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Mathematical models

Tomas Hanis

Smart Driving Solutions

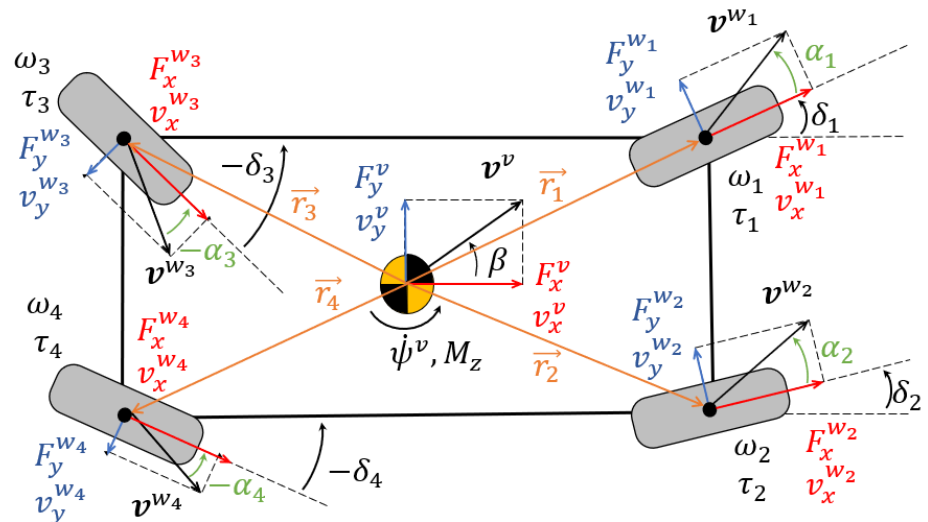
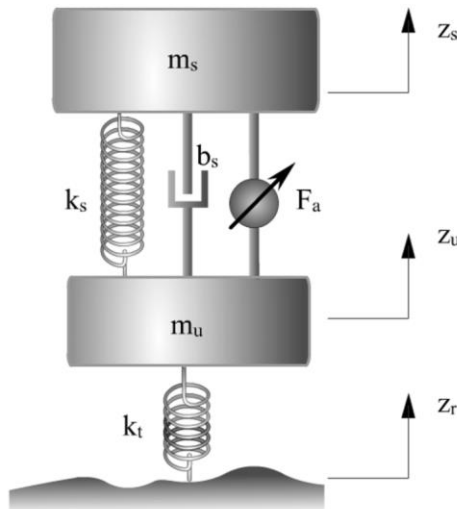
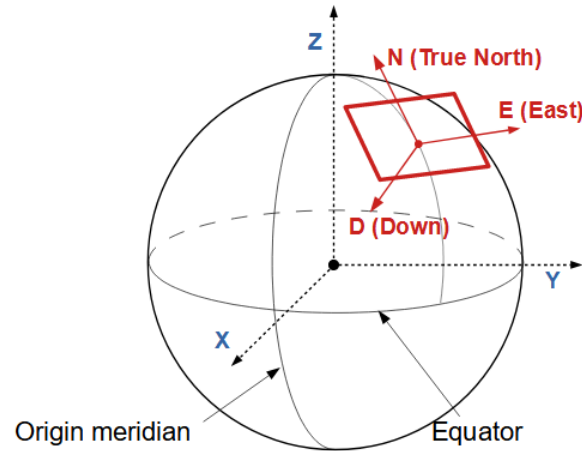
Department of Control Engineering

CTU in Prague - FEE

Coordinate systems

Important points

- Inertial frame – NED
- Vehicle coordinate system
 - Body – Center of Gravity
 - Body – Wheel
- Wheel
 - Contact patch
 - Sprung/Unsprung mass



Vehicle models

Are the forces considered?

- ✗ Kinematic model
- ✓ Dynamic model

Is body motion considered?

- ✗ Single-track model
- ✓ Twin-track model

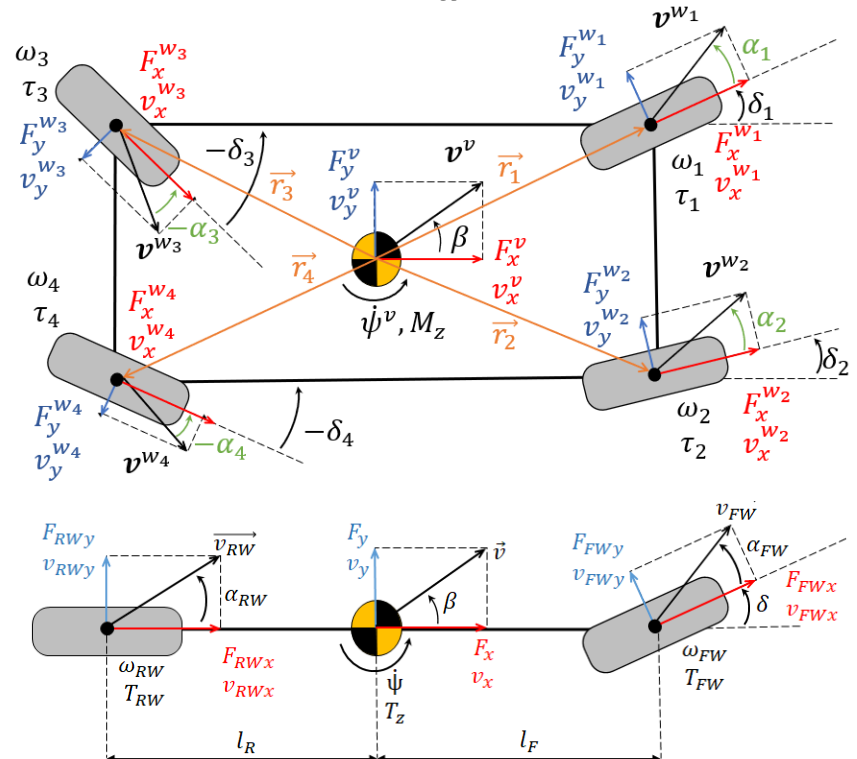
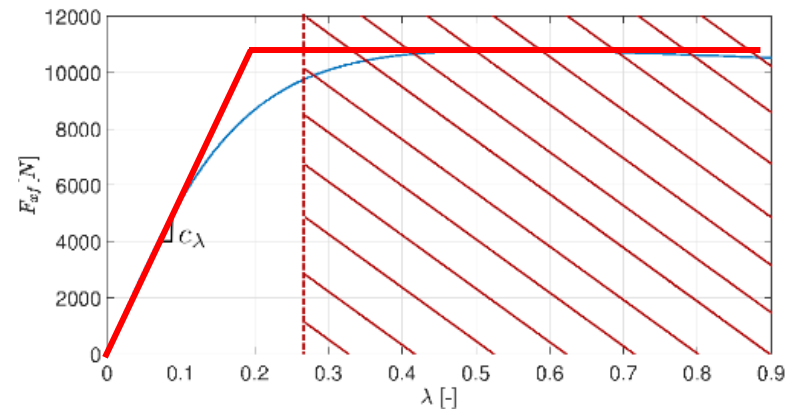
Steering model

