Assignment #9 10/10/2017

#91 Using the right hand Rule, magnetic field for z>0

will be in -9 diseetion and for zko in the +ý dixeetion.

Taloe an Amperian loop of width ward height 22 and apply Ampere's law!

Similarly for 1217a, we get

Vector potential 
$$\vec{A}$$
:  $\vec{\nabla} \times \vec{A} = \vec{B}$ 

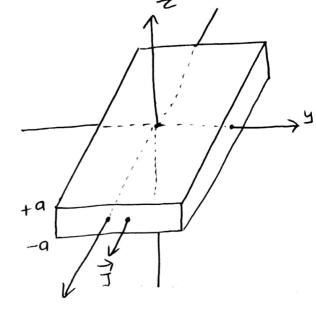
So, 
$$\left(\frac{\partial An}{\partial z} - \frac{\partial Az}{\partial x}\right) = \begin{cases} -\mu_0 z J \\ +\mu_0 \alpha z \end{cases}$$

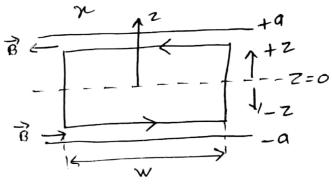
If we take Az = 0, Hen!

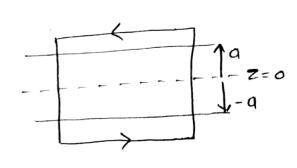
$$A_n = -\frac{\mu_0 J}{2} z^2$$

$$\mp \mu_0 J a z + C$$

121<9 12139







|2|79 (-ve sign for 2>0) +ve sign for 2<0)

121 < 9

(2)

continuity of potential at z = ± a gives:

$$\frac{1}{2} - \frac{\mu_0 J a^2}{2} = -\mu_0 J a^2 + c \Rightarrow c = \frac{\mu_0 J a^2}{2}$$

So, 
$$\overrightarrow{A}_1 = \frac{\mu_0 J}{2} z^2 \hat{\iota}$$

$$= \left(\frac{\mu_0 J a^2}{2} + \mu_0 J az\right) \hat{\iota}$$

Alternatively, we have.

$$\frac{\partial An'}{\partial z} = -\frac{\mu_0 z J}{2}$$

and

$$\frac{\partial Az}{\partial n} = + \frac{\mu_0 ZJ}{2}$$

This gives fox 2>0,

$$An = -\frac{\mu e J z^2}{4} \qquad (Z(a))$$

$$=-\frac{\mu_0 J_0}{2} z + c_1 \qquad (z>9)$$

۶

$$A_2 = \frac{\mu_0 z_J}{2} \chi \qquad z < a$$

$$= \pm \frac{\mu_0 \alpha J}{2} n + C_2 \qquad 7 > \alpha$$

So, 
$$\hat{A}_{2} = -\frac{\mu_{0}Jz^{2}}{4}\hat{i} + \frac{\mu_{0}Jz^{2}}{2}\hat{k}$$
 (2= \left(\frac{\mu\_{0}Ja^{2}}{4} - \frac{\mu\_{0}Jaz}{2}\right)\hat{i} + \frac{\mu\_{0}Jax}{2}\hat{k} (2>a)

$$\frac{So_{1}}{A_{2}-A_{1}} = \frac{hoJz^{2}}{4} \left(1 + \frac{hoJz}{2}\right) \left(1 + \frac{hoJax}{2}\right) \left(1$$

This difference can be shown as the gradient of a function forms) such that, (for 270)

$$\frac{\partial f}{\partial n} = \frac{\mu_0 J z^2}{4}$$

$$\frac{\partial f}{\partial z} = \frac{\mu_0 J z^n}{2}$$
(z (a)

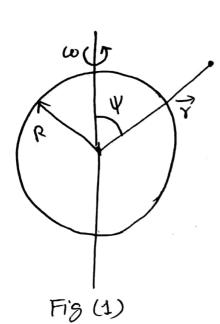
$$\frac{\partial f}{\partial n} = -\frac{\mu o J a^2}{4} + \frac{\mu o J a Z}{2}$$

