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### WHEEL MOBILE ROBOTS LECTURE- 02 - KINEMATICS

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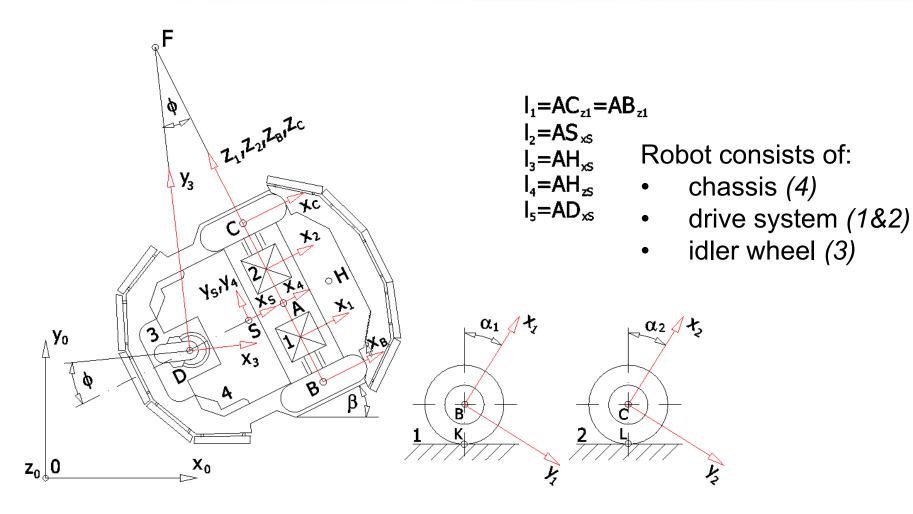


#### **Mobile robots - kinematics**



- Kinematics of arbitrarily selected point belonging to a particular section of the system can be analyzed with the use of socalled kinematic equations
- Each movable part must be connected with







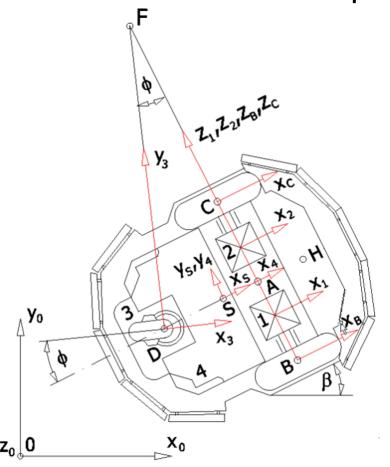
Proper coordinate system was connected with particular parts of the model:

- chassis (4) and x<sub>4</sub>y<sub>4</sub>z<sub>4</sub> coordinate system (CS) with the origin in the mass center of the part
- x<sub>1</sub>y<sub>1</sub>z<sub>1</sub> and x<sub>2</sub>y<sub>2</sub>z<sub>2</sub> CSs are connected with driving systems with origins in points B and C
- x<sub>0</sub>y<sub>0</sub>z<sub>0</sub> CS is stationary coordinate system and is base frame of reference

Kinematic description of the model is based on equations for characteristic points of the robot and assumes that it travels with constant velocity of the point A  $V_A$ 



Kinematic equation for point H has form of:



$$\bar{r}_H = T_{4,0,H} \bar{\rho}_H$$



Transformation matrix of the frame of reference  $x_4y_4z_4$  to  $x_0y_0z_0$  for point H has form of:

$$T_{4,0,H} = \begin{bmatrix} \cos(\beta) & -\sin(\beta) & 0 & x_A + l_3 \cos(\beta) \\ \sin(\beta) & \cos(\beta) & 0 & y_A + l_3 \sin(\beta) \\ 0 & 0 & 1 & r_1 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

Positioning vector of the point H with reference to the  $\mathbf{x_4y_4z_4}$  has form of:  $\rho_H = \begin{bmatrix} 0 \\ 0 \\ -l_4 \end{bmatrix}$ 



