then actually analyses the parametrised system

$$\begin{aligned}\frac{\partial u_1}{\partial t} &= -5/3\varepsilon \frac{\partial u_2}{\partial x}, \\ \frac{\partial u_2}{\partial t} &= \varepsilon \left(-\frac{\partial u_1}{\partial x} - \frac{\partial u_3}{\partial x} \right), \\ \frac{\partial u_3}{\partial t} &= -4/3\varepsilon \frac{\partial u_2}{\partial x} - \epsilon^{-1}u_3.\end{aligned}$$

Be wary of the distinction between the system parameter ϵ , and the procedure’s artificial parameter ε that counts the number of spatial derivatives in each term.

The invariant manifold The slow manifold is expressed in terms of a series in space derivatives of parameters $s_j := u_j$ —the pressure and velocity.

$$\begin{aligned} u_1 &= O(\varepsilon^4) + s_1 \\ u_2 &= O(\varepsilon^4) + s_2 \\ u_3 &= -4/9\varepsilon^3 \frac{\partial^3 s_2}{\partial x^3} \epsilon^3 - 4/3\varepsilon^2 \frac{\partial^2 s_1}{\partial x^2} \epsilon^2 - 4/3\varepsilon \frac{\partial s_2}{\partial x} \epsilon + O(\varepsilon^4) \end{aligned}$$

Invariant manifold PDEs The system evolves according to these two PDE that describes the effective long-wave dynamics with higher-order wave dispersion:

$$\begin{aligned} \frac{\partial s_1}{\partial t} &= -5/3\varepsilon \frac{\partial s_2}{\partial x} + O(\varepsilon^5), \\ \frac{\partial s_1}{\partial t} &= 4/9\varepsilon^4 \frac{\partial^4 s_2}{\partial x^4} \epsilon^3 + 4/3\varepsilon^3 \frac{\partial^3 s_1}{\partial x^3} \epsilon^2 + 4/3\varepsilon^2 \frac{\partial^2 s_2}{\partial x^2} \epsilon - \varepsilon \frac{\partial s_1}{\partial x} + O(\varepsilon^5) \end{aligned}$$

Project initial conditions et al. To project initial conditions onto the slow manifold, or non-autonomous forcing, or modifications of the original system, or to quantify uncertainty (Roberts 1989, 2000, 2015, Ch.12), use the projection defined by the following two derived vectors.

$$\begin{aligned} \vec{z}_1 &= \begin{bmatrix} z_{11} \\ z_{12} \\ z_{13} \end{bmatrix} = \begin{bmatrix} -20/9\varepsilon^4 \partial_x^4 \epsilon^4 + O(\varepsilon^5) + 1 \\ -20/9\varepsilon^3 \partial_x^3 \epsilon^3 + O(\varepsilon^5) \\ 35/9\varepsilon^4 \partial_x^4 \epsilon^4 - 5/3\varepsilon^2 \partial_x^2 \epsilon^2 + O(\varepsilon^5) \end{bmatrix}, \\ \vec{z}_2 &= \begin{bmatrix} z_{21} \\ z_{22} \\ z_{23} \end{bmatrix} = \begin{bmatrix} -4/3\varepsilon^3 \partial_x^3 \epsilon^3 + O(\varepsilon^5) \\ 8/9\varepsilon^4 \partial_x^4 \epsilon^4 - 4/3\varepsilon^2 \partial_x^2 \epsilon^2 + O(\varepsilon^5) + 1 \\ \varepsilon^3 \partial_x^3 \epsilon^3 - \varepsilon \partial_x \epsilon + O(\varepsilon^5) \end{bmatrix}. \end{aligned}$$

7.4 randWalkHetero: including spatial heterogeneity

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What if the governing PDEs have heterogeneous coefficients? We can still analyse such systems provided the heterogeneity is also slowly-varying in space, that is, if the underlying system has functional graduations.

Here introduce the technique via a modification of the random walker in 2D of Section 7.2. Let the West walking be done a speeds that vary in $x_1 x_2$ -space, say at speed $w(x_1, x_2)$.

Let $u_j(x_1, x_2, t)$ be the probability of the walker being at position (x_1, x_2) and walking in the j th of the mentioned directions.

