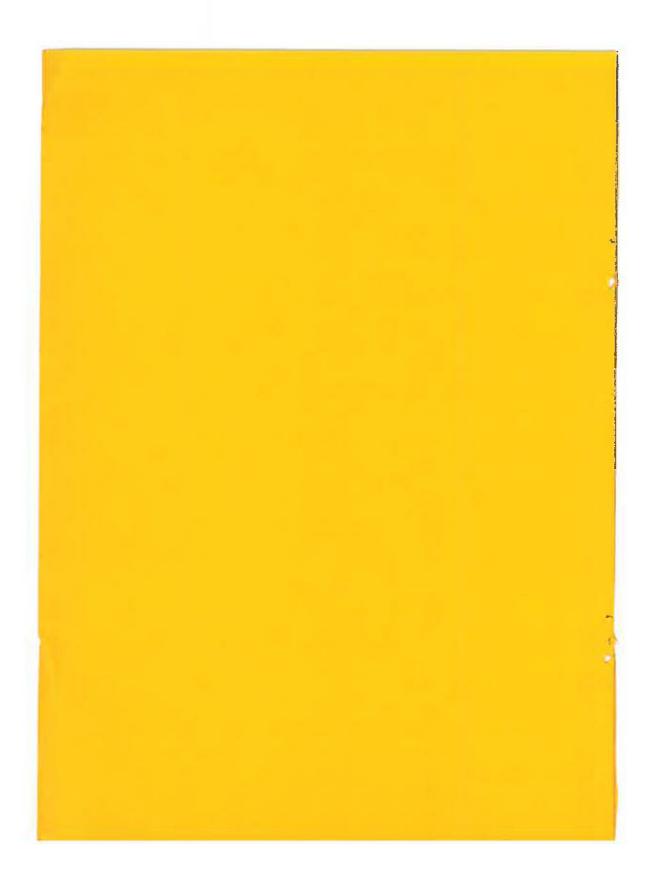
### WORKING PAPER 431

STRUCTURAL DYNAMICS AND SPATIAL ANALYSIS: FROM EQUILIBRIUM BALANCING MODELS TO EXTENDED ECONOMIC MODELS FOR BOTH PERFECT AND IMPERFECT MARKETS

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## 1. Background and outline of the argument

The model presented by Harris and Wilson (1978) can be represented as follows:

$$S_{i,j} = A_i E_i W_j^{\alpha} e^{-\beta C_i j}$$
 (1)

$$A_{i} = 1/\sum_{k} W_{k}^{\alpha} e^{-\beta C_{i} k}$$
 (2)

with  $\{W_j\}$  being determined so that

$$D_{j} = C_{j} \tag{3}$$

where

$$D_{\mathbf{j}} = \sum_{\mathbf{i}} S_{\mathbf{i},\mathbf{j}} \tag{4}$$

and  $\mathbf{C}_{\mathbf{j}}$  is usually taken for illustration as

$$^{C}\mathbf{j}=\mathbf{k_{j}}\mathbf{w_{j}}\tag{5}$$

This model can represent a wide variety of situations. A typical example has  $E_i$  as the amount of expenditure on retail goods by the residents of some zone i,  $W_j$  as the available retail floorspace in zone j (and taken as an attractiveness factor),  $c_{ij}$  as a measure of travel cost from i to j, and then  $S_{ij}$  is the flow of expenditure from residents of i to shops in j.  $\alpha$  and  $\beta$  are parameters. The  $A_i$ s are balancing factors calculated in (2) to ensure that

$$\sum_{j} S_{ij} = E_{i}$$
(6)

The total revenue attracted to j is the sum  $D_j$  given in (4) and it is assumed that the cost of supplying retail facilities is given by (5) – or some more appropriately complicated and realistic function. The structural variables  $\{W_j\}$  are then obtained by solving the equilibrium condition (3). By substituting for  $S_{ij}$  from (1) and (2) into (4), and then for  $D_j$  and  $C_j$  from (4) and (5) into (3), this condition can be seen to be

$$\sum_{i} \frac{E_{i}W_{j}^{\alpha}e^{-\beta C_{i}j}}{\sum_{i}W_{k}^{\alpha}e^{-\beta C_{i}k}} = k_{j}W_{j}$$
 (7)

which shows explicitly that the variables  $\{W_j\}$  are the solutions to a set of interdependent non-linear simultaneous equations.

Harris and Wilson (1978) showed the nature of the bifurcation properties of this model: that the spatial pattern  $\{W_j\}$  changes abruptly at certain critical values of parameters, like  $\alpha$  and  $\beta$  (or even  $\{E_i\}$  and  $\{c_{ij}\}$ ). Examples and further analyses of such changes have been presented by Wilson and Clarke (1979), Clarke and Wilson (1983). This model has been further explored theoretically and empirically by such authors as Phiri (1980), Leonardi (1981-A, 1981-B), Harris, Choukroun and Wilson (1982), Lombardo and Rabino (1983), Rijk and Vorst (1983-A, 1983-B), Kaashoek and Vorst (1984), Chudzynska and Slodkowski (1984), M. Clarke (1984), Dumain, Saint-Julien and Sanders (1984), Roy and Brotchie (1984), Fotheringham (1985) and G. Clarke (1985).

The model can be interpreted as representing retailers adjusting floorspace provision in a system where consumers gain some external benefits associated with  $W_j$ -size (measured by  $W_j^\alpha$  in the interaction model) relative to the costs of travelling (measured by  $e^{-\beta C_1 j}$ ). Typically, high  $\alpha$  and low  $\beta$  will generate ( $W_j$ )-systems with a small number of large centres; and vice versa.

It is now appropriate to consider extending this model in two ways: first, to attempt to make the model more realistic by also considering adjustment of the prices of goods and of land rent as part of the equilibrating process; and secondly, to use ideas which have been successfully deployed in other contexts to incorporate the consequences of market imperfections on the structure-patterns,  $\{W_i\}$ . These two developments should obviously be applied

1.5

in combination, but for clarity and ease of presentation, we first consider them separately. In section 2, therefore, we explore the task of making the Harris and Wilson (1978) model more realistically "economic"; and in section 3, we apply entropy-maximising methods to the problem of representing market imperfections. In section 4, we outline the potential range of application of these ideas. This is wide, partly because of the range of different situations, partly because of different possible levels of aggregation in each case. We also note that in all these situations, both ideas can be incorporated simultaneously though we largely leave such developments as an exercise for the reader. The main aim now, therefore, is to capture the essence of the ideas in the simplest model frameworks in which they can be represented.

# 2. Prices, land rents and perfect markets

For illustrative purposes, let us focus on four kinds of agents :

- (i) consumers;
- (ii) retailers;
- (iii) land owners/developers; and
- (iv) suppliers of goods to retailers.

The last category is itself essentially a chain - from wholesalers via different (linked) manufacturers but we consider it a single type for present purposes. We will also include as a fixed constant the cost of capital, labour and so on. Consider, then, the system of interest implied by these definitions exhibited as Figure 1. There are four markets, or balancing operations:

- \* Consumer retailer (the spatial balancing of demand for goods and retail outlets)
- \* Retailer supply retailer demand for facilities (retailer of facilities balancing of revenue and costs)
- \* Retailer demand ~ land supply (land market) for facilities
- \* Consumers suppliers of retail goods (aggregate demand-supply relationships, mediated by retailers).

These are all "markets" in a scmewhat unusual sense, which needs further elaboration. The complications arise from the spatial structure of the problem which means that there is no simple aggregate demand-supply relationship, either for goods or for the provision of retail facilities. It should also be noted that it is a reasonable approximation to consider the retail land market in isolation from other uses. Retailing is not an intensive use like residential or agricultural uses; and so the retailer can be considered to pay a "land rent" in proportion to store size, but essentially for the privilege of using that location.