After evaluation of the formula  $\bar{r}_H = T_{4.0,H} \bar{\rho}_H$ we obtained equation of motion of the point H written in two equivalent forms:

$$r_{H} = \begin{bmatrix} x_{A} + l_{3} \cos(\beta) \\ y_{A} + l_{3} \sin(\beta) \\ r_{1} - l_{4} \\ 1 \end{bmatrix}$$

$$r_{H} = \begin{bmatrix} x_{A} + l_{3} \cos(\beta) \\ y_{A} + l_{3} \sin(\beta) \\ r_{1} - l_{4} \\ 1 \end{bmatrix} \begin{bmatrix} x_{H} \\ y_{H} \\ z_{H} \\ 1 \end{bmatrix} = \begin{bmatrix} x_{A} + l_{3} \cos(\beta) \\ y_{A} + l_{3} \sin(\beta) \\ r_{1} - l_{4} \\ 1 \end{bmatrix}$$



In the next step the equation for the circular path are presented:

$$x_{H} = R \sin(\phi)$$

$$y_{H} = R(1 - \cos(\phi))$$

$$z_{H} = r_{1} - l_{4}$$

After comparison of the equation of motion with path formulae we get:

$$R\sin(\phi) = x_A + l_3\cos(\beta)$$
$$R(1-\cos(\phi) = y_A + l_3\sin(\beta)$$



Differentiating with respect to time equations for point H

$$R\sin(\phi) = x_A + l_3\cos(\beta) \& R(1-\cos(\phi)) = y_A + l_3\sin(\beta)$$

we obtain equation for speed of the point H along x and y axis

$$\dot{x}_A - l_3 \dot{\beta} \sin(\beta) - R \dot{\phi} \cos(\phi) = 0$$

$$\dot{y}_A + l_3 \beta \cos(\beta) - R \dot{\phi} \sin(\phi) = 0$$



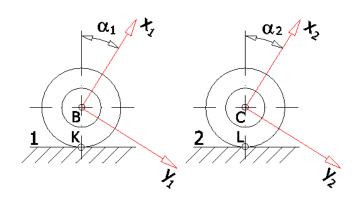
Next characteristic point is point A for which constant speed was assumed and projection of speed vectors on to X and Y axis of the base reference frame was made.

$$\dot{x}_A - v_A \cos(\beta) = 0$$
$$\dot{y}_A - v_A \sin(\beta) = 0$$



To fully describe parameters of motion of our structure we need angular velocities and rotation angles of the wheels (1&2).

Those velocities are derived from equations for velocity of the tangent points between wheel and ground (assuming no slip)



for wheel 1:

$$\overline{r}_K = T_{4,0,K} T_{1,4} \overline{\rho}_K$$



Transformation matrix of the frame of reference  $x_4y_4z_4$  to  $x_0y_0z_0$  for point K has form of:

$$T_{4,0,K} = \begin{bmatrix} \cos(\beta) & -\sin(\beta) & 0 & x_A + l_1 \sin(\beta) \\ \sin(\beta) & \cos(\beta) & 0 & y_A - l_1 \cos(\beta) \\ 0 & 0 & 1 & r_1 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$



Transformation matrix of the frame of reference  $x_1y_1z_1$  to  $x_4y_4z_4$  for point K has form of:

$$T_{1,4} = \begin{bmatrix} \sin(\alpha_1) & \cos(\alpha_1) & 0 & 0 \\ 0 & 0 & 1 & 0 \\ \cos(\alpha_1) & -\sin(\alpha_1) & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$



Positioning vector for the point K with respect to  $\mathbf{x_1y_1z_1}$  reference frame has form of:

$$\rho_K = \begin{bmatrix} -r_1 \cos(\alpha_1) \\ r_1 \sin(\alpha_1) \\ 0 \\ 1 \end{bmatrix}$$

