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Section 1.
Introduction

1.1 INTRODUCTION

The Canberra Model 2007P Tube Base-Preamplifier provides the high voltage divider network for correctly biasing essentially all 10-stage photomultiplier tubes (PMT) used for nuclear spectroscopy. This network is intended for use with a positive high voltage for tubes which operate with their photocathodes near ground potential. The network includes a focus control for adjusting the detector resolution performance, and a gain trim control for matching outputs of several detectors when used in arrays.

Designed to be compatible with the Canberra Model 802 series Scintillation Detectors (or equivalent), the tube base connects directly to the pins of the PMT, providing a compact integrally mounted assembly.

The Canberra Model 2007P Tube Base-Preamplifier also contains a low noise charge-sensitive preamplifier. The preamplifier recovers the charge pulse at the anode pin of the PMT directly and converts it to a positive voltage pulse output. The peak amplitude of each output pulse is linearly proportional to the total charge output of the PMT during each amplified photo event. The pulse is set to decay at a nominal 50 μsec time constant, and interfaces directly with any of Canberra's spectroscopy amplifiers.

The Model 2007P includes a diode protection network on the preamplifier input to prevent damage to the circuitry from the inadvertent sudden application or removal of PMT bias voltage. A test input is also provided to aid system testing, gain calibration, or troubleshooting. Preamplifier power is usually derived from the associated pulse shaping amplifier. A ten-foot long power cable in supplied with the Model 2007P.

Section 2.
Specifications

2.1 INPUTS

DETECTOR—The preamplifier is internally connected to pin 11 of the Tube Base socket (PMT anode).
TEST INPUT—Accepts a positive - or negative - polarity tail pulse from a test-pulse generator. Charge coupled at 30 picocoulombs per volt to preamplifier input. Voltage gain to output is 130 mV/V nominal. Input impedance is≈ 93 ohms.
HV INPUT—PMT bias-voltage range, 0 to + 2000 V dc. Anode series resistance 1M ohms. Bias network total resistance: 6.66 M ohms to 7.16 M ohms, depending on the position of the GAIN control.

2.2 OUTPUTS

ENERGY OUTPUT—Provides unipolar positive pulses linearly proportional in peak amplitude to charge delivered at PMT anode.

Decay time constant 50 microseconds nominal. Rise time less than 20 nanoseconds. Delivers up to 10 V peak. Output impedance ≈ 93 ohms, series connected; direct coupled.

2.3 PERFORMANCE

INTEGRAL NON-LINEARITY—less than ± 0.04% for up to 10 volt output.
GAIN DRIFT—Less than ± 0.01%/°C (± 100 ppm/°C).
NOISE—Less than 1×10^{-16} coulombs rms referred to input.
CHARGE SENSITIVITY—4.5 mV/picocoulomb

2.4 CONNECTOR TYPES

HIGH VOLTAGE—SHV
ENERGY OUTPUT, TEST INPUT—BNC
TUBE SOCKET—14-pin (Cinch Jones 3M-14 or equivalent)
POWER—Amphenol 17-20090

2.5 CONTROLS

FOCUS—Single-turn screwdriver adjusted potentiometer to adjust voltage at grid of PMT. Range 72 to 145 V per 1000 V dc of high voltage input.
GAIN—Single-turn screwdriver adjusted rheostat to adjust anode bias. Adjustment range: 92% to 100% of applied high voltage.

2.6 POWER REQUIREMENTS

HIGH VOLTAGE—Bias network requires 150 μA per 1000 V dc
± 12 V dc—15 mA dc nominal

2.7 PHYSICAL

SIZE—Diameter 5.8 cm (2.3 in.)
LENGTH—7.6 cm (3.0 in.)
NET WEIGHT—0.7 kg (1.5 lb.)

Section 3.
Installation

3.1 GENERAL
The Model 2007P is intended to provide a convenient package for interfacing with the photomultiplier tube (PMT). As specific mounting details differ significantly between applications, only the following general considerations can be offered.

3.2 DETECTOR MOUNTING
The tube base preamp is intended to mount coaxially with the Model 802 series scintillation detectors simply by mating the PMT pins into the tube socket. The scintillator should, of course, be handled with care in mating, and protected from shock.