- ✗ Parallel steering
- ✓ Ackerman steering
- ✓ Steering allocation

Suspension model

- ✗ Kinematic, Single/Twin-track
- ✓ Quarter/Half/Full model

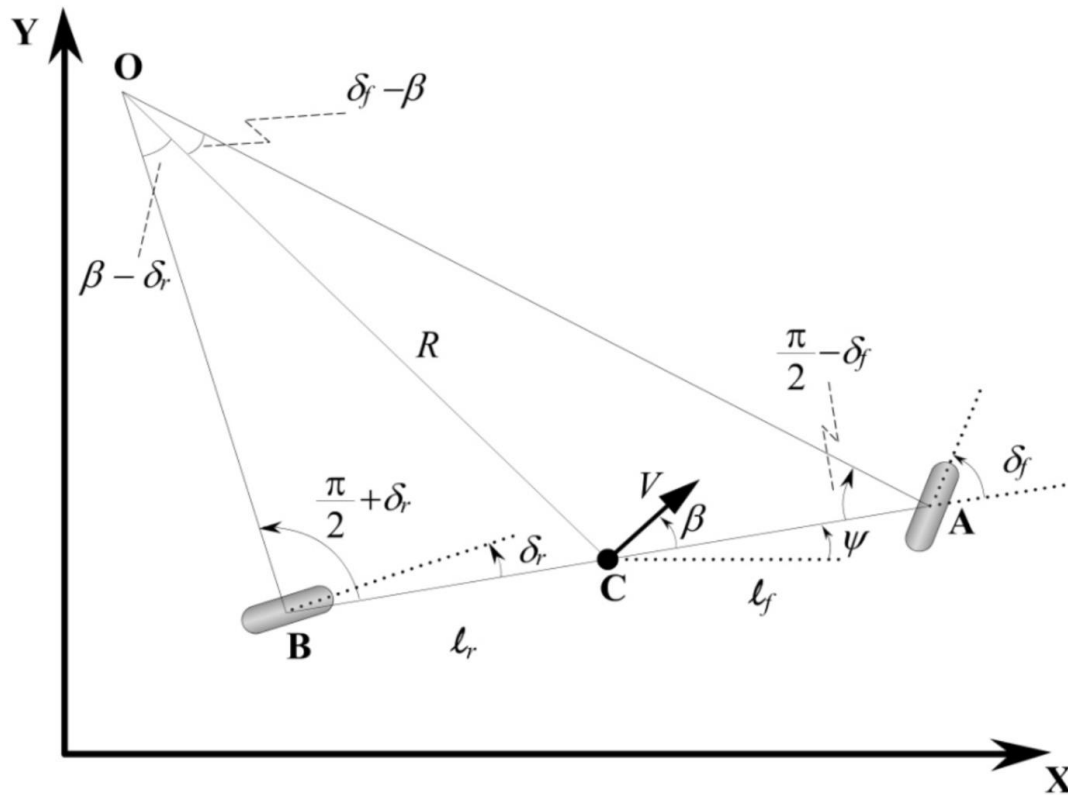
$$\vec{v} = f(F_x, F_y)$$



Kinematic model

Assumptions

- Wheel velocity vectors are in direction of wheels (slow motion, $v < 5 \text{ km/h}$)



$$\dot{X} = V \cos(\psi + \beta)$$

$$\dot{Y} = V \sin(\psi + \beta)$$

$$\dot{\psi} = \frac{V \cos(\beta)}{l_f + l_r} (\tan \delta_f - \tan \delta_r)$$

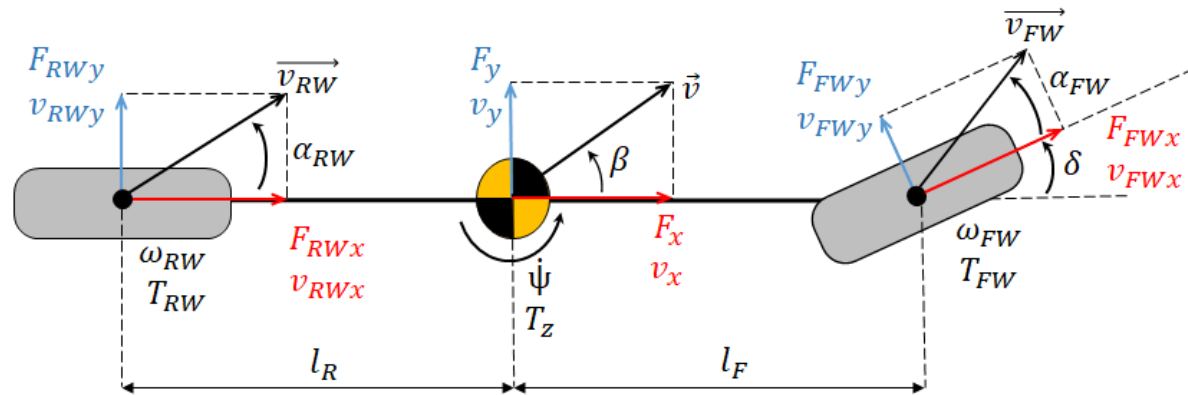
$$\beta = \tan^{-1} \left(\frac{l_r \tan \delta_f + l_f \tan \delta_r}{l_f + l_r} \right)$$