After differentiating of equation of motion for the point K we get:

$$\overline{v}_K = \dot{T}_{4,0,K} \dot{T}_{1,4} \overline{\rho}_K$$



After substitution of all part of the equation of motion for point K we get equations for velocities for point K

$$\begin{bmatrix} \dot{x}_K \\ \dot{y}_K \\ \dot{z}_K \\ 0 \end{bmatrix} = \begin{bmatrix} \dot{x}_A - r_1 \dot{\alpha}_1 \cos(\beta) + l_1 \dot{\beta} \cos(\beta) \\ \dot{y}_A - r_1 \dot{\alpha}_1 \sin(\beta) + l_1 \dot{\beta} \sin(\beta) \\ 0 \\ 0 \end{bmatrix}$$



Having in mind the fact that  $V_K = 0$  (no-slip condition) in scalar form we get:

$$\dot{x}_A - r_1 \dot{\alpha}_1 \cos(\beta) + l_1 \dot{\beta} \cos(\beta)$$

$$\dot{y}_A - r_1 \dot{\alpha}_1 \sin(\beta) + l_1 \dot{\beta} \sin(\beta)$$



For the second wheel we proceed in similar manner.

The equation for motion of the point L (tangent point between 2 wheel and the ground) was derived:

$$\bar{r}_L = T_{4,0,L} T_{2,4} \bar{\rho}_L$$



Transformation matrix of the frame of reference  $x_4y_4z_4$  to  $x_0y_0z_0$  for point L has form of:

$$T_{4,0,L} = \begin{bmatrix} \cos(\beta) & -\sin(\beta) & 0 & x_A - l_1 \sin(\beta) \\ \sin(\beta) & \cos(\beta) & 0 & y_A + l_1 \cos(\beta) \\ 0 & 0 & 1 & r_2 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$



Transformation matrix of the frame of reference  $x_2y_2z_2$  to  $x_4y_4z_4$  for point L has form of:

$$T_{2,4} = \begin{bmatrix} \sin(\alpha_2) & \cos(\alpha_2) & 0 & 0 \\ 0 & 0 & 1 & 0 \\ \cos(\alpha_2) & -\sin(\alpha_2) & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$



Positioning vector for the point L with respect to  $\mathbf{x_2y_2z_2}$  reference frame has form of:

$$\rho_L = \begin{bmatrix} -r_2 \cos(\alpha_2) \\ r_2 \sin(\alpha_2) \\ 0 \\ 1 \end{bmatrix}$$

After differentiating of equation of motion for the point L we get:

$$\overline{v}_L = \dot{T}_{4,0,L} \dot{T}_{2,4} \overline{\rho}_L$$



After substitution of all part of the equation of motion for point L we get equations for velocities for point L

$$\begin{bmatrix} \dot{x}_L \\ \dot{y}_L \\ \dot{z}_L \\ 0 \end{bmatrix} = \begin{bmatrix} \dot{x}_A - r_2 \dot{\alpha}_2 \cos(\beta) - l_1 \dot{\beta} \cos(\beta) \\ \dot{y}_A - r_2 \dot{\alpha}_2 \sin(\beta) - l_1 \dot{\beta} \sin(\beta) \\ 0 \\ 0 \end{bmatrix}$$



Having in mind the fact that  $V_L = 0$  (no-slip condition) in scalar form we get:

$$\dot{x}_A - r_2 \dot{\alpha}_2 \cos(\beta) - l_1 \dot{\beta} \cos(\beta)$$
$$\dot{y}_A - r_2 \dot{\alpha}_2 \sin(\beta) - l_1 \dot{\beta} \sin(\beta)$$



Summing up, we obtained system of equations describing motion of the two-wheeled robot:

$$\dot{x}_A - l_3 \dot{\beta} \sin(\beta) - R \dot{\phi} \cos(\phi) = 0$$

$$\dot{y}_A + l_3 \dot{\beta} \cos(\beta) - R \dot{\phi} \sin(\phi) = 0$$

$$\dot{x}_A - v_A \cos(\beta) = 0$$

$$\dot{y}_A - v_A \sin(\beta) = 0$$

$$\dot{x}_A - r_1 \dot{\alpha}_1 \cos(\beta) + l_1 \dot{\beta} \cos(\beta) = 0$$

#### calculation of:

- displacement
- velocity
- acceleration
- angle of rotation
- angular velocities
- solving simple and inverse kinematic problems