3.3 PRECAUTIONS
Consistent with good operating practice for the PMT, the high voltage full bias should not be applied immediately; it should be raised and lowered over several seconds. The Model 2007P is diode protected for occasional faults and for high-voltage arcing. A primary consideration here will be the instantaneous noise current in the PMT, which may take a considerable time to settle.

Steady state dissipation in the PMT bias network has been minimized, in order to prevent degradation of background "dark" currents due to local heating. Hence no particular care need be expended in providing any heat sinking for the tube base.

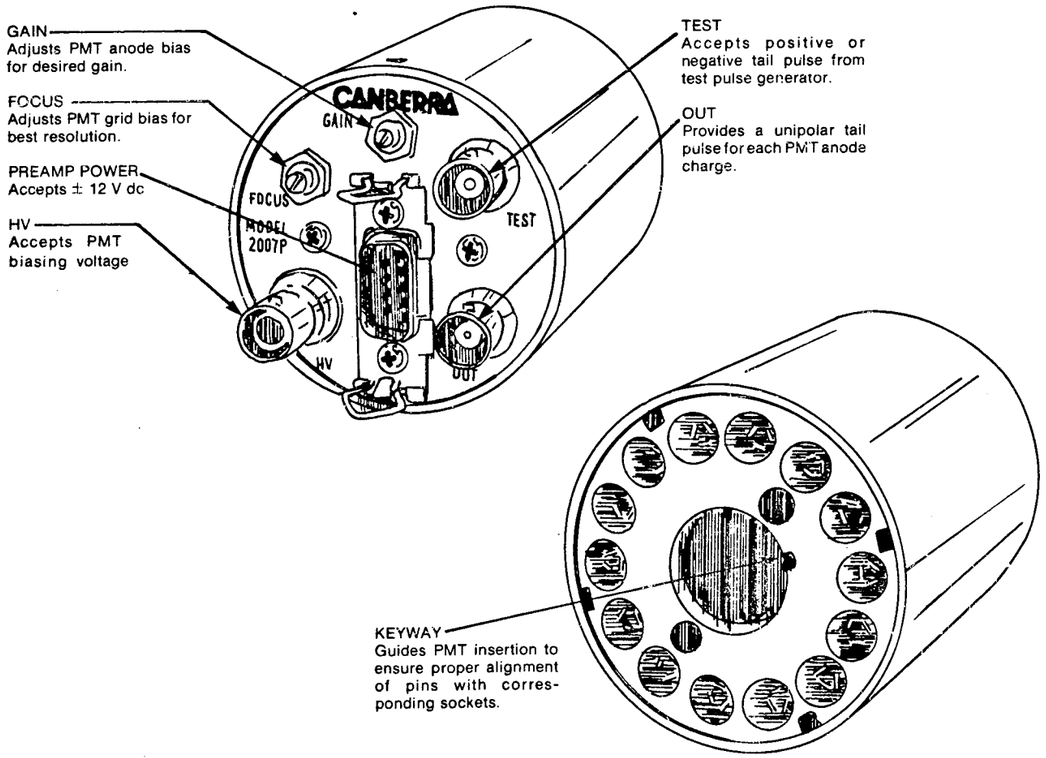


Figure 2-1
Model 2007P
Front and Rear Panels

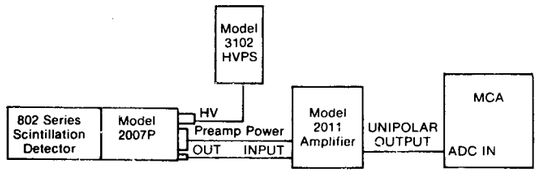
Section 4.
Operating Instructions

4.1 GENERAL
The purpose of this section is to familiarize the user with a typical setup incorporating the Model 2007P Photomultiplier Tube Base/Preamplifier. The following discussion of a typical configuration will give the user sufficient familiarity with the Model 2007P to permit its proper use in any system.

4.2 SETUP
Connect the Model 2007P to the Photomultiplier Tube (PMT). Be certain to align the key on the PMT with the keyway on the Model 2007P before attempting to insert the PMT pins into the tube base socket. See the rear panel photograph (Figure 2-1) for the location of the keyway.