With these preliminary comments, further elaboration can be obtained by resorting to algebraic notation and defining different kinds of prices. as shown in Figure 2. We are assuming that it is reasonable to work with one composite goods for illustrative purposes, so the "prices" can all be regarded as price indexes. The boxes correspond to those on Figure 1.  $E_{\hat{i}}$  is the demand for goods (measured in the units of goods) by consumer at i and  $\hat{p}_{\hat{i}}$  is the price of goods at i perceived by these consumers (and we will define it more precisely shortly).  $p^{\hat{G}}$  is the (non-spatial) price of goods to retailers and  $\lambda$  is the coefficient which represents their "other costs" (which should also be taken to include "normal" profits).  $r_{\hat{j}}$  is land rent. The portrait of the retailers at  $\hat{j}$  is represented by the variables  $(D_{\hat{j}}, W_{\hat{j}}, F_{\hat{j}}, P_{\hat{j}}, C_{\hat{j}})$ .  $D_{\hat{j}}$  is total revenue attracted to  $\hat{j}$  and  $C_{\hat{j}}$  the total cost.  $W_{\hat{j}}$  is the "attractiveness" of  $\hat{j}$  to consumers and this is now distinguished from floorspace which we denote by  $F_{\hat{j}}$ .  $P_{\hat{j}}$  is the price of goods as sold at the retail centre. Retailers are then assumed to fix  $F_{\hat{j}}$  and  $P_{\hat{j}}$  by a mechanism to be specified, such that  $D_{\hat{j}}$  and  $C_{\hat{j}}$  balance.

There is a problem in constructing  $\hat{\textbf{p}}_i$  . One possibility is to take

$$\hat{P}_{ij} = P_j + C_{ij}$$
 (8)

with a j-subscript added on the left-hand side. But this implies simultaneous determination of destination. It may be better to make an approximation and take

$$\hat{P}_{i} = \frac{\sum_{j} p_{j} e^{-\beta c_{i} j}}{\sum_{j} \sum_{j} e^{-\beta c_{i} j}}$$
(9)

That is,  $\hat{\textbf{p}}_{i}$  is a sum of  $\textbf{P}_{i}$  's weighted by travel cost,with (probably) a being

taken from the spatial interaction model.

The variables  $\{\hat{p}_i\}$ ,  $\{p_j\}$ ,  $\{F_j\}$  and  $\{r_j\}$ , and possibly  $p^G$ , are all to be adjusted within a dynamical model framework. Assume, therefore, that it is reasonable to start with known initial values of them and then to specify the framework of a model, together with an adjustment procedure. An example of a model which will then illustrate all the main ideas is the following:

$$\hat{p}_{i} = \frac{\sum_{j=0}^{i} p_{j} e^{-\beta C_{ij}}}{\sum_{j=0}^{i} e^{-\beta C_{ij}}}$$
(10)

$$E_{i} = E_{i}^{0}(\hat{p}_{i})^{-Y_{1}} \tag{11}$$

for some constant  $E_1^0$ . This makes consumer demand at i a function of  $\hat{p}_1$ . The attractiveness of retailing facilities at j can be taken as a combination of consumer scale economies related to floorspace and possible price discounts:

$$W_{j} = F_{j}^{\alpha_{1}} p_{j}^{-\alpha_{2}}$$
 (12)

then the spatial interaction model is

$$S_{ij} = A_i E_i W_j e^{-\beta C_i j}$$
 (13)

with

$$A_{i} = 1/\sum_{k} e^{-\beta C_{i} k}$$
 (14)

Revenues are given by

$$^{D}\mathbf{j}^{\mathbf{z}}\mathbf{p}\mathbf{j}_{i}^{\mathbf{z}s}\mathbf{i}\mathbf{j}$$
 (15)

and costs by

$$c_j = (p^6 + \lambda + r_j)F_j \tag{16}$$

For the present, we assume  $p^G$  to be fixed and given, though an obvious extension is to integrate it into an aggregate demand-supply model. We then have to add mechanisms to adjust  $F_j$ ,  $p_j$  and  $r_j$ . Assume initially that  $p^G$  is fixed, say in a national market which is not influenced by this particular area. This is equivalent to making the assumption that an aggregate supply  $\frac{F_j}{F_j}(\hat{p}_i)^{-\gamma_1}$  will be available at price  $p^G$  to the retailer.

We now have to specify an adjustment procedure. We can use a 3-D "cobweb" mechanism similar in style to that used by Wilson and Birkin (1985) in the context of agricultural location:

$$\Delta F_{j} = \epsilon_{1}(D_{j} - C_{j}) f_{1}(F_{j})$$
 (17)

$$\Delta p_{j} = -\epsilon_{2}(D_{j} - C_{j})f_{2}(p_{j}) \qquad (18)$$

$$\Delta r_{j} = \epsilon_{3}(D_{j} - C_{3})f_{3}(r_{i}) \tag{19}$$

The functions  $f_1$ ,  $f_2$ , and  $f_3$  determine the nature of these differentials for very small values of  $F_j$ ,  $p_j$  and  $r_j$  respectively.  $\epsilon_1$ ,  $\epsilon_2$  and  $\epsilon_3$  represent the relative strengths of the agents in different spatial "markets".  $\epsilon_1$  will be the greatest of the three if spatial competition for store size among retailers is the dominant process;  $\epsilon_3$  if land owners dominate and can extract any surplus in rent.  $\epsilon_2$  determines the significance of retailers' attitudes to price adjustment (or possibly consumers' ability to force them down). Note also that  $\epsilon_2$  could, for some services, have an opposite sign: if  $D_j > C_j$ , prices could be increased – perhaps for "good" restaurants where  $F_j$  cannot be expanded.

For the illustrative results below, the following functional forms were used for (17)-(19):

$$\Delta F_{j} = \epsilon_{j}(D_{j} - C_{j}) \qquad (17A)$$

$$\Delta p_{j} = -\epsilon_{2}(D_{j} - C_{j})p_{j} \qquad (18A)$$

$$\Delta r_{j} = \epsilon_{3} (D_{j} - C_{j}) r_{j}$$
 (19A)

Then:

$$F_{j}^{\text{new}} = F_{j}^{\text{old}} + F_{j}$$
 (20)

$$p_{j}^{\text{new}} = p_{j}^{\text{old}} + p_{j}$$
 (21)

$$r_{j}^{\text{new}} = r_{j}^{\text{old}} + r_{j}$$
 (22)

This scheme has the advantage that  $\epsilon_1^{-1}$ ,  $\epsilon_2^{-2}$ 0,  $\epsilon_3^{-2}$ 0 reproduces the usual iterative scheme for solving the Harris and Wilson (1978) model – when  $C_1^{-1} = F_1^{-1}$ . That scheme (see Clarke and Clarke, 1984) is

$$F_{j}^{\text{new}} = D_{j} \tag{23}$$

which would arise from

$$\Delta F_{j} = D_{j} - F_{j}^{old}$$
 (24)

which is (17A) with  $c_1$ =1. This has advantages for testing all the relevant computer programmes. A similar exercise shows that if  $C_j$ =  $Kw'_j$ , then  $c_1$ = K has the same property.

The properties of this model have been explored with the 129-zone grid system shown in Figure 3. In the results presented here, equal  $E_i^0$ 's have been used together with equal starting values for  $\{F_{\hat{j}}\}, \{p_{\hat{j}}\}$  and  $\{r_{\hat{j}}\}$ . We set  $p_{\hat{j}}=1$  initially for all  $\hat{j}$ . Equation (10) then shows that all the  $\hat{p}_{\hat{j}}$ 's

are 1 initially. We took  $p^G+\lambda=0.5$  and  $r_j=0.5$ , so the multiplicative constant for  $F_j$  was 1 initially though it could change if  $r_j$  changed. Then  $\underline{e}=(\epsilon_1, \epsilon_2, \epsilon_3)=(1, 0, 0)$  is essentially the Harris and Wilson (1978) model. An  $(F_j)$ -grid plot is shown for this case for reference on Figure 4.1; Figures 4.2 and 4.3 shown the unadjusted prices  $(p_j)$  and rents  $(r_j)$  since  $\epsilon_2=\epsilon_3=0$ . Figures 5.1 and 5.2 show the results of a run with the same parameter values, except that  $\epsilon_3=0.1 \pm 0$  and rent adjustment is now possible. The surface is as might be expected. In Figure 6, the results of a run with  $\underline{\epsilon}=(1, 0.1, 0.1)$  are shown. In this case, the price variations had bounds put on so they could not be reduced below 0.8 nor increased beyond 1.2 and these are visible, in an expected way, with the results shown.

In Figures 7 and 8, we show the consequences of a change in  $\alpha$  and  $\beta$  values. Figure 7.1 shows a very different pattern with only four centres but no central centre. When rent adjustment is allowed, this pattern is modified and there is a very different, but consistent, rent surface as shown in Figure 8.2. With both price and rent adjustment, we get the results shown in Figure 9.