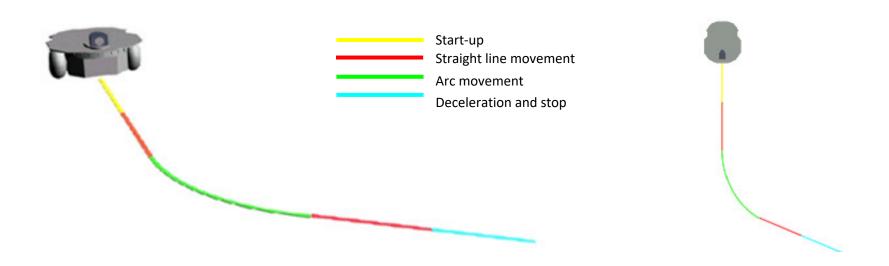
### $\sqrt{l_5^2 \dot{\beta}^2 + v_4^2} - r_3 \dot{\alpha}_3 = 0$

#### calculation of:

 kinematic parameters of idler wheel



Based on previously derived equations of motion for our robot we conduct simulation of inverse kinematic problem for proposed path:



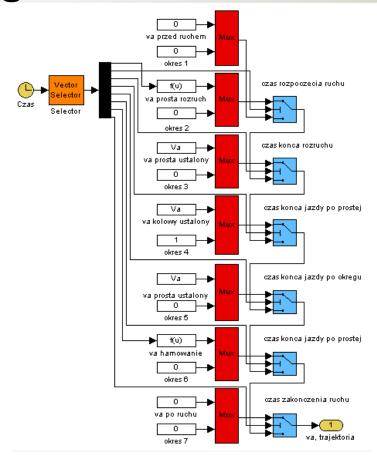


We assume working conditions and physical features of the robot:

- Point A velocity v<sub>A</sub>=0.3 [m/s],
- Start-up 2 [s],
- Straight line movement 0.5 [s],
- Acr movement 4.7 [s] with R=1.5 [m],
- Angle of chassis rotation 0°-54°,
- Straight line movement 0.5 [s],
- Deceleration and stop 2 [s].

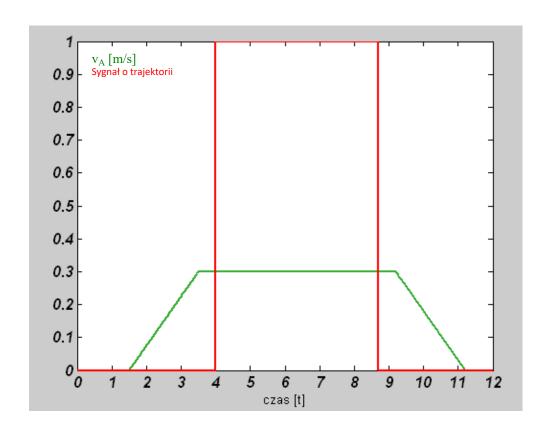
l <sub>1</sub> [m]	l <sub>3</sub> [m]	l <sub>4</sub> [m]	l <sub>5</sub> [m]	r <sub>1</sub> [m]	r <sub>2</sub> [m]	r <sub>3</sub> [m]
0.163	0.07	0.2	0.07	0.0825	0.0825	0.035