Using a small screwdriver, turn the Model 2007P GAIN control to its extreme clockwise position, which will provide the highest possible gain, and adjust the FOCUS control to about mid-range.

Connect a high-voltage cable between the Model 2007P HV connector and the High Voltage Power Supply. Connect a signal cable between the Model 2007P OUT connector and the amplifier's input. Connect the preamplifier power cable between the preamp power (9-pin) connectors on the Model 2007P and the amplifier. Note that for a PMT, the amplifier must be capable of 0.5 μ sec shaping.



Model 2007P in a Typical System
Figure 4-1

4.3 THE GAIN CONTROL
The GAIN control is used to match the gain of two or more PMTs in a multiple detector system. If a single PMT is being used, the control should be left in the extreme clockwise position.

To match the gain of several PMTs, it is necessary to know the gain of the each detector. Collect several thousand counts in a peak of ^{137}Cs (for instance) and record the number of the peak channel. Repeat for each PMT.

Place the MCA's cursor in the lowest recorded channel found in the preceding paragraph and adjust the GAIN controls of each PMT in turn so that all will collect the peak in that same peak channel.

4.4 THE FOCUS CONTROL
The FOCUS control is used to obtain the best possible resolution with a given PMT. Resolution is defined as the ability of the detector to differentiate between two peaks that are close together in energy. Thus the narrower the peak the better the peak separation and the better the resolution.

Start with the FOCUS control set about the middle of its range. By checking the resolution several times with a slight adjustment of the FOCUS control each time, the point of best resolution can be found.

4.5 RESOLUTION
The full width of the peak at half of its maximum value (FWHM) is used to determine the resolution by:

$$\text{Resolution} = \frac{\text{FWHM}}{\text{Peak Position}}$$

where Peak Position and FWHM are expressed in channels. The performance of a scintillation detector is usually specified in terms of its resolution for the 662 keV peak of ^{137}Cesium.

To determine the resolution, collect a peak of 10 000 counts of ^{137}Cs. Half maximum of the peak would be 5 000 counts, but it is unlikely that there will be a channel that contains exactly 5 000 counts. Therefore, it is necessary to interpolate the data.

Record the following information:

a. The peak channel. That is, the channel with 10 000 counts.
b. The counts in the channel just below FWHM on the left side of the peak. Counts $< 5\,000$.
c. The counts in the channel at or just above FWHM on the left side of the peak. Counts $\geq 5\,000$.
d. The number of the channel at or just above FWHM on the left side of the peak.
e. The number of the channel at or just above FWHM on the right side of the peak.
f. The counts in the channel at or just above FWHM on the right side of the peak. Counts $\geq 5\,000$.
g. The counts in the channel just below FWHM on the right side of the peak. Counts $< 5\,000$.

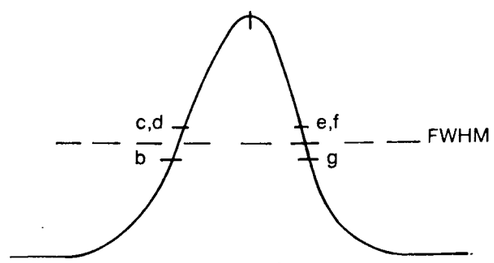


Figure 4-2

Using the information gathered above, apply the following formula:

$$\frac{e\text{-}d + \frac{b}{c} + \frac{f}{g}}{a} = \text{resolution expressed as a decimal fraction.}$$

The resolution will be in the range of 0.06 to 0.09 (6% to 9%) for a Canberra Series 802 Scintillation Detector.

By adjusting the FOCUS control slightly to one side or the other of mid-range and doing another resolution check, it will be apparent that the resolution has been improved (the number is smaller) or has been degraded (the number is larger).

By doing several successive approximations, the best resolution will be found. The FOCUS control can be left in that position as long as the same PMT and Model 2007P are associated. It would be helpful however, to check for best resolution from time to time to be sure that there is no change with time.

Section 5.
Theory of Operation

5.1 GENERAL

The Model 2007P essentially consists of two functionally separate sesctions. The voltage divider provides the photomultiplier tube (PMT) with the proper operating potentials and the preamplifier converts the charge output of the PMT into a proportional voltage.

