

Industrial Robots

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2.

Mechanics of manipulators 3

Geometrical model

Inverse Kinematics (Inverse Kinematic Problem)

Problems:

- formulation of the inverse kinematics problem
- Analytical solution methods to the inverse kinematics

Problem formulation

Input data - Given:

Position and orientation: $x, y, z, \varphi, \theta, \psi$

Results - Find:

Joint variables: q_1, q_2, \dots, q_n

Classification of the inverse kinematics solution methods

● **Analytical - algebraic**

- geometric

● Numerical

A set of equations:

Assumed position and orientation

Geometrical model

$${}^o \underline{\tau}_e = \begin{bmatrix} N_x & O_x & A_x & P_x \\ N_y & O_y & A_y & P_y \\ N_z & O_z & A_z & P_z \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$${}^0 \underline{T}_e = \begin{bmatrix} f_{11} & f_{12} & f_{13} & f_{14} \\ f_{21} & f_{22} & f_{23} & f_{24} \\ f_{31} & f_{32} & f_{33} & f_{34} \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

e.g. for a SCARA manipulator

$${}^0 \underline{\tau}_4 = \begin{bmatrix} -0.259 & -0.966 & 0 & 0.933 \\ -0.966 & 0.259 & 0 & 0.250 \\ 0 & 0 & -1 & -0.200 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$${}^0 \underline{T}_4 = \begin{bmatrix} C_{12}C_4 + S_{12}S_4 & -C_{12}S_4 + S_{12}C_4 & 0 & a_1C_1 + a_2C_{12} \\ S_{12}C_4 - C_{12}S_4 & -C_{12}C_4 - S_{12}S_4 & 0 & a_1S_1 + a_2S_{12} \\ 0 & 0 & -1 & -d_3 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

A set of 12 nonlinear algebraic equations
only 6 of equations are mutually independent

$$N_x = f_{11}(q_1, q_2, \dots, q_e)$$

$$N_y = f_{21}(q_1, q_2, \dots, q_e)$$

$$N_z = f_{31}(q_1, q_2, \dots, q_e)$$

$$O_x = f_{12}(q_1, q_2, \dots, q_e)$$

$$O_y = f_{22}(q_1, q_2, \dots, q_e)$$

$$O_z = f_{32}(q_1, q_2, \dots, q_e)$$

$$A_x = f_{13}(q_1, q_2, \dots, q_e)$$

$$A_y = f_{23}(q_1, q_2, \dots, q_e)$$

$$A_z = f_{33}(q_1, q_2, \dots, q_e)$$

$$P_x = f_{14}(q_1, q_2, \dots, q_e)$$

$$P_y = f_{24}(q_1, q_2, \dots, q_e)$$

$$P_z = f_{34}(q_1, q_2, \dots, q_e)$$

There is no general solution method of such the set
One should determine:

- does a solution exist?
- how many solutions are there?

A general solution method:

The assumed position and orientation:

$${}^o \underline{\tau}_e = \begin{bmatrix} N_x & O_x & A_x & P_x \\ N_y & O_y & A_y & P_y \\ N_z & O_z & A_z & P_z \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$${}^0 \underline{\tau}_e = {}^0 T_e = \underline{A}_1 \underline{A}_2 \dots \underline{A}_e$$

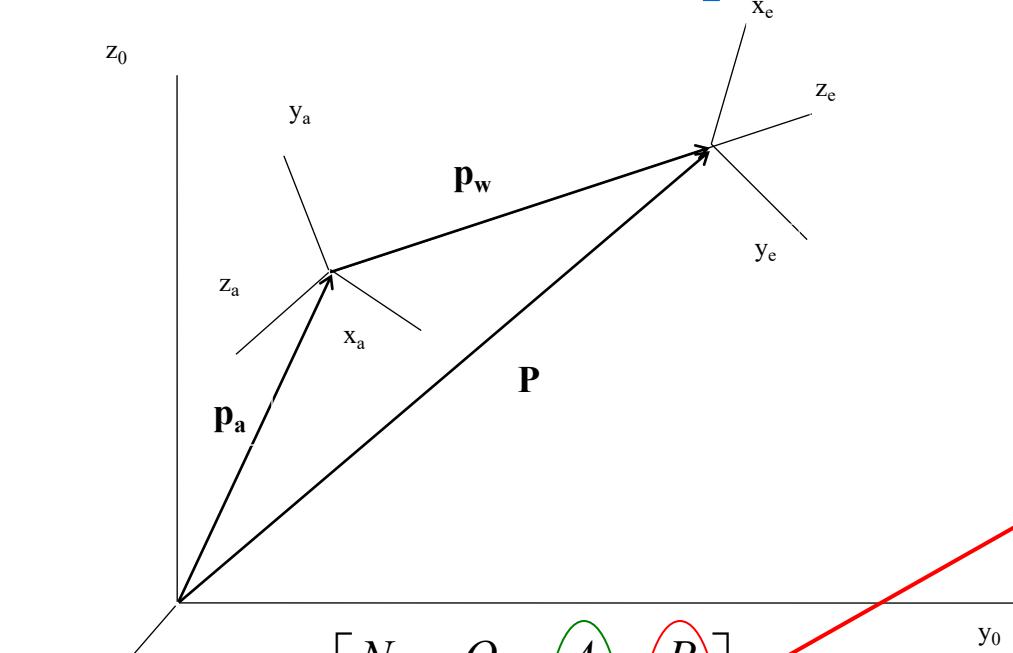
$$\underline{A}_1^{-1} {}^0 \underline{\tau}_6 = \underline{A}_2 \underline{A}_3 \underline{A}_4 \underline{A}_5 \underline{A}_6$$

$$\underline{A}_2^{-1} \left(\underline{\alpha}_1^{-1} {}^0 \underline{\tau}_6 \right) = \underline{A}_3 \underline{A}_4 \underline{A}_5 \underline{A}_6$$

A 2 step method applicable to manipulators with intersecting
3 wrist motion axes

$$\begin{aligned}
 {}^0 \underline{T}_e &= {}^0 \underline{T}_a {}^a \underline{T}_e = \begin{bmatrix} \underline{R}_a & \overline{\underline{P}}_a \\ 0 & 1 \end{bmatrix} \begin{bmatrix} {}^a \underline{R}_w & {}^a \overline{\underline{P}}_w \\ 0 & 1 \end{bmatrix} = \\
 &= \begin{bmatrix} \underline{R}_a {}^a \underline{R}_w & \overline{\underline{P}}_a + \underline{R}_a {}^a \overline{\underline{P}}_w \\ 0 & 1 \end{bmatrix} = \begin{bmatrix} \underline{R}_w & \overline{\underline{P}}_a + \overline{\underline{P}}_w \\ 0 & 1 \end{bmatrix}
 \end{aligned}$$

Formulation of a set of equations – IDEA and the INITIAL STEP



$${}^o\tau_e = \begin{bmatrix} N_x & O_x & A_x & P_x \\ N_y & O_y & A_y & P_y \\ N_z & O_z & A_z & P_z \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

A length of p_w vector is known
Its direction corresponds to the axis z_e

$$\bar{p}_w = \begin{bmatrix} A_x \\ A_y \\ A_z \end{bmatrix} |\bar{p}_w|$$

$$\begin{bmatrix} p_{ax} \\ p_{ay} \\ p_{az} \end{bmatrix} = \begin{bmatrix} P_x \\ P_y \\ P_z \end{bmatrix} - \begin{bmatrix} A_x \\ A_y \\ A_z \end{bmatrix} |\bar{p}_w|$$

$$\begin{aligned} \bar{P} &= \bar{p}_a + \bar{p}_w \\ \bar{p}_a &= \bar{P} - \bar{p}_w \end{aligned}$$

$$\bar{P} = \begin{bmatrix} P_x \\ P_y \\ P_z \end{bmatrix}$$

The first step

The following set of 3 equations
should be solved:

$$p_{ax} = g_1(q_1, q_2, q_3)$$

$$p_{ay} = g_2(q_1, q_2, q_3)$$

$$p_{az} = g_3(q_1, q_2, q_3)$$

SCARA

$$\left| \bar{p}_w \right| = \bar{0}$$

$$0.933 = a_1 C_1 + a_2 C_{12}$$

$$0.25 = a_1 S_1 + a_2 S_{12}$$

$$-0.2 = -d_3$$

In the result values of: q_1, q_2, q_3 variables are calculated.

They should be substituted into the 3rd link orientation matrix \underline{R}_3
In order to evaluate a \underline{r}_3 matrix (**it is composed of numbers only!**)

The second step

$$q_1, q_2, q_3 \xrightarrow{\hspace{1cm}} \underline{R}_3$$

$${}^o\tau_e = \begin{bmatrix} N_x & O_x & A_x & P_x \\ N_y & O_y & A_y & P_y \\ N_z & O_z & A_z & P_z \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$${}^0\underline{r}_e = {}^0\underline{r}_3 {}^3\underline{R}_e$$

$${}^3\underline{R}_e = {}^0\underline{r}_3 {}^T {}^0\underline{r}_e = \begin{bmatrix} n_{wx} & o_{wx} & a_{wx} \\ n_{wy} & o_{wy} & a_{wy} \\ n_{wz} & o_{wz} & a_{wz} \end{bmatrix}$$

The following set of equations should be solved (only 3 equations are independent)

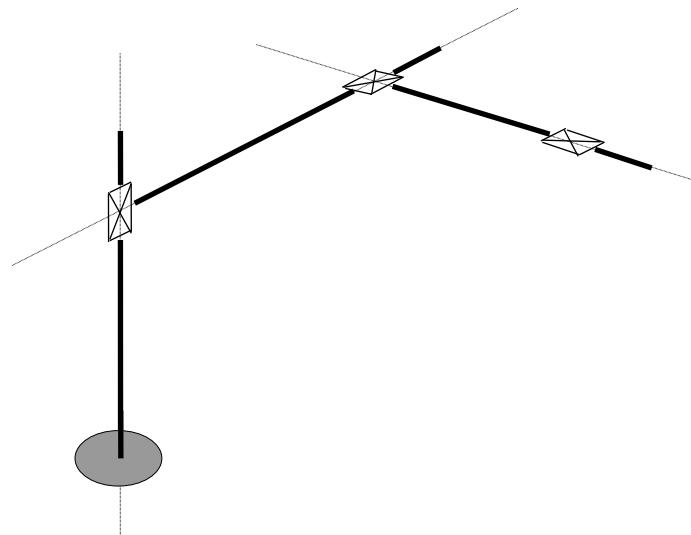
$$\begin{bmatrix} n_{wx} & o_{wx} & a_{wx} \\ n_{wy} & o_{wy} & a_{wy} \\ n_{wz} & o_{wz} & a_{wz} \end{bmatrix} = \underline{R}_4 \underline{R}_5 \underline{R}_6 = \begin{bmatrix} h_{11}(q_4, q_5, q_6) & h_{12}(q_4, q_5, q_6) & h_{13}(q_4, q_5, q_6) \\ h_{21}(q_4, q_5, q_6) & h_{22}(q_4, q_5, q_6) & h_{23}(q_4, q_5, q_6) \\ h_{31}(q_4, q_5, q_6) & h_{32}(q_4, q_5, q_6) & h_{33}(q_4, q_5, q_6) \end{bmatrix}$$

