

# Chapter 11

## 3D Rigid Bodies

11/19/24

The governing laws of motion for a particle are

$$\text{Newton's Laws} \quad (2) \bar{F}_p = m_p \bar{a}_{p/0} = \frac{d}{dt} (\bar{p}_{p/0})$$

The governing laws of motion for a rigid body

$$\text{Euler's Laws} \quad (1) \bar{F}_G = m_G \bar{a}_{G/0} = \frac{d}{dt} (\bar{p}_{G/0})$$

$$(2) M_G = \frac{d}{dt} (\bar{h}_G)$$

The transport equation allows us to compute  $\frac{d}{dt}$  w/o coordinates!

$$\begin{aligned} \bar{F}_G &= \frac{d}{dt} (\bar{p}_{G/0}) = \overset{C}{\cancel{\frac{d}{dt}}} (\bar{p}_{G/0}) + \bar{\omega}^I \overset{I}{\cancel{C}} \times \bar{p}_{G/0} \\ &= \overset{C}{\cancel{\frac{d}{dt}}} (m_G \bar{v}_{G/0}) + \bar{\omega}^I \overset{I}{\cancel{C}} \times (m_G \bar{v}_{G/0}) \end{aligned}$$

In aerospace engineering it is common to use

$$[\bar{v}_{G/0}]_c = \begin{bmatrix} u \\ v \\ w \end{bmatrix}_c$$

$$[\bar{v}_{G/0}]_I = \begin{bmatrix} \dot{x} \\ \dot{y} \\ \dot{z} \end{bmatrix}_I = \bar{R}^I_c \begin{bmatrix} u \\ v \\ w \end{bmatrix}_c$$

$$[\bar{\omega}^I]_c = \begin{bmatrix} p \\ q \\ r \end{bmatrix}_c$$

$$\begin{bmatrix} F_1 \\ F_2 \\ F_3 \end{bmatrix}_C = m\alpha \frac{d}{dt} \begin{bmatrix} u \\ v \\ w \end{bmatrix}_C + \begin{bmatrix} p \\ q \\ r \end{bmatrix}_C \times m\alpha \begin{bmatrix} u \\ v \\ w \end{bmatrix}_C$$

$$= m\alpha \begin{bmatrix} \dot{u} \\ \dot{v} \\ \dot{w} \end{bmatrix}_C + m\alpha \begin{bmatrix} 0 & -r & q \\ r & 0 & -p \\ -q & p & 0 \end{bmatrix} \begin{bmatrix} u \\ v \\ w \end{bmatrix}_C$$

Using the transport equation on the rotational dynamics

$$\bar{M}_G = \frac{d}{dt} (\bar{I}\bar{\omega}_G) = \frac{d}{dt} (\bar{I}\bar{\omega}_G) + \bar{\omega}_G^C \times \bar{I}\bar{\omega}_G$$

Recall in 2D, for a planar rigid body

$$\bar{I}\bar{\omega}_G = \bar{I}\bar{\omega}_G \bar{\omega}$$

In 3D the moment of inertia  $MOT$  becomes a

$3 \times 3$  matrix  $(\bar{I}\bar{\omega}_G)_C$

$$\Rightarrow \begin{bmatrix} \bar{I}\bar{\omega}_G \end{bmatrix}_C = \begin{bmatrix} \bar{I}\bar{\omega}_G \end{bmatrix}_C \begin{bmatrix} \bar{\omega}_G^C \end{bmatrix}_C$$

$$\begin{bmatrix} 3 \times 1 \end{bmatrix} = \begin{bmatrix} 3 \times 3 \end{bmatrix} \begin{bmatrix} 3 \times 1 \end{bmatrix}$$

$\bar{I}\bar{\omega}_G$

$\bar{\omega}_G^C$

## Qualitative Rotational Dynamics

Rapidly Spinning  
RB

let C be the body frame

let B be the intermediate frame that shares the spin axis with C

$${}^T\bar{\omega}^C = \underbrace{{}^T\bar{\omega}^B}_{\text{precession}} + \underbrace{{}^B\bar{\omega}^C}_{\text{Spin}}$$

$$\begin{aligned} \text{Eq L : } \bar{M}_G &= \frac{d}{dt} ({}^T\bar{h}_G) \quad ) \text{ T.E.} \\ &= \frac{d}{dt} ({}^T\bar{h}_G) + {}^T\bar{\omega}^C \times \bar{h}_G \\ &= \frac{d}{dt} ({}^T\bar{h}_G) + \underbrace{{}^T\bar{\omega}^B \times \bar{h}_G}_{\text{?}} \end{aligned}$$

