

MECHATRONIC DESIGN

Lab 1: Introduction to Finite Difference (FD) method

The goal of the first laboratory is to approximate solutions to differential equations, i.e., to find a function (or some discrete approximation to this function) that satisfies a given relationship between various of its derivatives on some given region of space and/or time, along with some boundary conditions along the edges of this domain. In general, this is a difficult problem, and only rarely can an analytic formula be found for the solution. **A finite difference method proceeds by replacing the derivatives in the differential equations with finite difference approximations.** This gives a large but finite algebraic system of equations to be solved in place of the differential equation, something that can be done on a computer.

Before tackling this problem, we first consider the more basic question of how we can approximate the derivatives of a known function by finite difference formulas based only on values of the function itself at discrete points. Besides providing a basis for the later development of finite difference methods for solving differential equations, this allows us to investigate several key concepts such as the *order of accuracy* of an approximation in the simplest possible setting.

Let $u(x)$ represent a function of one variable that, unless otherwise stated, will always be assumed to be smooth, meaning that we can differentiate the function several times and each derivative is a well-defined bounded function over an interval containing a particular point of interest \bar{x} .

Suppose we want to approximate $\frac{\partial u(\bar{x})}{\partial \bar{x}}$ by a finite difference approximation based only on values of u at a finite number of points near \bar{x} . One obvious choice would be to use

$$\frac{\partial u(\bar{x})}{\partial \bar{x}} \approx \frac{u(\bar{x} + \Delta x) - u(\bar{x})}{\Delta x} \quad (1)$$

for some small value of Δx . Note that $\frac{\partial u(\bar{x})}{\partial \bar{x}}$ is the slope of the line interpolating u at the points \bar{x} and $\bar{x} + \Delta x$ (see Figure 1.)

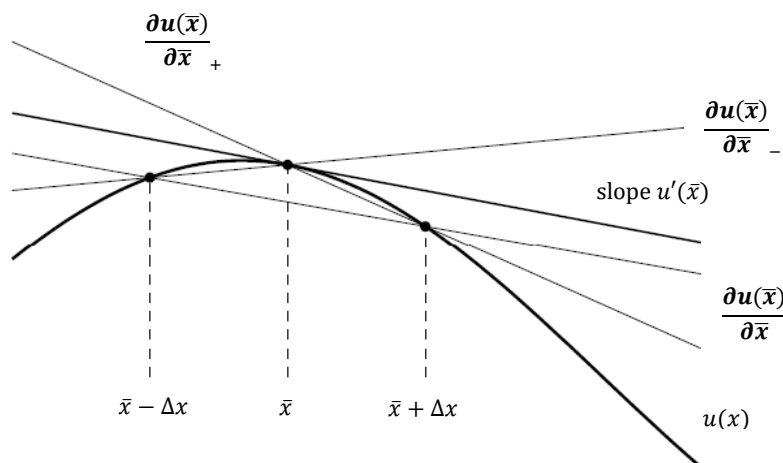


Figure. 1. Various approximations to $\frac{\partial u(\bar{x})}{\partial \bar{x}}$ interpreted as the slope of secant lines.

Equation (1) is a **one-sided approximation** to $\frac{\partial u(\bar{x})}{\partial \bar{x}}$ since $u(x)$ is evaluated only at values of $x \geq \bar{x}$. Another one-sided approximation would be

$$\frac{\partial u(\bar{x})}{\partial \bar{x}} \approx \frac{u(\bar{x}) - u(\bar{x} - \Delta x)}{\Delta x} \quad (2)$$

Each of these formulas gives a *first order accurate* approximation to $u'(\bar{x})$, meaning that the size of the error is roughly proportional to Δx itself.