THE FIRST STEP - Examples

A. The Cartesian arm PPP

$$\underline{T}_3 = \begin{bmatrix} 1 & 0 & 0 & a_2 \\ 0 & 0 & -1 & -d_3 \\ 0 & 1 & 0 & d_1 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

To be calculated: d_1, a_2, d_3



$$p_{ax} = a_2$$

$$p_{ay} = -d_3$$

$$p_{az} = d_1$$



$$d_1 = p_{az}$$

$$a_2 = p_{ax}$$

$$d_3 = -p_{ay}$$

There is only 1 solution

The solution is always achievable

B. The cylindrical arm PRP

$$\underline{T}_3 = \begin{bmatrix} C_2 & 0 & -S_2 & a_2 C_2 - d_3 S_2 \\ S_2 & 0 & C_2 & a_2 S_2 + d_3 C_2 \\ 0 & -1 & 0 & d_1 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

To be calculated: d_1 , θ_2 , d_3 .

$$p_{ax} = a_2 C_2 - d_3 S_2$$

$$p_{ay} = a_2 S_2 + d_3 C_2$$

$$p_{az} = d_1$$



$$d_1 = p_{az}$$

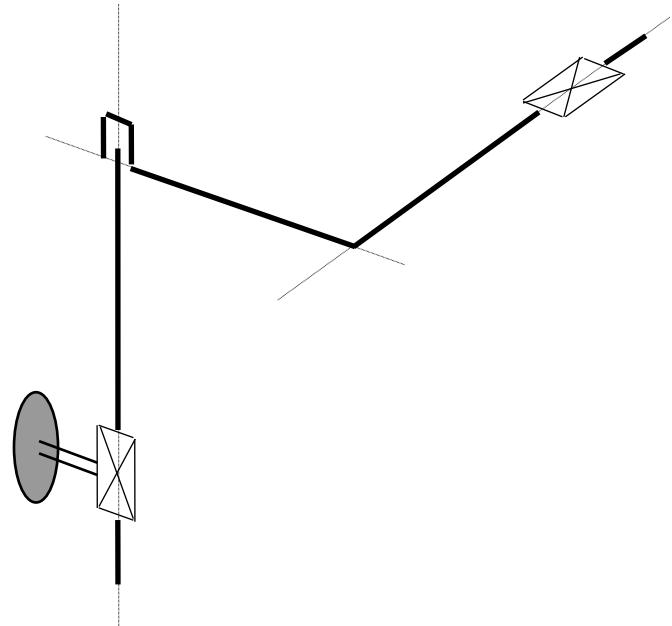
$$d_3^2 S_2^2 + a_2^2 C_2^2 - 2a_2 d_3 S_2 C_2 = p_{ax}^2$$

$$d_3^2 C_2^2 + a_2^2 S_2^2 + 2a_2 d_3 S_2 C_2 = p_{ay}^2$$



$$d_3^2 + a_2^2 = p_{ax}^2 + p_{ay}^2$$

$$d_3 = \pm \sqrt{p_{ax}^2 + p_{ay}^2 - a_2^2}$$



The 1st equation:

$$p_{ax} = a_2 C_2 - d_3 S_2$$

Is in a form of:

$$-A \sin \theta + B \cos \theta = D$$

where:

$$A = d_3$$

$$D = p_{ax}$$

$$B = a_2$$

$$\theta = \theta_2$$

Substitution:

$$A = r \cos \phi$$



$$r = \sqrt{A^2 + B^2}$$

$$B = r \sin \phi$$

$$\phi = \arctan \frac{B}{A}$$

The general form of the 1st equation:

$$-\cos \phi \sin \theta + \sin \phi \cos \theta = \frac{D}{r}$$

$$\sin(\phi - \theta) = \frac{D}{r} \quad \longrightarrow \quad \cos(\phi - \theta) = \pm \sqrt{1 - \frac{D^2}{r^2}}$$

$$\tan(\phi - \theta) = \frac{\frac{D}{r}}{\pm \sqrt{1 - \left(\frac{D}{r}\right)^2}} = \frac{D}{\pm \sqrt{r^2 - D^2}} = \frac{D}{\pm \sqrt{A^2 + B^2 - D^2}}$$

$$\theta = \arctan\left(\frac{B}{A}\right) - \arctan\left(\frac{D}{\pm \sqrt{A^2 + B^2 - D^2}}\right)$$

$$\theta_2 = \arctan\left(\frac{a_2}{d_3}\right) - \arctan\left(\frac{p_{ax}}{\pm \sqrt{d_3^2 + a_2^2 - p_{ax}^2}}\right)$$

$$d_1 = p_{az}$$

$$\theta_2 = \arctan\left(\frac{a_2}{d_3}\right) - \arctan\left(\frac{p_{ax}}{\pm\sqrt{d_3^2 + a_2^2 - p_{ax}^2}}\right)$$

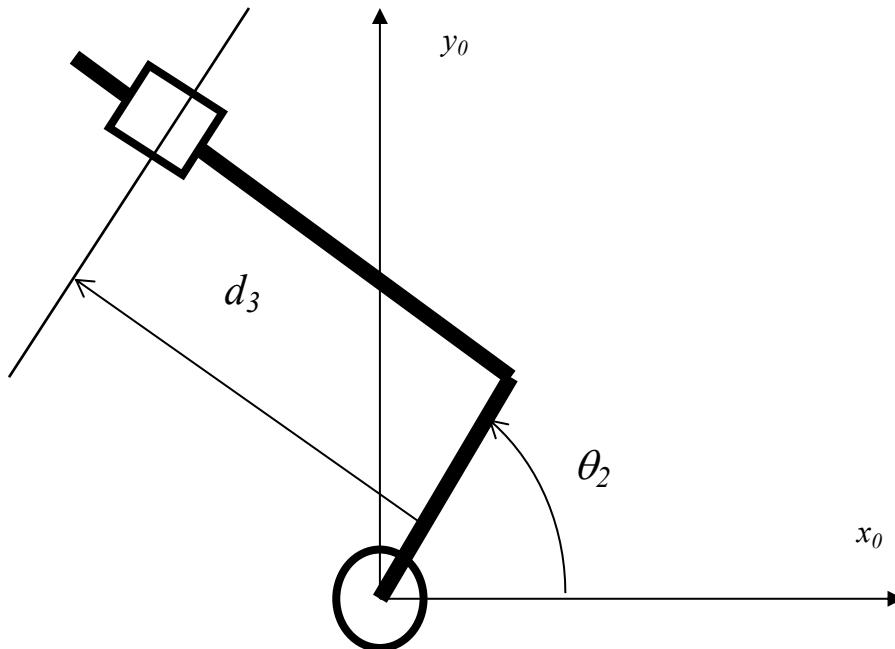
$$d_3 = \pm\sqrt{p_{ax}^2 + p_{ay}^2 - a_2^2}$$

4 solutions:

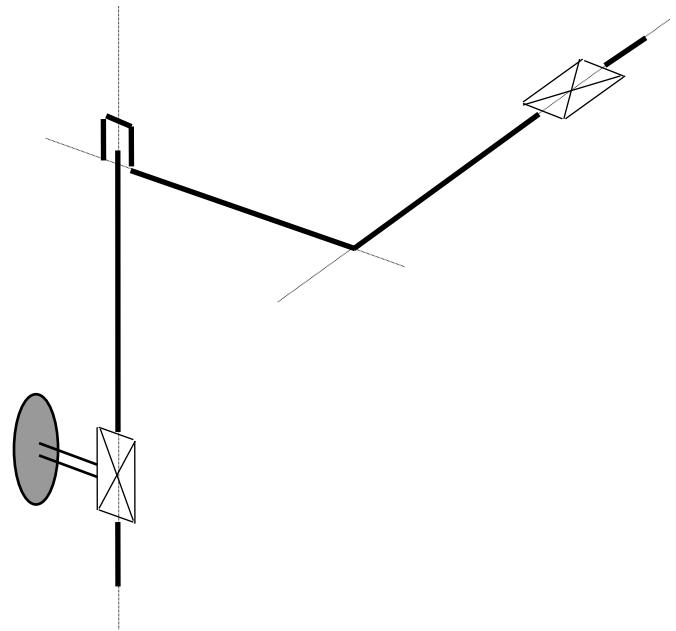
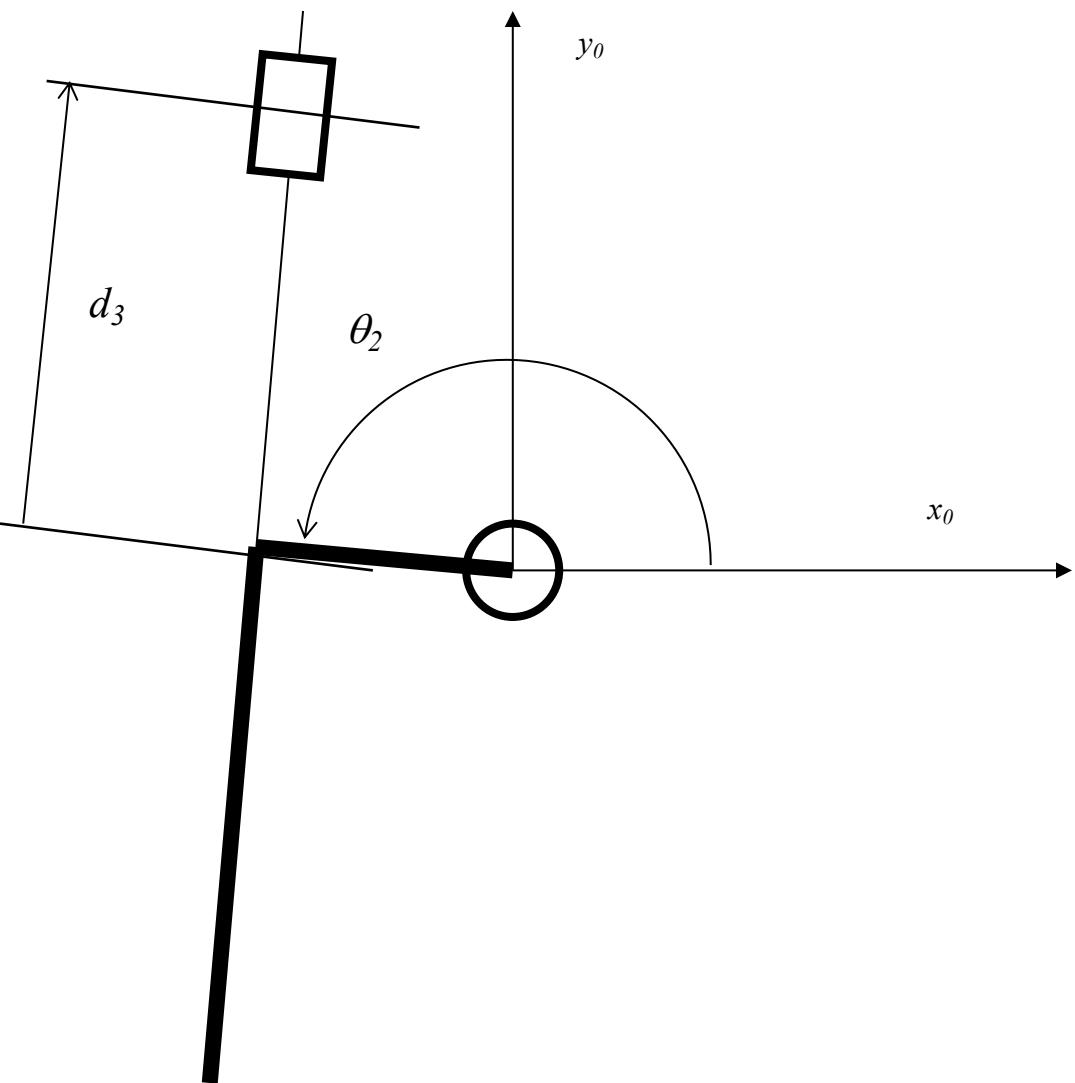
d_1	d_1	d_1	d_1
θ_{21}	θ_{22}	θ_{23}	θ_{24}
d_{31}	d_{31}	d_{32}	d_{32}

