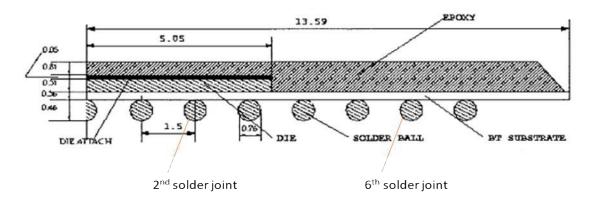
# ME 571 Project 2 Report

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### **Summary**

The purpose of the project was to make use of the analytical model provided, as developed by Heinrich and supplemented by data from Zhang, to understand the causes of uncertainty in the fatigue life of soldered joints in the PBGA. Using the derived analytical expression, *First Order Reliability Methods* were applied to the equation to understand the main variable leading to uncertainty in the measure fatigue life. Owing to the large amount of equations involved with various variables, Matlab's symbolic toolbox was used to assist with the calculations.



#### **Question 1**

To achieve the goal of finding the main variable causing the uncertainty in fatigue life, First Order Reliability Method(FORM) was applied to the expression derived by Heinrich and provided in the *Project 2 Manual*. The relation between shear displacement( $\Delta u$ ) between the package, taking into account the solder joint stiffness was derived for the various variables. There are nine independent variables( $r_d$ ,  $r_m$ ,  $E_d$ ,  $E_m$ ,  $\alpha_d$ ,  $\alpha_m$ ,  $\alpha_p$ ,  $\beta_1$ ,  $\beta_2$ ) in the equations which, each of which was normally distributed  $\sim N(\mu, \sigma)$ . Alongside these, there are four deterministic quantities in the expressions which are: r,  $\Delta T$ ,  $v_d$ ,  $v_m$ . To obtain the expression for mean of shear displacement( $\mu_{\Delta u}$ ), the expressions from the manual were changed to input the mean value of the normal variables while the actual value of the deterministic quantities. These relations for  $\mu_{\Delta u}$  are shown in eqn.1-3.

$$\overline{\Delta u} = \begin{cases} \overline{\beta_1} [\left(\overline{\alpha_d} - \overline{\alpha_p}\right) + \overline{A_1}(\overline{\alpha_m} - \overline{\alpha_d})r\Delta T & 0 \le r \le r_d \\ \overline{\beta_2} [\left(\overline{\alpha_m} - \overline{\alpha_p}\right) + \overline{A_2}(\overline{\alpha_d} - \overline{\alpha_m})r\Delta T & r_d \le r \le r_m \end{cases}, 0 \le \beta_1, \beta_2 \le 1 \dots eqn.1$$

$$\overline{A_1} = \frac{(1 - v_d)\left[1 - \left(\frac{\overline{r_d}}{\overline{r_m}}\right)^2\right]}{(1 - v_d)\left[1 - \left(\frac{\overline{r_d}}{\overline{r_m}}\right)^2\right] + \frac{\overline{E_d}}{\overline{E_m}}\left[(1 + v_m) + (1 - v_m)\left(\frac{\overline{r_d}}{\overline{r_m}}\right)^2\right]} \qquad \dots eqn. 2$$

$$A_{2} = \frac{\frac{\overline{E_{d}}}{\overline{E_{m}}} \left[ (1 + v_{m}) \left( \frac{\overline{r_{d}}}{r} \right)^{2} + (1 - v_{m}) \left( \frac{\overline{r_{d}}}{\overline{r_{m}}} \right)^{2} \right]}{(1 - v_{d}) \left[ 1 - \left( \frac{\overline{r_{d}}}{\overline{r_{m}}} \right)^{2} \right] + \frac{\overline{E_{d}}}{\overline{E_{m}}} \left[ (1 + v_{m}) + (1 - v_{m}) \left( \frac{\overline{r_{d}}}{\overline{r_{m}}} \right)^{2} \right]} \dots eqn.3$$

For the second part of this process, the FORM method was applied onto the equations above. The general equation for first reliability methods to obtain the variance is shown below in eqn. 4. For this equation, each of the variable replacing x is one of the nine independent variables talked about above. The *Symbolic* toolbox in Matlab was used to help find the derivatives and the expressions. (The FORM expressions  $\sigma^2(\Delta u)$  for can be seen in the Appendix below.)

$$var(\Delta u) = \sigma^2(\Delta u) = \sum_{i=1}^n \left(\frac{\partial \Delta u}{\partial x_i}\right)^2 * var(x_i)$$
 ... eqn. 4

Question 2The second question of the project involves the use of the derived expressions in part 1 to obtain certain characteristics. The following data was provided in the project manual: 1. Mean and CV (Coefficient of Variation) Data for 7 independent variables, 2. Shear displacement for the  $2^{nd}$  and  $6^{th}$  joints To make use of the data, the COV was changed into variance by multiplying the CV to mean and squaring the value. After that, the experimental data provided in Table 2 of the *Project Manual* was used. It was seen that the  $2^{nd}$  solder joint fails in the first part of the piecewise range while the  $6^{th}$  joint fails in the second range of the shear displacement equations. Using the  $\Delta u$  data