For a rapidly spinning rigid body, we have

$$\| {}^B\bar{\omega}^C \| \gg \| {}^T\bar{\omega}^B \|$$

spin >> precession

Using intuition for 2D rigid body

$${}^T\bar{h}_G \approx I_G {}^T\bar{\omega}^C \approx I_G {}^B\bar{\omega}^C$$

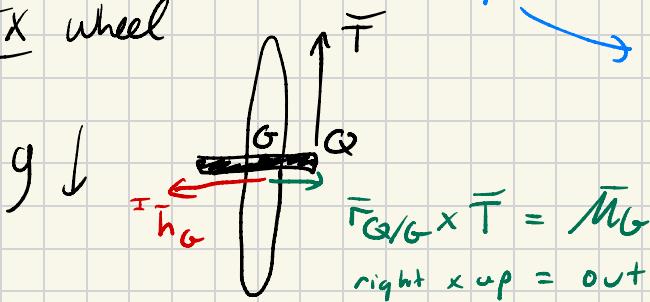
$$\bar{M}_G = \frac{\partial}{\partial t} (\bar{I} \bar{h}_G) + \bar{I} \bar{w}^B \times \bar{h}_G$$

$\approx 0$  (assuming constant spin rate)

$$\Rightarrow \boxed{\bar{M}_G \approx \bar{I} \bar{w}^B \times \bar{h}_G}$$

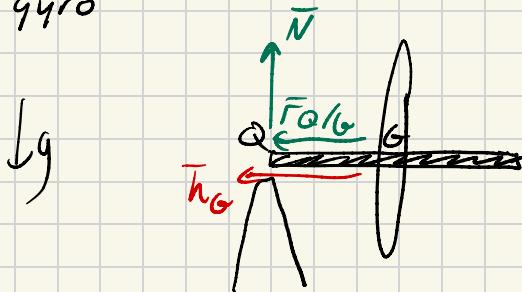
out                      unknown      left  
                            up

Ex wheel



precesses  
CCW from above

Ex gyro



$$\bar{M}_G \approx \bar{I} \bar{w}^B \times \bar{h}_G$$

$$\underline{\text{in}} \approx \underline{\text{down}} \times \underline{\text{left}}$$

precesses  
CW from above

## COM of 3D RB

$$\lim_{N \rightarrow \infty} \bar{F}_{G,0} = \frac{1}{m_0} \sum_{k=1}^N m_k \bar{r}_{k,0}$$

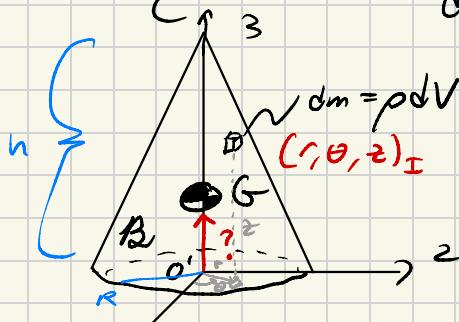
$$= \frac{1}{m_0} \int_A dm \bar{r}_{dm,0}$$

$$\rho dA \quad (2D)$$

$$\rho dV \quad (3D)$$

Ex Cone (Cylindrical Coordinates)  $(r, \theta, z)_I$

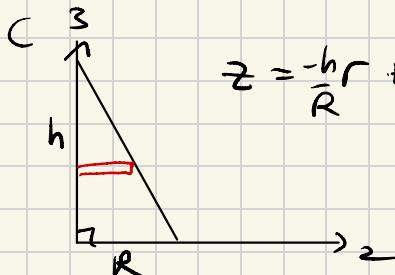
$$dV = r dr d\theta dz$$



$$\bar{F}_{G,0} = \frac{\rho}{m} \iiint_A r dr d\theta dz \bar{r}_{dm,0}$$

$$\bar{r}_{dm,0} = r \cos \hat{c}_1 + r \sin \hat{c}_2 + z \hat{c}_3$$

$$\bar{F}_{G,0} = \frac{\rho}{m} \iiint_0^h \int_0^{2\pi} \int_0^R \frac{R(h-z)}{h} r dr d\theta dz \left( r \cos \hat{c}_1 + r \sin \hat{c}_2 + z \hat{c}_3 \right)$$



$$z = -\frac{h}{R}r + h \Rightarrow r = \frac{-R}{h}(z-h)$$

$$= \frac{R(h-z)}{h}$$

$$T_{Glo} = \left[ \frac{\rho}{m} \int_0^h \int_0^{2\pi} \int_0^R r dr d\theta dz \right] C_3 = \dots = \frac{h}{4} C_3$$