Another possibility is to use the **centered approximation**

$$\frac{\partial u(\bar{x})}{\partial \bar{x}} \approx \frac{u(\bar{x} + \Delta x) - u(\bar{x} - \Delta x)}{2\Delta x} \quad (3)$$

Equation (3) is the slope of the line interpolating u at $\bar{x} - \Delta x$ and $\bar{x} + \Delta x$ and is simply the average of the two one-sided approximations defined above using Eqs. (1) and (2). **From Figure 1 it should be clear that we would expect $\frac{\partial u(\bar{x})}{\partial \bar{x}}$ to give a better approximation than either of the one-sided approximations.** In fact, this gives a second order accurate approximation - the error is proportional to Δx^2 and hence is much smaller than the error in a first order approximation when Δx is small ($\Delta x < 1$).

How are the above finite difference approximations and truncation errors analyzed? The standard approach is to expand each of the function values of u in a Taylor series about the point \bar{x} , e.g.,

$$u(\bar{x} + \Delta x) = u(\bar{x}) + \Delta x \cdot \frac{\partial u(\bar{x})}{\partial \bar{x}} + \frac{1}{2} \Delta x^2 \cdot \frac{\partial^2 u(\bar{x})}{\partial \bar{x}^2} + \frac{1}{6} \Delta x^3 \cdot \frac{\partial^3 u(\bar{x})}{\partial \bar{x}^3} + O(\Delta x^4) \quad (4)$$

$$u(\bar{x} - \Delta x) = u(\bar{x}) - \Delta x \cdot \frac{\partial u(\bar{x})}{\partial \bar{x}} + \frac{1}{2} \Delta x^2 \cdot \frac{\partial^2 u(\bar{x})}{\partial \bar{x}^2} - \frac{1}{6} \Delta x^3 \cdot \frac{\partial^3 u(\bar{x})}{\partial \bar{x}^3} + O(\Delta x^4) \quad (5)$$

Using Equation (4) allows us to compute that

$$\frac{\partial u(\bar{x})}{\partial \bar{x}}_+ \approx \frac{u(\bar{x} + \Delta x) - u(\bar{x})}{\Delta x} \approx \frac{\partial u(\bar{x})}{\partial \bar{x}} + \frac{1}{2} \Delta x \cdot \frac{\partial^2 u(\bar{x})}{\partial \bar{x}^2} + \frac{1}{6} \Delta x^2 \cdot \frac{\partial^3 u(\bar{x})}{\partial \bar{x}^3} + O(\Delta x^3) \quad (6)$$

Recall that \bar{x} is a fixed point so that $\frac{\partial^2 u(\bar{x})}{\partial \bar{x}^2}$, $\frac{\partial^3 u(\bar{x})}{\partial \bar{x}^3}$, etc., are fixed constants independent of Δx . They depend on u of course, but the function is also fixed as we vary Δx .

For Δx sufficiently small, the error will be dominated by the first term $\frac{1}{2} \Delta x \cdot \frac{\partial^2 u(\bar{x})}{\partial \bar{x}^2}$ and all the other terms will be negligible compared to this term, so we expect the error to behave roughly like a constant times Δx , where the constant has the value $\frac{1}{2} \frac{\partial^2 u(\bar{x})}{\partial \bar{x}^2}$.

Similarly, from Equation (5) we can compute that the error in $D_- u(\bar{x})$ is

$$\frac{\partial u(\bar{x})}{\partial \bar{x}}_- \approx \frac{u(\bar{x}) - u(\bar{x} - \Delta x)}{\Delta x} \approx \frac{\partial u(\bar{x})}{\partial \bar{x}} + \frac{1}{2} \Delta x \cdot \frac{\partial^2 u(\bar{x})}{\partial \bar{x}^2} - \frac{1}{6} \Delta x^2 \cdot \frac{\partial^3 u(\bar{x})}{\partial \bar{x}^3} + O(\Delta x^3). \quad (7)$$