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Single-track model



Inputs

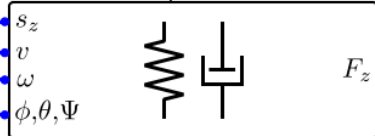
δ
 τ

States

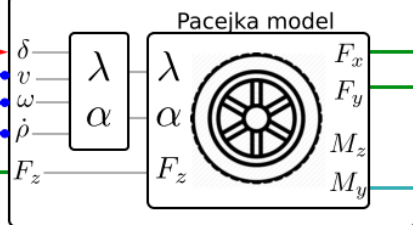
s
 v
 ω
 ϕ, θ, Ψ
 $\dot{\rho}$

Chassis

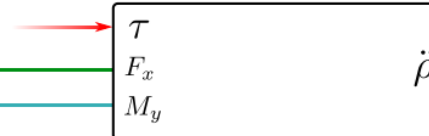
Suspension



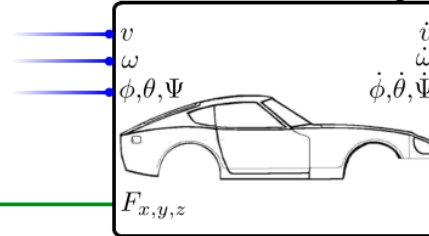
Tire interface



Powertrain



Vehicle Body



State derivatives

v
 \dot{v}
 $\dot{\omega}$
 $\dot{\phi}, \dot{\theta}, \dot{\Psi}$
 $\ddot{\rho}$