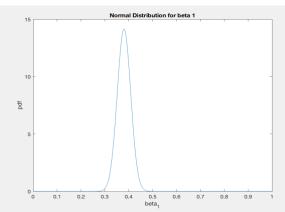


FIGURE 1. BETA 1 DISTRIBUTION

provided as another input to the equation, 4 equations were obtained, each with one unknown. As there is  $\beta_1$  in the first range, the two equations from the first range  $(0 \le r \le r_d)$  was used to obtain the  $\mu$  and  $\sigma$  value for  $\beta_1$ . Same procedure was used to obtain  $\beta_2$  using the equations ranging from  $r_d \le r \le r_m$ . Table 1 below shows the results of the statistics obtained on the two parameters. Fig. 1 and Fig. 2 also show the normal distribution of the statistics of the two beta parameters.

Table 1. Parameter Statistics		
Variable	μ	σ
$oldsymbol{eta}_1$	0.3708	0.02818
$oldsymbol{eta}_2$	0.2712	0.05744

#### **Question 3**

For the third question, the derived equations from question 1 were evaluated using the known values of all the variables. The value of  $\mu_{\Delta u}$  and  $\sigma^2(\Delta u)$  was evaluated for all the joints, at different values of r. The function of fatigue life was provided to us in the manual. To calculate the mean, the equation was written in the following form:

$$\overline{\emptyset(\Delta u)} = \frac{1}{\overline{\Delta u^2}} \dots eqn. 5$$

For the purpose of evaluating the variance of phi, FORM was again applied on the fatigue life function provided. The final equation of the form put in Matlab for evaluation is:

$$var(\emptyset) = \sigma^2(\emptyset) = \frac{\partial \emptyset}{\partial \Delta u}^2 * var(\Delta u) \dots eqn. 6$$

Evaluating each of the expressions for each joint, the value of the mean and standard deviation for each of the joint value was obtained and recorded in the table. The highlighted value in red is fr the critical join. It is join number 3 as it has the lowest  $\mu_{\phi}$  value amongst all the 7 joints. An image of the distribution for joint 7 is also attached below in Figure 3.

Table 2. Statistics for each joint		
Joint Number	$\mu_{\phi}$	$\sigma_\phi$
1	$2.002 * 10^{12}$	$3.9713 * 10^{11}$
2	$0.5004 * 10^{12}$	$9.9275 * 10^{10}$
3	$0.2224 * 10^{12}$	$4.4159 * 10^{10}$
4	$0.4117 * 10^{12}$	$2.3381*10^{11}$
5	$0.5208 * 10^{12}$	$3.0871 * 10^{11}$
6	$0.5951 * 10^{12}$	$3.7567 * 10^{11}$
7	$0.6354 * 10^{12}$	$4.3096 * 10^{11}$

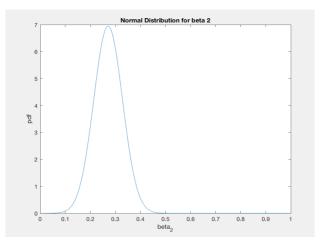


FIGURE 2. BETA 2 DISTRIBUTION

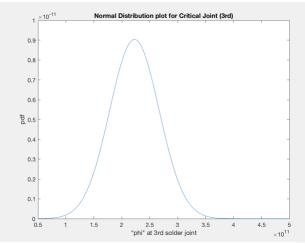


FIGURE 3. CRITICAL JOINT DISTRIBUTION

### **Question 4**

The goal of the last question was to figure out which variable has the highest effect on the fatigue life. For this purpose, FORM was used again. Same general formula used to calculate variance in question 1(eqn. 4) was used to find the variance of phi in terms of each of the independent variables. The difference between using eqn. 4 in each of the questions is that in question 4, instead of summing the terms, each term was considered separately using the method: (Differnetial ( $\emptyset_{variable}$ ) \* variance(variable). This was done for each of the 9 variables separately. With all the variables known and r being constant in all the equations, the values were compared to see which variance value was the greatest.

After performing the calculations in Matlab, it was found that  $\beta_1$  has the biggest effect on the fatigue life. To interpret the results, the fatigue life is most affected by the way  $\beta_1$  changes in the equations. Changing the value of  $\beta_1$  would affect the fatigue life the joint the most.