Specifically, the bias network chosen for the PMT provides the nominal distribution of accelerating potentials between dynode sections that has found to yield the best performance for nuclear applications. Capacitors C9 and C10, provided between the anode and upper two dynodes, bypass large signal current occuring under moderately high pulse amplitude conditions. RV3 permits independent control of PMT grid potential for optimization of resolution, while RV2 permits PMT gain to be adjusted by modifying the potential applied at the top of the divider string.

The preamplifier section functions as an operational integrator with Q1 in the common source configuration providing a high open loop gain by virtue of the ac bootstrap action furnished by C5. Q1 also allows a high input impedance by virtue of its gate input, while Q2 provides current gain and low output impedance. The loop is then closed by the integrating capacitor C3, with R5 providing dc stability in addition to facilitating the discharge of C3. RV1 enables the adjustment of output dc offset at the same time allowing the gate of Q1 to be biased slightly negative.

The sensitivity of the preamp to charge may be calculated by noting that all charge transferred from the PMT anode through C2 collects on C3, creating a potential difference across C3 according to the relation,

Q=CV or V/Q = 1/C3
For the 2007P since C3 = 220 pF,
V/Q = 1/220 pF = 4.5 mV/pC

Filtering of the HV input is provided by C8 while standard LC decoupling of the low voltage supply lines is employed to minimize problems caused by noise pickup in the power cable.

5.2 EQUIPMENT REQUIRED FOR CHECKOUT

1. Calibrated dual trace Oscilloscope (scope), rated dc-100 MHz minimum, with vertical sensitivity of at least 50 mV/cm and a time base sweep of at least 20 ns/cm.
2. Reference Pulser with a rise time less than 20 nsec (Canberra Model 1407 or equivalent).
3. High Voltage Power Supply (HVPS).
4. DC Voltmeter (DVM) with rated accuracy to 0.1% with a 10M ohm input impedance.
5. Model 2000 NIM Bin and Power Supply, or equivalent.
6. Preamplifier power source with Preamp Power Connector. Note that all Canberra amplifiers are equipped with preamp power connectors.
7. Shielded coaxial cable, RG-62, BNC-BNC as required, lengths as short as practicable, herein referred to as "coax".
8. Shielded coaxial cable, RG-59, SHV-SHV as required, lengths as short as practicable, herein referred to as "HV coax".

5.3 INITIAL SETUP FOR CHECKOUT

1. Model 2007P:

GAIN	fully CW
FOCUS	fully CCW

2. Model 1407 Pulser:

RISE TIME	MIN
FALL TIME	400 μsec
ATTENUATION	X2
LINE/OFF/90Hz	90 Hz
NORMALIZE	fully CW
POS/NEG	NEG

3. Oscilloscope

CHANNEL 1	1 V/cm
CHANNEL 2	50 mV/cm
DISPLAY	ALT,EXT TRIG
SLOPE	(-)
TIME BASE	20 μsec/cm

5.4 CHECKOUT PROCEDURE

1. Connect the preamp power cable from the 2007P to the source of preamp power.
2. Using a length of coax, connect the OUTPUT of the 2007P to channel 2 of the scope.
3. Apply power to the 2007P and verify the dc level on the scope channel 2 trace is 0 ± 50 mV.
4. Connect the 1407 NORMAL output to the scope external trigger input and the 1407 ATTEN output to the scope channel 1 input using suitable coax lengths.
5. Adjust the 1407 PULSE HEIGHT control for a -5V signal on the channel 1 trace.
6. Remove the cable from the Scope channel 1 input and connect it to the 2007P TEST input.
7. Move the cable from the scope channel 2 input to channel 1 input and set the channel 1 range to 0.2 V/cm.
8. Verify the signal on the channel 1 trace to be > + 1 volt.
9. Adjust the 1407 PULSE HEIGHT control for a 1 V signal on the channel 1 trace.
10. Verify the slow fall time from 1 V peak to 360 mV to be between 35 and 65 μsec.
11. Expand the scope time base to 10 nsec/cm and verify the fast rise time from the 10 - 90% levels to be < 20 nsec.
12. Disconnect all coax from the 2007P and using HV coax connect the HVPS to the HV connector on the 2007P.
13. Make sure the 2007P is resting on a nonconductive surface and increase HVPS to + 100 V dc.
14. Use the DVM to measure the potential, with respect to chassis ground (pin 14), of each pin in the 2007P socket. The range of acceptable potentials is given below in dc volts.