$m = \rho V = \rho \frac{\pi R^2 h}{3}$

## Moment of Inertia of 3D RB

Recall Ch. 9

$$\begin{aligned} {}^I \bar{h}_{Gc} &= \sum_{k=1}^N m_k \left[ {}^I \bar{w}_c \right] \left( \bar{r}_{u/G} \cdot \bar{r}_{u/G} \right) - \bar{r}_{u/G} \left( \bar{r}_{u/G} \cdot {}^I \bar{w}_c \right) \\ \left[ {}^I \bar{h}_{Gc} \right]_c &= \sum_{k=1}^N m_k \left( \left[ {}^I \bar{w}_c \right]_c \| \bar{r}_{u/G} \|^2 - \left[ \bar{r}_{u/G} \right]_c \left( \bar{r}_{u/G} \right)_c^T \left[ {}^I \bar{w}_c \right]_c \right) \\ &= \sum_{k=1}^N m_k \left( \| \bar{r}_{u/G} \|^2 \underbrace{\begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix}}_{3 \times 3 \text{ identity}} - \left[ \bar{r}_{u/G} \right]_c \left( \bar{r}_{u/G} \right)_c^T \left[ {}^I \bar{w}_c \right]_c \right) \\ &= \left[ {}^I I_G \right]_c \left[ {}^I \bar{w}_c \right]_c \end{aligned}$$

where

$$\left[ {}^I I_G \right]_c = \sum_{k=1}^N m_k \left( \| \bar{r}_{u/G} \|^2 \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix} - \left[ \bar{r}_{u/G} \right]_c \left( \bar{r}_{u/G} \right)_c^T \right)$$

as  $N \rightarrow \infty$

$$\left( {}^I I_G \right)_c = \left\{ \begin{array}{l} dm \left( \| \bar{r}_{dm/G} \|^2 \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix} - \left[ \bar{r}_{dm/G} \right]_c \left( \bar{r}_{dm/G} \right)_c^T \right) \\ \# \end{array} \right.$$

Ex Cartesian coordinates  $(x, y, z)_c$

$$\vec{r}_{dm/G} = x \hat{C}_1 + y \hat{C}_2 + z \hat{C}_3$$

$$\|\vec{r}_{dm/G}\|^2 = x^2 + y^2 + z^2$$

$$[\vec{r}_{dm/G}]_c [\vec{r}_{dm/G}]_c^T = \begin{bmatrix} x \\ y \\ z \end{bmatrix}_c \begin{bmatrix} x & y & z \end{bmatrix}_c$$

$$= \begin{bmatrix} x^2 & xy & xz \\ xy & y^2 & yz \\ xz & yz & z^2 \end{bmatrix}$$

$$[\mathbb{I}_G]_c = \rho \int_B dx dy dz \begin{bmatrix} y^2 + z^2 & -xy & -xz \\ -xy & x^2 + z^2 & -yz \\ -xz & -yz & x^2 + y^2 \end{bmatrix}$$

Ex 11.6 Cube  $2l \times 2l \times 2l = 8l^3$

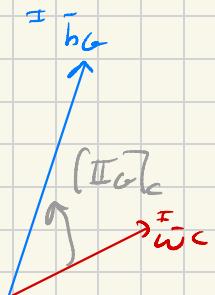
$$[\mathbb{I}_G]_c = \frac{m}{8l^3} \iiint_{-l}^l dx dy dz \begin{bmatrix} y^2 + z^2 & -xy & -xz \\ -xy & x^2 + z^2 & -yz \\ -xz & -yz & x^2 + y^2 \end{bmatrix}$$

$$= \dots = \frac{2}{3} ml^2 \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

AM of a 3D RB

$$\left[ {}^I \bar{h}_G \right]_c = \left[ {}^I I_G \right]_c \left( {}^I \bar{\omega}^c \right)_c$$