#### **Lessons Learnt**

- FORM method on multiple variables and seeing how it effects the parameters
- Understanding how to find variables that effect the uncertainty the most
- Symbolic toolbox on Matlab

# **Appendices:**

### Command Script Window for Question 1 as example

var\_del\_1 =

```
beta1^2*deltat^2*r^2*var alphap + deltat^2*r^2*var beta1*(alphap - alphad + ((rd^2/rm^2 -
1)*(alphad - alpham)*(phid - 1))/((rd^2/rm^2 - 1)*(phid - 1) - (Ed*(phim + (rd^2*(phim - 1))/rm^2 -
1))/Em))^2 + beta^2*deltat^2*r^2*var rd*((^2rd*(alphad - alpham)*(phid - 1))/(rm^2*((rd^2/rm^2 -
1)*(phid - 1) - (Ed*(phim + (rd^2*(phim - 1))/rm^2 - 1))/Em)) - (((2*rd*(phid - 1))/rm^2 - (2*Ed*rd*(phim
- 1))/(Em*rm^2))*(rd^2/rm^2 - 1)*(alphad - alpham)*(phid - 1))/((rd^2/rm^2 - 1)*(phid - 1) - (Ed*(phim +
(rd^2*(phim - 1))/rm^2 - 1))/Em)^2)^2 + beta1^2*deltat^2*r^2*var_alphad*(((rd^2/rm^2 - 1)*(phid -
1))/((rd^2/rm^2 - 1)*(phid - 1) - (Ed*(phim + (rd^2*(phim - 1))/rm^2 - 1))/Em) - 1)^2 +
beta1^2*deltat^2*r^2*var rm*(((rd^2/rm^2 - 1)*(alphad - alpham)*(phid - 1)*((2*rd^2*(phid - 1))/rm^3
- (2*Ed*rd^2*(phim - 1))/(Em*rm^3)))/((rd^2/rm^2 - 1)*(phid - 1) - (Ed*(phim + (rd^2*(phim - 1))/rm^2 -
1))/Em)<sup>2</sup> - (2*rd<sup>2</sup>*(alphad - alpham)*(phid - 1))/(rm<sup>3</sup>*((rd<sup>2</sup>/rm<sup>2</sup> - 1)*(phid - 1) - (Ed*(phim +
(rd^2*(phim)\n - 1))/rm^2 - 1))/Em)))^2 + (beta1^2*deltat^2*r^2*var_alpham*(rd^2/rm^2 - 1)^2*(phid)))^2 + (beta1^2*deltat^2*r^2*r^2*var_alpham*(rd^2/rm^2 - 1)^2*(phid)))
- 1)^2)/((rd^2/rm^2 - 1)*(phid - 1) - (Ed*(phim + (rd^2*(phim - 1))/rm^2 - 1))/Em)^2 +
(beta1^2*deltat^2*r^2*var_Ed*(rd^2/rm^2 - 1)^2*(alphad - alpham)^2*(phid - 1)^2*(phim +
(rd^2*(phim - 1))/rm^2 - 1)^2)/(Em^2*((rd^2/rm^2 - 1)*(phid - 1) - (Ed*(phim + (rd^2*(phim - 1))/rm^2 -
1))/Em)^4) + (Ed^2*beta1^2*deltat^2*r^2*var Em*(rd^2/rm^2 - 1)^2*(alphad - alpham)^2*(phid -
1)^2*(phim + (rd^2*(phim - 1))/rm^2 - 1)^2)/(Em^4*((rd^2/rm^2 - 1)*(phid - 1) - (Ed*(phim +
(rd^2*(phim - 1))/rm^2 - 1))/Em)^4)
```