While much more experimentation could be usefully carried out, the results do seem plausible in character. One feature, for example, particularly in the case of rent adjustment, is that the  $\mathbf{F}_j$  pattern is more dispersed when price and rent adjustments are allowed. This is to be expected in that it is no longer the case that all balancing has to be achieved through floorspace adjustments. This is one kind of "dispersion". We now pursue another through the possibility of entropy functions representing imperfections in markets.

### Imperfect markets: sub-optional equilibrium models.

The idea of this section is developed and explained in relation to the Harris and Wilson (1978) model as sketched in section 1 above. The economic extensions of section 2 could obviously be added, however. The idea arises from a problem : the  $D_j$ - $C_j$  balancing mechanism is "optimal" in the sense that the transportation problem of linear programming is optimal. It ought to be possible, therefore, to seek to develop a suboptimal version analogous to the entropy-maximising trip distribution model which has the transportation problem of linear programming as a limiting case. (c.f. Wilson, 1967, Evans, 1973, Wilson and Senior, 1974, Senior and Wilson, 1974.)

If this development can be achieved, there are at least three potential advantages: (i) the new model would be more general with the Harris and Wilson (1978) model as a special case; (ii) the "sub-optimal" model may generate more realistic patterns in many cases – and there should be an appropriate parameter to calibrate in relation to this; (iii) the new model should generate an explicit formula for  ${\sf F}_j$  (or  ${\sf W}_j$ ) which may provide more analytical clues even in relation to the limiting case.

To make progress, we need to recall the mathematical programming version of the Harris and Wilson (1978) model :

$$\max_{\{S_{ij},F_{j}\}} Z = -\sum_{ij} S_{ij} (\log S_{ij}-1)$$

+ 
$$\sum_{i=1}^{n} (E_i - \sum_{j=1}^{n} j_j)$$
  
+  $\sum_{j=1}^{n} j_j (F_j - \sum_{j=1}^{n} j_j)$   
+ $\alpha (\sum_{j=1}^{n} S_{i,j} \log F_j - H)$   
+  $\beta (C - \sum_{j=1}^{n} S_{j,j} C_{i,j})$  (25)

To proceed in the manner of Wilson and Senior (1974), we need to add an entropy term, say,  $-\frac{7}{3}F_{j}(\log F_{j}-1)$ , into the objective function and we need to find a way of relaxing the constraint.

$$F_{j} = \sum_{i} S_{i,j}$$
 (26)

which is represented in the Lagrangian (25) as  $\sum_{i,j} (F_j - \sum_{i,j})$ . If we are responding to market imperfections, then we would expect

$$F_{j} > \sum_{i} S_{ij}$$
 (27)

One way to express this is

$$\sum_{j} (c_{j} - D_{j})^{2} = B$$
 (28)

The new mathematical programming problem and "relaxed" model can now be written:

$$\begin{cases}
\text{Max} & Z = -\sum_{j}^{\infty} (\log F_{j} - 1) - \sum_{j}^{\infty} S_{jj} (\log S_{jj} - 1) \\
+ \sum_{i}^{\infty} (E_{i} - \sum_{j}^{\infty} S_{ij}) \\
+ \lambda \sum_{i}^{\infty} (C_{j} - \sum_{i}^{\infty} S_{ij})^{2} - B \end{bmatrix} \\
+ \alpha \left[ \sum_{i}^{\infty} S_{ij} \log F_{j} - H \right] \\
+ \beta \left[ C - \sum_{i}^{\infty} S_{ij} C_{ij} \right] \tag{29}$$

If we solve

$$\frac{\partial Z}{\partial S_{i,j}} = 0 \tag{30}$$

for S<sub>ij</sub> and

$$\frac{\partial Z}{\partial F_{i,j}} = 0$$

for  $F_{j}$  , keeping  $\lambda$  ,  $\alpha$  and  $\beta$  as parameters which can in principle be found by solving the relevant constraint equations,we get:

$$S_{ij} = A_i E_i e^{-\lambda(D_j - F_j)} F_j^{\alpha} e^{-\beta C_{ij}}$$
(32)

with

$$A_{\tilde{1}} = \frac{1}{2} \sum_{k} e^{-\lambda (D_{k} - F_{k})} F_{k}^{\alpha} e^{-\beta C_{\tilde{1}} k}$$
(33)

$$F_{j} = e^{\lambda(D_{j} - F_{j})} e^{\alpha D_{j}/F_{j}}$$
(34)

We assumed for simplicity that  $\mathbf{C}_j = \mathbf{F}_j$ . The details of the derivation are given in the Appendix, along with some alternative models obtained from different ways of relaxing the  $\mathbf{D}_j - \mathbf{C}_j$  constraint, and which either offer new insights or the possibilities of application in different situations.

Equations (32)-(34) are quite striking. There is a new form of spatial interaction model, through the term  $e^{-\lambda(D_j-F_j)}$  and, most important of all, an explicit formula for  $F_j$ . The equations have to be solved iteratively. Starting with initial values of  $\{F_j\}$  and  $\{D_j\}$  - the latter most obviously set to  $\{F_j\}$  - (32)-(34) have to be initially solved for  $S_{ij}$ ,  $A_i$  and  $F_j$ ; and then reiterated until convergence. A reasonable conjecture would then be that large  $\lambda$  would correspond to small  $\beta$ ; and as  $\lambda \leftrightarrow \infty$ , the solutions of (32)-(34) would tend towards those of the Harris and Wilson (1978) model, as presented in Section 1 above. A summarised example of the results of this model are shown as Figure 10. In Figure 10.1, the  $F_j$ 's do not sum to  $\Sigma E_i$ , showing that the process has not converged. In Figure 10.2, the results of a run are shown where this condition is enforced. More research is currently needed on finding good iterative procedures for these entropy-structure equations.

### 4. Dynamics and further extensions.

The perfect market model is set up as a dynamic model; the imperfect market entropy model is an equilibrium model. The first step in this concluding part of the argument, therefore, is to make the entropy model dynamic. This provides the basis for integrating the two sets of ideas. We then consider a number of extensions to the models and finally make some comments on the empirical development of the models.

Equations (32)-(34) for the equilibrium  $\{F_j\}$  values in the entropy model clearly have to be solved iteratively. Experience has shown that this iterative process is a sensitively-balanced one and there may be practical as well as theoretical reasons for solving them in steps. We

can see how to do this as follows. Rewrite (34) as

$$F_{j}^{\text{new}} = e^{\lambda(D_{j} - F_{j})} e^{\alpha D_{j}/F_{j}}$$
(35)

(with  $\mathbf{F}_{\mathbf{j}}$  as the old value). This represents a stage in the iteration. Hence

$$\Delta F_{j} = F_{j}^{\text{new}} - F_{j}^{\text{old}} = e^{\lambda(D_{j} - F_{j})} e^{\alpha D_{j}/F_{j}} - F_{i}$$
 (36)

and we can then add an  $\boldsymbol{\varepsilon}_1$  factor which we would expect to be less than 1:

$$\Delta F_{j} = \epsilon_{i} \left[ e^{\lambda (D_{j} - F_{j})} e^{\alpha D_{j} / F_{j}} - F_{i} \right]$$
(37)

$$F_{\mathbf{j}}^{\text{new}} = \Delta F_{\mathbf{j}} + F_{\mathbf{j}}$$
 (38)

Equations (32), (33) and (37), (38) then provide an iterative scheme. If the sole interest is in finding equilibrium solutions, then  $\epsilon_1$  should be chosen to achieve this in the smallest number of iterations, and experience should show what constitutes good values for these purposes. However, it could also be argued that real processes are dynamic and that the iterative scheme could be taken as the evolution of the system over time. In that case, we need estimates of empirical values of  $\epsilon_1$  in relation to whatever time period is chosen.