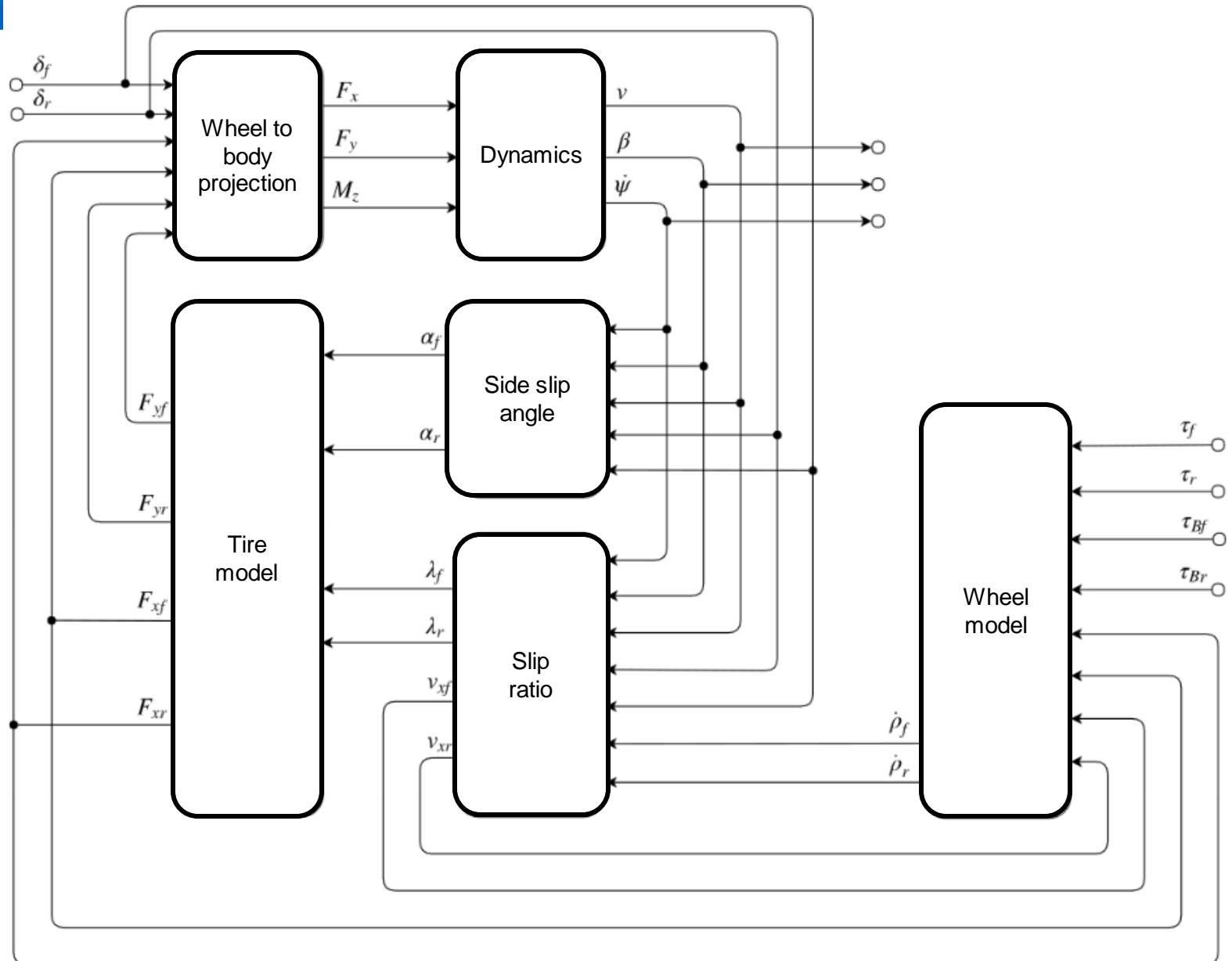
$\frac{1}{s}$



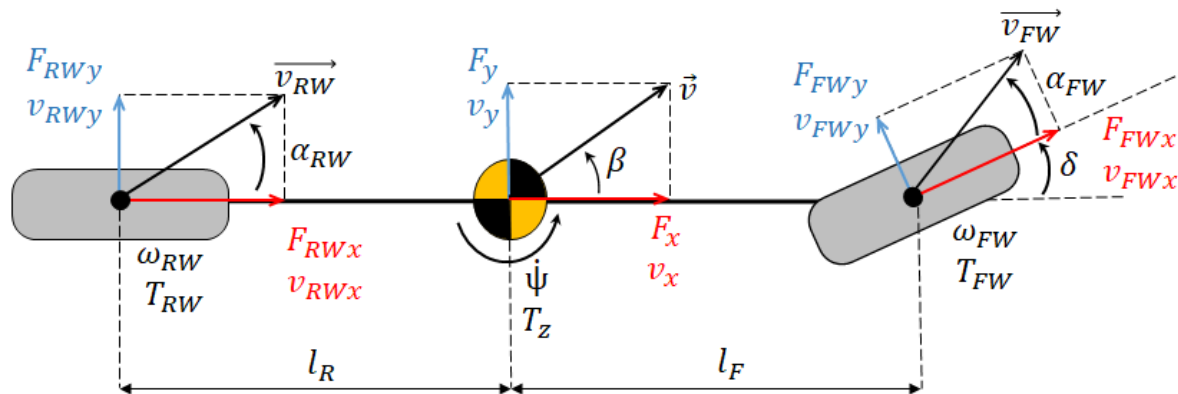
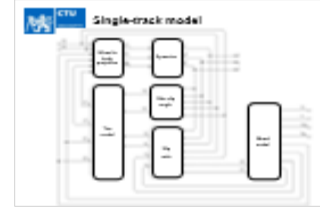
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Single-track model



ST model – dynamics



\vec{v}

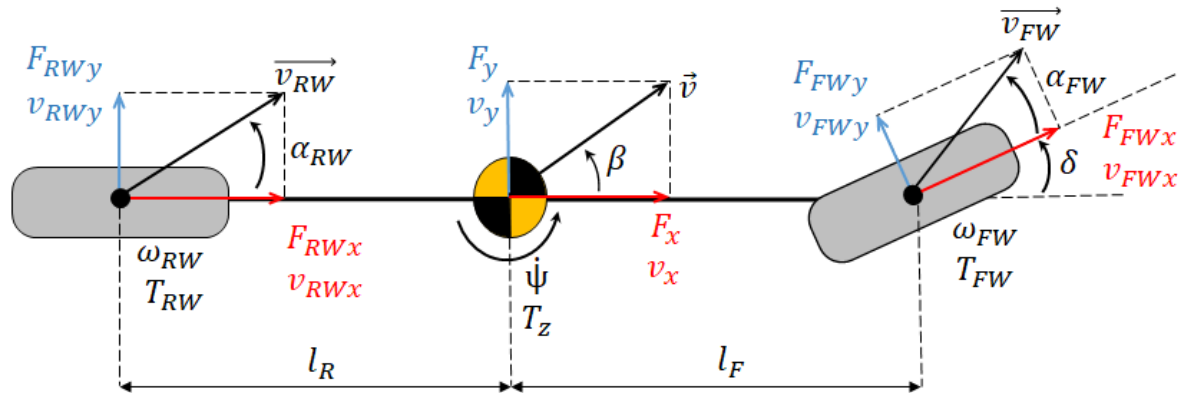
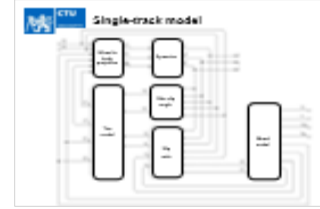
$$\begin{bmatrix} v_x \\ v_y \end{bmatrix} \leftrightarrow \begin{bmatrix} \beta \\ |\vec{v}| \end{bmatrix}$$

$$\begin{aligned} m\dot{v}_x &= F_x \\ m(\dot{v}_y + \dot{\psi}v_x) &= F_y \\ I_z\ddot{\psi} &= T_z \end{aligned}$$

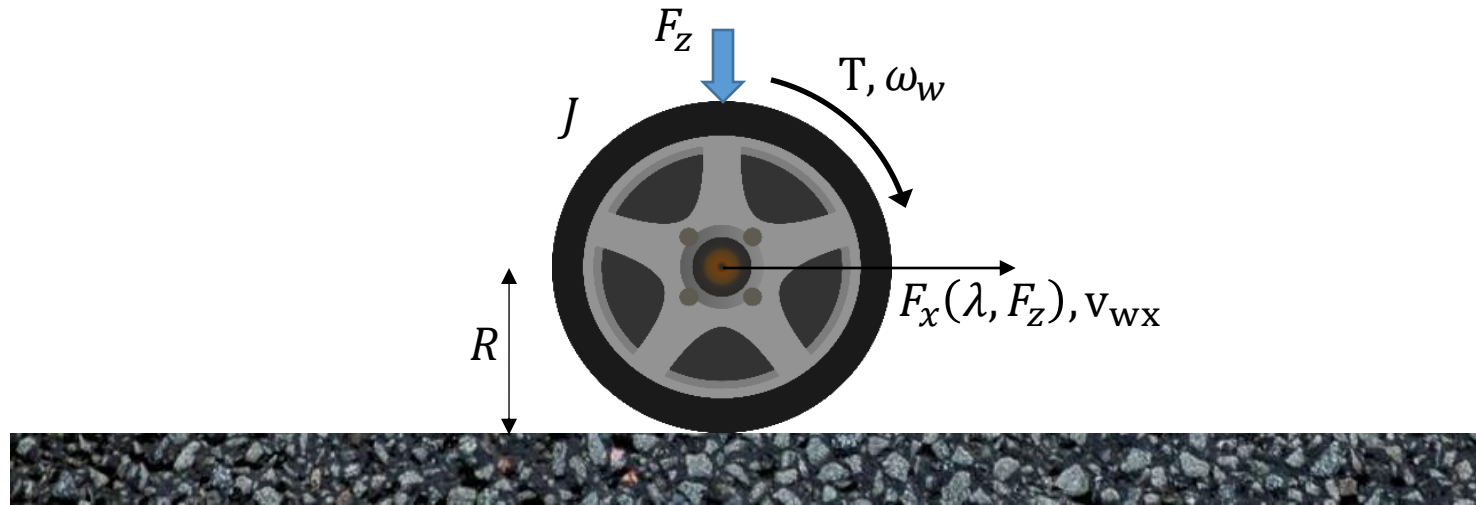
$$\begin{aligned} -m|\vec{v}|(\dot{\beta} + \dot{\psi})\sin\beta + m|\vec{v}|\cos\beta &= F_x \\ m|\vec{v}|(\dot{\beta} + \dot{\psi})\cos\beta + m|\vec{v}|\sin\beta &= F_y \\ I_z\ddot{\psi} &= T_z \end{aligned}$$