PIN					
	1	13 - 15.4	8	63.1 - 69.7
	2	20.7 - 22.9	9	72.2 - 79.9
	3	27.4 - 30.2	10	80.8 - 91.6
	4	33.7 - 37.3	11	89.8 - 99.2
	5	40.5 - 44.7	12	no connection
	6	47.4 - 52.4	13	7.6 - 8.4
	7	54.8 - 60.6	14	ground

15. Turn the FOCUS control to CW. Pin 13 should now be 14 to 15.4 V. Turn GAIN control to CCW. Pin 10 should now be 70.9 to 82.7 V. Reduce HVPS to zero and turn OFF.

CANBERRA

BASIC WARRANTY

Equipment manufactured by Canberra Industries, Inc. is warranteed against defects in materials and workmanship for a period of twelve months from date of shipment, provided that the equipment has been used in a proper manner as detailed in the instruction manuals. During the warranty period, repairs or replacement will be made at Canberra's option on a return to factory basis. The transportation cost, including insurance to and from Canberra, is the responsibility of the Customer except for defects discovered within 30 days after receipt of equipment where shipping expense will be paid by Canberra to and from Canberra.

The customer must obtain an authorized customer service return number before returning any equipment to the Canberra factory. *Compliance with this provision by the customer shall be a condition of this warranty.* In giving shipping instructions, Canberra shall not be deemed to have assumed any responsibility or liability in connection with the shipment.

The Canberra Basic Warranty applies only to equipment manufactured by Canberra which is returned to the factory. If equipment must be repaired at the customer's site, the actual repair labor and parts will be provided at no charge during the warranty period. However, travel expenses to and from the customer's site, (travel time labor, and living expenses while on site), shall be paid by the customer unless an On-Site Warranty Option has been purchased. This option may only be purchased prior to shipment of the equipment to the customer.

The express warranties set forth herein are the only warranties with respect to the products, or any materials or components purchased from others and furnished by Canberra, and there are no other warranties, expressed or implied. The warranty of merchantibility is expressly limited as herein provided and all warranties of fitness are expressly disclaimed and excluded. Canberra shall have no liability for any special, indirect or consequential damages, whether from loss of production or otherwise, arising from any breach of warranty hereunder or defect or failure of any product or products sold hereunder.

EXCLUSIONS
Warranty service is contingent upon the proper use of all equipment and does not cover equipment which has been modified without Canberra's written approval or which has been subjected to unusual physical or electrical stress as determined by Canberra Service personnel. Canberra Industries shall be under no obligation to furnish warranty service (preventive or remedial): (1) if adjustment, repair or parts replacement is required because of accident, neglect, misuse, failure of electrical power, air conditioning, humidity control, transportation, or causes other than ordinary use; (2) if the equipment is maintained or repaired or if attempts to repair or service equipment are made by other than Canberra personnel without the prior approval of Canberra.

This warranty does not cover detector damage caused by warm-up or by neutrons or heavy charged particles. Damage from these causes is readily identifiable as described in the manual accompanying each detector.

Although Canberra may frequently supply, as part of systems, equipment manufactured by other companies, the only warranty that shall apply to such non-Canberra equipment is that warranty offered by the original manufacturer, if any.

Canberra will, upon request, offer, as an option, warranty coverage for non-Canberra equipment such as computers and peripherals sold as part of a system supplied by Canberra. Quotations on this coverage may be obtained by contacting Canberra Customer Service or any of our sales staff.

SOFTWARE
Canberra warrants software media from defects discovered within 30 days after receipt.

Canberra assumes no responsibility for user-written programs or programs published as part of information exchange in Canberra periodicals.

Engineering assistance for software development is available and can be contracted through the Sales Department.