In solving (32)-(34), we made the assumption that  $C_j = F_j$ . More generally, if  $C_j = C_j(F_i)$ , the model can be rewritten, and if we combine this with (37) and (38) above, we get

$$S_{ij} = A_i \epsilon_i e^{-\lambda (D_j - C_j)} \partial_{\beta}^{\alpha C_j} F_j^{\alpha} e^{-\beta C_{ij}}$$
(39)

$$A_{j} = \frac{1}{L_{p}} e^{-\lambda(D_{j} - C_{j})} \frac{\partial C_{j}}{\partial F_{j}} F_{j}^{\alpha} e^{-\beta C_{j}}$$
(40)

$$\Delta F_{j} = \epsilon_{1} \left[ e^{\lambda (D_{j} - F_{j}) \frac{\partial C_{j}}{\partial F_{j}}} e^{\alpha D_{j} / F_{j}} - F_{j} \right]$$
(41)

$$F_{j}^{\text{new}} = F_{j} + \Delta F_{j}$$
 (42)

This model is now in a form where it can be combined with the "economic" model of Section 2. Equations (39) and (40) replace (13) and (14); and equations (41) and (42) replace (17A) and (20). In effect, equations (41)

and (42) (with the modification to  $S_{ij}$  in (39) and (49)) offer an alternative  $F_j$ -adjustment mechanism.  $C_j$  in these equations would then be taken from (16).

We thus now have the entropy model formulated as a dynamic model and we have shown how to integrate it into the economic model. For any of these models, as already noted for the dynamic entropy model, we can consider the parameters  $\epsilon_1$ ,  $\epsilon_2$  and  $\epsilon_3$  as taking values which aid the rapid search for an equilibrium solution or as being empirical parameters which need to be estimated. In either case, we need to be aware of the bifurcation properties of the models with respect to the  $\epsilon$ -parameters: see May (1976); Wilson, (1981-A, 1981-B); Clarke and Wilson (1983).

In further theoretical explorations or empirical developments with these models, there are many alternative formulations of particular elements of the models. For example, the  $\Delta F_j$  adjustment in (17A) could be taken as

$$\Delta F_{j} = \varepsilon_{1}(D_{j} - C_{j})^{\mu} f_{1}(F_{j}) \tag{43}$$

for some parameter,  $\mu$ . It would also be possible to experiment with alternative rent mechanisms. (19A) and (22), for example, might be replaced by

$$r_{j} = f(\sum_{i} j/F_{j})$$
 (44)

That is, the rent could be a function of <u>turnover</u> per square foot directly what is called a more active determination of land rents in Wilson and Birkin (1985).

Much research needs to be done on the iterative processes associated with these models, whether it is considered as a path to equilibrium only the end state of which constitutes some kind of reality; or as a dynamic trajectory, the whole of which is intended to be realistic - possibly governed by underlying and shifting equilibrium states which are not actually reached. In both these cases, the possibilities of multiple equilibria are important and should be explored. In empirical work, there is the advantage that the starting values - an historical or current postion - are known. Indices could be calculated which show the "distance" from equilibrium and the likely direction of change.

It is clear that these items have, potentially, a wide range of application: both in relation to different kinds of systems and to possibilities of different levels of aggregation in each case. More experience will undoubtedly lead to refinement of the ideas.

#### REFERENCES

- Chudzynska, I. and Slodkowski, Z. (1984) Equilibrium of a gravity demand model, Environment and Planning A, 16, pp. 185-200.
- Clarke, G. (1985) Retail centre useage and structure : empirical, theoretical and dynamic explorations, forthcoming Ph.D. thesis, University of Leeds.
- Clarke, G.P. and Clarke, M. (1984) EQILIB: a computer programme to solve the equilibrium version of the production - constrained spatial interaction model. Computer Manual 24, School of Geography, University of Leeds.
- Clarke, M. (1984) Integrating dynamic models of urban structure and activities, Ph.D. thesis, School of Geography. University of Leeds.
- Clarke, M. and Wilson, A.G. (1983) The dynamics of urban spatial structure: progress and problems, *Journal of Regional Science*, 13, pp. 1-18.
- Evans, S. (1973) A relationship between the gravity model for trip distribution and the transportation problem in linear programming. Transportation Research, 7, pp. 39-61.
- Fotheringham, A.S. (1985) Equilibrium and the competing destination model, paper presented to the IBG Annual Conference, Leeds.
- Harris, B., Choukroun, J.-M. and Wilson, A.G. (1982) Economics of scale and the existence of supply-side equilibria in a production-constrained spatial-interaction model, Environment and Planning, A, 14, pp.813-827.
- Harris, B. and Wilson, A.G. (1978) Equilibrium values and dynamics of attractiveness terms in production-constrained spatial-interaction models, Environment and Planning, A, 10, pp. 371-388.
- Kaashoek, J.F. and Vorst, A.C.F. (1984) The cusp catastrophe in the urban retail model, Environment and Planning, A, 16, pp. 851-862.
- Leonardi, G. (1981-A) A unifying framework for public facility location problems Part 1: a critical review and some unsolved problems, Environment and Planning, A, 13, pp.1001-1028.
- Leonardi, G. (1981-B) A unifying framework for public facility location problems Part 2: some new models and extensions, *Environment and Planning*, A, 13, pp.1085-1108.
- Lombardo, S.R. and Rabino, G.A. (1983) Non-linear dynamic models for spatial interaction: the results of some numerical experiments, paper presented to the 23rd European Congress, Regional Science Association, Poitiers, France.
- May, R.M. (1976) Simple mathematical models with very complicated dynamics, Nature, 261, pp. 459-467.
- Phiri, P. (1980) Calculation of the equilibrium configuration of shopping facility sizes, Environment and Planning, A, 12, pp.983-1000.

- Pumain, D., Saint-Julien, T. and Sanders, L. (1984) Vers une modélisation de la dynamique vitra-urbaine, *L'Espace Geographique*, 2, pp. 125-135.
- Rijk, F.J.A. and Vorst, A.C.F. (1983-A) Equilibrium points in an urban retail model and their connection with dynamical systems, Regional Science and Urban Economics, 13, pp. 383-399.
- Rijk, F.J.A. and Vorst, A.C.F. (1983-B) On the uniqueness and existence of equilibrium points in an urban retail model, Environment and Planning, A, 15, pp.475-482.
- Roy, J.R. and Brotchie, J.F. (1984) Some supply and demand considerations in urban spatial interaction models, *Environment and Planning*, A, 16, pp.1137-1147.
- Senior, M.L. and Wilson, A.G. (1984) Exploration and syntheses of linear programming and spatial interaction models of residential location, *Geographical Analysis*, 7, pp.209-238.
- Wilson, A.G. (1967) A statistical theory of spatial distribution models. Transportation Research, I, pp.253-269.
- Wilson, A.G. (1981-A) Catastrophe theory and bifurcation: applications to urban and regional systems, Croom Helm, London; University of California Press, Berkeley.
- Wilson, A.G. (1981-B) Some new sources of instability and oscillation in dynamic models of shopping centres and other urban structures, Sistemi Urbani, 3, pp. 391-401.
- Wilson, A.G. and Birkin, M. (1985) Dynamic models of agricultural location in a spatial interaction framework, Working Paper 399, School of Geography, University of Leeds.
- Wilson, A.G. and Clarke, M. (1979) Some illustrations of catastrophe theory applied to urban retailing structures, in Breheny, M. (ed.) Developments in urban and regional analysis, Pion, London, pp.5-27.
- Wilson, A.G. and Crouchley, R. (1983) The optimum sizes and locations of schools, Working Paper 369, School of Geography, University of Leeds.
- Wilson, A.G. and Senior, M.L. (1974) Some relationships between entropy maximising models, mathematical programming models and their duals, Journal of Regional Science, 14, pp.207-215.

Appendix Derivation of the entropy-structure model; and some alternative models.