Then the non-dimensional PDEs for these probabilities may be

$$\begin{aligned}\frac{\partial u_1}{\partial t} &= -\frac{\partial u_1}{\partial x_1} - \frac{\partial u_1}{\partial x_2} - u_1 + u_2, \\ \frac{\partial u_2}{\partial t} &= +w(x_1, x_2) \frac{\partial u_2}{\partial x_1} + u_1 - 2u_2 + u_3, \\ \frac{\partial u_3}{\partial t} &= -\frac{\partial u_3}{\partial x_1} + \frac{\partial u_3}{\partial x_2} + u_2 - u_3.\end{aligned}$$

We code the equivalent system obtained by defining a new variable $u_4 := w$ such that $\partial u_4 / \partial t = 0$ so that u_4 may vary in space but not in time:

$$\begin{aligned}\frac{\partial u_1}{\partial t} &= -\frac{\partial u_1}{\partial x_1} - \frac{\partial u_1}{\partial x_2} - u_1 + u_2, \\ \frac{\partial u_2}{\partial t} &= +u_4 \frac{\partial u_2}{\partial x_1} + u_1 - 2u_2 + u_3, \\ \frac{\partial u_3}{\partial t} &= -\frac{\partial u_3}{\partial x_1} + \frac{\partial u_3}{\partial x_2} + u_2 - u_3, \\ \frac{\partial u_4}{\partial t} &= 0.\end{aligned}$$

Then in the output, $w = u_4 = s_2$.

Start by loading the procedure.

```
320 in_tex ".../invariantManifold.tex"$
```

In the printed output, group terms depending upon order of spatial derivatives (which are assumed ‘small’).

```
321 factor small;
```

The following procedure call constructs the slow manifold for this system to errors $\mathcal{O}(\vec{\nabla}^5)$.

```
322 invariantmanifold( {x_1,x_2},
323   mat((-pdf(u1,x_1)-pdf(u1,x_2)+(u2-u1)
324     ,+u4*pdf(u2,x_1)           +(u1-2*u2+u3)
325     ,-pdf(u3,x_1)+pdf(u3,x_2)+(u2-u3)
326     ,0)),
327   mat(( 0,0 )),
328   mat( (1/3,1/3,1/3,0),(0,0,0,1) ),
329   mat( (1,1,1,0),(0,0,0,1) ),
330   3 )$
331 end;
```

The procedure then actually analyses the parametrised system

$$\begin{aligned}\frac{\partial u_1}{\partial t} &= \varepsilon \left(-\frac{\partial u_1}{\partial x_1} - \frac{\partial u_1}{\partial x_2} \right) - u_1 + u_2, \\ \frac{\partial u_2}{\partial t} &= \varepsilon u_4 \frac{\partial u_2}{\partial x_1} + u_1 - 2u_2 + u_3. \\ \frac{\partial u_3}{\partial t} &= \varepsilon \left(-\frac{\partial u_3}{\partial x_1} + \frac{\partial u_3}{\partial x_2} \right) + u_2 - u_3.\end{aligned}$$

Consequently the procedure's artificial parameter ε counts the number of spatial derivatives in each term.

The invariant manifold Five iterations constructs the slow manifold model. The slow manifold is expressed in terms of a series in space derivatives.

$$\begin{aligned} u_1 &= \varepsilon \left(-1/27 \frac{\partial s_1}{\partial x_1} s_2 - 1/27 \frac{\partial s_1}{\partial x_1} - 1/3 \frac{\partial s_1}{\partial x_2} \right) + O(\varepsilon^2) + 1/3s_1 \\ u_2 &= \varepsilon \left(2/27 \frac{\partial s_1}{\partial x_1} s_2 + 2/27 \frac{\partial s_1}{\partial x_1} \right) + O(\varepsilon^2) + 1/3s_1 \\ u_3 &= \varepsilon \left(-1/27 \frac{\partial s_1}{\partial x_1} s_2 - 1/27 \frac{\partial s_1}{\partial x_1} + 1/3 \frac{\partial s_1}{\partial x_2} \right) + O(\varepsilon^2) + 1/3s_1 \\ u_4 &= O(\varepsilon^2) + s_2 \end{aligned}$$