2 appropriate solutions

$$d_3 \geq 0$$



$d_3 < 0$

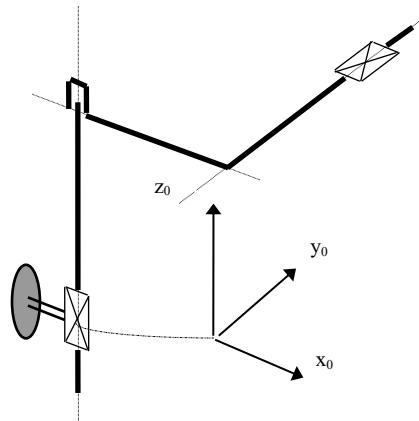


Analysis of existence of a solution:

$$\theta_2 = \arctan\left(\frac{a_2}{d_3}\right) - \arctan\left(\frac{p_{ax}}{\pm\sqrt{d_3^2 + a_2^2 - p_{ax}^2}}\right)$$

$$\arctan\left(\frac{a_2}{d_3}\right) = \arctan\left(\frac{0}{0}\right) \quad \xrightarrow{\text{blue arrow}} \quad a_2 = 0 \quad d_3 = 0$$

$$\arctan\left(\frac{p_{ax}}{\pm\sqrt{d_3^2 + a_2^2 - p_{ax}^2}}\right) = \arctan\left(\frac{0}{0}\right) \quad \xleftarrow{\text{blue arrow}} \quad p_{ax} = 0$$



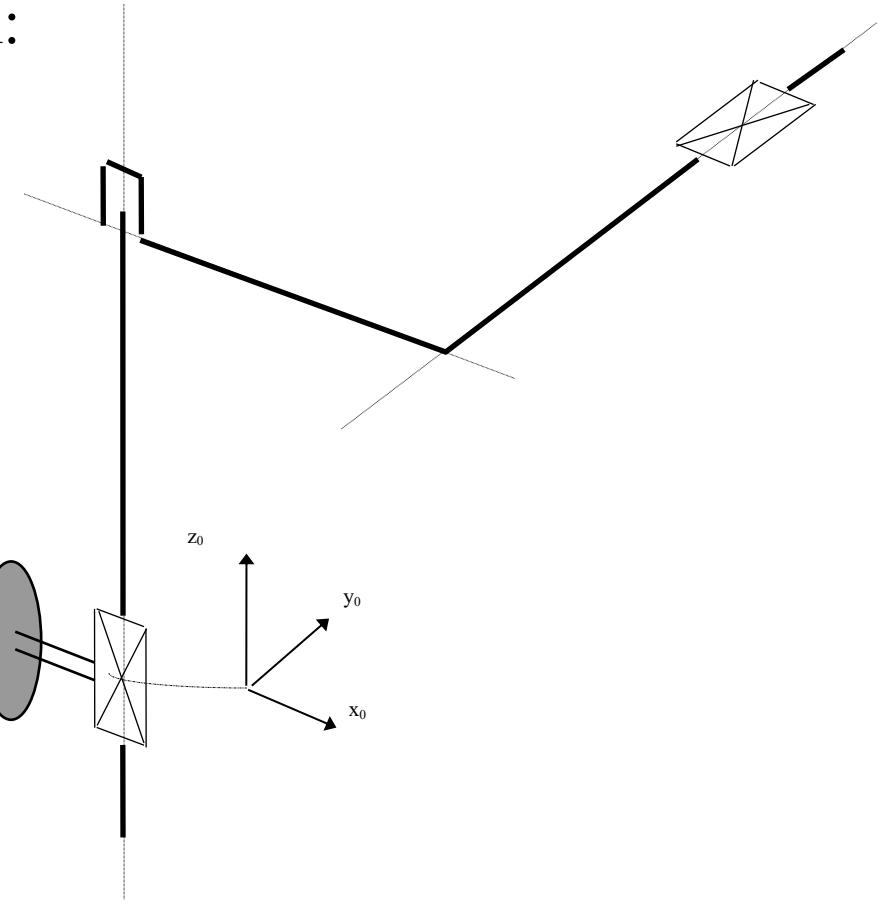
The solution of the inverse problem is indefinite
There is infinite number of values of θ_2

Analysis of existence of a solution:

$$d_3 = \pm \sqrt{p_{ax}^2 + p_{ay}^2 - a_2^2}$$

The solution always exists as:

$$p_{ax}^2 + p_{ay}^2 \geq a_2^2$$

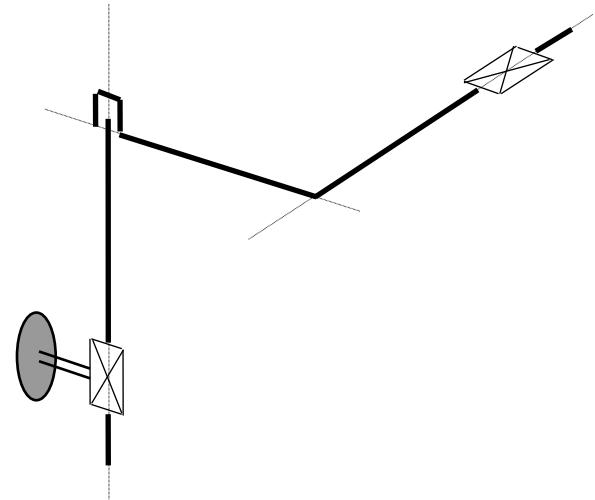


A numerical example, a PRP arm:

Known values of parameters:

$$\begin{aligned}a_2 &= 0.1 \text{ m} & d_1 &\in [0,1] \text{ m} \\ \theta_2 &\in [-90^\circ, 135^\circ] & d_3 &\in [0.3,1] \text{ m}\end{aligned}$$

$${}^0 T_3 = \begin{bmatrix} \frac{1}{\sqrt{2}} & 0 & -\frac{1}{\sqrt{2}} & -0.2\sqrt{2} \\ \frac{1}{\sqrt{2}} & 0 & \frac{1}{\sqrt{2}} & 0.3\sqrt{2} \\ 0 & -1 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$



To be determined:

$$d_1, \theta_2, d_3$$

The solution:

$$d_1 = p_{az} = 0$$

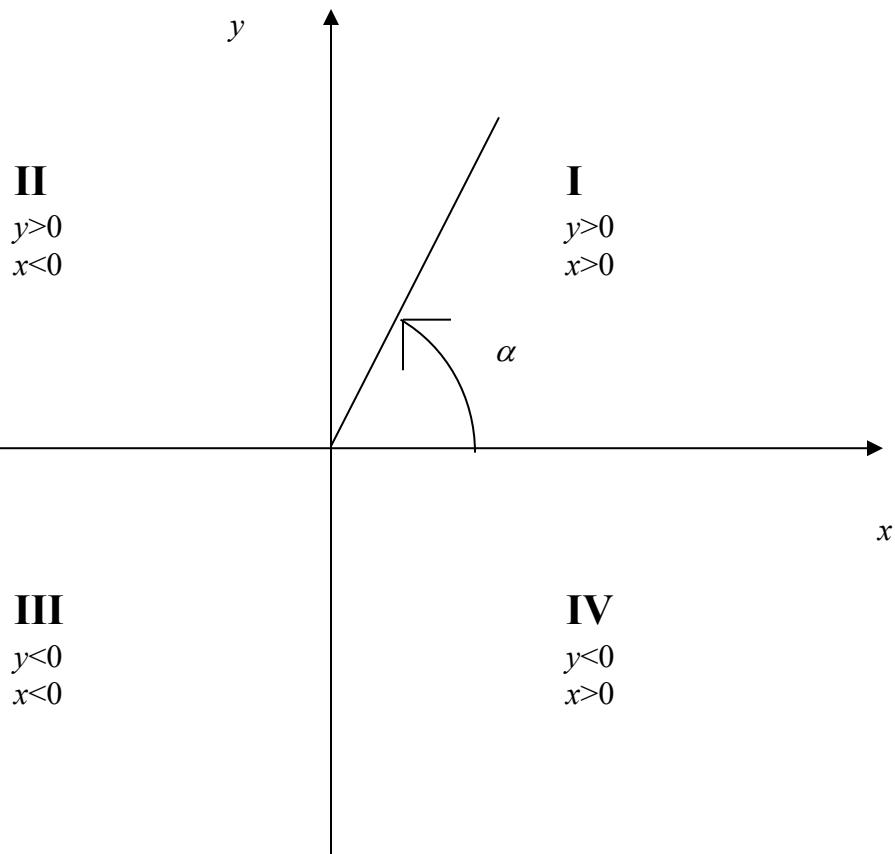


$${}^0 T_3 = \begin{bmatrix} \frac{1}{\sqrt{2}} & 0 & -\frac{1}{\sqrt{2}} & -0.2\sqrt{2} \\ \frac{1}{\sqrt{2}} & 0 & \frac{1}{\sqrt{2}} & 0.3\sqrt{2} \\ 0 & -1 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$d_3 = \pm \sqrt{{p_{ax}}^2 + {p_{ay}}^2 - {a_2}^2} = \pm \sqrt{0.08 + 0.18 - 0.01} = \pm \sqrt{0.25} = \pm 0.5$$