Subtracting Equation (5) from (4) gives

$$u(\bar{x} + \Delta x) - u(\bar{x} - \Delta x) = 2\Delta x \cdot \frac{\partial u(\bar{x})}{\partial \bar{x}} + \frac{1}{3} \Delta x^3 \cdot \frac{\partial^3 u(\bar{x})}{\partial \bar{x}^3} + O(\Delta x^5) \quad (8)$$

so the central difference approximation is

$$\frac{\partial u(\bar{x})}{\partial \bar{x}} \approx \frac{u(\bar{x} + \Delta x) - u(\bar{x} - \Delta x)}{2\Delta x} \approx \frac{\partial u(\bar{x})}{\partial \bar{x}} + \frac{1}{6} \Delta x^2 \cdot \frac{\partial^3 u(\bar{x})}{\partial \bar{x}^3} + O(\Delta x^4) \quad (9)$$

This confirms the second order accuracy of this approximation. Note that all the odd order terms drop out of the Taylor series expansion (9) for $\frac{\partial u(\bar{x})}{\partial \bar{x}}$. This is typical with centered approximations and typically leads to a higher order approximation.

Approximations to the second order derivative $\frac{\partial^2 u(\bar{x})}{\partial \bar{x}^2}$ can be obtained in an analogous manner (using Taylor series) leading to

$$\frac{\partial^2 u(\bar{x})}{\partial \bar{x}^2} \approx \frac{u(\bar{x} + \Delta x) - 2u(\bar{x}) + u(\bar{x} - \Delta x)}{\Delta x^2} + O(\Delta x^2) \quad (10)$$

The second order mixed derivative $\frac{\partial^2 u(\bar{x}, \bar{y})}{\partial \bar{x} \partial \bar{y}}$ is:

$$\frac{\partial^2 u(\bar{x}, \bar{y})}{\partial \bar{x} \partial \bar{y}} \approx \frac{u(\bar{x} + \Delta x, \bar{y} + \Delta y) - u(\bar{x} - \Delta x, \bar{y} + \Delta y) - u(\bar{x} + \Delta x, \bar{y} - \Delta y) + u(\bar{x} - \Delta x, \bar{y} - \Delta y)}{4\Delta x \Delta y} + O(\Delta x^2, \Delta y^2)$$

Tasks to do:

Task 1:

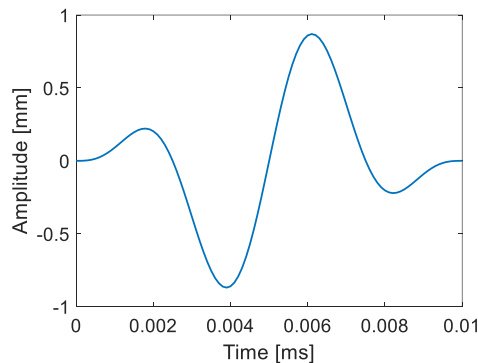
Solve a one-dimensional acoustic wave equation using finite difference method for an **aluminum/copper/steel** rod. Implement a source code in MATLAB to obtain wave displacement in time and space domains. The one-dimensional wave equation is:

$$\frac{\partial^2 u(x, t)}{\partial t^2} = c^2 \frac{\partial^2 u(x, t)}{\partial x^2}, \quad (11)$$

$$c = \sqrt{\frac{E}{\rho}}, \quad 0 \leq x \leq L, \quad t \geq 0$$

where E is Young's modulus, ρ is mass density, L is the length of the rod.

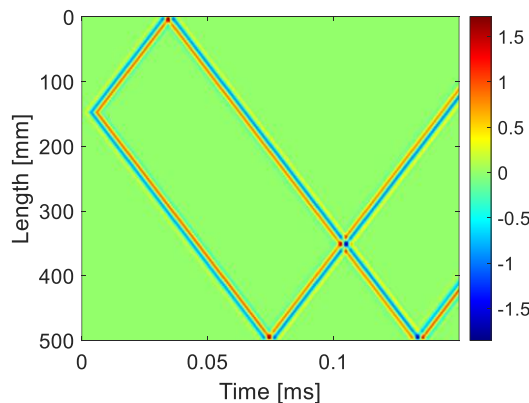
Use the following constant parameters for your calculations: $\Delta x = 1 \text{ mm}$, $\Delta t = 0.12 \text{ } \mu\text{s}$. The excitation signal is a 200 kHz two cycle sine wave modulated by a Hanning window:



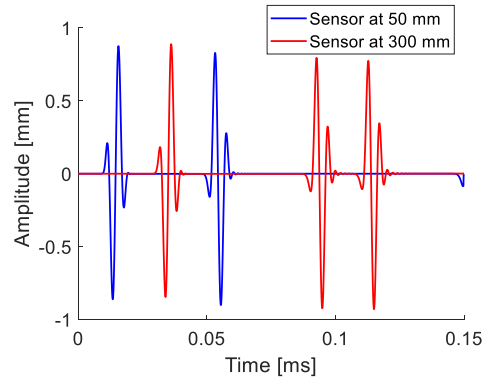
Calculate the wave speed of the simulated wave motion.

Exemplary results:

A spatio-temporal acoustic wave motion data with an excitation located at 150 mm:



Temporal acoustic wave motion data measured at 50 and 300 mm:



Task 2:

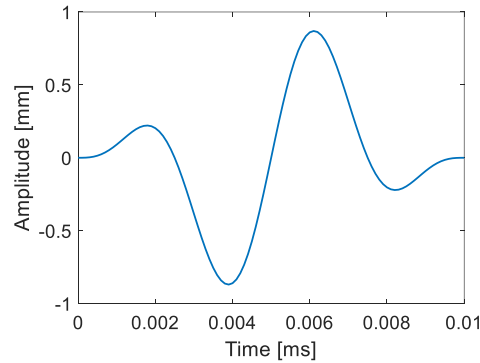
Solve a two-dimensional acoustic wave equation using finite difference method for an **aluminum** plate. Implement a source code in MATLAB to obtain wave displacement in time and space domains. The two-dimensional acoustic wave equation is:

$$\frac{\partial^2 u(x,y,t)}{\partial t^2} = c^2 \left(\frac{\partial^2 u(x,y,t)}{\partial x^2} + \frac{\partial^2 u(x,y,t)}{\partial y^2} \right), \quad (12)$$

$$c = \sqrt{\frac{E}{\rho}}, \quad 0 \leq x \leq L_1, \quad 0 \leq y \leq L_2, \quad t \geq 0$$

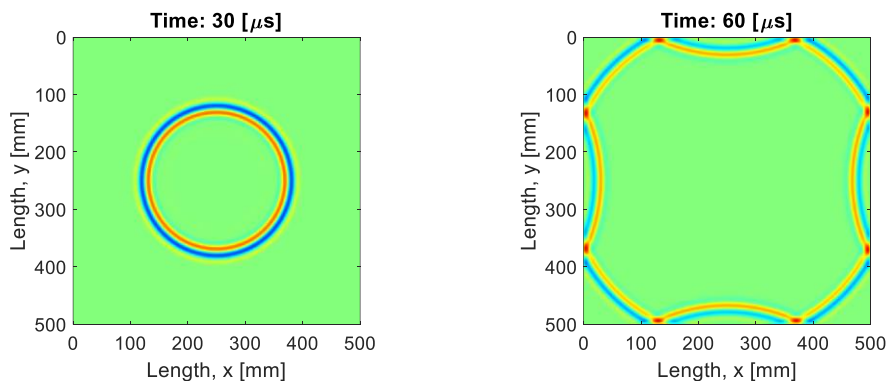
where E is Young's modulus, ρ mass density, L is the length of the rod. Use the following constant parameters for your calculations: $\Delta x = \Delta y = 1 \text{ mm}$, $\Delta t = 0.12 \text{ }\mu\text{s}$.