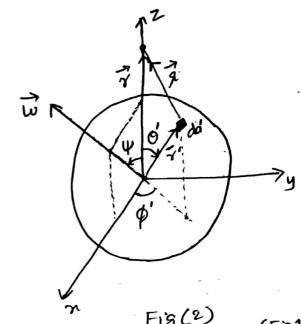
$$\frac{\partial f}{\partial z} = \frac{\mu o a J x}{2}$$
(Z>9)

So, 
$$f(n,y) = \frac{\mu_0 J z^2 \pi}{4}$$
 (2(9)

$$=-\frac{\mu_0 \int_0^2 x + \frac{\mu_0 \int_0^2 az x}{2} (z>a)$$

# 9.2 To salve this problem, firstly we will calculate the (9)
Verbox potential for a spherical shell a carrying a uniform suffere
charge density (0), spinning at angular velocity to.





Most common would be to set the balos axis along  $\vec{w}$  but calculations will be easies if we but  $\vec{v}$   $\vec{v}$  along  $\hat{z}$  and  $\vec{w}$  is tilted at angle  $\psi$  (Fig2) and  $\vec{w}$  lies in the z plane.

Vector potential for surface current:

$$\vec{A}(\vec{r}) = \frac{\mu_0}{u\pi} \int \frac{\vec{K}(\vec{r}')}{g} da'$$

$$\vec{R} = \sqrt{R^2 + \chi^2} - 2RR \cos \alpha'$$

$$d\alpha' = R^2 \sin \alpha' d\alpha' d\alpha'$$

Velocity of point  $\vec{r}'$  is given by  $\vec{w} \times \vec{r}' \leq 0$ ,  $\vec{v} = \vec{w} \times \vec{r}' = \begin{bmatrix} \vec{v} & \vec$ 

$$= R \omega \left( - \left( \cos \psi \sin \phi' \sin \phi' \right) \hat{x} + \left( \cos \psi \sin \phi' \cos \phi' - \sin \psi \cos \phi' \right) \hat{y} + \left( \sin \psi \sin \phi' \sin \phi' \right) \hat{z} \right]$$

(5)

Each term which invalve sing or cosp' will vanish be cause 
$$\int_{0}^{2\pi} \sin \phi' d\phi' = \int_{0}^{2\pi} \cos \phi' d\phi' = 0$$

So, 
$$A(\vec{x}) = -\frac{\mu_0 R^3 \sigma_w \sin \psi}{2} \int_{0}^{\pi} \frac{\cos \phi' \sin \phi' d\phi'}{\sqrt{R^2 + N^2 - 2RN \cos \phi'}} \hat{y}$$

substituting u = coso', integral be comes

$$\int \frac{u \, du}{\sqrt{R^2 + \chi^2 - 2RRu}} = -\frac{(R^2 + \chi^2 + R\chi u)}{3R^2 \chi^2} \sqrt{R^2 + \chi^2 - 2R\chi u} \Big|_{-1}^{+1}$$

$$= -\frac{1}{3R^23^2} \left[ (R^2 + 3R^2 + RX) | R - X) - (R^2 + 3R^2 - RX) (R + X) \right]$$

If point  $\vec{\gamma}$  lies inside the sphere, RTX, and the expression reduces to  $\left(\frac{2Y}{3R^2}\right)$ , and if  $\vec{\gamma}$  lies outside the sphere, then R(Y, it reduces to  $\left(\frac{2R}{3X^2}\right)$ . Also,  $(\vec{\omega} \times \vec{x}) = -\omega \gamma \sin \psi \cdot \vec{y}$ . So,

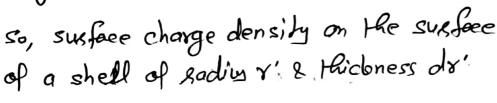
$$\vec{A}(\vec{r}) = \begin{cases} \frac{\mu_0 R \sigma}{3} (\vec{\omega} \times \vec{r}) & \gamma < R \\ \frac{\mu_0 R'' \sigma}{3 \gamma^3} (\vec{\omega} \times \vec{r}) & \gamma > R \end{cases}$$

Let's revert back to natural consdinates as Fig(1) where  $\vec{\omega}$  is in 2 disertion, puopuo  $\gamma \sin \hat{\phi}$   $\gamma \in R$ 

Lisedian, 
$$\mu \in \mathbb{R}$$
  $\frac{\mu \circ \mathcal{R} \circ \sigma}{3} \gamma \sin \sigma \hat{\phi}$   $\gamma \in \mathbb{R}$   $\frac{\mu \circ \mathcal{R}' \circ \sigma}{3} \frac{\sin \sigma}{\gamma^2} \hat{\phi}$   $\chi > \mathbb{R}$ .

New we will calculate magnetic field due to uniformly charged sphere.

A uniformly charged sphere can be divided into shells, with each shell carrying total charge = unx'2 dx' p



$$\sigma(x') = \frac{u\pi x'^2 dx' P}{u\pi x'^2} = P dx'$$

This shell produces fallowing veetor potential

$$\frac{d\vec{A}(Y,0,\phi)}{d\vec{A}(Y,0,\phi)} = \begin{cases}
\frac{\mu_0 Y' \omega P dY'}{3} Y \sin \theta & X \leq X' \\
\frac{\mu_0 Y'' \omega P dY'}{3} \frac{\sin \theta}{Y^2} & Y >, Y'
\end{cases}$$

So, total votar potential due to entire sphere is

$$\vec{A}(\gamma,0,\phi) = \frac{\mu_0 \omega f}{3} \frac{\sin \theta}{\hat{\gamma}^2} \int_0^{\gamma' u} d\gamma' \hat{\theta} + \frac{\mu_0 \omega f}{3} \gamma \sin \theta \int_{\gamma'}^{\gamma' u} d\gamma' \hat{\phi}$$

$$= \frac{\mu_0 \omega \rho \sin \theta}{3} \left( \frac{R^2 \gamma}{2} - \frac{\gamma^2}{2} + \frac{\gamma^3}{5} \right) \hat{\phi}$$

$$\overline{A}(Y,0,\phi) = \frac{\mu_0 \omega P}{3} \left( \frac{R^2 Y}{2} - \frac{3Y^3}{10} \right) \sin \alpha \hat{\phi}$$

So, 
$$\vec{B} = \vec{\nabla} \times \vec{A} = \frac{1}{Y \sin \theta} \frac{\partial}{\partial \theta} (\sin \theta A \phi) \hat{Y} - \frac{1}{Y} \frac{\partial}{\partial Y} (Y A \phi) \hat{\theta}$$

$$= \frac{\mu_0 \omega \rho}{3} \frac{1}{\gamma \sin \phi} \left( \frac{\rho^2 \gamma}{2} - \frac{3 \sqrt[3]{3}}{10} \right) 2 \sin \phi \cos \phi - \frac{\mu_0 \omega \rho}{3} \frac{1}{\gamma} \left( \rho^2 \gamma - \frac{6}{5} \gamma^3 \right) \sin \phi \cos \phi$$

$$= \frac{\mu_0 \omega P}{3} \left[ \left( R^2 - \frac{3}{5} \gamma^2 \right) \cos \hat{\gamma} - \left( R^2 - \frac{6 \gamma^2}{5} \right) \sin \hat{\phi} \right]$$

= 
$$\frac{\mu_0 \omega Q}{\frac{4}{3}\pi R^3.3} \left( \left( R^2 - \frac{3}{5} \gamma^2 \right) \cos 0 \hat{\gamma} - \left( R^2 - \frac{6 \gamma^2}{5} \right) \sin 0 \hat{0} \right)$$

$$\Rightarrow \vec{B} = \frac{\mu_0 \omega \Omega}{u \pi R^3} \left( \left( R^2 - \frac{3}{5} r^2 \right) \cos \hat{r} - \left( R^2 - \frac{6 r^2}{5} \right) \sin \hat{o} \hat{o} \right)$$

CHECK: 
$$\vec{\nabla} \cdot \vec{B} = \frac{1}{\gamma^2} \frac{\partial}{\partial y} (\gamma^2 B_y) + \frac{1}{\gamma \sin \theta} \frac{\partial}{\partial \theta} (\sin \theta_0)$$

$$= \frac{\mu_0 \omega Q}{u \pi R^3} \left[ \frac{1}{\gamma^2} \frac{\partial}{\partial y} \left( R^2 \gamma^2 - \frac{3 y^4}{5} \right) \cos \phi - \frac{1}{\gamma \sin \phi} \frac{\partial}{\partial \phi} \left\{ \left( R^2 - \frac{6 y^2}{5} \right) \sin \phi \right\} \right]$$

$$\vec{\nabla} \times \vec{B} = \frac{1}{Y} \left( \frac{\partial}{\partial Y} (YBO) - \frac{\partial BY}{YOO} \right) \vec{\phi}$$

$$= \frac{\mu_0 \omega G}{u \pi R^3 Y} \left( -\left(R^2 - \frac{18Y^2}{5}\right) \sin O + \left(R^2 - \frac{3}{5}Y^2\right) \sin O \right) \vec{\phi}$$

$$\vec{\nabla} \times \vec{B} = \frac{3\mu_0 \omega GY}{u \pi R^3} \sin O \vec{\phi}$$

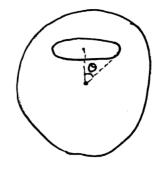
R.H.S. should be equal to MOJ. So let's check if it matches.

$$\frac{1}{\int (Y,0,\phi)} = \frac{\text{cussent due to the Ring shown } \hat{\phi}}{\text{asea}}$$

$$= \frac{\omega}{2\pi} \cdot 2\pi \hat{\gamma}^2 d\hat{\gamma} \sin \phi \cdot P$$

$$= \frac{\psi}{2\pi} \cdot 2\pi \hat{\gamma}^2 d\hat{\gamma} \sin \phi \cdot P$$

$$= \frac{\psi}{2\pi} \cdot 2\pi \hat{\gamma}^2 d\hat{\gamma} \sin \phi \cdot P$$



$$= \frac{3\omega \times a \sin 0}{4} \phi$$

B is correct as it correctly satisfies both divergence and curl equations.

# 9.3 The field will be in g for 200 and -y fox 2>0 sheet of 60.dl = Mo Iene = B.21 - HO K.1 - fox 270 + fox 2(0 ⇒ B= + Mok g  $\vec{B} = \vec{\nabla} \times \vec{A}$ for By,  $\Rightarrow$  By =  $\left(\frac{\partial An}{\partial z} - \frac{\partial Az}{\partial n}\right)$ (1) If  $A_n=0 \Rightarrow A_z=+\frac{h_0 k_N}{2}$ 270 2(0 270 = + (ho KZ 2 <0

(i) If 
$$Az=0 \Rightarrow Ax = -\frac{\mu_0 k^2}{2}$$
 270
$$= + \frac{\mu_0 k^2}{2}$$
 2(0

Calculating A from direct integration:

Naw,  $\exists (\vec{r}') = K S(\vec{r}') \hat{x}$ 

Because 
$$\int \overline{J}(\overline{z}')dz'$$
  
=  $\int K \delta(z')dz'$   
=  $K$ 

So,  $\vec{A}(\vec{x}) = \frac{\mu_0 K \hat{x}}{u \pi} \int_{\sqrt{(n-n')^2 + (y-y')^2 + z^2}} dn' dy'$ Nau, Ram elechostotics, uniformly charged sheet in ny plane,

the electoration to landial,  $\phi(\vec{Y}) = \frac{\sigma}{4\pi6} \int \frac{dx'dy'}{\sqrt{(x-x')^2 + (y-y')^2 + 2^2}} = \frac{-\sigma^2}{260}$ 

So, 
$$\int \frac{d^{3}d^{3}}{\sqrt{(3-3^{2})^{2}+(3-3^{2})^{2}+2^{2}}} = \mp 2\pi Z$$

# 9.4 The problem requires calculation of field B due to a finite size square loop. Field due to each wire of the loop will be the same and after addition andy vertical component services.

$$\overrightarrow{B}_{1} = \frac{\text{MoI}}{\text{UT}} \int \frac{d\overrightarrow{J}' \times (\overrightarrow{Y} - \overrightarrow{Y}')}{|\overrightarrow{Y} - \overrightarrow{Y}'|^{3}}$$

$$= \frac{\text{MoI}}{\text{UT}} \int \frac{dy' \widehat{J} \times (z \widehat{k} - \frac{w}{2} \widehat{l} - y' \widehat{J})}{\left(\frac{w^{2}}{4} + y'^{2} + z^{2}\right)^{3/2}}$$

$$= \frac{\mu_0 I}{u\pi} \left( \frac{dy'(z\hat{l} + \frac{w^2}{2}\hat{l})}{(\frac{w^2}{4} + y'^2 + z^2)^{3/2}} \right)$$

there side, we get

From the wire on the other side, we get

$$\vec{B}_{2} = \frac{\mu_{0}I}{u_{T}} \int \frac{-dy'\hat{j} \times (z\hat{k} + \frac{w}{2}\hat{i} - y'\hat{j})}{(\frac{w^{2}}{4} + z^{2} + y'^{2})^{3/2}} = \frac{\mu_{0}I}{u_{T}} \int \frac{dy'(-z\hat{i} + \frac{w}{2}\hat{k})}{(\frac{w^{2}}{u} + z^{2} + y'^{2})^{3/2}}$$

So) 
$$\vec{B}_1 + \vec{B}_2 = \vec{B}_{1+2} = \frac{\mu_0 I W}{u \pi} \int_{-w/2}^{w/2} \frac{dy'}{(\frac{w^2}{4} + z^2 + y'^2)^{3/2}}$$

Substitute  $y' = \sqrt{\frac{w^2}{u} + z^2}$  tano  $\Rightarrow dy' = \sqrt{\frac{w^2}{u} + z^2}$  sec<sup>2</sup>o do

limit from 
$$Q = -\tan^{-1}\left(\frac{w}{2\sqrt{\frac{w^2}{u}+z^2}}\right)$$
 to

$$G = + \tan^{-1} \left( \frac{w}{2\sqrt{\frac{w^2+z^2}{u}+z^2}} \right)$$

$$\Rightarrow B_{H2} = \frac{\mu_0 I W}{u \pi} \frac{1}{\left(\frac{W^2}{u} + Z^2\right)} \cdot \int_{0}^{+ t_0 \pi^2} \frac{W}{2\sqrt{W_u^2 + Z^2}} d\theta$$

$$- t_0 \pi^2 \left(\frac{W}{2\sqrt{W_u^2 + Z^2}}\right)$$

$$\vec{B}_{H2} = \frac{\mu_0 I W}{u \pi} \frac{1}{\left(\frac{W^2}{u} + 2^2\right)} 2 \tan \left(\frac{W}{2\sqrt{\frac{W^2}{u} + 2^2}}\right) \hat{z}$$

so, total field for all 4 wixes of the loop,

$$\vec{B}(z) = \frac{\text{NoIW}}{u\pi} \frac{1}{\left(\frac{w^2}{u} + z^2\right)} \cdot y + \tan^{-1} \left(\frac{w}{2\sqrt{\frac{w^2}{u} + z^2}}\right)$$

$$\Rightarrow \overrightarrow{B}(z) = \frac{\mu_0 TW}{\pi} \frac{4}{(w^2 + uz^2)} \tan^{-1} \left(\frac{w}{w^2 + uz^2}\right).$$

For z>>w, we get

$$\vec{B} \approx \frac{\mu_0 I W}{\pi} \frac{U}{U z^2} \cdot \frac{W}{2z} = \frac{\mu_0}{u \pi} \left( \frac{2 I w^2}{z^3} \right)$$

Mognetic field due to mognetic dipale,

$$\vec{R} = \frac{\mu_0}{4\pi} \frac{3(\vec{m} \cdot \hat{z})\hat{z} - \vec{m}}{z^3}$$

$$\vec{B} = \frac{\mu_0}{4\pi} \frac{2IW^2}{z^3} \hat{z} \implies \text{Same as above.}$$