First, we derive (32)-(34) from (29)-(31).

$$\frac{\partial Z}{\partial S_{i,j}} = -\log S_{i,j} - a_i - 2\lambda(C_j - \sum_i S_{i,j}) + \alpha \log F_j - \beta C_{i,j} = 0$$
 (A1)

So, absorbing the 2 into the  $\lambda$  changing the sign of  $\lambda$ , and putting  $C_{,j} = F_{,j}$  ,

$$S_{ij} = e^{-a_i}e^{-\lambda(D_j - F_j)}F_j^{\alpha}e^{-\beta C_{ij}}$$
(A2)

(putting  $D_j = \sum_{i} S_{ij}$ ). Put

$$e^{-a_i} = A_i E_i \tag{A3}$$

in the usual way and solve the appropriate constraint equation for  $\mathbf{A}_{\hat{\mathbf{j}}}$  . Then

$$S_{ij} = A_i E_i e^{-\lambda (D_j - F_j)} F_j^{\alpha} e^{-\beta C_{ij}}$$
(A4)

with

$$A_{i} = \frac{1}{k} e^{-\lambda(D_{k} - F_{k})} F_{k}^{\alpha} e^{-\beta C_{ik}}$$
(A5)

$$\frac{\partial Z}{\partial F_{i}} = -\log F_{j} + 2\lambda (C_{j} - \sum_{i} S_{ij}) + \alpha \sum_{i} S_{ij} / F_{j} = 0 \qquad (A6)$$

(so again absorbing 2 into the  $\lambda$  and changing the sign  $\,$  , putting D  $_j$  =  $_i^{\Sigma S}{}_{i\,j}$  and putting C  $_i$  = F  $_j$  )

$$F_{j} = e^{\lambda(D_{j} - F_{j})} e^{\alpha D_{j}/F_{j}}$$
(A7)

In the more general case where  $C_j = C_j(F_j)$ , a factor  $\frac{\partial C_j}{\partial F_j}$  appears on the term associated with  $\lambda$ , to give equations (39)-(42) of section 4.

This model seems to be the best of the alternatives considered. For the record, it is worth briefly indicating what these other alternatives were. To devise the above model, the constraint

$$c_{j} = v_{j} \tag{A8}$$

was replaced by

$$\frac{\mathbf{r}(\mathbf{C_j} + \mathbf{D_j})^2 = \mathbf{B}}{\mathbf{A9}}$$

An apparently simpler alternative is

$$\sum_{j} (\mathbf{F_j} - \mathbf{D_j}) = \mathbf{B} \tag{A10}$$

(with  $C_j = F_j$  again for simplicity of illustration.) Or,

$$\sum_{j} (F_{j} - D_{j}) = \hat{k} F_{j}$$
 (A11)

Or, these aggregate alternatives could be replaced by equivalent zonal constraints :

$$F_{j} = \sum_{i} S_{ij} + B \tag{A12}$$

or

$$F_{j} = \sum_{i} S_{ij} + \hat{k} F_{j}$$
 (A13)

Call the main model in the text El. Then the models associated with constraints (A10)-(A13) can be called E2-E5. We quote the results below. The derivations are straightforward and can be accomplished along the lines of the algebra for model E1 presented above.

## Model E2

$$S_{ij} = A_i E_i F_j^{\alpha} e^{-\beta C i j}$$
 (A14)

$$A_{i} = \frac{1}{\kappa} \Gamma_{k}^{\alpha} e^{-\beta C_{i} k}$$
 (A15)

$$F_{\mathbf{j}} = \frac{1/\Sigma F_{\mathbf{k}}^{\alpha} e^{-\beta C_{\mathbf{j}}} \mathbf{k}}{\sum_{\substack{k \ E e^{\alpha D_{\mathbf{k}}}/F_{\mathbf{k}}}}}$$
(A15)

with

$$F = \sum_{j} F_{j} = \sum_{i} F_{j} + B$$
 (A17)

This is an attractive-looking model, with the spatial interaction formulae

unchanged and a simple expression for  $F_j$ . The problem is that the model does not have good limiting properties. As B+O, then  $\Sigma F_j = \Sigma E_j$ , but unlike model E1 (Figure 11), there remains a positive and negative dispersion around the Harris and Wilson model values. See Figures 11 and 12 for model E3 with floorspace excesses of 5% and 0.5% respectively. Compare Figure 12 with Figure 7: it is still very dispersed.

### Model E3

The same equation holdsbut with

$$F = \sum_{j} F_{j} = (\sum_{i} E_{j})/(1 - \hat{k})$$
 (A18)

# Models E4 and E5

For both models, the following equations hold:

$$S_{ij} = A_i E_i B_j F_j^{\alpha} e^{-\beta C_i j}$$
 (A19)

$$A_{i} = \frac{1}{k} B_{k} F_{k}^{\alpha} e^{-\beta C_{i} k}$$
 (A20)

$$F_{j} = \frac{1}{B_{j}} e^{\alpha D_{j}/F_{j}}$$
 (A21)

Then for model E4

$$B_{j} = \frac{F_{j} - B}{F_{j}^{\alpha} E_{i} e^{-\beta C_{i} j}}$$
 (A22)

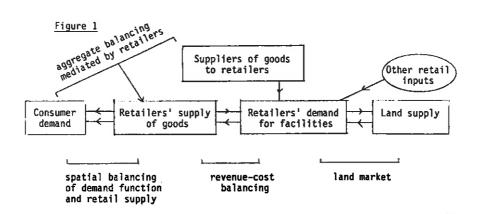
and for model E5

$$B_{j} = \frac{(1 - \hat{k})F_{j}}{F_{j}^{\alpha} \Sigma A_{j} E_{j} e^{-\beta C_{j} j}}$$
(A23)

An example of a run with model E5 is given on Figure 13  $\pm$  c.f. Figures 7, 10, 11 and 12. In the limit as B+O or k+O,

$$B_{j} = \frac{F_{j}^{1-\alpha}}{\sum_{i} A_{i} E_{i} e^{-\beta C_{i} j}}$$
(A24)

and the model becomes the usual quasi-doubly-constrained model - c.f. Wilson and Crouchley (1983).





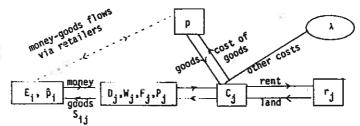


FIGURE 3. The hypothetical grid system

				x¹	x²	X3	x <sup>4</sup>	x <sup>s</sup>			20	
			X <sup>6</sup>	x <sup>7</sup>	XB	X <sub>a</sub>	X <sup>10</sup>	<b>X</b> <sup>11</sup>	X12			
		X <sup>13</sup>	X 14	X <sup>15</sup>	X <sup>16</sup>	X <sup>17</sup>	X18	X <sub>1a</sub>	X <sup>20</sup>	<b>X</b> <sup>21</sup>		
	x 22	x <sup>23</sup>	X 24	X <sup>25</sup>	X <sup>26</sup>	X <sup>27</sup>	X <sup>28</sup>	X <sup>29</sup>	X <sub>30</sub>	X <sup>31</sup>	X <sub>3</sub> 5	
X 33	x <sup>34</sup>	x 35	x <sup>36</sup>	x <sup>37</sup>	X <sup>38</sup>	. X <sub>3 9</sub>	X <sup>b0</sup>	X <sup>51</sup>	X <sup>42</sup>	X <sub>+3</sub>	x**	X 5
X 46	x**	x**	X <sup>49</sup>	X <sup>50</sup>	X <sup>51</sup>	<b>x</b> <sup>52</sup>	X 53	x <sup>54</sup>	x <sup>55</sup>	x <sup>56</sup>	x <sup>57</sup>	X <sup>58</sup>
x <sup>59</sup>	x <sup>60</sup>	X <sub>61</sub>	X <sup>62</sup>	X <sup>63</sup>	X <sup>64</sup>	⊗5⁵	X <sup>66</sup>	X <sup>67</sup>	X <sup>68</sup>	X <sup>6.9</sup>	χ°	x 71
X 72	x <sup>73</sup>	x <sup>74</sup>	x <sup>75</sup>	x <sup>76</sup>	x <sup>77</sup>	x <sup>78</sup>	x <sup>79</sup>	x <sup>80</sup>	<b>x</b> <sup>81</sup>	x <sup>82</sup>	x <sup>83</sup>	x <sup>84</sup>
X 85	x <sup>86</sup>	X <sup>87</sup>	X <sub>8.8</sub>	x <sup>89</sup>	X <sup>90</sup>	X <sup>91</sup>	X <sup>92</sup>	X <sup>93</sup>	x <sup>94</sup> .	X <sup>95</sup>	x <sup>96</sup>	X <sup>97</sup>
	x <sup>98</sup>	x <sup>99</sup>	X <sup>100</sup>	<b>X</b> <sup>101</sup>	X <sup>102</sup>	x <sup>103</sup>	x <sup>104</sup>	X <sup>105</sup>	x <sup>106</sup>	<b>x</b> <sup>107</sup>	X <sub>108</sub>	
		X <sup>109</sup>	X <sup>110</sup>	<b>x</b> <sup>111</sup>	x <sup>112</sup>	X <sup>113</sup>	x <sup>114</sup>	x <sup>115</sup>	x <sup>116</sup>	x <sup>117</sup>		
			X <sup>118</sup>	X <sup>119</sup>	X <sup>120</sup>	X <sup>121</sup>	X <sup>122</sup>	X <sup>123</sup>	X <sup>124</sup>			
				X <sup>125</sup>	X <sup>126</sup>	X <sup>127</sup>	X <sup>128</sup>	X <sup>129</sup>				