↑  
Symmetric matrix



Suppose  $\left[ {}^I I_G \right]_c = \begin{bmatrix} I_1 & 0 & 0 \\ 0 & I_2 & 0 \\ 0 & 0 & I_3 \end{bmatrix}$

$$\left[ {}^I \bar{h}_G \right]_c = \begin{bmatrix} I_1 & 0 & 0 \\ 0 & I_2 & 0 \\ 0 & 0 & I_3 \end{bmatrix} \begin{bmatrix} w_1 \\ w_2 \\ w_3 \end{bmatrix}_c = \begin{bmatrix} I_1 w_1 \\ I_2 w_2 \\ I_3 w_3 \end{bmatrix}_c$$

\* key idea: it is always (wlog) possible to choose a body frame in which the MOI matrix is diagonal.

Rotation Dynamics of 3D RB

E2L  $\frac{d}{dt} \left( {}^I \bar{h}_G \right) = \bar{M}_G$

$$\bar{M}_G = {}^C \frac{d}{dt} \left( {}^I \bar{h}_G \right) + {}^I \bar{\omega}^c \times {}^I \bar{h}_G$$

let  $\left[ \bar{M}_G \right]_c = \begin{bmatrix} M_1 \\ M_2 \\ M_3 \end{bmatrix}_c$  and  $\left[ I_G \right]_c = \begin{bmatrix} I_1 & 0 & 0 \\ 0 & I_2 & 0 \\ 0 & 0 & I_3 \end{bmatrix}$

$$\begin{bmatrix} M_1 \\ M_2 \\ M_3 \end{bmatrix}_C = \frac{d}{dt} \begin{bmatrix} I_1 w_1 \\ I_2 w_2 \\ I_3 w_3 \end{bmatrix}_C + \begin{bmatrix} 0 & -w_3 & w_2 \\ w_3 & 0 & -w_1 \\ -w_2 & w_1 & 0 \end{bmatrix} \begin{bmatrix} I_1 w_1 \\ I_2 w_2 \\ I_3 w_3 \end{bmatrix}_C$$

$$\hat{c}_1: \dot{\omega}_1 = \frac{((I_2 - I_3)w_2 w_3 + M_1)}{I_1}$$

$$\hat{c}_2: \dot{\omega}_2 = \frac{((I_3 - I_1)w_1 w_3 + M_2)}{I_2}$$

$$\hat{c}_3: \dot{\omega}_3 = \frac{((I_1 - I_2)w_1 w_2 + M_3)}{I_3}$$

$$\dot{\psi} = \left( \cancel{q} \sin \phi + \cancel{r} \cos \phi \right) \sec \theta$$

$$\dot{\Theta} = \cancel{q} \sin \phi - \cancel{r} \cos \phi$$

$$\dot{\phi} = \cancel{q} \sin \phi + \cancel{r} \cos \phi \tan \theta + \cancel{p}$$

3-2-1

Free Rigid Body  $\bar{M}_G = 0, \bar{F}_G = 0$

$$\bar{F}_G = \frac{d}{dt} \begin{pmatrix} I_1 \bar{\omega}_1 \\ I_2 \bar{\omega}_2 \\ I_3 \bar{\omega}_3 \end{pmatrix} \Rightarrow \bar{I} \bar{\omega}_G \text{ conserved}$$

$$\bar{M}_G = \frac{d}{dt} \begin{pmatrix} I_1 \bar{h}_G \\ I_2 \bar{h}_G \\ I_3 \bar{h}_G \end{pmatrix} \Rightarrow \bar{h}_G \text{ conserved}$$

$$\dot{\omega}_1 = \frac{(I_2 - I_3)w_2 w_3}{I_1} = 0$$

$$\dot{\omega}_2 = \frac{(I_3 - I_1)w_1 w_3}{I_2} = 0$$

$$\dot{\omega}_3 = \frac{(I_1 - I_2)w_1 w_2}{I_3} = 0$$

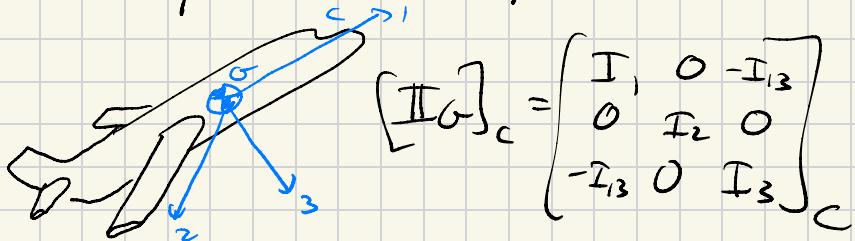
@ equilibrium

(let  $I_3 > I_2 > I_1$ )

- Stable (1)**  $\omega_1 \neq 0, \omega_2 = 0, \omega_3 = 0$  spinning  $\hat{c}_1$
- Unstable (2)**  $\omega_2 \neq 0, \omega_1 = 0, \omega_3 = 0$  spinning  $\hat{c}_2$
- Stable (3)**  $\omega_3 \neq 0, \omega_1 = 0, \omega_2 = 0$  spinning  $\hat{c}_3$
- Stable (4)**  $\omega_1 = \omega_2 = \omega_3 = 0$  not rotating

Key idea: Spin about the intermediate axis  
is unstable!!

### Ex 11.11 Rotational dynamics of an airplane



Recall  $\bar{\mathbb{M}}\omega = \frac{d}{dt}(\mathbb{I}\bar{h}_G) = \frac{d}{dt}(\bar{I}\bar{h}_G) + \bar{\omega} \times \bar{h}_G$

$$[\bar{h}_G]_c = [\mathbb{I}\omega]_c [\bar{\omega}]_c$$

$$= \begin{bmatrix} I_1 & 0 & -I_{13} \\ 0 & I_2 & 0 \\ -I_{13} & 0 & I_3 \end{bmatrix} \begin{bmatrix} P \\ Q \\ R \end{bmatrix}_c$$

$$= \begin{bmatrix} I_1 P - I_{13} R \\ I_2 Q \\ I_3 R - I_{13} P \end{bmatrix}_c$$

$$\begin{bmatrix} M_1 \\ M_2 \\ M_3 \end{bmatrix}_C = \begin{bmatrix} I_{11}\dot{p} - I_{13}\dot{r} \\ I_{22}\dot{q} \\ I_{33}\dot{r} - I_{13}\dot{p} \end{bmatrix} + \begin{bmatrix} 0 & r & q \\ r & 0 & -p \\ -q & p & 0 \end{bmatrix} \begin{bmatrix} I_{11}p - I_{13}r \\ I_{22}q \\ I_{33}r - I_{13}p \end{bmatrix}$$

$$\hat{C}_1: M_1 = I_{11}\dot{p} - I_{13}\dot{r} + q(I_{33}r - I_{13}p) - I_{22}qr$$

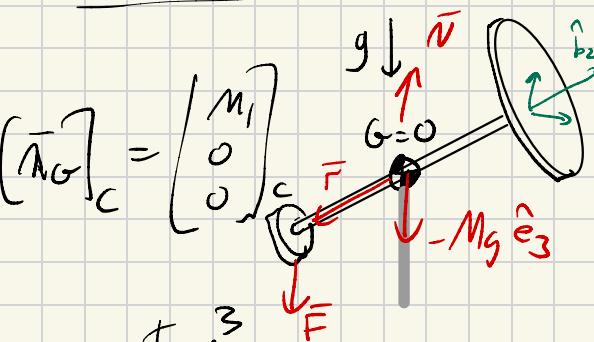
$$\hat{C}_2: M_2 = I_{22}\dot{q} + r(I_{11}p - I_{13}r) - p(I_{33}r - I_{13}p)$$

$$\hat{C}_3: M_3 = I_{33}\dot{r} - I_{13}\dot{p} + I_{22}pq - q(I_{11}p - I_{13}r)$$

$$\begin{bmatrix} \dot{p} \\ \dot{q} \\ \dot{r} \end{bmatrix} = \dots$$

rotational dynamics of  
an airplane

Ex 11.13

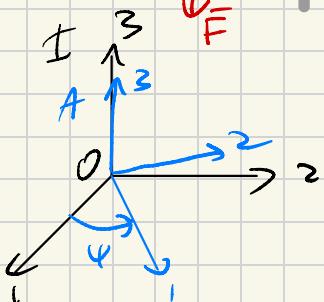


$$[\bar{\lambda}_G]_C = \begin{bmatrix} m_1 \\ 0 \\ 0 \end{bmatrix}_C$$

$$\bar{M}_G = \frac{\bar{I}_{\bar{A}}}{\bar{\omega}_G} (\bar{I} \bar{h}_G)$$

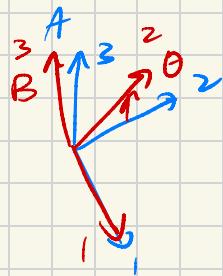
$$(\bar{I} \bar{h}_G)_C = ([\bar{I} \bar{G}]_C (\bar{I} \bar{\omega}_C)_C$$

$$= \begin{bmatrix} I_1 & 0 & 0 \\ 0 & I_2 & 0 \\ 0 & 0 & I_3 \end{bmatrix} \begin{bmatrix} \bar{\omega}_1 \\ \bar{\omega}_2 \\ \bar{\omega}_3 \end{bmatrix}_C$$



$${}^I \bar{\omega}^A = \dot{\psi} \hat{a}_3$$

$${}^I R^A = \begin{bmatrix} C_1 & -S_1 & 0 \\ S_1 & C_1 & 0 \\ 0 & 0 & 1 \end{bmatrix}$$



$${}^A \bar{\omega} {}^B = \dot{\theta} \hat{b}_1$$

$${}^A R {}^B = \begin{bmatrix} 1 & 0 & 0 \\ 0 & \cos \theta & -\sin \theta \\ 0 & \sin \theta & \cos \theta \end{bmatrix}$$

$$\hat{c}_2 = \hat{b}_2$$

Spin axis

$$C = (G, \hat{c}_1, \hat{c}_2, \hat{c}_3) \text{ body frame } {}^B \bar{\omega} {}^C = \omega \hat{b}_2$$

$${}^B R {}^C = \begin{bmatrix} \cos \phi & 0 & \sin \phi \\ 0 & 1 & 0 \\ -\sin \phi & 0 & \cos \phi \end{bmatrix}$$

$$[I_G]_B = {}^B R {}^C [I_G]_C ({}^B R {}^C)^T$$

$$= \begin{pmatrix} \cos \phi & 0 & \sin \phi \\ 0 & 1 & 0 \\ -\sin \phi & 0 & \cos \phi \end{pmatrix} \begin{pmatrix} I_1 & 0 & 0 \\ 0 & I_2 & 0 \\ 0 & 0 & I_3 \end{pmatrix} \begin{pmatrix} \cos \phi & 0 & -\sin \phi \\ 0 & 1 & 0 \\ \sin \phi & 0 & \cos \phi \end{pmatrix}$$

$$= \begin{pmatrix} \cos \phi I_1 & 0 & \sin \phi I_1 \\ 0 & I_2 & 0 \\ -\sin \phi I_1 & 0 & \cos \phi I_1 \end{pmatrix} \begin{pmatrix} \cos \phi & 0 & -\sin \phi \\ 0 & 1 & 0 \\ \sin \phi & 0 & \cos \phi \end{pmatrix}$$

$$= \begin{pmatrix} \cos^2 \phi I_1 + \sin^2 \phi I_3 & 0 & \cos \phi \sin \phi I_1 \\ 0 & I_2 & 0 \\ -\cos \phi \sin \phi I_1 & 0 & \cos^2 \phi I_1 + \sin^2 \phi I_3 \end{pmatrix}$$

$$\bar{M}_G = \frac{\partial}{\partial \epsilon} (\bar{F}_{\bar{h}_G}) + \bar{F}_{\bar{w}} \bar{B}_x \bar{I}_{\bar{h}_G}$$

$$\begin{bmatrix} M_1 \\ 0 \\ 0 \end{bmatrix}_B = \frac{\partial}{\partial \epsilon} \begin{bmatrix} I_1 w_1 \\ I_2 w_2 \\ I_3 w_3 \end{bmatrix} + \begin{bmatrix} 0 - w_3 w_2 \\ w_3 0 - w_1 \\ w_2 w_1 0 \end{bmatrix} \begin{bmatrix} I_1 w_1 \\ I_2 w_2 \\ I_3 w_3 \end{bmatrix}$$

$$\hat{b}_1: M_1 = I_1 w_1 + (I_2 - I_1) w_2 w_2$$

$$\hat{b}_2: 0 = I_2 w_2$$

$$\hat{b}_3: 0 = I_3 w_3 + (I_2 - I_1) w_1 w_2$$

$$\begin{aligned} \bar{F}_{\bar{w}}^c &= \bar{F}_{\bar{w}}^A + \bar{F}_{\bar{w}}^B + \bar{F}_{\bar{w}}^C \\ &= \dot{\gamma} \hat{a}_3 + \dot{\theta} \hat{b}_1 + \dot{\Sigma} \hat{c}_2 \end{aligned}$$

$$\begin{bmatrix} \bar{F}_{\bar{w}}^c \end{bmatrix}_c = \begin{bmatrix} w_1 \\ w_2 \\ w_3 \end{bmatrix}_c = \begin{bmatrix} C_R^A \end{bmatrix}^A \begin{bmatrix} 0 \\ 0 \\ \dot{\gamma} \end{bmatrix}_A + \begin{bmatrix} C_R^B \end{bmatrix}^B \begin{bmatrix} \dot{\theta} \\ 0 \\ 0 \end{bmatrix}_B + \begin{bmatrix} 0 \\ \dot{\Sigma} \\ 0 \end{bmatrix}_C$$

$$C_R^A = C_R^B R^B R^A$$

$$= \begin{bmatrix} C_R^A & 0 & -S_R^A \\ 0 & 1 & 0 \\ S_R^A & 0 & C_R^A \end{bmatrix} \begin{bmatrix} 1 & 0 & 0 \\ 0 & C_R^B & S_R^B \\ 0 & -S_R^B & C_R^B \end{bmatrix} = \begin{bmatrix} C_R^A & S_R^A & -S_R^A C_R^B \\ 0 & C_R^B & S_R^B \\ S_R^A & -C_R^A S_R^B & C_R^A C_R^B \end{bmatrix}$$

$$\begin{bmatrix} w_1 \\ w_2 \\ w_3 \end{bmatrix}_c = \begin{bmatrix} C_R^A & S_R^A & -S_R^A C_R^B \\ 0 & C_R^B & S_R^B \\ S_R^A & -C_R^A S_R^B & C_R^A C_R^B \end{bmatrix} \begin{bmatrix} 0 \\ 0 \\ \dot{\gamma} \end{bmatrix}_A + \begin{bmatrix} C_R^B & 0 & -S_R^B \\ 0 & 1 & 0 \\ S_R^B & 0 & C_R^B \end{bmatrix} \begin{bmatrix} \dot{\theta} \\ 0 \\ 0 \end{bmatrix}_B + \begin{bmatrix} 0 \\ \dot{\Sigma} \\ 0 \end{bmatrix}_C$$

$$\left. \begin{array}{l} \omega_1 = -\dot{\theta} \cos \phi + \dot{\phi} \sin \phi \\ \omega_2 = \dot{\theta} \sin \phi + \dot{\phi} \cos \phi \\ \omega_3 = \dot{\phi} \cos \phi + \dot{\theta} \sin \phi \end{array} \right\} \rightarrow \left\{ \begin{array}{l} \dot{\phi} = \dots \\ \dot{\theta} = \dots \\ \dot{\phi} = \omega \end{array} \right.$$

kinematics

$$(3-1-2 \quad \psi, \theta, \phi)_{\perp}^c$$

pinned RB

let Q be fixed in C & I, then

recall Ch 9

$$\stackrel{I}{\frac{d}{dt}} (\stackrel{I}{h}_Q) = \stackrel{I}{M}_Q$$

$$[\stackrel{I}{h}_Q]_c = [\stackrel{I}{I}_Q]_c [\stackrel{I}{\bar{w}}]^c_c$$

\* parallel axis theorem (11.5)

$$\stackrel{I}{I}_G \rightarrow \stackrel{I}{I}_Q$$

3D RB Work & Energy

recall Ch 7, 9  $T_0 = T_{G/0} + T_G$

$$T_{G/0} = \frac{1}{2} m_0 / \|\stackrel{I}{v}_{G/0/0}\|^2$$

$$T_G = \frac{1}{2} \stackrel{I}{I}_G / \|\stackrel{I}{\bar{w}}\|^2$$

scalar

planar RB

3D RB

$$T_G = \frac{1}{2} {}^I\bar{\omega}^c \cdot {}^I\bar{h}_G \quad \underline{\text{3D RB}}$$

$$= \frac{1}{2} \left[ {}^I\bar{\omega}^c \right]_c^T \left[ {}^I\bar{h}_G \right]_c$$