ST – Wheel to body projection



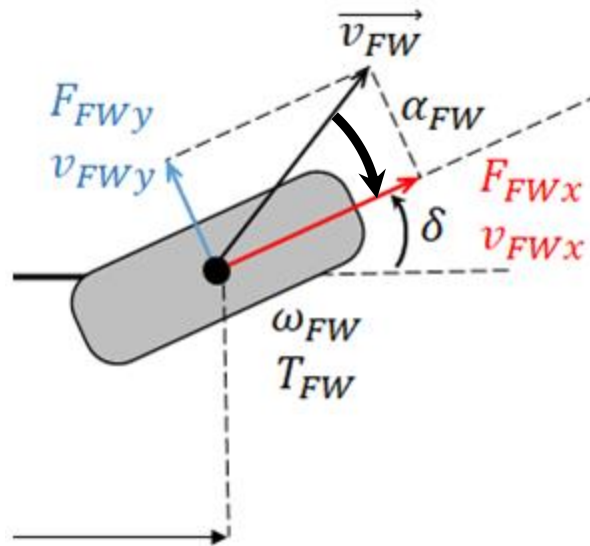
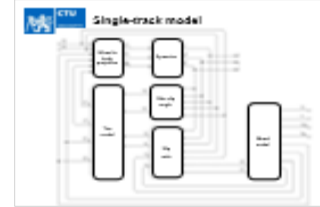
$$\begin{aligned}
 F_{xf} \cos \delta_f + F_{xr} \cos \delta_r - F_{yf} \sin \delta_f - F_{yr} \sin \delta_r &= F_x \\
 F_{yf} \cos \delta_f + F_{yr} \cos \delta_r + F_{xf} \sin \delta_f + F_{xr} \sin \delta_r &= F_y \\
 l_f F_{yf} \cos \delta_f - l_r F_{yr} \cos \delta_r + l_f F_{xf} \sin \delta_f - l_r F_{xr} \sin \delta_r &= T_z
 \end{aligned}$$



$$J\dot{\omega}_w = T - F_{wx}(\lambda, F_z)R - \text{sign}(\omega_w)T_b - k v_{wx}$$



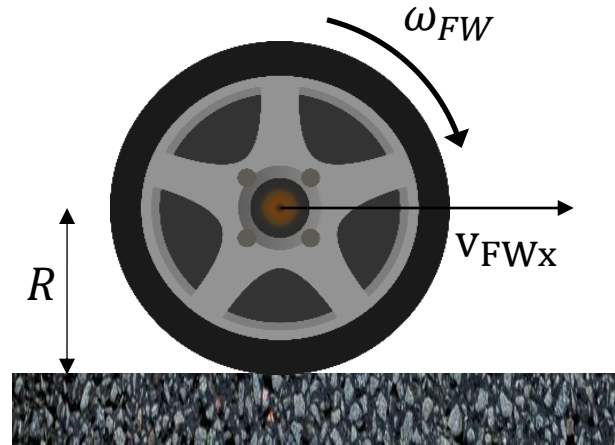
ST – Side slip angle



$$\alpha_{FW} = -\tan^{-1}\left(\frac{v_{FWy}}{v_{FWx}}\right)$$

$$\alpha_{FW} = -\tan^{-1}\left(\frac{(v_y + l_f \dot{\psi}) \cos \delta_f - v_x \sin \delta_f}{(v_y + l_f \dot{\psi}) \sin \delta_f + v_x \cos \delta_f}\right)$$