FIGURE 4:  $\alpha = 1.05$ ,  $\beta = 0.25$ ,  $\underline{\epsilon} = (1.0.0)$ 

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FIGURE 5:  $\alpha = 1.05$ ,  $\beta = 0.25$ ,  $\epsilon = \{1,0,0.1\}$ 

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3.0	0.0	0.0	0.0	0.4	0.4	0.4	0.4	0.4	0.0	0.0	0.0	0.0	
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0.0	0.0	0.4	1) . 4	0.4	0.4	0.4	0.4	0.4	0.4	3.4	0.0	0.0	
0.0	0.4	0.4	0.4	0 - 4	0.5	0.5	0.5	0.4	0.4	0.4	0.4	0.0	
0 - 4	0.4	0.4	3.4	0.5	U.5	0.6	0.5	0.5	0.4	0.4	0.4	0.4	
5.4	0 - 4	0.4	0.5	0.5	0.6	0.5	0.6	0.5	9.5	).4	0.4	0.4	
0.4	3.4	0.4	0.5	0.6	0.6	0.6	0.6	0.6	0.5	0.4	0.4	0.4	
0.4	0_4	0.4	0.5	0.5	0.6	0.6	0.6	0.5	0.5	0.4	0.4	0.4	
0.4	0.4	0.4	0 _ 4	0.5	0.5	0.6	0.5	0.5	0.4	0.4	0.4	0.4	
0.0	0.4	0.4	0 4	0.4	0.5	0.5	0.5	0.4	0.4	0.4	0.4	0.0	
0.0	0.0	J _ 4	0-4	0.4	0.4	0.4	0 . 4	0.4	0.4	0.4	0.0	0.0	
0.0	0.0	0.0	0.4	0.4	0.4	0.4	0.4	0.4	0.4	0.0	0.0	0.0	
0.0	0.0	9.0	0.0	0.4	0.4	0.4	0 _ 4	0.4	0.0	).0	0.0	0.0	

FIGURE 6:  $\alpha = 1.05$ ,  $\beta = 0.25$ ,  $\varepsilon = (1,0,0.01)$ 

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  F GRID PLOT
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# FIGURE 7 : $\alpha = 1.5$ , $\beta = 0.75$ , $\underline{\varepsilon} = (1.0.0)$

7.	1													
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116	RATION	PUMOE	. 20											
J.00000 0			0.00	U 11 ()	0.	00000		0.00000		0.000	000			
0.0000			0.00	ეიე	U.	00000		0.00000		J. ani	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0			
0.0	0.0	u . 0	0.0	0.0	J.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		
0.0	0.6	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		
<b>0.</b> t	J_0	0.0	Ú.Ü	0.0	0.0	322.5	0.0	0.0	0.0	0.0	0.0	0.0		
0.0	0.0	J. 0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0 <b>.</b> u	0.0	0.0		
0 <b>.</b> ú	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		
ů.C	0.0	0 . u	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		
0.6	0.0	322.5	0.0	7.0	0.0	0.0	0.0	0.0	0.0	322.5	0.0	0.0		
0.0	0 . 0	6.4	0.0	<b>0 _ 0</b>	0.0	G = 0	6.0	0.0	0.0	0.0	0.0	0.0		
0.6	0.0	V = 0	3.0	0.0	0.0	0.0	0.0	0_0	0.0	0.0	0.0	0.0		
0.0	6.0	0.0	0_0	0.0	3.0	0.0	0.0	0.0	0.0	0 <b>.</b> u	0.0	0.0		
0.0	<b>0.</b> €	0.0	J . i.	9-0	J. O	322.5	6.0	0.0	0.0	0.0	0.0	0.0		
0.0	U_U		0.0	J = U	J • G	0.0	0.0	0.0	0.0	0 <b>.</b> u	0.0	0.0		
Ú.i	u = 0	6.0	J.J	0.0	J)	0.0	0.0	0.0	0.0	0.0	0.0	0.0		

FIGURE 8 :  $\alpha = 1.5$ ,  $\beta = 0.75$ ,  $\underline{\varepsilon} = (1,0,0.01)$ 

8	.1											
	Sale : i	f										
	Ca Milai		· - 51									
	04.023			0961	0	_00003		0.0004	. 1	104.07	183	
	04.023			1061	-	-00003		0.0006	_	104.07		
U_U		U_U		104.3	U_0		0.0	104.C	u_0	0.0	0.0	0.0
0.0		ن ۽ ان	بايدان	3.0	0.0		0.0		0.0	0.0	0.0	0.0
U_ U		0.0	0.0	0.0	J.0		0.0		0_0	0.0	0.0	0.0
ن ۽ ن	<b>.</b>	0.0		3.3	Ü		0.0		5.0	0.0	0.0	0.0
104.0	v .			1.1	0.0	60	0.0		v . U	J. J	0.0	104.0
0.0	Ø <b>=</b> √	با ي ∪		5.0	o <b>.</b> 6	4.0		0.0	j. (*	0.4	6.0	0.0
U = 0	ئ <b>ە</b> ق	0.40	٠. :	6.6		11 - 0	0.4		0.0	J. U	0.0	0.0
ب م ان		3 <b>.</b> C	0.0	0.0	!	0.1	$t_{i}$ , $t_{i}$		6.8	ن ال	0.0	0.0
104.0	Jec	0.0	9 - 1.5	1	J <sub>a</sub> € <sub>i</sub>	0.4	0.6	0.0	0.0	U. J	0.0	104.0
<b>J</b> = 0	<b>.</b>	V . (	1.0		1 - 1.	2.0	0.0	0.0	0.0	0.0	0.0	0.0
Ų. u	6 . U	M = M	42 🕳 2.	1.0	J.:	i, 🚅 🕽	6.0	U.0	0.0	0.0	0.0	0.0
Ŭ	- ·	3 . 1		1 - 11	1.	)	1.7	G . :)	0.40	0.3	0.0	0.0
0-1	U	i. • 1	٠.	1 4	141	0.0		14.00	ΰ∎u	0.0	0.0	0.0
8.	2											
	- Lirebi											
	AATIJ'	. 1	4.5									
	1.045 _					7-240						
	1.049 3					1740		50145 50145		1-049		
0.0	2				2.4			1.3		1.049		
Uww					1.4	4		,		0.0	0.0	0.0
6.1	V = 1		7.4		1.	U.4	4	1.4	0.4	J.J 9.4	6.0	0.0
U_V	U			4		14	0.4	1.4	J 4	0.4	0.6 0.4	0.0
1.0	U . 4		7 - 4	1.4	4	1 4	0.4	U . 4	(1 4	7.9 11.4	0.4	0.0 1.0
0.4	W . 6		1.1		9.4	0.24	13 _ 4	1 4	0.4	0.4	0.4	
U . 4	v . ·				0.4	0.4	. 4	ú . 4	0.4	J 4	0.4	1) _ 4 U _ 4
0.4			(2)	4 4	4	2.4	4	1.4	0.4	3.4	0.4	0.4
1.0			-			0.4	0.4	J . 4	0.4	0.4	U.4	1.0
0.0				- 4		1.4				3.4	U . 4	0.0
0.0				04025	1.0	- 4	- 4		147	7. 7	0.0	3.0
V		*				- 4			1.77	1.3	U = 0	3.0
							-	-				W = 1

FIGURE 9 :  $\alpha = 1.5$ ,  $\beta = 0.75$ ,  $\underline{\varepsilon} = (1, 0.01, 0.01)$ 