The excitation signal is a 200 Hz two cycle sine wave modulated by a Hanning window:

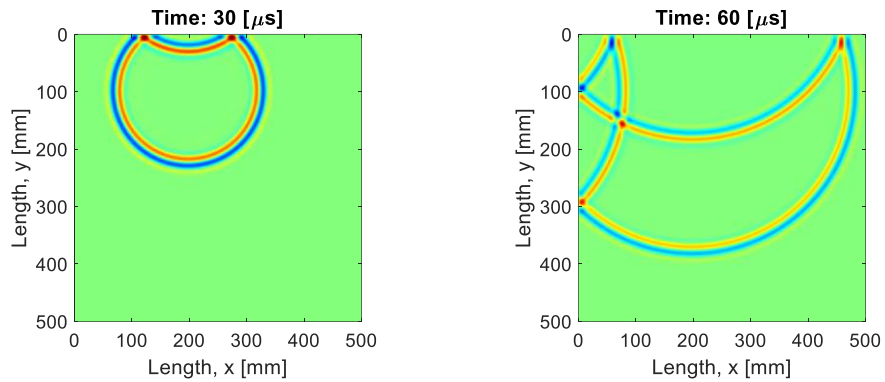


Exemplary results:

Wave motion data for the excitation located in the middle of the plate:

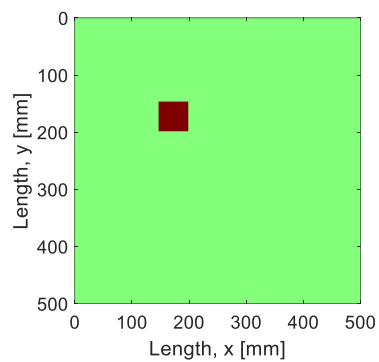


Wave motion data for the excitation located in at the location $x = 200$ mm, $y = 100$ mm:

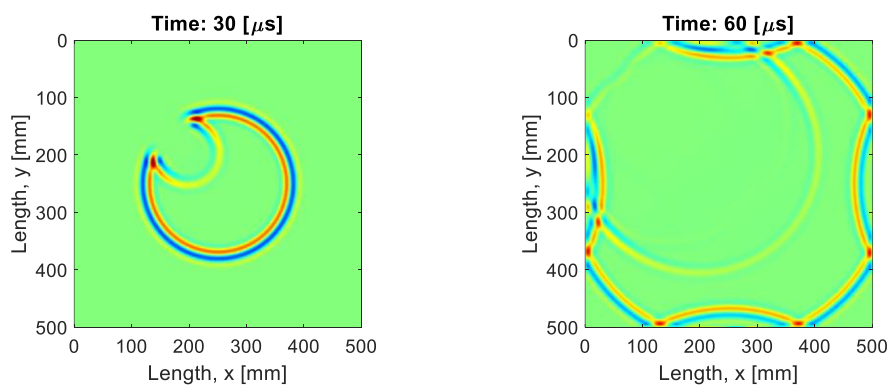


Task 3:

Repeat the simulations from Task 2 with the addition of discontinuity in your model, for example, as:



Exemplary results:



Task 4:

Solve two-dimensional elastodynamic wave equations for an isotropic, linear material using finite difference method for an aluminum plate. Implement a source code in MATLAB to obtain wave displacement in time and space domains.

$$\begin{cases} \rho \frac{\partial^2 u_x}{\partial t^2} = \frac{\partial \tau_{xx}}{\partial x} + \frac{\partial \tau_{xz}}{\partial z} + F_x \\ \rho \frac{\partial^2 u_z}{\partial t^2} = \frac{\partial \tau_{xz}}{\partial x} + \frac{\partial \tau_{zz}}{\partial z} + F_z \end{cases}$$

whereas stress-strain relations are as follow

$$\tau_{xx} = (\lambda + 2\mu) \frac{\partial u_x}{\partial x} + \lambda \frac{\partial u_z}{\partial z}$$

$$\tau_{zz} = (\lambda + 2\mu) \frac{\partial u_z}{\partial z} + \lambda \frac{\partial u_x}{\partial x}$$

$$\tau_{xz} = \mu \left(\frac{\partial u_x}{\partial z} + \frac{\partial u_z}{\partial x} \right)$$

where

ρ density,

μ shear modulus,

λ first Lamé constant

u displacement vector

F force vector

Exemplary results:

