$$\frac{1}{6n(s)} = \frac{6}{(s+3)^2}, \quad H(s) = Kp + \frac{Ki}{s}$$

$$= Kp \left( \frac{s + \frac{Ki}{Kp}}{s} \right)$$

$$= Kp \left( \frac{s + \frac{Ki}{Kp}}{s} \right)$$

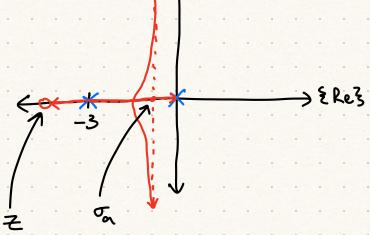
$$ii: (-\infty, -3) \quad L(s) = K \left( \frac{s + z}{(s+3)^2 s} \right), \quad K = 6 Kp, \quad z = \frac{Ki}{Kp}$$

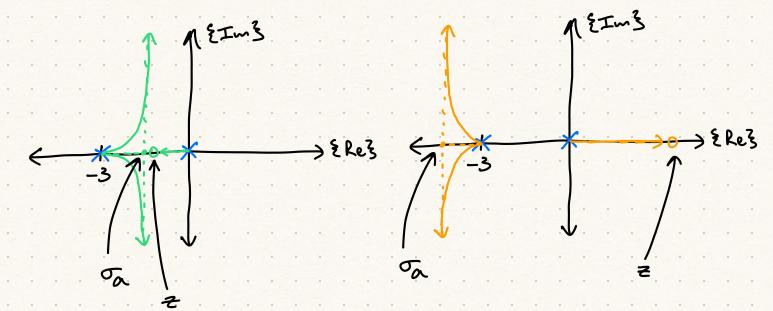
$$iii: (0, +\infty) \quad D(s) + KN(s) = 0$$

$$s^3 + 6s^2 + 9s + Ks + Kz = 0$$

$$N = 3, \quad M = 1 \Rightarrow \sigma = \frac{-3 - 3 + 0 - \left( -\frac{Ki}{Kp} \right)}{2} = -3 + \frac{Ki}{2Kp}$$

$$\alpha L = \pm 90^{\circ}$$





- b) case iii is unstable, as it mandates a singular RHP zero and its LHP branch is unstable
  - c) Want: X < 0

$$\Delta = \frac{-6+2}{2} \Rightarrow 266$$

2>0 to avoid case iii

L> zero must lie between (-6,0)

Need: 4 L(s) / - 180°

Let: 
$$\neq L(s) = 180^{\circ}$$
, atam  $\left(\frac{\omega}{2}\right) - \frac{\pi}{2} - 2$  atam  $\left(\frac{\omega}{3}\right) = -\pi$ 

$$-\frac{T}{2} = \operatorname{atan}(\frac{\omega}{2}) - 2\operatorname{atan}(\frac{\omega}{3})$$

$$\Rightarrow \frac{\omega}{z} = \frac{9 - \omega^2}{-6\omega} \Rightarrow \omega^2 = -\frac{9z}{6-z} > 0$$

want this to be false

(-6,0)

$$\omega_{N} = \frac{2}{2}, K = \omega_{N}^{2}/6$$

$$K_{P} = K \rightarrow K_{P} = 0.75$$

$$K_{i} = K_{P} = 0.75$$

$$C_i = K_P = \rightarrow K_i = 2.25$$

$$\frac{2}{5(s)} = \frac{5(s-1)}{s-6}$$

a) 
$$H(s) = \frac{K}{s-p}$$
, with  $p>0$   
 $L(s) = \frac{5K(s-1)}{(s-6)(s-p)} \to 1+L(s)=0$ 

$$(s-p)(s-6)+5k(s-1)=0 \Rightarrow s^2+(-p-6)s+6p+5ks-5k=0$$

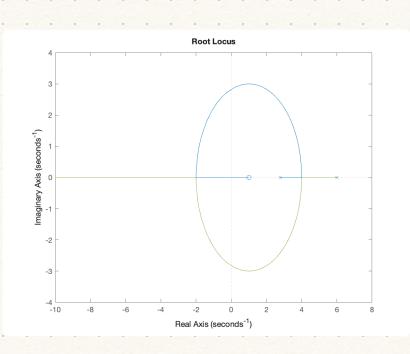
$$4) 5K - (p+6) > 0 & 6p - 5K > 0$$

$$\frac{p+6}{5} < K < \frac{6}{5}P \Rightarrow P > \frac{6}{5}$$

$$K = \left(\frac{8}{5}\right)^2 = \frac{64}{25}$$

$$P = \frac{64}{5} + 4 = \frac{84}{30} = \frac{14}{5}$$

$$H(s) = \frac{64}{25} \left( \frac{1}{s - \frac{14}{5}} \right)$$

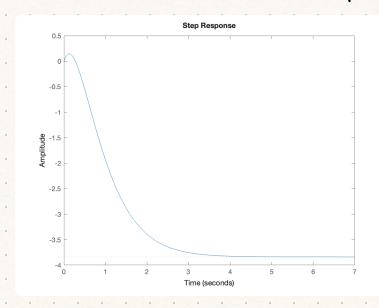


[1,5K-(P+6), GP-5K)0 1, 4, 4

c) 
$$y_{d}(t) = 1/(t)$$
,  $R(s) = \frac{H(s)}{1 + L(s)}$ ,  $U(s) = R(s) || Y_{d}(s) = \frac{1}{s} \Rightarrow U(s) = \frac{R(s)}{s} = \frac{H(s)}{s(1 + L(s))} = \frac{2.56(s - 6)}{s(s + 2)^{2}}$ 

$$u(t) = \frac{96}{25} \left( e^{-2t} + \frac{8}{3} t e^{-2t} - 1 \right)$$

## ult) is bounded, as all poles of RIS) are in LHP



R\_info = struct with fields:

RiseTime: 1.6515
TransientTime: 3.0421
SettlingTime: 3.0640
SettlingMin: -3.8400
SettlingMax: -3.4571

Overshoot: 0

Undershoot: 3.8196 Peak: 3.8400

PeakTime: 7.8058

H\_zoh = struct with fields:

Ad: 1.1185 Bd: 0.0847 Cd: 1.2800

Dd: 0

H\_tustin = struct with fields:

Ad: 1.1186 Bd: 0.3639 Cd: 0.3158 Dd: 0.0542

4 
$$G_1(s) = \frac{2}{s^2(s^2+3)}$$

a)  $H(s) = K$ ?

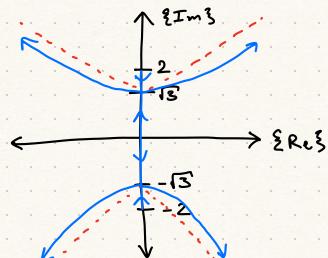
$$L(s) = \frac{2K}{s^2(s^2+3)} L'(s) = [(s-p)L(s)]$$
 $N-M=4 \Rightarrow d_1 = \pm 45, \pm 155, \pm 15$ 

$$L^{1}(s) = \frac{2\kappa}{s^{2}(s+13j)} \Rightarrow 4 L^{1}(p) = -180^{\circ} - 90^{\circ}$$
  
 $\delta = -90^{\circ}$ 

by symmetry, for 
$$s = -13$$
;  $\delta = 90^{\circ}$ 

$$L'(s) = \frac{2k}{s^2+3} \Rightarrow 4L'(p) = -180^{\circ}$$
  
 $\delta = \pm 180^{\circ}$ 

Will be unstable at all poles for sufficiently large K



b) Want: 
$$CLC - 1 \pm j$$
 & all else  $CLC - 4$ 
 $H(s) = \frac{b_3 s^3 + b_2 s^2 + b_1 s + b_0}{s^3 + a_2 s^2 + a_1 s + a_0}$  find:  $ZPK(H(s))$ 

Chaw Polys

 $CL: (s^3 + a_2 s^2 + a_1 s + a_0)(s^2 (s^2 + 3)) + (b_3 s^3 + b_2 s^2 + b_1 s + b_0)(2)$ 
 $T_{des}: (s - (-1 + j))(s - (-1 - j))(s + 4)^5$ 
 $L \Rightarrow a_2 = 22$   $b_3 = 1141.5$ 
 $a_1 = 199$   $b_2 = 1031$ 
 $a_0 = 984$   $b_1 = 2304$ 
 $a_0 = 1024$ 
 $a_0 =$ 

(L: (34+0353+0252+015+00)(52(52+3))+(6353+6252+615+60)(2)

Continuous-time zero/pole/gain model.

Continuous-time zero/pole/gain model.

poles  $T = 8 \times 1$  complex

zeros\_T = 3x1 complex -0.0625 + 1.3320i -0.0625 - 1.3320i -0.4116 + 0.0000i

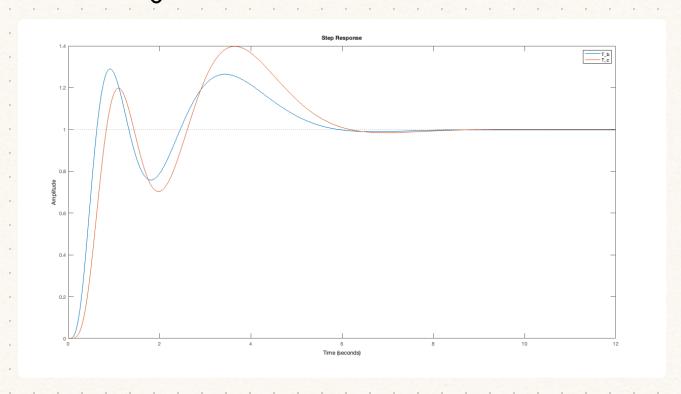
-4.0123 - 0.0214i

-3.9753 + 0.0000i -1.0000 + 1.0000i -1.0000 - 1.0000i

11194 (s+0.4116) (s^2 + 0.125s + 1.778)

Tdes: (s-(-1+j))(s-(-1-j))(s+4)6

d) Neither controllers are good, as they both home about (or over) 5.5s settling times, and significant authorst. This is due to the introduction of extra zeroes and their compensatory poles "spailing" our intended behavior of the designed poles



e) Otherwise, the benefit of C is that it has an extra pole, ensuring it has noise stability, which B does not