9.1		
F GRID PLOI		7.
TERATION NUMBER 4	1 00000 0.00000 0.000	100 mm
0.00000 0.4	00000 0.00000 0.000	0.0000
0.0 0.0 0.0 0.0		0.0 0.0 0.0 0.0 0.0 0.0 0.0
<u> </u>	0 0.0 15.8 284.5 15.8 0.0	0.0.0.0.0.0.0.0
0.0 0.0 0.0 0.0 =-0.0 0.0 0.0 0.0		
0.0 0.0 16.1 0.0	0 0.0 0.0 0.0 0.0	0.0 16.0 0.0 0.0
0.0 0.0 282.9 0.0		
0.0 0.0 0.0 0.0	0 0 0 <u>0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 </u>	0.0 0.0 0.0
0.0 0.0 0.0 0.0	0.0 1578 28775 1578 1070	יים היים מיים מיים
0.0 0.0 0.0 0.0		0.0 0.0 C.0 0.0
0.00 0.00 0.00 0.00	e organica concentrate organic	0.0 0.0 0.0
9.2		
ORIGINAL PRICE		
1.10465 1.16	0458 1.10432 1.1043	8 1.10405
1.10505 1.10	0624 1.10652 1.1062	
0.0 0.0 0.0 0.0		
0.0 0.0 1.1 1.1 = 0.0 1.1 1.1	1.1 1.2 0.8 1.2 1.1 1.1 1.1 1.1 1.1 1.1	1.1 1.1 0.0 0.0 1.1 1.1 1.1 0.0
1.1 1.1 1.1 1.1	1.1 1.1 1.1 1.1 1.1 1.1	1.1 1.1 1.1 1.1
F177 1.1 1.2 1.1	1.1 =1.1 1TF 1:1 1.F	1.7 1.2 1.1 1.1
1.1 1.1 0.8 1.1 1.1 1.1 1.2 1.1	1.1 1.1 1.1 1.1 1.1 1.1 1.1 1.1 1.1 1.1	1.1 0.8 1.1 1.1 1.1 1.2 1.1 1.1
1.1 1.1 1.1	1,1 1,1 1,1 1,1 1,1	1.1 1.1 1.1 1.1
0.0 0.0 1.1 1.1	1.1 1.1 1.1 1.1 1.1 1.1 1.1 1.1	1.1 1.1 1.1 0.0 L
0.0 0.0 0.0 1.1	1.1 1.1 1.1 1.1 1.1	1.1 0.0 0.0 0.0
0.6 0.0 0.0	1.9 1.7 1.7 1.1 1.1	0.0 0.0 0.0
9.3		
REWL PLUT		
TIERATION JUMBER 43 0.45195 0.45	5205 v.45207 0.4520	5 9.45195
0.45195	5285 0.45207 9.4520	5 0.45195
0.0 0.0 0.0 0.0	0.5 0.5 0.5 0.5 0.5 0.5 0.7 0.5 0.5 0.5	0.0 0.0 0.0 0.0
0.0 0.0 0.5 0.5	0.5 0.1 0.6 0.1 7.5	0.5 0.5 0.0 0.0
0.0 0.5 0.5 0.5	0.5 0.5 0.5 0.5 0.5	0.5 J.5 0.5 0.0 0.5 0.5 0.5 0.5
0.5 0.5 0.5 0.5 0.5 0.5 0.1 0.5	0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5	6 5 0 L 0 5 0 5
0.5 0.5 0.6 0.5	0.5 0.5 0.5 0.5 0.5	0.5 0.6 0.5 0.5 0.5 0.1 0.5 0.5
0.5 0.5 0.1 0.5 0.5 0.5 0.5 0.5	0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5	0.5 0.5 0.5 0.5
<u></u>	0.5 0.5 0.5 0.5 0.5	0.5 0.5 0.5 0.0 0.5 0.5 0.0 0.0
0.0 0.0 0.5 0.5	0.5 0.1 0.6 0.1 0.5 0.5 0.5 0.5 0.5	0.5 0.0 0.0 0.0
0.0 0.0 0.0 0.0	u.5 0.5 0.5 0.5 9.5	0.0 0.0 0.0