 $var_del_2 =$ 

```
beta2^2*deltat^2*r^2*var_alphap + deltat^2*r^2*var_beta2*(alpham - alphap + (Ed*((rd^2*(phim +
1))/r^2 - (rd^2*(phim - 1))/rm^2)*(alphad - alpham))/(Em*((rd^2/rm^2 - 1)*(phid - 1) + (Ed*(phim -
(rd^2*(phim - 1))/rm^2 + 1))/Em)))^2 + beta^2^2*deltat^2*r^2*var Em*((Ed*((rd^2*(phim + 1))/r^2 - 1)/Em)))^2 + beta^2^2*r^2*var Em*((Ed*((rd^2*(phim + 1))/r^2 - 1)/Em)))^2 + beta^2^2*r^2*var Em*((Ed*((rd^2*((rd^2*(phim + 1))/r^2 - 1)/Em))))^2 + beta^2^2*r^2*var Em*((Ed*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd^2*((rd
(rd^2*(phim - 1))/rm^2)*(alphad - alpham))/(Em^2*((rd^2/rm^2 - 1)*(phid - 1) + (Ed*(phim - (rd^2*(phim
- 1))/rm^2 + 1))/Em)) - (Ed^2*((rd^2*(phim + 1))/r^2 - (rd^2*(phim - 1))/rm^2)*(alphad - alpham)*(phim -
(rd^2*(phim - 1))/rm^2 + 1))/(Em^3*((rd^2/rm^2 - 1)*(phid - 1) + (Ed*(phim - (rd^2*(phim - 1))/rm^2 +
1))/Em)^2))^2 + beta2^2*deltat^2*r^2*var_Ed*((((rd^2*(phim + 1))/r^2 - (rd^2*(phim -
1))/rm^2)*(alphad - alpham))/(Em*((rd^2/rm^2 - 1)*(phid - 1) + (Ed*(phim - (rd^2*(phim - 1))/rm^2 +
1))/Em)) - (Ed*((rd^2*(phim + 1))/r^2 - (rd^2*(phim - 1))/rm^2)*(alphad - alpham)*(phim - (rd^2*(phim -
1)/rm<sup>2</sup> + 1))/(Em<sup>2</sup>*((rd<sup>2</sup>/rm<sup>2</sup> - 1)*(phid - 1) + (Ed*(phim - (rd<sup>2</sup>*(phim - 1))/rm<sup>2</sup> + 1))/Em)<sup>2</sup>))<sup>2</sup> +
beta2\\n^2*deltat^2*r^2*var_rm*((Ed*((rd^2*(phim + 1))/r^2 - (rd^2*(phim - 1))/rm^2)*(alphad - (rd^2*(phim
alpham)*((2*rd^2*(phid - 1))/rm^3 - (2*Ed*rd^2*(phim - 1))/(Em*rm^3)))/(Em*((rd^2/rm^2 - 1)*(phid -
1) + (Ed*(phim - (rd^2*(phim - 1))/rm^2 + 1))/Em)^2) + (2*Ed*rd^2*(alphad - alpham)*(phim -
1))/(Em*rm^3*((rd^2/rm^2 - 1)*(phid - 1) + (Ed*(phim - (rd^2*(phim - 1))/rm^2 + 1))/Em)))^2 +
beta2^2*deltat^2*r^2*var_alpham*((Ed*((rd^2*(phim + 1))/r^2 - (rd^2*(phim -
1))/rm^2))/(Em*((rd^2/rm^2 - 1)*(phid - 1) + (Ed*(phim - (rd^2*(phim - 1))/rm^2 + 1))/Em)) - 1)^2 +
beta 2^2*deltat^2*r^2*var\_rd*((Ed*((2*rd*(phim+1))/r^2 - (2*rd*(phim-1))/rm^2)*(alphad-rd*((Ed*((2*rd*(phim+1))/r^2 - (2*rd*(phim-1))/rm^2)*(alphad-rd*((Ed*((2*rd*(phim+1))/r^2 - (2*rd*(phim-1))/rm^2)*(alphad-rd*((Ed*((2*rd*(phim+1))/r^2 - (2*rd*(phim-1))/rm^2)*(alphad-rd*((Ed*((2*rd*(phim+1))/r^2 - (2*rd*(phim-1))/rm^2)*(alphad-rd*((Ed*((2*rd*(phim+1))/rm^2) + (2*rd*(phim-1))/rm^2)*(alphad-rd*((Ed*((2*rd*(phim+1))/rm^2) + (2*rd*(phim-1))/rm^2)*(alphad-rd*((Ed*((2*rd*(phim+1))/rm^2) + (2*rd*(phim-1))/rm^2)*(alphad-rd*((Ed*((2*rd*(phim+1))/rm^2) + (2*rd*(phim-1))/rm^2)*(alphad-rd*((Ed*((2*rd*(phim+1))/rm^2) + (2*rd*(phim-1))/rm^2)*(alphad-rd*((Ed*((2*rd*(phim+1))/rm^2) + (2*rd*((Ed*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2*rd*((2
alpham))/(Em*((rd^2/rm^2 - 1)*(phid - 1) + (Ed*(phim - (rd^2*(phim - 1))/rm^2 + 1))/Em)) -
(Ed*((rd^2*(phim + 1))/r^2 - (rd^2*(phim - 1))/rm^2)*((2*rd*(phid - 1))/rm^2 - (2*Ed*rd*(phim - 1))/rm^2)*((2*rd*(phim - 1))/rm^2 - (2*Ed*rd*(phim - 1))/rm^2)*((2*rd*(phid - 1))/rm^2 - (2*Ed*rd*(phim - 1))/rm^2)*((2*rd*(phid - 1))/rm^2 - (2*Ed*rd*(phid - 1))/rm^2)*((2*rd*(phid - 1))/rm^2 - (2*Ed*rd*(phid - 1))/rm^2)*((2*rd*(phid - 1))/rm^2)*(
1))/(Em*rm^2))*(alphad - alpham))/(Em*((rd^2/rm^2 - 1)*(phid - 1) + (Ed*(phim - (rd^2*(phim - 1))/rm^2
```

```
+ 1))/Em)^2))^2 + (Ed^2*beta2^2*deltat^2*r^2*var_alphad*((rd^2*(phim\\n + 1))/r^2 - (rd^2*(phim - 1))/rm^2)^2)/(Em^2*((rd^2/rm^2 - 1)*(phid - 1) + (Ed*(phim - (rd^2*(phim - 1))/rm^2 + 1))/Em)^2)

mu_delt1 =

-deltat*mu_beta1*r*(mu_alphap - mu_alphad + ((mu_rd^2/mu_rm^2 - 1)*(mu_alphad - mu_alpham)*(phid - 1))/((mu_rd^2/mu_rm^2 - 1)*(phid - 1) - (mu_Ed*(phim + (mu_rd^2*(phim - 1))/mu_rm^2 - 1))/mu_Em))

mu_delt2 =

-deltat*mu_beta2*r*(mu_alphap - mu_alpham + (mu_Ed*(mu_alphad - mu_alpham)*((mu_rd^2*(phim - 1))/mu_rm^2 - (mu_rd^2*(phim + 1))/r^2))/(mu_Em*((mu_rd^2/mu_rm^2 - 1)*(phid - 1) + (mu_Ed*(phim - (mu_rd^2*(phim - 1))/mu_rm^2 + 1))/mu_Em)))
```