Atan2

quadrants I and IV:



$$\text{atan} 2\left(\frac{y}{x}\right) = \arctan\left(\frac{y}{x}\right)$$

quadrants II and III:

$$\text{atan} 2\left(\frac{y}{x}\right) = \arctan\left(\frac{y}{x}\right) \pm \pi$$

$$\theta_2 = \arctan\left(\frac{a_2}{d_{31}}\right) - \arctan\left(\frac{p_{ax}}{\pm\sqrt{d_{31}^2 + a_2^2 - p_{ax}^2}}\right) =$$

$$= \arctan\left(\frac{0.1}{0.5}\right) - \arctan\left(\frac{-0.2\sqrt{2}}{\pm\sqrt{0.25+0.01-0.08}}\right) = 11.31^\circ - \arctan\left(\frac{-2}{\pm 3}\right)$$

$$d_{3I}=0.5$$

$$\text{atan} 2\left(\frac{-2}{3}\right) = \arctan\left(-\frac{2}{3}\right) = -33.69^\circ$$

IV quadrant

$$\text{atan} 2\left(\frac{-2}{-3}\right) = \arctan\left(\frac{2}{3}\right) + \pi = 33.69^\circ + 180^\circ = 213.69^\circ$$

III quadrant

$$\theta_{21} = 11.31^\circ - (-33.69^\circ) = 45^\circ$$

$$\theta_{22} = 11.31^\circ - 213.69^\circ = -202.38^\circ$$

Verification of the results by substitution of θ_{21} , θ_{22} , d_{31} to:

$$p_{ax} = a_2 C_2 - d_3 S_2$$

$$p_{ay} = a_2 S_2 + d_3 C_2$$

Results:

$$p_{ax}(\theta_{21}) \approx -0.283 \approx -0.2\sqrt{2}$$

$$p_{ax}(\theta_{22}) \approx -0.283 \approx -0.2\sqrt{2}$$

$$p_{ay}(\theta_{21}) = 0.424 \approx 0.3\sqrt{2}$$

$$p_{ay}(\theta_{22}) = -0.424 \approx -0.3\sqrt{2}$$

$${}^0 \underline{T}_3 = \begin{bmatrix} \frac{1}{\sqrt{2}} & 0 & -\frac{1}{\sqrt{2}} & -0.2\sqrt{2} \\ \frac{1}{\sqrt{2}} & 0 & \frac{1}{\sqrt{2}} & 0.3\sqrt{2} \\ 0 & -1 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$\theta_2 = \theta_{21} = 45^\circ$$

$d_{32} = -0.5$

$$\begin{aligned}\theta_2 &= \arctan\left(\frac{a_2}{d_{32}}\right) - \arctan\left(\frac{p_{ax}}{\pm\sqrt{d_{32}^2 + a_2^2 - p_{ax}^2}}\right) = \\ &= \arctan\left(\frac{0.1}{-0.5}\right) - \arctan\left(\frac{-0.2\sqrt{2}}{\pm\sqrt{0.25 + 0.01 - 0.08}}\right) = \arctan\left(\frac{1}{-5}\right) - \arctan\left(\frac{-2}{\pm 3}\right)\end{aligned}$$

$$\text{atan } 2\left(\frac{1}{-5}\right) = \arctan\left(-\frac{1}{5}\right) + \pi = -11.31^\circ + 180^\circ = 168.69^\circ$$

$$\theta_{23} = 168.69^\circ - (-33.69^\circ) = 202.38^\circ$$

$$\theta_{24} = 168.69^\circ - 213.69^\circ = -45^\circ$$

Verification of the results by substitution of θ_{23} , θ_{24} , d_{32} to:

$$p_{ax} = a_2 C_2 - d_3 S_2$$

$$p_{ay} = a_2 S_2 + d_3 C_2$$

results:

$$p_{ax}(\theta_{23}) \approx -0.283 \approx -0.2\sqrt{2}$$

$$p_{ax}(\theta_{24}) \approx -0.283 \approx -0.2\sqrt{2}$$

$$p_{ay}(\theta_{23}) = 0.424 \approx 0.3\sqrt{2}$$

$$p_{ay}(\theta_{24}) = -0.424 \approx -0.3\sqrt{2}$$

$${}^0 \underline{T}_3 = \begin{bmatrix} \frac{1}{\sqrt{2}} & 0 & -\frac{1}{\sqrt{2}} & -0.2\sqrt{2} \\ \frac{1}{\sqrt{2}} & 0 & \frac{1}{\sqrt{2}} & 0.3\sqrt{2} \\ 0 & -1 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$\theta_2 = \theta_{23} = 202.38^\circ$$

2 solutions:

$$d_1 = 0$$

$$\theta_2 = 45^\circ$$

$$d_3 = 0.5$$

$$d_1 = 0$$

$$\theta_2 = 202,38^\circ$$

$$d_3 = -0.5$$

$$a_2 = 0.1 \text{ m}$$

$$\theta_2 \in [-90^\circ, 135^\circ]$$

$$d_1 \in [0,1] \text{ m}$$

$$d_3 \in [0.3,1] \text{ m}$$

The alternative method of solution:

$$p_{ax} = a_2 C_2 - d_3 S_2$$

$$p_{ay} = a_2 S_2 + d_3 C_2$$



$$\begin{bmatrix} -d_3 & a_2 \\ a_2 & d_3 \end{bmatrix} \begin{bmatrix} S_2 \\ C_2 \end{bmatrix} = \begin{bmatrix} p_{ax} \\ p_{ay} \end{bmatrix}$$

$$S_2 = \frac{a_2 p_{ay} - d_3 p_{ax}}{a_2^2 + d_3^2}$$

$$C_2 = \frac{a_2 p_{ax} + d_3 p_{ay}}{a_2^2 + d_3^2}$$

$$\tan(\theta_2) = \frac{a_2 p_{ay} - d_3 p_{ax}}{a_2 p_{ax} + d_3 p_{ay}}$$

Another alternative method of solution:

$$\theta_2 = \arcsin\left(\frac{a_2 p_{ay} - d_3 p_{ax}}{\sqrt{a_2^2 + d_3^2}}\right)$$

$$d_3=0.5$$

$$\theta_2 = \arccos\left(\frac{a_2 p_{ax} + d_3 p_{ay}}{\sqrt{a_2^2 + d_3^2}}\right)$$

$$\theta_2 = \arcsin(0.707) = 45^\circ \quad \text{or}$$

$$\theta_2 = 180^\circ - 45^\circ = 135^\circ$$

$$\theta_2 = \arccos(0.707) = 45^\circ \quad \text{or}$$

$$\theta_2 = -45^\circ$$



$$\theta_2 = 45^\circ$$

$$d_3=-0.5$$

$$\theta_2 = \arcsin(-0.381) = -22.38^\circ \quad \text{or} \quad \theta_2 = 180^\circ - (-22.38)^\circ = 202.38^\circ$$

$$\theta_2 = \arccos(-0.925) = 157.61^\circ \quad \text{or} \quad \theta_2 = -157.61^\circ = 202.38^\circ$$

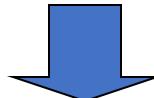
$$\theta_2 = 202.38^\circ$$

C. The spherical RRP arm

$$T_3 = \begin{bmatrix} C_1C_2 & -S_1 & C_1S_2 & d_3C_1S_2 \\ S_1C_2 & C_1 & S_1S_2 & d_3S_1S_2 \\ -S_2 & 0 & C_2 & d_1 + d_3C_2 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

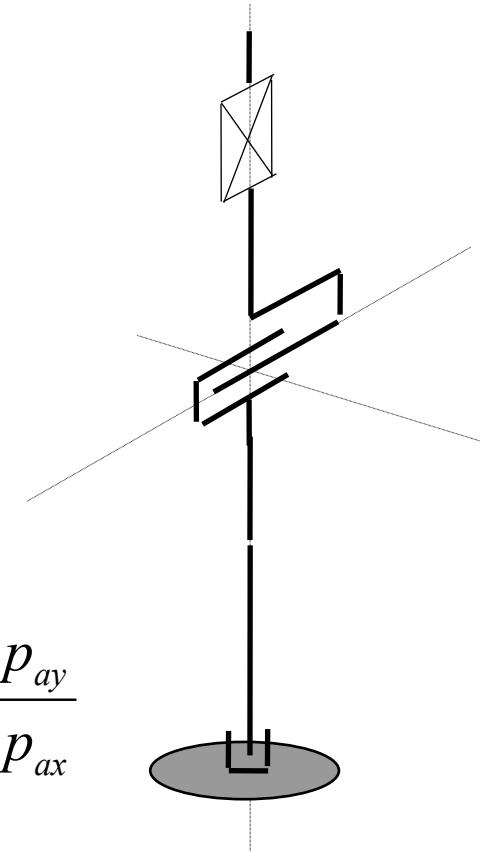
To be determined: θ_1, θ_2, d_3 .