ST – Slip ratio



$$v_{FWci} = \omega_{FW} \cdot R$$

$$v_{FWx} = (v_y + l_f \psi) \sin \delta_f + v_x \cos \delta_f$$

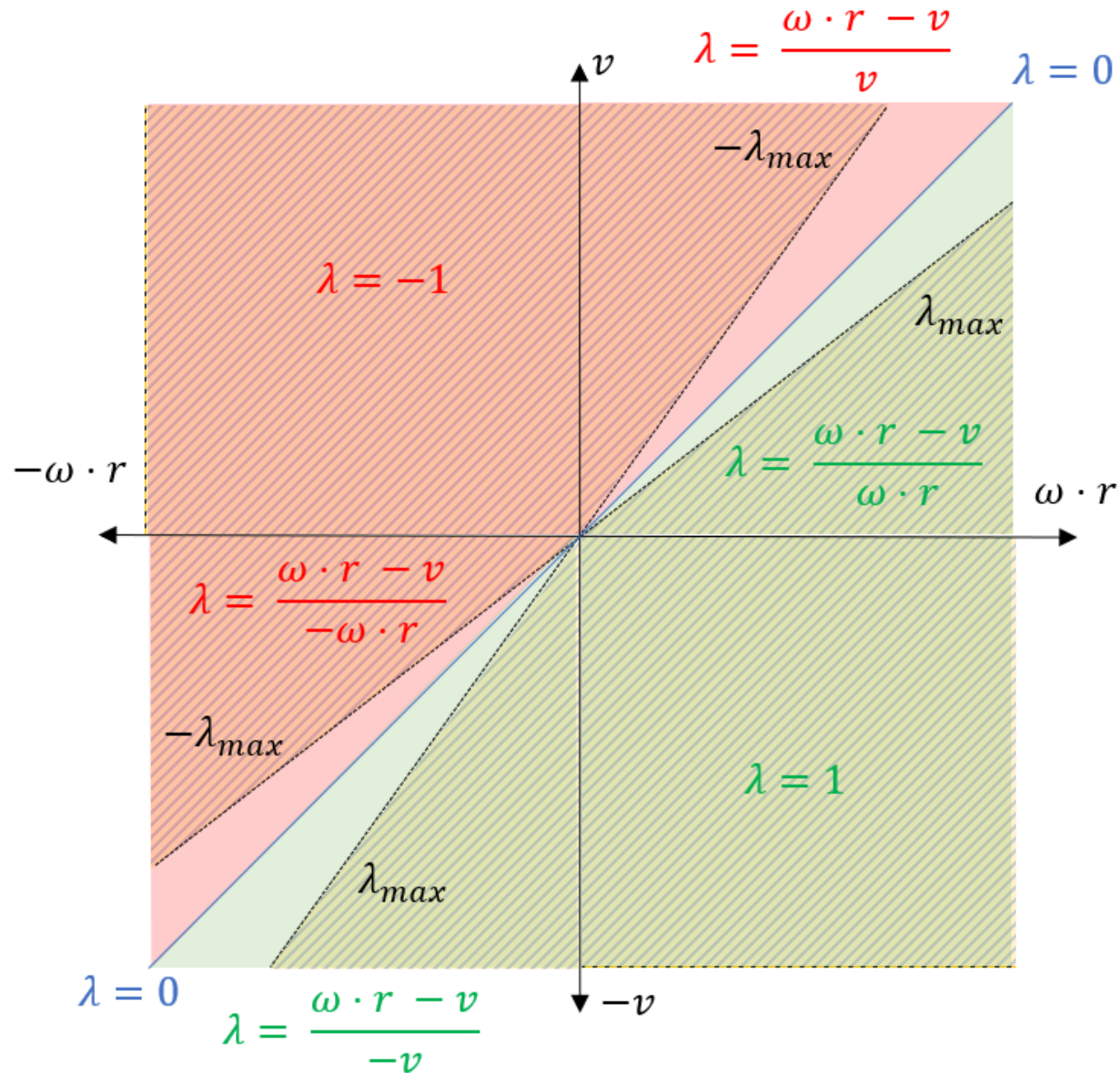
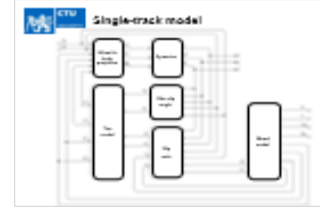
$$\lambda_{FW} = \frac{v_{FWci} - v_{FWx}}{\max(|v_{FWx}|, |v_{FWci}|)}$$



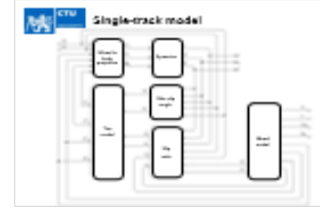
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ST – Slip ratio



ST – Tire model (1)



from experimental
data only

using similarity
method

through simple
physical model

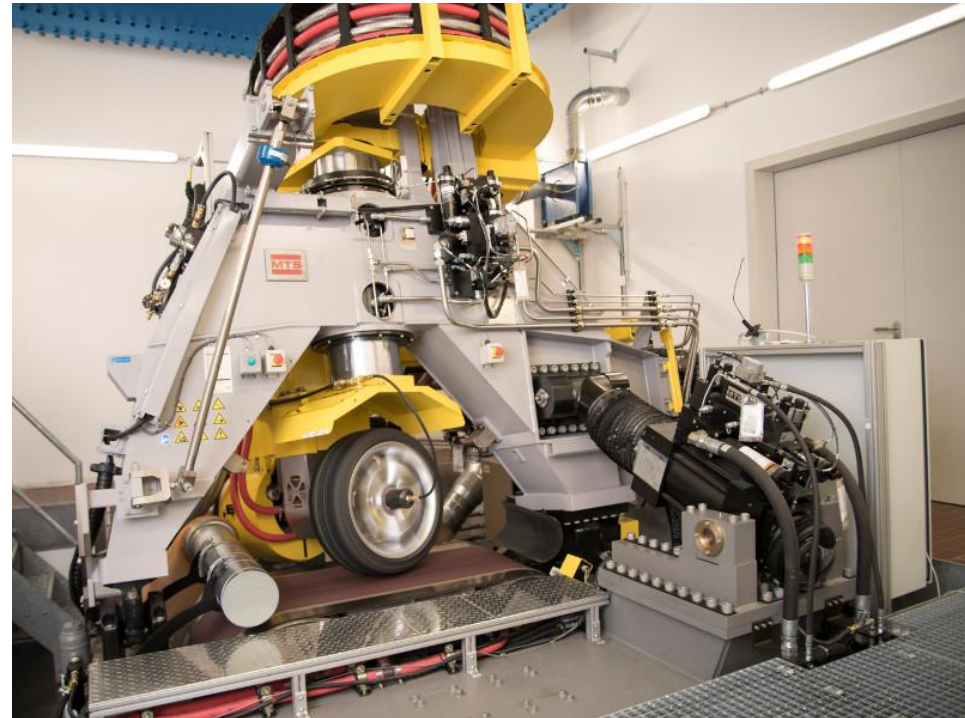
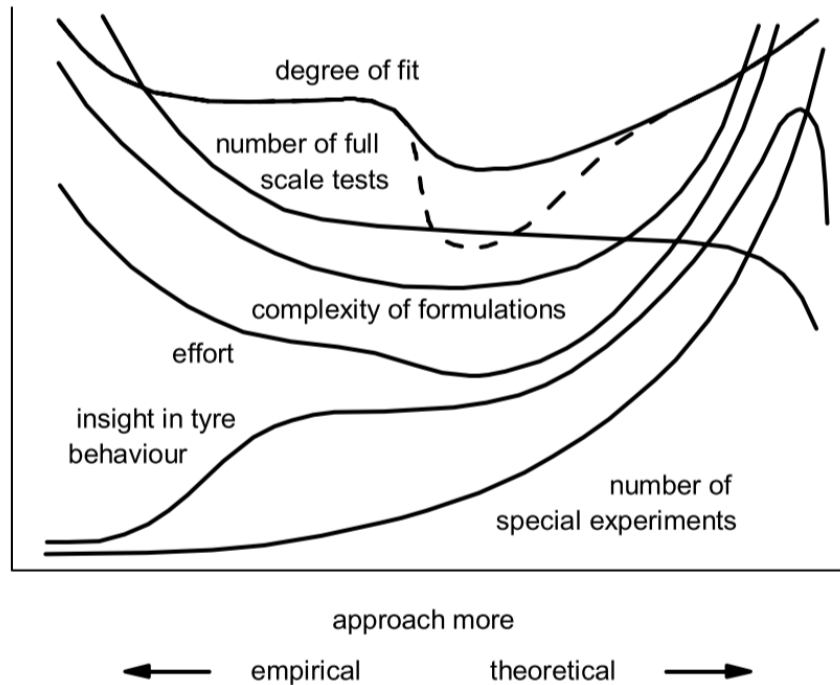
through complex
physical model