### Matlab Code

```
clear all
 %%UMATR SARWAR
%%ME 571-Reliability Based Design
 %INPUT DATA PROVIDED
del_2_joint = 10^-6 * [1.275 1.589 1.37 1.558 1.427 1.248 1.656 1.326 1.347 1.338];
del_6_joint = 10^-6 * [1.536 .46 1.356 1.714 1.508 1.499 1.231 1.127 .791 1.743];
mu_del_2_joint = mean(del_2_joint);
mu_del_6_joint = mean(del_6_joint);
var_del_2_joint = var(del_2_joint);
var_del_6_joint = var(del_6_joint);
%QUESTION 1
syms rd mu_rd var_rd rm mu_rm var_rm Em mu_Em var_Em Ed mu_Ed var_Ed alphad mu_alphad var_alphad alpham
mu_alpham var_alpham alphap mu_alphap var_alphap beta1 mu_beta1 var_beta1 beta2 mu_beta2 var_beta2 r
deltat phid phim
A 1 = ((1 - phid)*(1 - (rd/rm)^2)) / ((1 - phid)*(1 - (rd/rm)^2) + (Ed/Em)*((1 - phim) + (1 - phim)) + (1 - phim) + (1 -
phim) * (rd/rm)^2));
 A_2 = ((Ed/Em)*((1 + phim)*(rd/r)^2 + (1 - phim)*(rd/rm)^2)) / ((1 - phid)*(1 - (rd/rm)^2) + (1 - ph
 (Ed/Em)*((1 + phim) + (1 - phim)*(rd/rm)^2));
del 1 = beta1*((alphad - alphap) + A 1*(alpham - alphad))*r*deltat;
del_2 = beta2*((alpham - alphap) + A_2*(alphad - alpham))*r*deltat;
var beta1) + ((diff(del 1,beta2)^2) * var beta2)
var del 2 = ((diff(del 2,rd)^2) * var rd) + ((diff(del 2,rm)^2) * var rm) + ((diff(del 2,Ed)^2) * var rd) + ((diff(del 2,rd)^2) * var rm) + ((diff(del 2,Ed)^2) * var rd) + ((diff(del 2,rd)^2) * var rd) + ((diff(del 2,rd)
var_Ed) + ((diff(del_2,Em)^2) * var_Em) + ((diff(del_2,alphad)^2) * var_alphad) +
phim) + (1 - phim) * (mu rd/mu rm) ^2));
mu_A2 = ((mu_Ed/mu_Em)*((1 + phim)*(mu_rd/r)^2 + (1 - phim)*(mu_rd/mu_rm)^2)) / ((1 - phid)*(1 -
 (mu_rd/mu_rm)^2) + (mu_Ed/mu_Em)*((1 + phim) + (1 - phim)*(mu_rd/mu_rm)^2));
mu delt1 = mu beta1*((mu alphad - mu alphap) + mu A1*(mu alpham - mu alphad))*r*deltat
mu_delt2 = mu_beta2*((mu_alpham - mu_alphap) + mu_A2*(mu_alphad - mu_alpham))*r*deltat
%OUESTION 2
 %INPUT SETUP FOR QUESTION 2
deltat = -100;
mu rd = 5.05/1000; %Conversion of mm to m
var_rd = ((10/100) *mu_rd)^2;
mu rm = 13.59/1000; %Conversion of mm to m
var rm = ((10/100)*mu rm)^2;
mu Ed = 130*(10^9); %GPa to Pa Conversion
var_Ed = ((5/100)*mu_Ed)^2;
mu Em = 15.5*(10^9); %GPa to Pa Conversion
var_Em = ((5/100)*mu_Em)^2;
```

```
phid = 0.28;
phim = 0.25;
mu alphad = 2.62*(10^-6);
\overline{\text{var}} alphad = (.05*mu alphad)^2;
mu_alphap = 16*(10^{-6});
var alphap = (.05*mu alphap)^2;
mu alpham = 15*(10^{-6});
var_alpham = (.05*mu_alpham)^2;
r_0 = 0; r_1 = .0015; r_2 = r_1 + .0015; r_3 = r_2 + .0015; r_4 = r_3 + .0015; r_5 = r_4 + .0015; r_6 =
r_5 + .0015; r_7 = r_6 + .0015;
%Calculating mu beta1
r = .003;
mu delt1 = subs(mu delt1)
mean beta1 = (mu del 2 joint*684684565331771543098291650560000000) / 2545472288561474981500803282063;
%Calculating mu beta2
r = r_6;
mu delt2 = subs(mu delt2)
\overline{\text{mean beta2}} = (\text{mu del 6 joint*}33720472353036903117156694097920000000) /
161183833183396839077128098369423;
%Calculating var beta1
r = .003;
rd = mu rd;
rm = mu rm;
Ed = mu_Ed;
Em = mu Em;
alphad = mu alphad;
alpham = mu_alpham;
alphap = mu_alphap;
beta1 = .38\overline{0}1;
beta2 = .2712;
var del 1 = subs(var del 1)
variance betal = ((var del 2 joint -
742804162247811778803037710223233248099090360943835241553472614486117368081503200462168391680000000000)
* 468792954003556934441337498823432806950277276729809148313600000000000000) /
6479429171834392955946468963312955328100925058931072737535969;
var beta1 = .00079426;
cov_beta1_percent = ((variance_beta1^.5) / mean_beta1) * 100
%Calculating var beta2
r = .009;
rd = mu_rd;
rm = mu_rm;
Ed = mu_Ed;
Em = mu Em;
alphad = mu alphad;
alpham = mu_alpham;
alphap = mu_alphap;,
beta1 = .3801;
beta2 = .2712;
var del 2 = subs(var del 2)
variance beta2 = ((var del 6 joint -
00000)) * 113707025571192613769264500843563515030180205547360296254832640000000000000) /
25980228079693099998705779637851318160733208465877390831381352929;
var beta2 = .0033;
cov beta2 percent = ((variance beta2^.5) / mean beta2) * 100
%eta 1 and Beta 2 statistics
xB1 = 0:.000001:1;
normB1 = normpdf(xB1, .3802, .02818262);
xB2 = 0:.000001:1;
normB2 = normpdf(xB2, .2712, .05744562647);
figure
plot(xB1, normB1)
title('Normal Distribution for beta 1')
xlabel('beta 1')
ylabel('pdf')
figure
plot(xB2, normB2)
title('Normal Distribution for beta 2')
```

```
xlabel('beta_2')
ylabel('pdf')
%OUESTION 3
syms rd mu rd var rd rm mu rm var rm Ed mu Ed var Ed Em mu Em var Em alphad mu alphad var alphad alpham
mu_alpham var_alpham alphap mu_alphap var_alphap betal mu_betal var_betal beta2 mu_beta2 var_beta2 r
deltat phid phim
%aFirst Order Reliability method
 A1 = ((1 - phid)*(1 - (rd/rm)^2)) / ((1 - phid)*(1 - (rd/rm)^2) + (Ed/Em)*((1 - phim) + (1 - rd/rm)^2) + (rd/rm)^2) + (
phim) * (rd/rm) ^2));
A2 = ((Ed/Em)*((1 + phim)*(rd/r)^2 + (1 - phim)*(rd/rm)^2)) / ((1 - phid)*(1 - (rd/rm)^2) + (Ed/Em)*((1 + phim)*(rd/rm)^2)) / ((1 - phid)*(1 - (rd/rm)^2)) + (Ed/Em)*((1 + phim)*(rd/rm)^2)) / ((1 - phid)*(1 - (rd/rm)^2)) + (Ed/Em)*((1 + phim)*(rd/rm)^2)) / ((1 - phid)*(1 - (rd/rm)^2)) + (Ed/Em)*((1 + phim)*(rd/rm)^2)) / ((1 - phid)*(1 - (rd/rm)^2)) + (Ed/Em)*((1 + phim)*(rd/rm)^2)) / ((1 - phid)*(1 - (rd/rm)^2)) + (Ed/Em)*((1 + phid)*(rd/rm)^2)) / ((1 - phid)*(1 - (rd/rm)^2)) + (Ed/Em)*((1 + phid)*(rd/rm)^2)) / ((1 - phid)*(rd/rm)^
 + phim) + (1 - phim)*(rd/rm)^2);
delt 1 = beta1*((alphad - alphap) + A1*(alpham - alphad))*r*deltat;
phi1 = 1 / (delt 1^2);
delt 2 = beta2*((alpham - alphap) + A2*(alphad - alpham))*r*deltat;
phi2 = 1 / (delt 2^2);
((diff(phi1,Em)^2) * var Em) + ((diff(phi1,alphad)^2) * var alphad) + ((diff(phi1,alpham)^2) *
var_alpham) + ((diff(phil,alphap)^2) * var_alphap) + ((diff(phil,betal)^2) * var_betal) +
 ((diff(phi1,beta2)^2) * var beta2)
var_phi^2 = ((diff(phi2,rd)^2) * var_rd) + ((diff(phi2,rm)^2) * var_rm) + ((diff(phi2,Ed)^2) * var_Ed) + ((diff(phi2,rd)^2) * var_rd) + ((diff(phi2,rd)^2
((diff(phi2,Em)^2) * var_Em) + ((diff(phi2,alphad)^2) * var_alphad) + ((diff(phi2,alpham)^2) * var_alpham) + ((diff(phi2,alpham)^2) *
var_alpham) + ((diff(phi2,alphap)^2) * var_alphap) + ((diff(phi2,betal)^2) * var_betal) +
((diff(phi2,beta2)^2) * var beta2)
var_Ed) + ((diff(delt_1,Em)^2) * var_Em) + ((diff(delt_1,alphad)^2) * var_alphad) +
 ((diff(delt 1,alpham)^2) * var alpham) + ((diff(delt 1,alphap)^2) * var alphap) +
((diff(delt_1,betal)^2) * var_betal) + ((diff(delt_1,beta2)^2) * var_beta2);
var_delt2 = ((diff(delt_2,rd)^2) * var_rd) + ((diff(delt_2,rm)^2) * var_rm) + ((diff(delt_2,Ed)^2) *
var_Ed) + ((diff(delt_2,Em)^2) * var_Em) + ((diff(delt_2,alphad)^2) * var_alphad) +
 ((diff(delt 2,alpham)^2) * var alpham) + ((diff(delt 2,alphap)^2) * var alphap) +
 ((diff(delt 2, beta1)^2) * var beta1) + ((diff(delt 2, beta2)^2) * var beta2);
mu_A1 = ((1 - phid)*(1 - (mu_rd/mu_rm)^2)) / ((1 - phid)*(1 - (mu_rd/mu_rm)^2) + (mu_Ed/mu_Em)*((1 - phim) + (1 - phim) * (mu_rd/mu_rm)^2));
mu A2 = ((\text{mu Ed/mu Em})^{\frac{1}{2}}((1 + \text{phim})^{\frac{1}{2}}(\text{mu rd/r})^2 + (1 - \text{phim})^{\frac{1}{2}}(\text{mu rd/mu rm})^2)) / ((1 - \text{phid})^{\frac{1}{2}}(1 - \text{phid}
 (mu_rd/mu_rm)^2) + (mu_Ed/mu_Em)*((1 + phim) + (1 - phim)*(mu_rd/mu_rm)^2));
mu delt1 = mu beta1*((mu alphad - mu alphap) + mu A1*(mu alpham - mu alphad))*r*deltat;
mu_delt2 = mu_beta2*((mu_alpham - mu_alphap) + mu_A2*(mu_alphad - mu_alpham))*r*deltat;
mu_phi1 = 1 / (mu_delt1^2)
mu phi2 = 1 / (mu delt2^2)
%Setting all inputs again
rd = .00505; mu rd = .00505; var rd = 2.5503 * 10^-7; rm = .01359; mu rm = .01359; var rm = 1.8469 * 10^-6;
{\tt Ed} = 1.3 * 10^{-}\overline{11}; {\tt mu\_Ed} = 1.3 * 10^{-}11; {\tt var\_Ed} = 4.225 * 10^{-}19; {\tt Em} = \overline{1.55} * 10^{-}10; {\tt mu\_Em} = 1.55 * 10^{-}10; {\tt mu\_Em} = 1.
10^10; var Em = 6.0063 * 10^17; alphad = 2.62 * 10^6; mu alphad = 2.62 * 10^6; var alphad = 1.7161 * 10^6
alpham = 1.5 * 10^{-5}; mu\_alpham = 1.5 * 10^{-5}; var\_alpham = 5.625 * 10^{-13}; alphap = 1.6 * 10^{-5}; mu\_alphap = 1.6 * 10^
= 1.6 * 10^-5; var_alphap = 6.4 * 10^-13; beta1 = .3801; mu_beta1 = .3801; var_beta1 = 7.9426 * 10^-4; beta2 = .2712; mu_beta2 = .2712; var_beta2 = .0033; deltat = -100; phid = .28; phim = .25;
%Changing equations to make them in terms of r
mu_delt1 = subs(mu_delt1)
mu delt2 = subs(mu delt2)
var delt1 = subs(var delt1)
var_delt2 = subs(var_delt2)
%Calculating mean and variance of phi at each joint
i = 1; %Loop counter
for r = 0.0015:0.0015:0.0105
                     if r < 0.005
                                       mean delta u(i,:) =
  mean_phi_joints(i,:) = 1 / (mean_delta_u(i,:) ^ 2);
                                       variance_delta_u(i,:) =
   (208164637460033\overline{6}52969\overline{0}249706467831252630285198666002239324787416271574569132194975977905440385289*r^2)
 variance phi joints(i,:) = ((-2 / (mean delta u(i,:) ^ 3)) ^ 2) * variance delta u(i,:);
                    else
```

```
mean delta u(i,:) =
 400033718015630516779865487917/210752952206480644482229338112000000))/25
                mean_phi_joints(i,:) = 1 / (mean_delta_u(i,:) ^ 2);
                variance_delta_u(i,:) = subs(var_delt2);
                variance phi joints(i,:) = ((-2 / (mean delta u(i,:) ^ 3)) ^ 2) * variance delta u(i,:);
        end
        i = 1+i
end
mean_delta_u_joints = mean_delta_u;
variance_delta_u_joints = variance_delta_u;
mean_phi_joints = mean_phi_joints
variance_phi_joints = variance_phi_joints
std_dev_phi_joints = variance_phi_joints .^ .5
%Plotting for critical point(3rd Joint selected from analysis)
xphi 3rd = 0.05*10^12:1000000:.5*10^12;