$$\begin{aligned} p_{ax} &= d_3C_1S_2 & \xrightarrow{\text{blue arrow}} \frac{d_3S_1S_2}{d_3C_1S_2} &= \frac{p_{ay}}{p_{ax}} \Rightarrow \tan(\theta_1) = \frac{p_{ay}}{p_{ax}} \\ p_{ay} &= d_3S_1S_2 \\ p_{az} &= d_1 + d_3C_2 \end{aligned}$$



$$\boxed{\theta_1 = \arctan\left(\frac{p_{ay}}{p_{ax}}\right) + n\pi}$$

$$n = -1, 0, 1$$



$$\begin{aligned} p_{ax}^2 &= d_3^2 C_1^2 S_2^2 \\ p_{ay}^2 &= d_3^2 S_1^2 S_2^2 \end{aligned} \quad \xrightarrow{\text{blue arrow}} \quad \begin{aligned} p_{ax}^2 + p_{ay}^2 &= d_3^2 S_2^2 \\ (p_{az} - d_1)^2 &= d_3^2 C_2^2 \end{aligned}$$

$$\frac{d_3^2 S_2^2}{d_3^2 C_2^2} = \frac{p_{ax}^2 + p_{ay}^2}{(p_{az} - d_1)^2} \Rightarrow \operatorname{tg}(\theta_2) = \frac{\pm \sqrt{p_{ax}^2 + p_{ay}^2}}{p_{az} - d_1}$$

$$\boxed{\theta_2 = \arctan\left(\frac{\pm \sqrt{p_{ax}^2 + p_{ay}^2}}{p_{az} - d_1}\right) + n\pi} \quad n = -1, 0, 1$$

$$\boxed{d_3 = \pm \sqrt{p_{ax}^2 + p_{ay}^2 + (p_{az} - d_1)^2}}$$

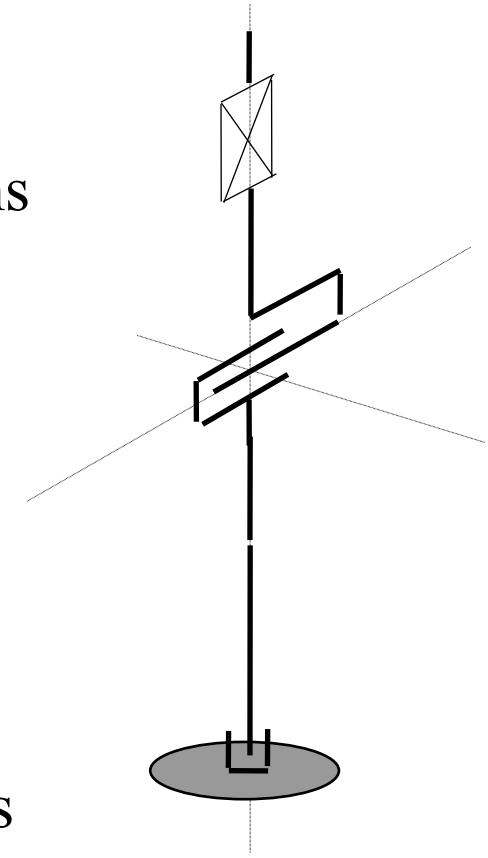
The spherical RRP arm - solutions

$$\theta_1 = \arctan\left(\frac{p_{ay}}{p_{ax}}\right) + n\pi \quad n = -1, 0, 1 \quad 2 \text{ solutions}$$

$$\theta_2 = \arctan\left(\frac{\pm\sqrt{p_{ax}^2 + p_{ay}^2}}{p_{az} - d_1}\right) + n\pi \quad n = -1, 0, 1 \quad 4 \text{ solutions}$$

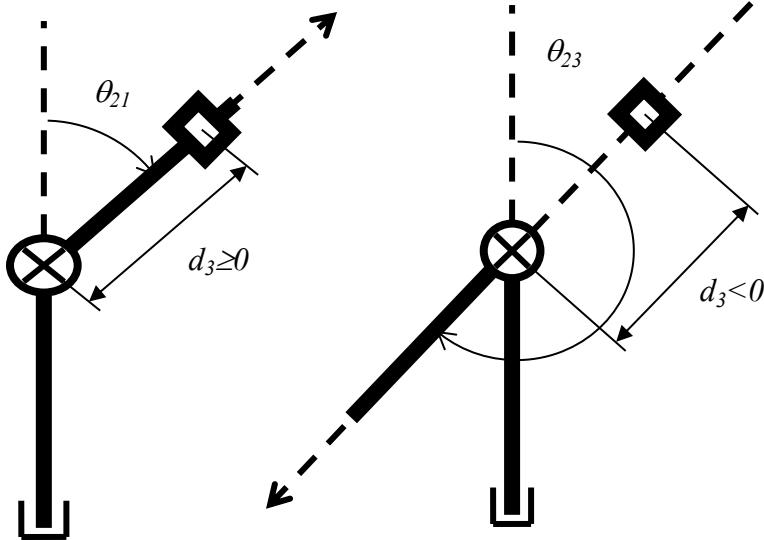
$$d_3 = \sqrt{p_{ax}^2 + p_{ay}^2 + (p_{az} - d_1)^2} \quad 2 \text{ solutions}$$

Altogether: $2 \times 4 \times 2 = 16$ solutions



Analysis of number of solutions – 4 appropriate results:

$$\theta_{11} = \arctan\left(\frac{p_{ay}}{p_{ax}}\right)$$



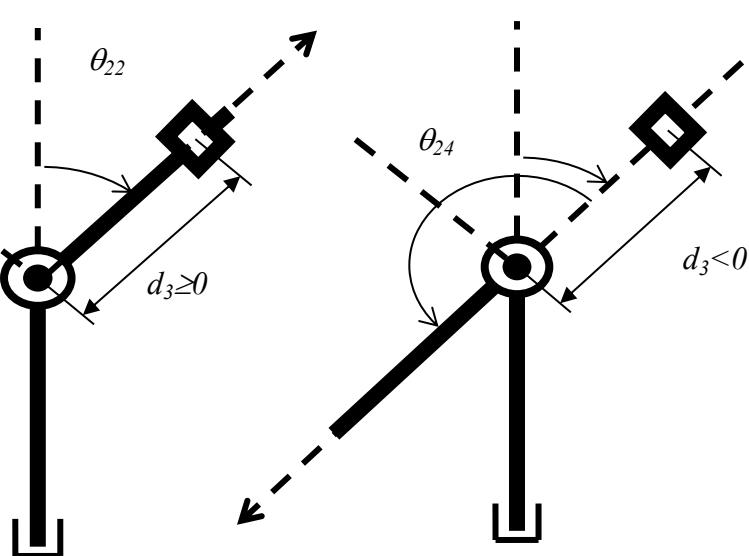
$$\theta_{11} = \arctan\left(\frac{p_{ay}}{p_{ax}}\right)$$

$$\theta_{21} = \arctan\left(\frac{\sqrt{p_{ax}^2 + p_{ay}^2}}{p_{az} - d_1}\right)$$

$$\theta_{23} = \arctan\left(\frac{\sqrt{p_{ax}^2 + p_{ay}^2}}{p_{az} - d_1}\right) \pm \pi$$

$$\theta_{12} = \arctan\left(\frac{p_{ay}}{p_{ax}}\right) \pm \pi$$

$$\theta_{22} = \arctan\left(\frac{-\sqrt{p_{ax}^2 + p_{ay}^2}}{p_{az} - d_1}\right)$$



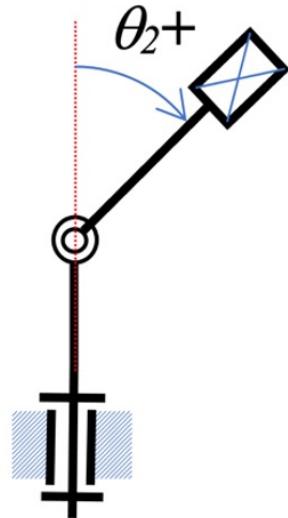
$$\theta_{12} = \arctan\left(\frac{p_{ay}}{p_{ax}}\right) \pm \pi$$

$$\theta_{24} = \arctan\left(\frac{-\sqrt{p_{ax}^2 + p_{ay}^2}}{p_{az} - d_1}\right) \pm \pi$$

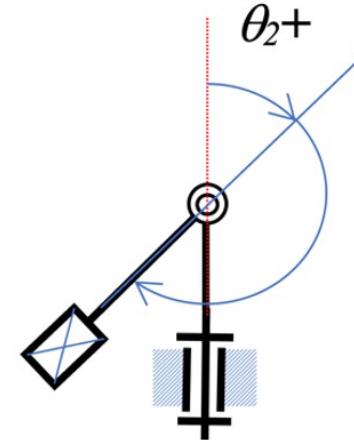
For θ_{11} and $d_3 > 0$ there are 4 solutions

$$\theta_{21} = \frac{\sqrt{p_{ax}^2 + p_{ay}^2}}{p_{az} - d_1}$$

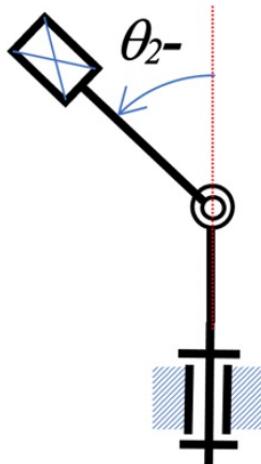
The only
correct
solution



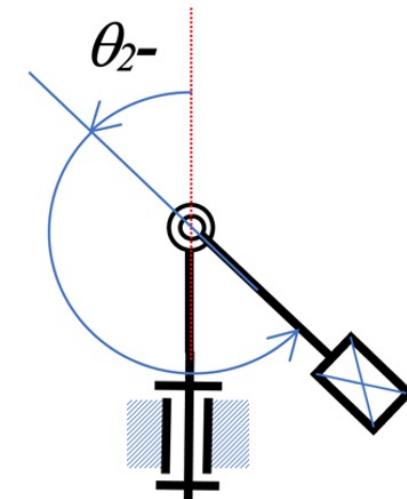
$$\theta_{23} = \frac{\sqrt{p_{ax}^2 + p_{ay}^2}}{p_{az} - d_1} \pm \pi$$



$$\theta_{22} = \frac{-\sqrt{p_{ax}^2 + p_{ay}^2}}{p_{az} - d_1}$$



$$\theta_{24} = \frac{-\sqrt{p_{ax}^2 + p_{ay}^2}}{p_{az} - d_1} \pm \pi$$



Analysis of existence of a solution:

$$\arctan\left(\frac{p_{ay}}{p_{ax}}\right) = \arctan\left(\frac{0}{0}\right) \quad \longrightarrow$$

$$\begin{aligned} p_{ax} &= 0 \\ p_{ay} &= 0 \end{aligned}$$

Infinite number of solutions.

The θ_1 angle can take any value

$$\arctan\left(\frac{\sqrt{p_{ax}^2 + p_{ay}^2}}{p_{az} - d_1}\right) = \arctan\left(\frac{0}{0}\right) \quad \longrightarrow$$

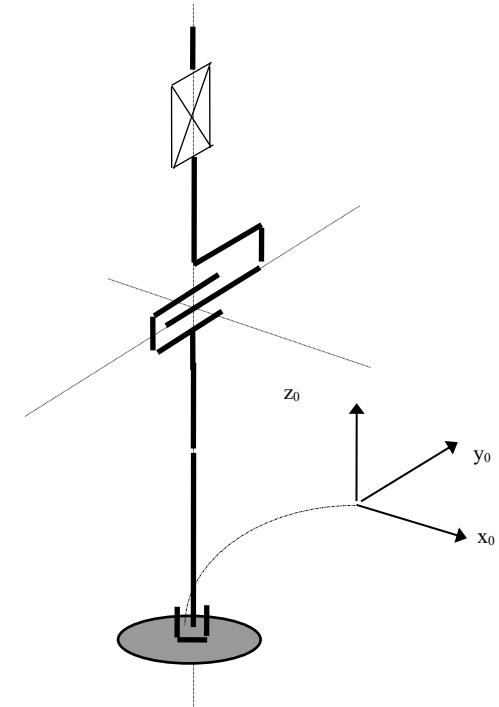
$$\begin{aligned} p_{ax} &= 0 \\ p_{ay} &= 0 \\ p_{az} &= d_1 \end{aligned}$$

Infinite number of solutions.

The θ_2 angle can take any value

$$p_{ax}^2 + p_{ay}^2 + (p_{az} - d_1)^2 \geq 0$$

A solution for d_3 always exists



D. The anthropomorphic RRR arm

$$\underline{T}_3 = \begin{bmatrix} C_1C_{23} & -S_1 & C_1S_{23} & a_2C_1C_2 \\ S_1C_{23} & C_1 & S_1S_{23} & a_2S_1C_2 \\ -S_{23} & 0 & C_{23} & d_1 - a_2S_2 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

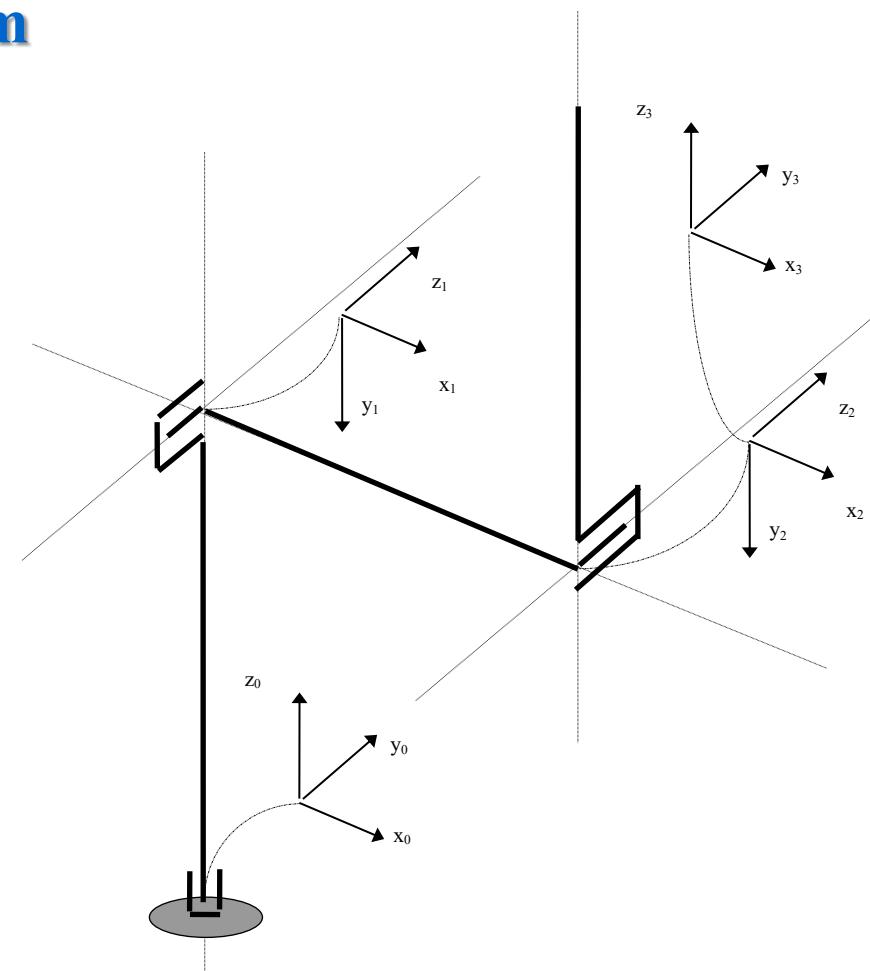
To be determined: $\theta_1, \theta_2, \theta_3$.

Remark !

Coordinate frame No. 3 is located at the beginning of the 3rd link

Coordinates of the 3rd link tip with respect to the 3rd coordinate system:

$$\underline{p}_4^* = \begin{bmatrix} 0 \\ 0 \\ d_4 \\ 1 \end{bmatrix}$$



Coordinates of the arm's tip with respect to the reference frame

$$\bar{p}_a = {}^0 T_3 \bar{p}_4^*$$

$$\begin{bmatrix} p_{ax} \\ p_{ay} \\ p_{az} \\ 1 \end{bmatrix} = \begin{bmatrix} C_1 C_{23} & -S_1 & C_1 S_{23} & a_2 C_1 C_2 \\ S_1 C_{23} & C_1 & S_1 S_{23} & a_2 S_1 C_2 \\ -S_{23} & 0 & C_{23} & d_1 - a_2 S_2 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 0 \\ 0 \\ d_4 \\ 1 \end{bmatrix} = \begin{bmatrix} C_1 S_{23} d_4 + a_2 C_1 C_2 \\ S_1 S_{23} d_4 + a_2 S_1 C_2 \\ C_{23} d_4 + d_1 - a_2 S_2 \\ 1 \end{bmatrix}$$

A set of equations to be solved:

$$p_{ax} = C_1 S_{23} d_4 + a_2 C_1 C_2$$



$$p_{ay} = S_1 S_{23} d_4 + a_2 S_1 C_2$$

$$p_{az} = C_{23} d_4 + d_1 - a_2 S_2$$

$$p_{ax} = C_1 (S_{23} d_4 + a_2 C_2)$$

$$p_{ay} = S_1 (S_{23} d_4 + a_2 C_2)$$

$$\theta_1 = \arctan\left(\frac{p_{ay}}{p_{ax}}\right) + n\pi$$

$$n = -1, 0, 1$$

$$\begin{aligned} p_{ax} &= C_1(S_{23}d_4 + a_2C_2) \\ p_{ay} &= S_1(S_{23}d_4 + a_2C_2) \end{aligned}$$

$$(S_{23}d_4 + a_2C_2)^2 = p_{ax}^2 + p_{ay}^2$$

$$p_{az} = C_{23}d_4 + d_1 - a_2S_2$$

$$S_{23}d_4 = \alpha - a_2C_2$$

$$C_{23}d_4 = p_{az} - d_1 + a_2S_2$$

$$\alpha = \pm \sqrt{p_{ax}^2 + p_{ay}^2}$$

$$d_4^2 = \alpha^2 + a_2^2C_2^2 - 2a_2\alpha C_2 + p_{az}^2 + d_1^2 + a_2^2S_2^2 - 2p_{az}d_1 + 2a_2p_{az}S_2 - 2a_2d_1S_2$$

$$2a_2(-(p_{az} - d_1)S_2 + \alpha C_2) = \alpha^2 + p_{az}^2 + d_1^2 + a_2^2 - 2p_{az}d_1 - d_4^2$$

$$-(p_{az} - d_1)S_2 + \alpha C_2 = \frac{\alpha^2 + p_{az}^2 + d_1^2 + a_2^2 - 2p_{az}d_1 - d_4^2}{2a_2} = \beta$$

$$-A \sin \theta + B \cos \theta = D$$

$$\theta = \arctan\left(\frac{B}{A}\right) - \arctan\left(\frac{D}{\pm\sqrt{A^2 + B^2 - D^2}}\right)$$

$A = p_{az} - d_1$
 $B = \alpha$
 $D = \beta$

$$\theta_2 = \arctan\left(\frac{\alpha}{p_{az} - d_1}\right) - \arctan\left(\frac{\beta}{\pm\sqrt{(p_{az} - d_1)^2 + (\alpha)^2 - \beta^2}}\right)$$

$$S_{23}d_4 = \alpha - a_2C_2$$

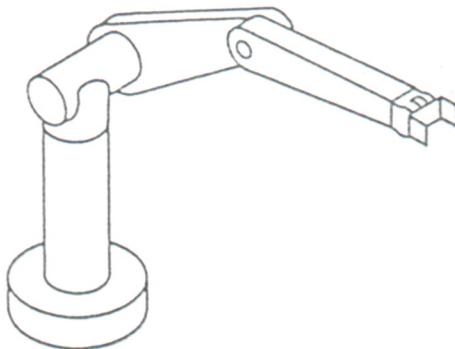
$$C_{23}d_4 = p_{az} - d_1 + a_2S_2$$


$$\tan(\theta_2 + \theta_3) = \frac{\alpha - a_2C_2}{p_{az} - d_1 + a_2S_2}$$

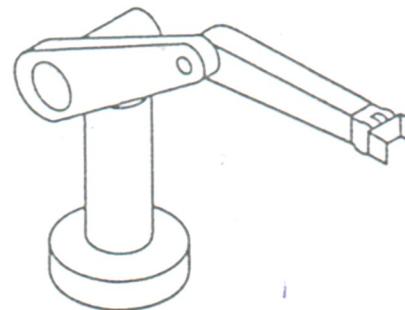
$$\alpha = \pm\sqrt{p_{ax}^2 + p_{ay}^2}$$

$$\theta_3 = \arctan\left(\frac{\alpha - a_2C_2}{p_{az} - d_1 + a_2S_2}\right) - \theta_2$$

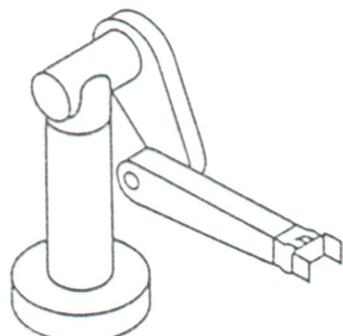
There are 4 correct solutions



LEFT and ABOVE Arm



RIGHT and ABOVE Arm



LEFT and BELOW Arm



RIGHT and BELOW Arm

$$\theta_1 = \arctan\left(\frac{p_{ay}}{p_{ax}}\right) + n\pi$$

$$n = -1, 0, 1$$

(Fu)

$$\theta_2 = \arctan\left(\frac{\alpha}{p_{az} - d_1}\right) - \arctan\left(\frac{\beta}{\pm\sqrt{(p_{az} - d_1)^2 + (\alpha)^2} - \beta^2}\right)$$

$$\theta_3 = \arctan\left(\frac{\alpha - a_2 C_2}{p_{az} - d_1 + a_2 S_2}\right) - \theta_2$$

Analysis of existence and a number of solutions

$$\theta_1 = \arctan\left(\frac{p_{ay}}{p_{ax}}\right) + n\pi$$

$$n = -1, 0, 1$$

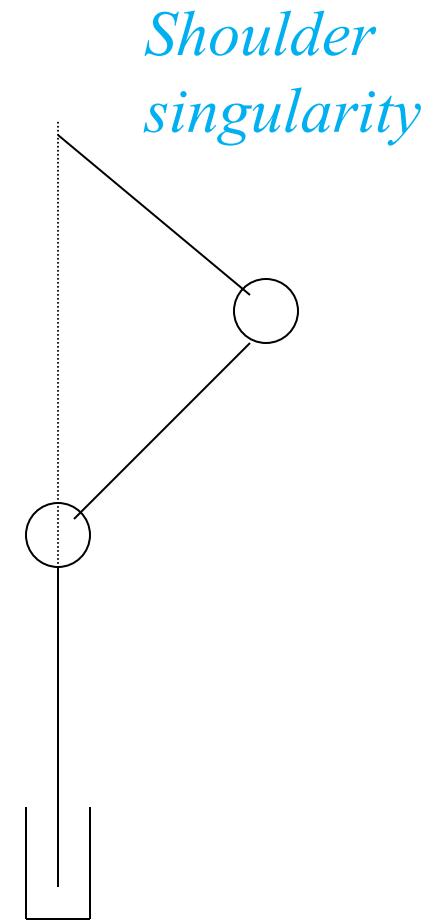
$$\arctan\left(\frac{p_{ay}}{p_{ax}}\right) = \arctan\left(\frac{0}{0}\right)$$



$$\boxed{\begin{aligned} p_{ax} &= 0 \\ p_{ay} &= 0 \end{aligned}}$$

Infinite number of solutions.