fitting full scale
tyre test data
by regression
techniques

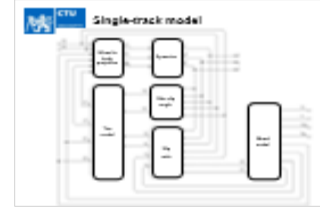
distorting,
rescaling and
combining
basic
characteristics

using simple
mechanical
representation,
possibly closed
form solution

describing tyre
in greater detail,
computer simulation,
finite element
method

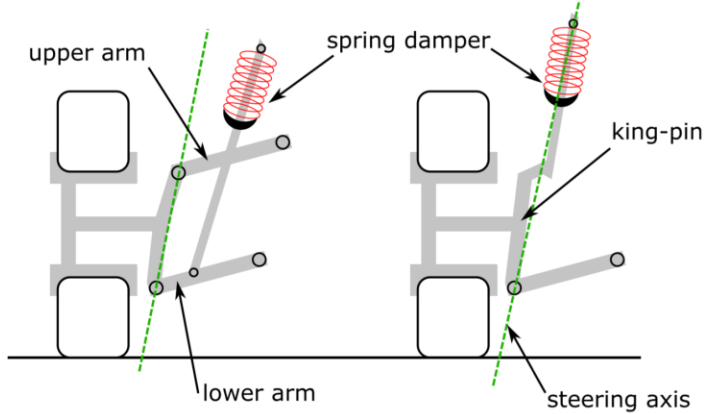


ST – Tire model (2)