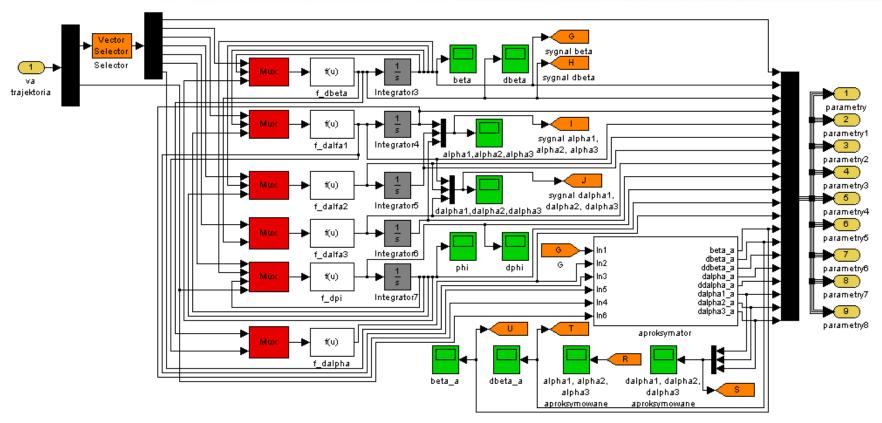
Speed and trajectory generator model





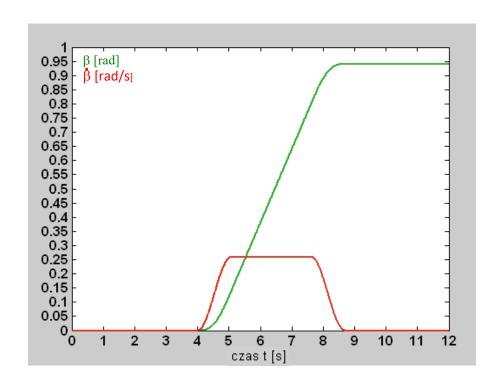
Output from speed and trajectory generator model





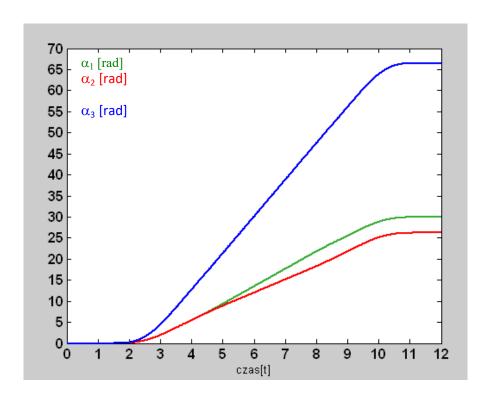
Model of inverse kinematic solver (as input there is trajectory from previously discused model)





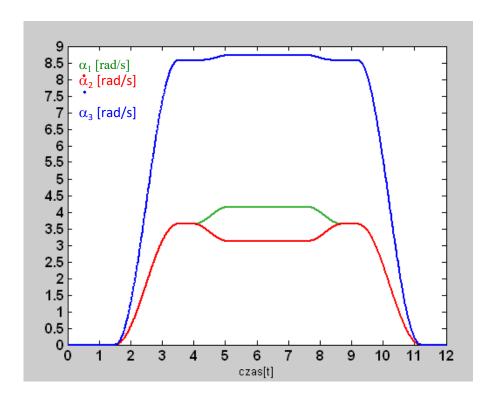
Output for the angle of rotation of the chassis and its angular velocity





Output for the angle of rotation of wheels 1,2 and 3





Output for the angular speed of wheels 1,2 and 3



Based on the results from inverse kinematic problem we can check correctness of our results by plotting the path as a result of simple kinematic problem.