The angle θ_1 can take any value



THE SECOND STEP

$$q_1, q_2, q_3 \rightarrow \underline{R}_3$$

$${}^o \underline{\tau}_e = \begin{bmatrix} N_x & O_x & A_x & P_x \\ N_y & O_y & A_y & P_y \\ N_z & O_z & A_z & P_z \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$${}^0 \underline{r}_3 {}^T \underline{r}_e = \begin{bmatrix} n_{wx} & o_{wx} & a_{wx} \\ n_{wy} & o_{wy} & a_{wy} \\ n_{wz} & o_{wz} & a_{wz} \end{bmatrix}$$

A set of equations (only 3 equations are independent)

$$\begin{bmatrix} n_{wx} & o_{wx} & a_{wx} \\ n_{wy} & o_{wy} & a_{wy} \\ n_{wz} & o_{wz} & a_{wz} \end{bmatrix} = \underline{R}_4 \underline{R}_5 \underline{R}_6 \quad \longrightarrow$$

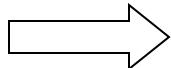
$$\underline{R}_4^{-1} \begin{bmatrix} n_{wx} & o_{wx} & a_{wx} \\ n_{wy} & o_{wy} & a_{wy} \\ n_{wz} & o_{wz} & a_{wz} \end{bmatrix} = \underline{R}_5 \underline{R}_6$$

THE SECOND STEP - Examples

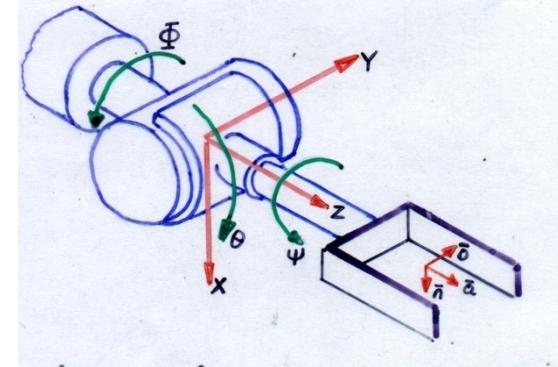
A. The Spherical (Euler) wrist:

$$\begin{bmatrix} C_4 n_{wx} + S_4 n_{wy} & C_4 o_{wx} + S_4 o_{wy} & C_4 a_{wx} + S_4 a_{wy} \\ -n_{wz} & -o_{wz} & -a_{wz} \\ -S_4 n_{wx} + C_4 n_{wy} & -S_4 o_{wx} + C_4 o_{wy} & -S_4 a_{wx} + C_4 a_{wy} \end{bmatrix} = \begin{bmatrix} C_5 C_6 & -C_5 S_6 & S_5 \\ S_5 C_6 & -S_5 S_6 & -C_5 \\ S_6 & C_6 & 0 \end{bmatrix}$$

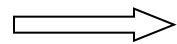
[3,3]



$$\theta_4 = \arctan\left(\frac{a_{wy}}{a_{wx}}\right)$$

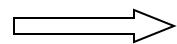


[1,3], [2,3]



$$\theta_5 = \arctan\left(\frac{C_4 a_{wx} + S_4 a_{wy}}{a_{wz}}\right)$$

[3,1], [3,2]



$$\theta_6 = \arctan\left(\frac{-S_4 n_{wx} + C_4 n_{wy}}{-S_4 o_{wx} + C_4 o_{wy}}\right)$$

$$\theta_4 = \arctan\left(\frac{a_{wy}}{a_{wx}}\right)$$



$$\sin(\theta_4) = \frac{a_{wy}}{\pm \sqrt{a_{wx}^2 + a_{wy}^2}}$$

$$\cos(\theta_4) = \frac{a_{wx}}{\pm \sqrt{a_{wx}^2 + a_{wy}^2}}$$

If $a_{wz}=1$, then:

$$a_{wx} = 0 \quad \text{and} \quad a_{wy} = 0$$

$$\theta_5 = \arctan\left(\frac{C_4 a_{wx} + S_4 a_{wy}}{a_{wz}}\right) = \arctan\left(\frac{\pm \sqrt{a_{wx}^2 + a_{wy}^2}}{a_{wz}}\right) = \arctan\left(\frac{\pm 0}{1}\right) = 0 \quad \text{or} \quad \pm \pi$$

$a_{wz}=-1$

$$\theta_4 = \arctan\left(\frac{0}{0}\right)$$

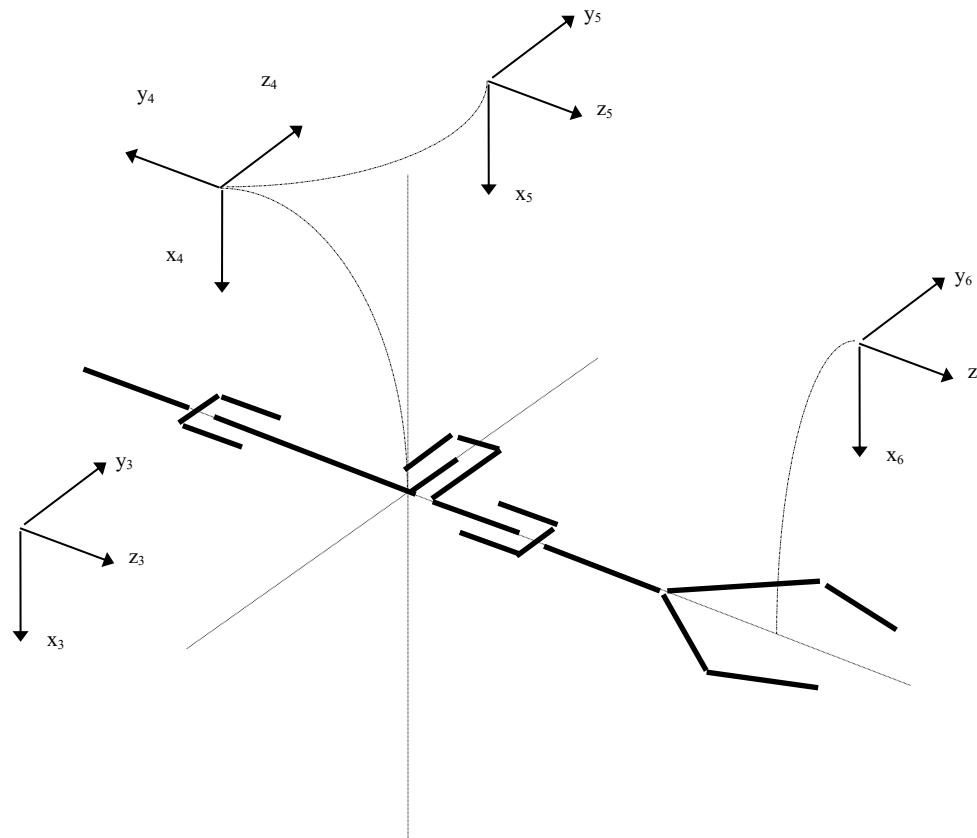


$$\theta_4 = ?$$

$$\theta_6 = ?$$

for $\theta_5=0^\circ$ the 4th and 6th axes of motion are collinear

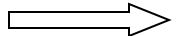
There is an infinite number of the: θ_4 and θ_6 values of pairs corresponding to the command end-effector orientation.



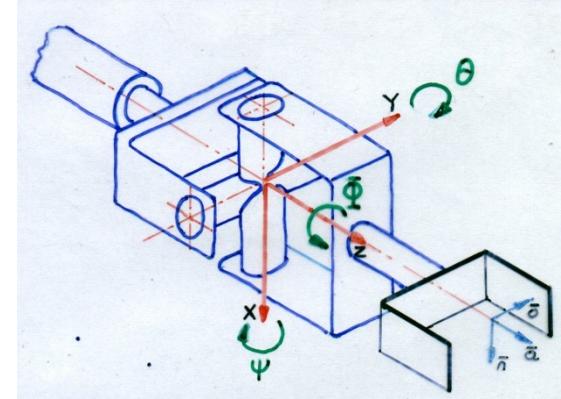
B. The Spherical (RPY) wrist:

$$\begin{bmatrix} C_4 n_{wx} + S_4 n_{wy} & C_4 o_{wx} + S_4 o_{wy} & C_4 a_{wx} + S_4 a_{wy} \\ -n_{wz} & -o_{wz} & -a_{wz} \\ -S_4 n_{wx} + C_4 n_{wy} & -S_4 o_{wx} + C_4 o_{wy} & -S_4 a_{wx} + C_4 a_{wy} \end{bmatrix} = \begin{bmatrix} C_5 & S_5 S_6 & S_5 C_6 \\ S_5 & -C_5 S_6 & -C_5 C_6 \\ 0 & C_6 & -S_6 \end{bmatrix}$$

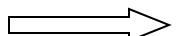
[3,1]



$$\theta_4 = \arctan\left(\frac{n_{wy}}{n_{wx}}\right)$$

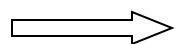


[1,1], [2,1]



$$\theta_5 = \arctan\left(\frac{-n_{wz}}{C_4 n_{wx} + S_4 n_{wy}}\right)$$

[3,2], [3,3]