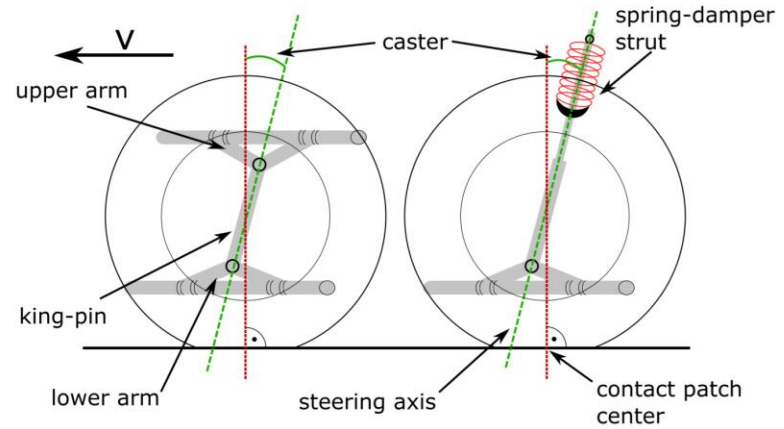


Double wishbone

McPherson

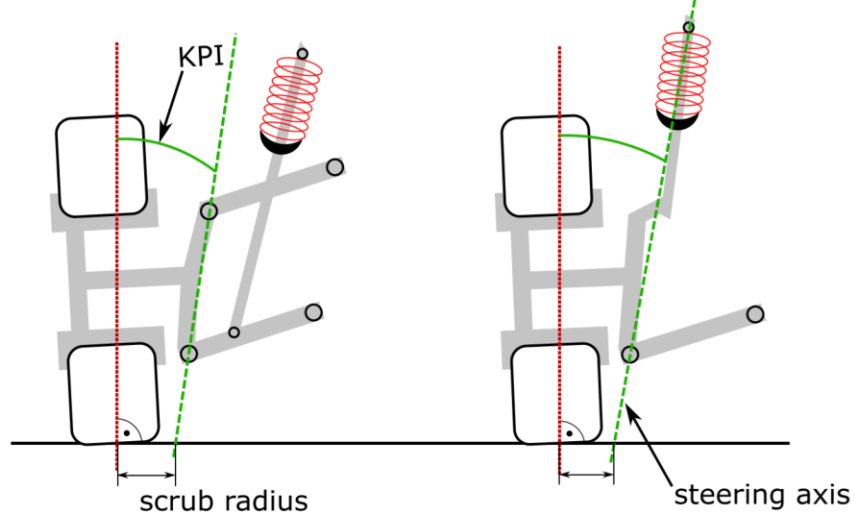


Double wishbone McPherson



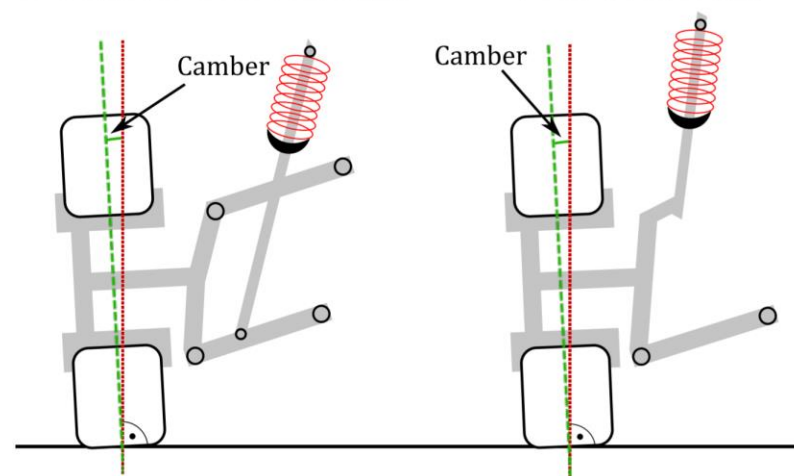
Double wishbone

McPherson

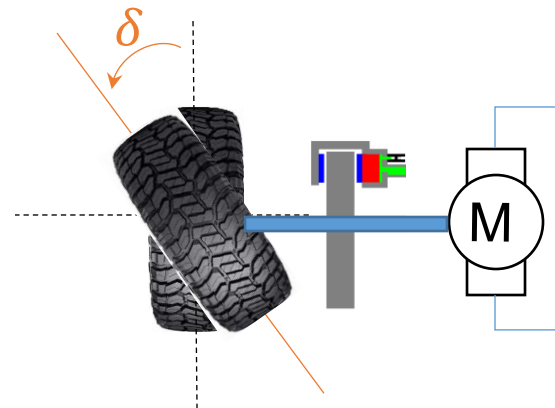
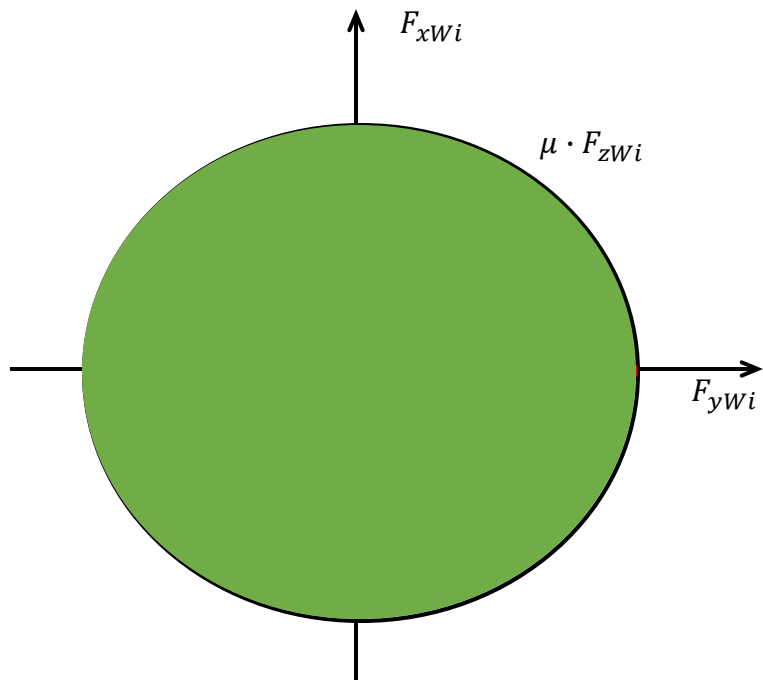
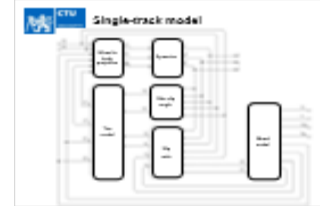


Double wishbone

McPherson

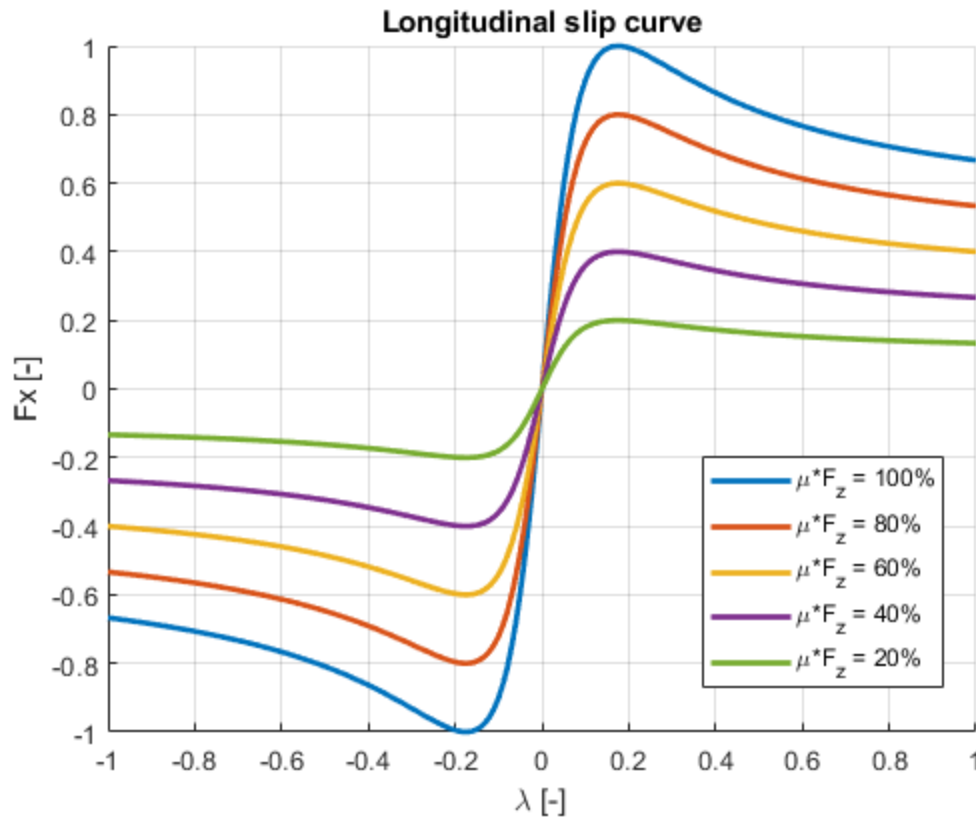
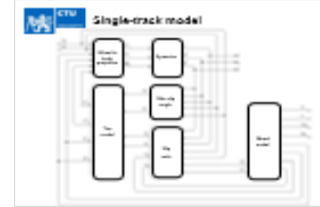


ST – Tire model (3)





ST – Tire model (4)



$$F_{FWx} = D\mu F_{FWz} \sin\left(C \tan^{-1}\left(B\lambda_{FW} - E\left(B\lambda_{FW} - \tan^{-1}(B\lambda_{FW})\right)\right)\right)$$