Invariant manifold PDEs The system evolves according to this PDE that describes the effective movement of the random walker: an advection-diffusion PDE, with anisotropic diffusion, and gradients of $w = s_2$ included:

$$\begin{aligned} \frac{\partial s_1}{\partial t} &= \varepsilon^2 \left(2/27 \frac{\partial s_2}{\partial x_1} \frac{\partial s_1}{\partial x_1} s_2 + 2/27 \frac{\partial s_2}{\partial x_1} \frac{\partial s_1}{\partial x_1} + 2/27 \frac{\partial^2 s_1}{\partial x_1^2} s_2^2 + 4/27 \frac{\partial^2 s_1}{\partial x_1^2} s_2 + \right. \\ &\quad \left. 2/27 \frac{\partial^2 s_1}{\partial x_2^2} + 2/3 \frac{\partial^2 s_1}{\partial x_2^2} \right) + \varepsilon \left(1/3 \frac{\partial s_1}{\partial x_1} s_2 - 2/3 \frac{\partial s_1}{\partial x_1} \right) + O(\varepsilon^3) \\ \frac{\partial s_2}{\partial t} &= 0 \end{aligned}$$

So, if $w = s_2 < 2$ then, on average, the walker will drift in the $+x_1$ -direction, but with significant and growing spread in the $x_1 x_2$ -meadow.

Project initial conditions et al. To project initial conditions onto the slow manifold, or non-autonomous forcing, or modifications of the original system, or to quantify uncertainty (Roberts 1989, 2000, 2015, Ch.12), use the projection defined by the following derived vector. *Warning: this needs checking.*

$$\begin{aligned} \vec{z}_1 &= [z_{11} \ z_{12} \ z_{13} \ z_{14}]^T \\ &= \begin{bmatrix} \varepsilon^2 \left(-1/27 \partial_{x_1}^2 s_2^2 - 2/27 \partial_{x_1}^2 s_2 - 1/27 \partial_{x_1}^2 + 4/9 \partial_{x_1} \partial_{x_2} s_2 + \right. \\ \left. 4/9 \partial_{x_1} \partial_{x_2} - 5/9 \partial_{x_2}^2 \right) + \varepsilon \left(-1/9 \partial_{x_1} s_2 - 1/9 \partial_{x_1} - \partial_{x_2} \right) + O(\varepsilon^3) + 1 \\ -8/9 \varepsilon^2 \partial_{x_2}^2 + \varepsilon \left(2/9 \partial_{x_1} s_2 + 2/9 \partial_{x_1} \right) + O(\varepsilon^3) + 1 \\ \varepsilon^2 \left(-1/27 \partial_{x_1}^2 s_2^2 - 2/27 \partial_{x_1}^2 s_2 - 1/27 \partial_{x_1}^2 - 4/9 \partial_{x_1} \partial_{x_2} s_2 - \right. \\ \left. 4/9 \partial_{x_1} \partial_{x_2} - 5/9 \partial_{x_2}^2 \right) + \varepsilon \left(-1/9 \partial_{x_1} s_2 - 1/9 \partial_{x_1} + \partial_{x_2} \right) + O(\varepsilon^3) + 1 \\ \varepsilon^2 \left(-2/81 \frac{\partial s_1}{\partial x_1} \partial_{x_1} s_2 - 2/81 \frac{\partial s_1}{\partial x_1} \partial_{x_1} \right) + O(\varepsilon^3) \end{bmatrix} \\ \vec{z}_2 &= [0 \ 0 \ 0 \ 1]^T. \end{aligned}$$

7.5 ddeHopfSpace: DDE with Hopf bifurcation and spatial structure

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Model a delayed ‘logistic’ advection-diffusion PDE system in one variable with

$$\frac{du}{dt} = -[1 + u(t)]u(t - \pi/2) - A\frac{\partial u(t)}{\partial x} + D\frac{\partial^2 u(t)}{\partial x^2},$$

for slow variations in space x .