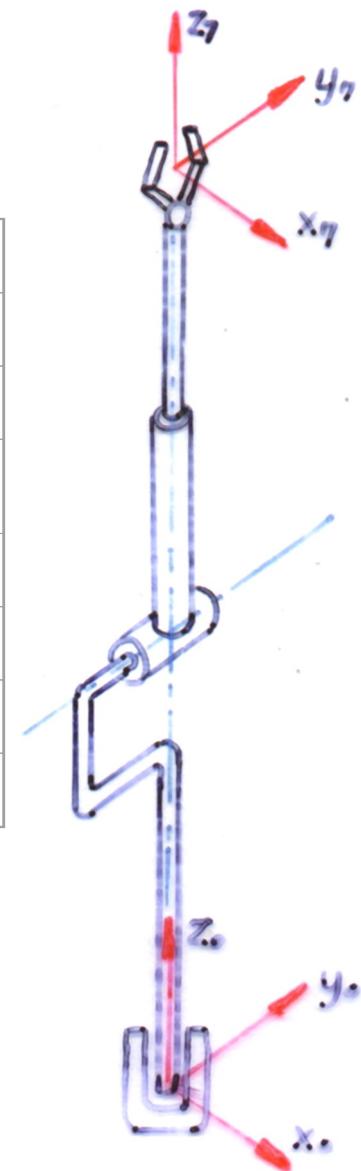


$$\alpha_6 = \arctan\left(\frac{S_4 a_{wx} - C_4 a_{wy}}{-S_4 o_{wx} + C_4 o_{wy}}\right)$$

Example of a RRP+RPY manipulator

Geometrical model:

Link No.	θ	d	a	α	joint motion range
1	$\theta_1 \nu$	d_1	0	-90°	-150°÷150°
2	$\theta_2 \nu$	0	0	90°	30°÷120°
3	0	$d_3 \nu$	0	0	$d_p \div d_k$ ($d_p > 0$ i $d_k > 0$)
4	$\theta_4 \nu$	d_4	0	-90°	-120°÷120°
5	$\theta_5 \nu$	0	0	90°	-60°÷60°
6	0	0	0	$\alpha_6 \nu$	-90°÷90°
6	0	d_7	0	0	-



Problem formulation:

The following pose of an end-effector is specified:

$$\underline{\tau}_t = \begin{bmatrix} -\frac{1}{\sqrt{2}} & \frac{1}{2\sqrt{2}} & \frac{\sqrt{3}}{2\sqrt{2}} & \frac{\sqrt{3}}{2\sqrt{2}}d_7 + L \\ \frac{1}{\sqrt{2}} & \frac{1}{2\sqrt{2}} & \frac{\sqrt{3}}{2\sqrt{2}} & \frac{\sqrt{3}}{2\sqrt{2}}d_7 \\ 0 & \frac{\sqrt{3}}{2} & -\frac{1}{2} & -\frac{1}{2}d_7 + d_1 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

d_1, d_7 and L –
- positive constant values

To be determined:

Values of $\theta_1, \theta_2, d_3, \theta_4, \theta_5, \alpha_6$ joint coordinates

Determination of the arm tip position:

$$A_x = \frac{\sqrt{3}}{2\sqrt{2}}$$

$$A_y = \frac{\sqrt{3}}{2\sqrt{2}}$$

$$A_z = -\frac{1}{2}$$

$$|p_w| = d_7$$



$$p_{wx} = \frac{\sqrt{3}}{2\sqrt{2}} d_7$$

$$p_{wy} = \frac{\sqrt{3}}{2\sqrt{2}} d_7$$

$$p_{wz} = -\frac{1}{2} d_7$$

$$p_{ax} = P_x - p_{wx} = \frac{\sqrt{3}}{2\sqrt{2}} d_7 + L - \frac{\sqrt{3}}{2\sqrt{2}} d_7 = L$$

$$p_{ay} = P_y - p_{wy} = \frac{\sqrt{3}}{2\sqrt{2}} d_7 - \frac{\sqrt{3}}{2\sqrt{2}} d_7 = 0$$

$$p_{az} = P_z - p_{wz} = -\frac{1}{2} d_7 + d_1 + \frac{1}{2} d_7 = d_1$$

Solution No 1

$$\theta_{11} = \arctan\left(\frac{p_{ay}}{p_{ax}}\right) = \arctan\left(\frac{0}{L}\right) = 0^\circ$$

$$p_{ax} = L$$

$$p_{ay} = 0$$

$$p_{az} = d_1$$

$$\theta_{21} = \arctan\left(\frac{\sqrt{p_{ax}^2 + p_{ay}^2}}{p_{az} - d_1}\right) = \arctan\left(\frac{\sqrt{L^2 + 0^2}}{d_1 - d_1}\right) = \tan 2\left(\frac{L}{0}\right) = 90^\circ$$

$$d_{31} = \sqrt{p_{ax}^2 + p_{ay}^2 + (p_{az} - d_1)^2} = \sqrt{L^2 + 0^2 + (d_1 - d_1)^2} = L$$

Solution No 2

$$\theta_{12} = \arctan\left(\frac{p_{ay}}{p_{ax}}\right) \pm 180^\circ = \text{atan2}\left(\frac{0}{L}\right) \pm 180^\circ = \pm 180^\circ$$

$$\theta_{22} = \arctan\left(\frac{-\sqrt{p_{ax}^2 + p_{ay}^2}}{p_{az} - d_1}\right) = \arctan\left(\frac{-\sqrt{L^2 + 0^2}}{d_1 - d_1}\right) = \text{atan2}\left(\frac{-L}{0}\right) = -90^\circ$$

$$d_{31} = \sqrt{p_{ax}^2 + p_{ay}^2 + (p_{az} - d_1)^2} = \sqrt{L^2 + 0^2 + (d_1 - d_1)^2} = L$$

Solution No 3

$$\theta_{11} = \arctan\left(\frac{p_{ay}}{p_{ax}}\right) = \operatorname{arctg}\left(\frac{0}{L}\right) = 0^\circ$$

$$p_{ax} = L$$

$$p_{ay} = 0$$

$$p_{az} = d_1$$

$$\theta_{23} = \arctan\left(\frac{\sqrt{p_{ax}^2 + p_{ay}^2}}{p_{az} - d_1}\right) \pm 180^\circ = \arctan\left(\frac{\sqrt{L^2 + 0^2}}{d_1 - d_1}\right) \pm 180^\circ = \operatorname{atan2}\left(\frac{L}{0}\right) \pm 180^\circ = -90^\circ$$

$$d_{32} = -\sqrt{p_{ax}^2 + p_{ay}^2 + (p_{az} - d_1)^2} = -\sqrt{L^2 + 0^2 + (d_1 - d_1)^2} = -L$$

Solution No 4

$$\theta_{12} = \arctan\left(\frac{p_{ay}}{p_{ax}}\right) \pm 180^\circ = \operatorname{atan2}\left(\frac{0}{L}\right) \pm 180^\circ = \pm 180^\circ$$

$$\theta_{24} = \arctan\left(\frac{-\sqrt{p_{ax}^2 + p_{ay}^2}}{p_{az} - d_1}\right) \pm 180^\circ = \arctan\left(\frac{-\sqrt{L^2 + 0^2}}{d_1 - d_1}\right) \pm 180^\circ = \operatorname{atan2}\left(\frac{-L}{0}\right) \pm 180^\circ = 90^\circ$$

$$d_{32} = -\sqrt{p_{ax}^2 + p_{ay}^2 + (p_{az} - d_1)^2} = -\sqrt{L^2 + 0^2 + (d_1 - d_1)^2} = -L$$

θ_1	0°	180°	0°	180	-150°-150°
θ_2	90°	-90°	-90°	90°	30°-120°
d_3	L	L	-L	-L	>0

The only result consistent with the assumed motion ranges:

$$\theta_1 = 0^\circ \quad \theta_2 = 90^\circ \quad d_3 = L$$

$$\theta_1 = 0^\circ \quad \theta_2 = 90^\circ \quad d_3 = L$$

A substitution to \underline{R}_3

$$\underline{R}_3 = \begin{bmatrix} C_1C_2 & -S_1 & C_1S_2 \\ S_1C_2 & C_1 & S_1S_2 \\ -S_2 & 0 & C_2 \end{bmatrix} = \begin{bmatrix} 0 & 0 & 1 \\ 0 & 1 & 0 \\ -1 & 0 & 0 \end{bmatrix} \quad \underline{r}_3^{-1} = \underline{r}_3^T = \begin{bmatrix} 0 & 0 & -1 \\ 0 & 1 & 0 \\ 1 & 0 & 0 \end{bmatrix}$$

$${}^3\underline{r}_6 = \underline{r}_3^{-1} \underline{r}_6 = \begin{bmatrix} 0 & 0 & -1 \\ 0 & 1 & 0 \\ 1 & 0 & 0 \end{bmatrix} \begin{bmatrix} -\frac{1}{\sqrt{2}} & \frac{1}{2\sqrt{2}} & \frac{\sqrt{3}}{2\sqrt{2}} \\ \frac{1}{\sqrt{2}} & \frac{1}{2\sqrt{2}} & \frac{\sqrt{3}}{2\sqrt{2}} \\ 0 & \frac{\sqrt{3}}{2} & -\frac{1}{2} \end{bmatrix} = \begin{bmatrix} 0 & -\frac{\sqrt{3}}{2} & \frac{1}{2} \\ \frac{1}{\sqrt{2}} & \frac{1}{2\sqrt{2}} & \frac{\sqrt{3}}{2\sqrt{2}} \\ -\frac{1}{\sqrt{2}} & \frac{1}{2\sqrt{2}} & \frac{\sqrt{3}}{2\sqrt{2}} \end{bmatrix}$$

$$\begin{bmatrix} n_{wx} & o_{wx} & a_{wx} \\ n_{wy} & o_{wy} & a_{wy} \\ n_{wz} & o_{wz} & a_{wz} \end{bmatrix} = \begin{bmatrix} 0 & -\frac{\sqrt{3}}{2} & \frac{1}{2} \\ \frac{1}{\sqrt{2}} & \frac{1}{2\sqrt{2}} & \frac{\sqrt{3}}{2\sqrt{2}} \\ -\frac{1}{\sqrt{2}} & \frac{1}{2\sqrt{2}} & \frac{\sqrt{3}}{2\sqrt{2}} \end{bmatrix}$$

$$\theta_4 = \arctan\left(\frac{n_{wy}}{n_{wx}}\right) = \text{atan2}\left(\frac{1}{\sqrt{2}}, 0\right) = 90^\circ$$

$$\theta_5 = \arctan\left(\frac{-n_{wz}}{C_4 n_{wx} + S_4 n_{wy}}\right) = \text{atan2}\left(\frac{1}{\sqrt{2}}, 0 + \frac{1}{\sqrt{2}}\right) = 45^\circ$$

$$\alpha_6 = \arctan\left(\frac{S_4 a_{wx} - C_4 a_{wy}}{-S_4 o_{wx} + C_4 o_{wy}}\right) = \arctan\left(\frac{1 * \frac{1}{2} - 0 * \frac{\sqrt{3}}{2\sqrt{2}}}{-1 * \left(-\frac{\sqrt{3}}{2}\right) + 0 * \frac{1}{2\sqrt{2}}}\right) = \text{atan2}\left(\frac{1}{\sqrt{3}}\right) = 30^\circ$$

2.

Mechanics of manipulators 3

Geometrical model

Inverse Kinematics (Inverse Kinematic Problem)