INSTALLATION
Installation of equipment purchased from Canberra shall be the sole responsibility of the customer unless the installation is specifically contracted for at the prevailing Canberra field service rates. To insure timely installation after receipt of equipment, it is recommended that installation be contracted for at the time the equipment is ordered.

ON-SITE WARRANTY OPTION
The On-Site Warranty Option provides for free on-site warranty work (Canberra pays all travel and living expenses) within the first 90 days after delivery of equipment to the customer. If installation is ordered from Canberra, the 90 day period commences upon completion of the initial installation. After the 90 day period, labor and materials used on site will still be covered by the basic warranty, but the customer shall pay for all travel expenses—travel time labor and living expenses incurred for any on-site service.

A maintenance contract may be purchased covering the period after the 90 days on-site warranty period, or after initial installation of the equipment. This is to be contracted through Canberra Customer Service.

REPAIRS
Any Canberra-manufactured instrument no longer in its warranty period may be returned, freight prepaid, to our factory for repair,and realignment. When returning instruments for repair, contact the Customer Service Department for shipping instructions and an Authorized Customer Service Return Number.

All correspondence concerning repairs should include the Model number and a description of the problem observed.

Once repaired, all equipment passes through our normal preshipment checkout procedure. Return shipping expense on out-of-warranty repairs will be charged to the customer.

For instruments out of warranty, the customer must supply a purchase order number for the repair before the item will be returned.

SHIPPING DAMAGE
Shipments should be carefully examined when received for evidence of damage caused by shipping. If damage is found, immediately notify Canberra and the carrier making delivery, as the carrier is normally responsible for damage caused in shipment. Carefully preserve all documentation to establish your claim. Canberra will provide all possible assistance in processing damage claims.

Due to the delicate nature of cooled detectors (Ge and Si(Li)), Canberra requires that delivery to and from air freight terminals be handled with special care. Do not ship such Detectors without first obtaining advice from our Traffic Department.

RETURN SHIPMENTS
Canberra Customer Service Department must be notified in advance if equipment is to be returned for any reason. Canberra can suggest the best means of shipping and will be able to expedite the shipment in case it is lost or delayed in transit.

The customer must obtain an authorized customer service return number before returning any equipment to the Canberra factory. *Compliance with this provision by the customer shall be a condition of this warranty.* In giving shipping instructions, Canberra shall not be deemed to have assumed any responsibility or liability in connection with the shipment.