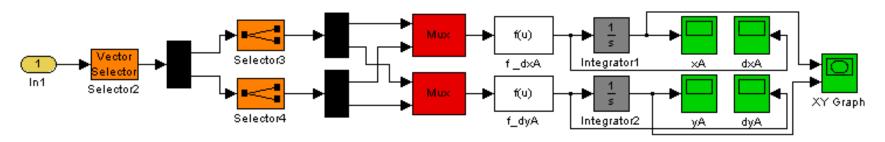


fig. Model solving simple kinematics problem



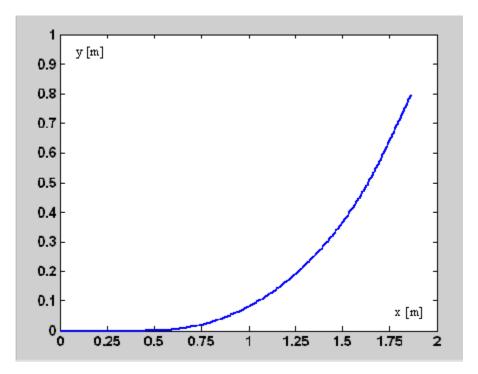


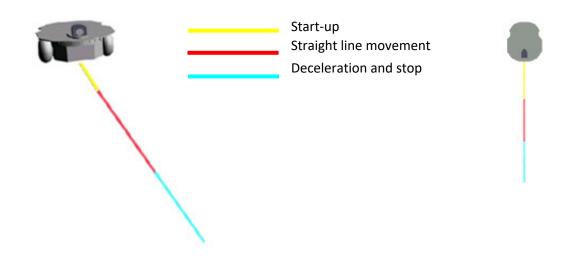
Fig. Output from simple kinematics solver - path

As a result we obtain previously defined path for inverse kinematics problem. That means our model is made in a proper way.

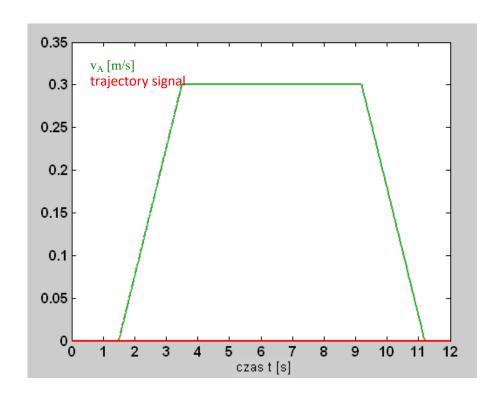


# Simulation of the inverse kinematic problem with the use of Matlab Simulink software (straight line path)

### Lets assume different path – straight line

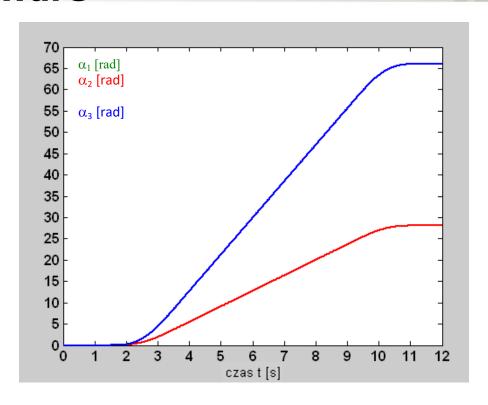






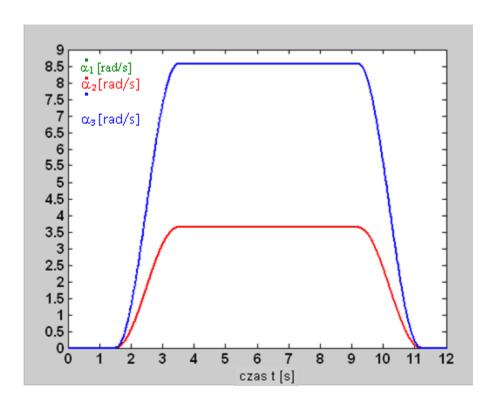
Output from speed and trajectory generator model





Output for the angle of rotation of wheels 1,2 and 3





Output for the angular speed of wheels 1,2 and 3



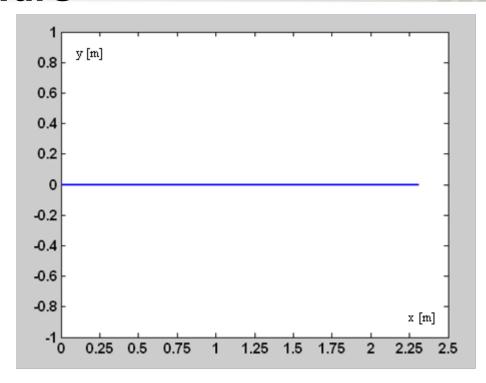


Fig. Output from simple kinematics solver - path

As a result we obtain previously defined path for inverse kinematics problem. That means our model is made in a proper way.



### **THANK YOU**