normphi_3rd = normpdf(xphi_3rd,10^12 * .2226,10^11 * .4417);
figure
plot(xphi 3rd, normphi 3rd)
title('Normal Distribution plot for Critical Joint (3rd)')
xlabel('"phi" at 3rd solder joint')
ylabel('pdf')
%OUESTION 4
clear
syms rd mu rd var rd rm mu rm var rm Ed mu Ed var Ed Em mu Em var Em alphad mu alphad var alphad alpham
mu alpham var alpham alphap mu alphap var alphap beta1 mu beta1 var beta1 beta2 mu beta2 var beta2 r
deltat phid phim
A1 = ((1 - phid)*(1 - (rd/rm)^2)) / ((1 - phid)*(1 - (rd/rm)^2) + (Ed/Em)*((1 - phim) + (1 - phim)) + (1 - phim) + (1 - 
phim) * (rd/rm) ^2));
A2 = ((Ed/Em)*((1 + phim)*(rd/r)^2 + (1 - phim)*(rd/rm)^2)) / ((1 - phid)*(1 - (rd/rm)^2) + (Ed/Em)*((1 + phim)*(rd/rm)^2)) / ((1 - phid)*(1 - (rd/rm)^2)) + (Ed/Em)*((1 + phim)*(rd/rm)^2)) / ((1 - phid)*(1 - (rd/rm)^2)) + (Ed/Em)*((1 + phim)*(rd/rm)^2)) / ((1 - phid)*(1 - (rd/rm)^2)) + (Ed/Em)*((1 + phim)*(rd/rm)^2)) / ((1 - phid)*(1 - (rd/rm)^2)) + (Ed/Em)*((1 + phim)*(rd/rm)^2)) / ((1 - phid)*(1 - (rd/rm)^2)) + (Ed/Em)*((1 + phid)*(rd/rm)^2)) / ((1 - phid)*(1 - (rd/rm)^2)) + (Ed/Em)*((1 + phid)*(rd/rm)^2)) / ((1 - phid)*(rd/rm)^
+ phim) + (1 - phim)*(rd/rm)^2));
delt 1 = beta1*((alphad - alphap) + A1*(alpham - alphad))*r*deltat;
phi1 = 1 / (delt_1^2);
delt 2 = beta2*((alpham - alphap) + A2*(alphad - alpham))*r*deltat;
phi2 = 1 / (delt_2^2);
%Partial differentials
((diff(phi1,Ed)^2) * var_Ed);
var phil Em = ((diff(phil,Em)^2) * var Em); var phil alphad = ((diff(phil,alphad)^2) * var alphad)
; var_phi1_alpham = ((diff(phi1,alpham)^2) * var_alpham);
var_phi1_alphap = ((diff(phi1,alphap)^2) * var_alphap);var_phi1_beta1 = ((diff(phi1,beta1)^2) *
var_beta1);var_phi1_beta2 = ((diff(phi1,beta2)^2) * var_beta2);
rd = .0051;mu_rd = .0051;var_rd = 2.5503 * 10^-7;rm = .0136;mu_rm = .0136;var_rm = 1.8469 * 10^-6;Ed =
1.3 * 10^1; mu_Ed = 1.3 * 10^1;
var Ed = 4.225 * 10^19;Em = 1.55 * 10^10;mu Em = 1.55 * 10^10;var Em = 6.0063 * 10^17;alphad = 2.62 *
10^{-6}; mu alphad = 2.62 * 10^{-6};
var alphad = 1.7161 * 10^-14; alpham = 1.5 * 10^-5; mu_alpham = 1.5 * 10^-5; var_alpham = 5.625 * 10^-
13;alphap = 1.6 * 10^-5;

mu_alphap = 1.6 * 10^-5;var_alphap = 6.4 * 10^-13;beta1 = .3801;mu_beta1 = .3801;var_beta1 = 7.9426 *
10^{-4}; beta2 = .2712;
mu beta2 = .2712; var beta2 = .0033; deltat = -100; phid = .28; phim = .25;
%Highest value for partial differential multiplied by variance calculated with r = 1 for all
subs(var phi1 rd); subs(var phi1 rm); subs(var phi1 Ed); subs(var phi1 Em); subs(var phi1 alphad); subs(var
phil_alpham);subs(var_phil_alphap);subs(var_phil_betal);subs(var_phil_beta2)
0015624884528429548794500054663
28\overline{3}8298522881492761609351163273874448154162888702282346263909422554805430723518995718483466858000150783
670109374191699006841561500382641
```

```
Ed eff =
9699527493598431323300065861758916144522614280610940310486650650700391381718814602913050441411878794118\\
71918227423152462193956759321
Em eff =
23972742474384154064652253107
alpahd eff =
35615754682269457386581870277963
alpham eff =
871918227423152462193956759321
alphap eff =
4706847264046808372159745610833889
betal eff=
1394230443986397756347968019802291753351877952649\\
beta2 eff = 0
```