ī

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FIGURE 10.1 : Entropy model £1
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F GRID FLCT
         ITERATION NUMBER 10
11.74884 13.43126
11.74864 13.48128 13.54690 13.48125 1
0.0 0.0 0.0 0.0 11.7 13.5 13.5 13.5 11.7 0.0
0.0 0.0 0.0 12.6 24.6 23.6 44.3 23.6 24.6 12.8
0.0 0.0 12.1 22.8 27.3 364.6 454.1 354.8 27.3 22.5 1
0.0 12.8 22.6 15.1 17.7 10.9 9.1 10.9 17.7 15.1 2
11.7 24.6 27.3 17.7 7.6 5.9 6.8 6.5 7.3 17.7 2
13.5 23.5 364.9 10.9 6.5 6.5 5.5 5.2 10.0 27.1
13.5 44.3 454.3 4.5
                                                                                                       13.54690
                                                                                                                                                      13.46125
                                                                                                                                                                                                    11.74894
                                                                                                                                                                                                      11.7469L
0.0 0.0
                                                                                                                                                                                                                                               0.5
                                                                            24.6 23.6 44.3 23.6 24.6 12.8 0.0 27.3 364.6 454.1 364.8 27.3 22.5 12.1 17.7 10.9 9.1 10.3 17.7 15.1 22.2 7.6 5.9 6.8 6.5 7.3 17.7 27.3 6.5 6.5 5.9 5.0 5.9 5.8 9.1 454.3 6.5 6.5 5.7 10.0 364.6 6.5 6.5 5.7 10.0 364.9 17.7 17.7 17.3 17.7 27.3 17.7 10.9 9.1 10.9 17.7 15.1 22.8 27.3 364.9 454.3 354.9 27.3 22.8 12.1 24.6 23.6 44.3 23.6 24.5 12.9 0.0 11.7 13.5 13.5 13.5 13.5 11.7 0.0 0.0
                                                                                                                                                                                                        0.0
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                                                                                                                                                                                                                      12.5
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44.3 13.5
23.6 13.5
24.5 11.7
12.8 0.0
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                   44.3 454.3
23.6 364.9
                                                           9.1
10.9
                   24.6 27.3
12.8 22.3
0.0 12.1
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15.1
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                                      0.0
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            5.0
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                                                                                                                                                                                                                                             0.5
0.5
  0.0
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                                                            a. o
```

FIGURE 10.2. : Entropy model - totals normalised (E1)

FIGURE 11: Entropy model E3  $\alpha = 1.5, \; \beta = 0.75, \; 5\% \; excess \; floorspace$ 

	RID FL									
ITE	RATION	NUMBE	R 37							
	5-9176 5-8176 0.0 0.0 0.0 6-4 9-2 17-4 9-2 5-4 0.0 0.0	7	6.80 6.80 0.0 5.4 9.3 12.1 12.2 12.5 12.6 12.9 13.2 12.1 9.3 6.4 0.0		04502 04602 7.0 12.0 14.7 12.6 11.2 10.5 11.2 12.6 14.7 12.6	6.8 11.4 14.3 12.9 11.4 10.7 10.7 11.4 12.9 11.4 6.8	5-8024 5-8 7-2 12-2 11-2 11-2 11-2 11-2 13-2 13-2 13	5.81 5.81 0.0 0.0 6.5 9.3 12.5 14.3 14.3 14.3 14.5 6.5 0.0	767 0.0 0.0 0.0 6.4 9.2 11.4 12.0 11.4 3.2 6.4 0.0	0.0 0.0 0.0 0.0 5.8 7.0 6.8 7.0 6.8 7.0 9.0
						_		 0.0	0.0	9-0

FIGURE 12: Entropy model E3  $\alpha = 1.5$ ,  $\beta = 0.75$ , 0.5% excess floorspace

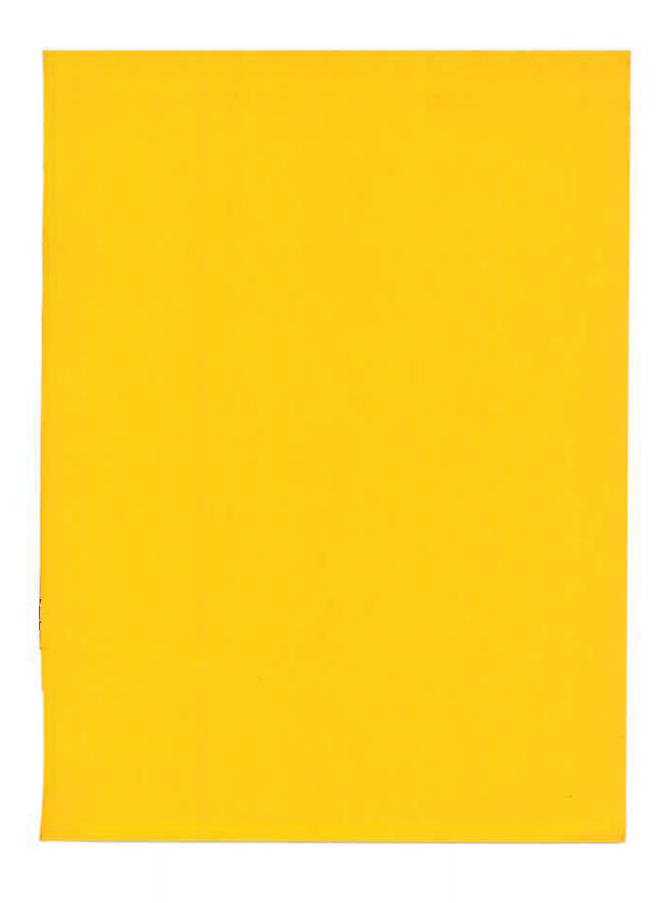
AD PL	) I							- 32			
8 A 1 I ON	NUMBE	₹ 10									
5.5371	7	6.27	685	6.	50994		6.2768	15	5.33	717	
<del>_</del>		6.27	685	6.	50944		6.2768	5	5.33	717	
0_0	0.0	0.0	5.3	6.3	6.5	6.3	5.3	0.0	0.0	0.0	0.0
ıi <b>.</b> ()	0.0	5.4	3.6	11.0	11.7	11.0	8.6	5.9	0.0	0.0	0.0
0.0	5.9	3.8	12.1	14.0	14.4	14.0	12.1	8.3	5.9	0.0	0.0
5.9	9.3	11.7	12.3	12.5	12.3	18.5	12.3	11.7	8.3	5.9	0.0
3.6	12.1	12.3	11.7	10.9	10.7	10.9	11.7	12.%	12.1	8.6	5.3
11.0	14.0	12.5	10.9	10.2	9.9	10.2	10.9	1?.5	14.0	11.0	6.3
11.7	14.4	1.2.3	10.7	9.9	9.7	9.9	10.7	12.3	14.4	11.7	6.5
1.0	14.0	12.5	10.4	10.2	9 6	10.7	10.0	12.5	14.0	11.0	6.3
0.6	12.1	12.8	11.7	10.9	10.7	10.0	11.7	12.3	12.1	8.6	5.3
5.0	4.8	11.7	12.8	12.5	12.	12.5	12.8	11.7	5.8	5.9	0.0
1.0	5 . 0	3.4	12.1	14.0	14.4	14.0	12.1	8.3	5.9	0.0	0.0
() ()	0.0	5.1	8.6	11.6	11.7	11.0	4.6	5.9	0.0	0.0	0.0
9.0	0.0	0.0	5.3	6.3	4.5	6.3	5.3	0.0	0.0	0.0	0.0
	8 Alion 5 - 3371 5 - 3371 5 - 3 6 6 - 0 6 - 0 7 - 9 8 - 6 11 - 9 11 - 7 11 - 0 6 - 6 5 - 9 11 - 0 0 - 0	5.53717 5.35717 0.0 0.0 0.0 5.9 5.9 5.3 8.6 12.1 11.0 14.0 21.7 14.4 11.0 14.0 6.6 12.1 5.9 5.2 0.0 5.9 0.0 5.9	**************************************	### ##################################	**************************************	SATION NUMBER         10           5-33717         6-27685         6-50994           0-0         0-0         5-3         6-3           0-0         0-0         5-3         6-3         6-5           0-0         5-9         3-6         11-0         11-7           0-0         5-9         3-8         12-1         14-0         14-4           5-9         5-3         11-7         12-3         12-5         12-3           3-6         12-1         12-3         11-7         10-9         10-2         9-9           11-0         14-0         12-5         10-9         10-2         9-9           21-7         14-4         12-3         10-7         9-9         9-7           11-0         14-0         12-5         10-9         10-2         9-9           6-6         12-1         12-8         11-7         10-9         10-7           5-9         3-8         11-7         12-8         12-5         12-3           1-0         5-9         3-8         12-1         14-0         14-4           0-0         5-9         3-8         12-1         14-0         14-4	**************************************	**************************************	**MAITON NUMBER** 10	### #### #############################	**MAITON NUMBER** 10   5-\$3717

FIGURE 13, Entropy model E5

P S	alo Fi	.01										
	ARTICA		(ia 3									
	3.7423		23.00	1111	29.	12363	,	7. 5595	2	29.74	240	
20.74242			23.06	1.54.		16845		5686		28.74		
0.0	0.0	7.0	ງ.ກ	27.7	. 5.7	24.2	29.7	29.7	0.0	0.0	0.0	0.0
0.0	0.0	0.0	33. ₹	ZÚ. ~	10.1	7 4	10.1	23.5	79.7	0.0	0.0	0.0
0.0	0.0	23.1	17, 1	4.C	1.0	0.€	1.0	4.0	17.1	26.1	0.0	0.0
0.0	26.7	17.1	3. t.	0. //	0.4	C. 3	J.L	າ.∘	3.6	17.1	29.7	0.0
2°.7 29.7	20.6	4.0	0	0.	Ç- 5	0.5	3.5	7.5	7. *	Ŀ.O	20.6	28.7
29.7	10.1	1.0	0.4	0.3	0.7	0.8	0.7	0.5	0.4	1.0	10.1	29.7
29.7	7.4 10.1	9.5	2-3	0.5	C.E	9.9	J. F	7.5	0.3	0.٤	7.4	29.2
27.7	20.€	1.0	0. E	C.5	0.7	0.9	J.7	7.5	0.11	1.0	10.1	2 3.7
1.0	23.7	4.0	.) .	0.	3.5	0.5	. J = 5	). =	0.8	Ŀ.O	20.5	28.7
0.0	0.0	17.1 29.1	3	С. 3	0.4	0.3	0.4	).¤	3. 5	17.1	28.7	0.0
0.0	0.0	).0	17.1 23.7	4. 0	1.0	3.5	1.0	0	17.1	26.1	0.0	0.0
0.0	3.0	0.)	), )	20. :	10.1	7.4	10.1	20.5	,6.4	0.0	0.0	0.0
0.0	9.0	9.3	1. /	28.5	2 : . 7	`=.2	20.7	79.7	0.0	J. 0	0.0	0.0

Figure 9. Entropy model (vi)

FG	RID F	LCI										
17 E	SAPIO:	غد ۱ ال ۱۹	. 10									
	1.743		13.43	128	13.	50600	1	3. 4612	5	11.74	een	
11.74884			13,48	129	13.	54690		3.4-12		11.74		
0.0	0.0	0.)	J. 0	11.7	13.5	13.5			<b>"</b> "	0.0	0.0	U. 0
0.0	0.0	0.0	12.°	24.6	43.€	ز _ نا ،،	23.6	24.8	12.8	6.0	0.0	0.0
C.U	0. u	12.1	22. ?	27.5	364.5	4 4 1	354.7	27.3	22.3	12.1		
J_()	12.8	22.8	15.1	17. 7	10.5	ş 1	15.0	17.7			0.0	0.0
11.7	24.6	27.3	17.7	7.1	5 5				15.1	22.	12.5	9.0
13.5		364.9	10.			÷ . 3		7.3	17.7	د . 7٪	24.6	11.7
13.5				7.0	4.5	5.5	6.5	٠, ٦	10.0	16 L . A	23. €	13.5
		450.3	∉.1		5.5	14 a 14	5.0	5 a	7 - 1	54 . 3	44.3	13.5
13.5	23.0	364.3	1.1		4.5		2.5	5.5		16.	23.6	
11.7	24.6	27.3	17.7	7	2.5			7.0		_		13.5
0	12. 1	22.3	1 . 1	17.	1( ¢	_			17.7	27.3	20.0	11.7
0.0	Ű. u	12.1				7.1	10.9	17.7	15.1	2	12.8	0.0
			2 7. 4	27. :		H14.3		27.3	ž".;	11	0.0	1.3
9.0	(دیدن	0.0	12.	24.5	43.6	L	23.5	24.5	12.7	<b>U</b> _0	U.0	0.0
Û <b>±</b> 17	0.0	1.1	), "	11.5	1 3. ~	15	13.5	11.7	7.0	^ - ·	0.0	J. J



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