$$= \frac{1}{2} \left[ {}^I\bar{\omega}^c \right]_c^T [{}^I\bar{I}\alpha]_c \left[ {}^I\bar{\omega}^c \right]_c$$

$$= \frac{1}{2} \begin{bmatrix} \omega_1 & \omega_2 & \omega_3 \end{bmatrix}_c^T \begin{bmatrix} I_1 & 0 & 0 \\ 0 & I_2 & 0 \\ 0 & 0 & I_3 \end{bmatrix}_c \begin{bmatrix} \omega_1 \\ \omega_2 \\ \omega_3 \end{bmatrix}_c$$

$$= \frac{1}{2} (I_1 \omega_1^2 + I_2 \omega_2^2 + I_3 \omega_3^2)$$

WE #1  $T_O(t_2) = T_O(t_1) + \omega^{(\text{tot})}$

+ WE #2  $U_O(t_2) = U_O(t_1) - \omega^{(c)}$

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WE #3  $E_O(t_2) = E_O(t_1) + \omega^{(nc)}$

\*  $E_O$  is conserved if  $\omega^{(nc)} = W_{G/O}^{(nc)} + W_G^{(nc)} = 0$

$\uparrow$   $\uparrow$   
translation rotation

### Total Energy of Airplane

$$E_O = T_O + U_O$$

$$= T_{G/O} + T_G + U_O$$

$$T_{G/O} = \frac{1}{2} m_O \| {}^F \bar{v}_{O/O} \|^2$$

$$\left[ \begin{smallmatrix} \bar{u} \\ \bar{v} \\ \bar{w} \end{smallmatrix} \right]_c = \left[ \begin{smallmatrix} u \\ v \\ w \end{smallmatrix} \right]_c$$

$$\|\bar{\vec{v}}_{\text{total}}\|^2 = u^2 + v^2 + w^2$$

$$T_{\text{Gyro}} = \frac{1}{2} m_G (u^2 + v^2 + w^2)$$

$$T_G = \frac{1}{2} \left[ \begin{smallmatrix} \bar{u} \\ \bar{v} \\ \bar{w} \end{smallmatrix} \right]_c^\top \left[ \begin{smallmatrix} I_G \end{smallmatrix} \right] \left[ \begin{smallmatrix} \bar{u} \\ \bar{v} \\ \bar{w} \end{smallmatrix} \right]_c$$

$$= \frac{1}{2} \left[ \begin{smallmatrix} p & q & r \end{smallmatrix} \right]_c \begin{pmatrix} I_1 & 0 & -I_3 \\ 0 & I_2 & 0 \\ -I_3 & 0 & I_3 \end{pmatrix} \begin{pmatrix} p \\ q \\ r \end{pmatrix}$$

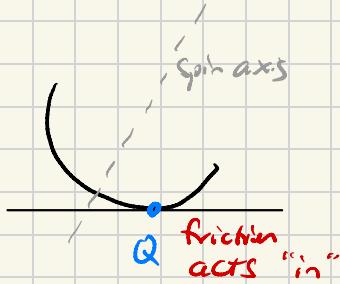
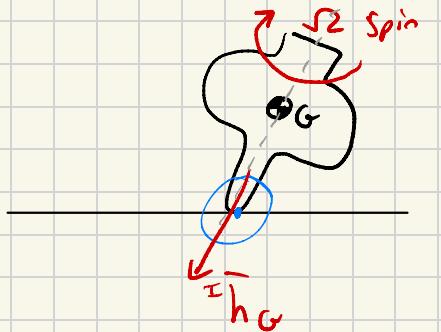
$$= \frac{1}{2} \left[ \begin{smallmatrix} p & q & r \end{smallmatrix} \right]_c \begin{pmatrix} I_1 p - I_{13} r \\ I_2 q \\ -I_{13} p + I_3 r \end{pmatrix}$$

$$T_G = \frac{1}{2} \left[ (I_1 p - I_{13} r) p + I_2 q^2 + (-I_{13} p + I_3 r) r \right]$$

$$U_o = U_o^{\text{(weight)}}$$

$$= m_G g h = m g z$$

Typhosis  
Ex 11.5



$$\bar{M}_G \approx \bar{\omega}^B \times \bar{h}_G$$

$\bar{\omega}_G \times \bar{F}$  out  $\times \downarrow \Rightarrow$  top self-righting