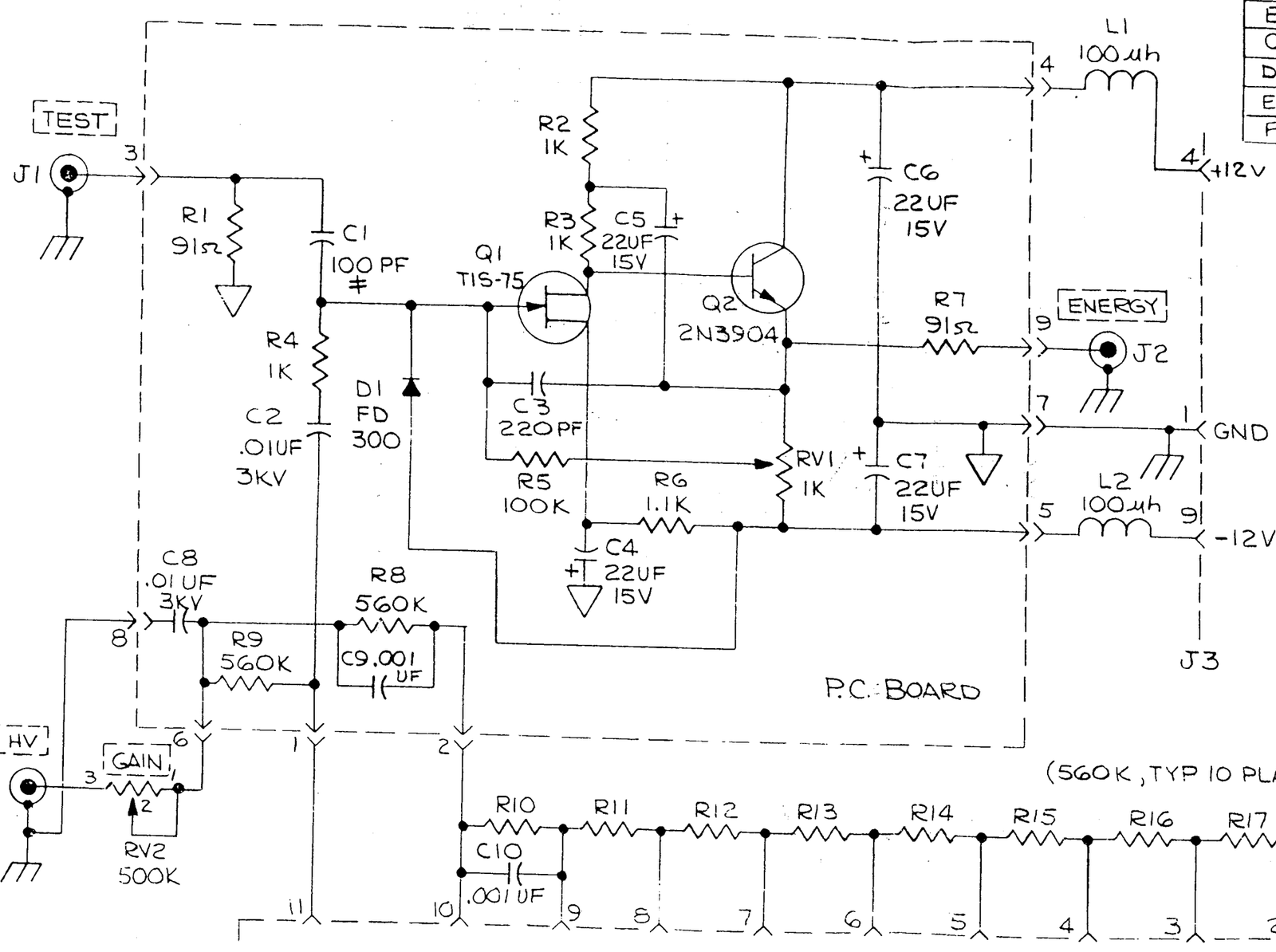
Equipment should be returned to your area service center or to Canberra, Meriden. For shipment from outside the U.S., our shipping address is:

Canberra Industries, Inc.
c/o EMO-TRANS, Inc.
Bradley International Airport
Windsor Locks, CT 06096 U.S.A.

SERVICE AND SERVICEABILITY
Canberra has gone to great lengths to insure that the instruments provided are functionally modular and therefore easy to service. In addition to modularity, Canberra has embarked on an extensive System Service Program to provide a totally responsive service capability. Complete Service Contracts with special arrangements for 24 hour response and weekend standby services are available from Canberra. For a detailed description of our Customer Service Program, please contact our Systems Service Department in Meriden, Connecticut, U.S.A.

Rev. 5/1/86

REV	CHANGE	ECN	BY	DATE	APPD
B	REDRAWN & INIT. RELEASE	2049	DRW	12-78	
C	SEE ECN	2060	JH	12-78	
D	REV WIRING ON RV2 SEE ECN	2088	ZP	1-24-78	
E	SEE ECN	2194	AM	4-10-79	
F	AR13002	4418	BAS	2-10-86	



NOTES:

1. THERE ARE NO FOUR WAY TIES ON THIS SCHEMATIC.
2. UNMARKED RESISTORS ARE ¼W, 5%
3. [ ] INDICATES REAR PANEL COMPONENT LOCATION.
4. # INDICATES MONO COG. CAPACITOR.

LAST COMPONENT REF. DESIGNATION	
CAPACITORS	C10
DIODES	D1
RESISTORS	R19
CONNECTORS	J4
VARIABLE RESISTORS	RV3
TRANSISTORS	Q2
INDUCTOR	L2

USED ON	DRAWN D. WEST	DATE 12-18-78
	CHKD R.W.L.	12/21/78
	APPD MECH	
	APPD ELEC	12/21/78
	NEXT ASSY	

SCHEMATIC
MODEL 2007P

CANBERRA

SCALE - H | DO NOT TEMPLATE DRAWING

DRAWING NO B-17403 | REV F

SHT 1 OF 1