Start by loading the procedure.

```
332 in_tex "../invariantManifold.tex"$
```

In the printed output, group terms with like powers of amplitudes s_j , the complex exponential, and the parameter a .

```
333 factor s,exp,A,D,df,small;
```

Execute the construction of the slow manifold for this system (ignore the warning messages about $u1$ declared, and then already defined, as an operator).

```
334 invariantmanifold({x},
335     mat((-1+u1)*u1(pi/2) -A*pdf(u1,x) +D*pdf(u1,x,x) ),
336     mat((i,-i)),
337     mat((1),(1)),
338     mat((1),(1)),
339     3)$
340 end;
```

The marginal modes are $e^{\pm it}$ so nominate the frequencies ± 1 . The eigenvectors are just $1 \cdot e^{\pm it}$. Because for delay differential equations the time dependence $e^{\pm i\omega t}$ is an integral part of the definition of the eigenvector; hence the coded eigenvectors can be the same, as here, because they are differentiated through the time dependence $e^{\pm i\omega t}$.

The code works for orders higher than three, but is slow: takes about a minute per iteration.

The procedure actually analyses the embedding system

$$\frac{du}{dt} = -[1 + \varepsilon u(t)]u(t - \pi/2) - A\frac{\partial u}{\partial x} + D\frac{\partial^2 u}{\partial x^2}.$$

The centre manifold These give the location of the invariant manifold in terms of parameters s_j .

$$u_1 = e^{-it}s_2 + e^{-2it}s_2^2\varepsilon(1/5i + 2/5) + e^{it}s_1 + e^{2it}s_1^2\varepsilon(-1/5i + 2/5) + O(\varepsilon^2)$$

Centre manifold ODEs The system evolves on the invariant manifold such that the parameters evolve according to these ODEs.

$$\begin{aligned}\dot{s}_1 &= \frac{\partial^2 s_1}{\partial x^2} A^2 \varepsilon^2 (-6i\pi^4 + 8i\pi^2 - \pi^5 + 12\pi^3) / (\pi^6 + 12\pi^4 + 48\pi^2 + 64) + \frac{\partial^2 s_1}{\partial x^2} D\varepsilon^2 (-2i\pi + 4) / (\pi^2 + 4) + \frac{\partial s_1}{\partial x} A\varepsilon (2i\pi - 4) / (\pi^2 + 4) + s_2 s_1^2 \varepsilon^2 (-2/5i\pi^5 - 12/5i\pi^4 - 16/5i\pi^3 - 96/5i\pi^2 - 32/5i\pi - 192/5i - 6/5\pi^5 + 4/5\pi^4 - 48/5\pi^3 + 32/5\pi^2 - 96/5\pi + 64/5) / (\pi^6 + 12\pi^4 + 48\pi^2 + 64) + O(\varepsilon^3) \\ \dot{s}_2 &= \frac{\partial^2 s_2}{\partial x^2} A^2 \varepsilon^2 (6i\pi^4 - 8i\pi^2 - \pi^5 + 12\pi^3) / (\pi^6 + 12\pi^4 + 48\pi^2 + 64) + \frac{\partial^2 s_2}{\partial x^2} D\varepsilon^2 (2i\pi + 4) / (\pi^2 + 4) + \frac{\partial s_2}{\partial x} A\varepsilon (-2i\pi - 4) / (\pi^2 + 4) + s_2^2 s_1 \varepsilon^2 (2/5i\pi^5 + 12/5i\pi^4 + 16/5i\pi^3 + 96/5i\pi^2 + 32/5i\pi + 192/5i - 6/5\pi^5 + 4/5\pi^4 - 48/5\pi^3 + 32/5\pi^2 - 96/5\pi + 64/5) / (\pi^6 + 12\pi^4 + 48\pi^2 + 64) + O(\varepsilon^3) \\ \dot{s}_1 &= \frac{\partial^2 s_1}{\partial x^2} A^2 \varepsilon^2 (-0.1895i + 0.02476) + \frac{\partial^2 s_1}{\partial x^2} D\varepsilon^2 (-0.453i + 0.2884) + \frac{\partial s_1}{\partial x} A\varepsilon (0.453i - 0.2884) + s_2 s_1^2 \varepsilon^2 (-0.2636i - 0.2141) + O(\varepsilon^3) \\ \dot{s}_2 &= \frac{\partial^2 s_2}{\partial x^2} A^2 \varepsilon^2 (0.1895i + 0.02476) + \frac{\partial^2 s_2}{\partial x^2} D\varepsilon^2 (0.453i + 0.2884) + \frac{\partial s_2}{\partial x} A\varepsilon (-0.453i - 0.2884) + s_2^2 s_1 \varepsilon^2 (0.2636i - 0.2141) + O(\varepsilon^3)\end{aligned}$$

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