

ENAE 432 0101

Homework 05: MATLAB & Transfer Functions

Due on March 7th, 2025 at 05:00 PM

Dr. Sanner, 09:00

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Problem 1:

Consider the family of transfer functions:

$$G(s) = \frac{6(\tau s + 1)}{s^2 + 2s + 4}.$$

1. Use MATLAB to generate the step response for this system in the three cases $\tau = 0$, $\tau = 1$, and $\tau = -1$. Use `hold on` to overlay all three responses on a single graph. Right-click on the resulting plot and use the "Characteristics" submenu to label the peak values and times. Click on the dots that appear to pop up a box with numerical details about each point.
2. Qualitatively, how do the responses in P01a agree with the class discussion regarding step responses for transfer functions containing zeros? Quantitatively, how do the numerical values for peak response and peak time agree with the class discussion in the specific case that $\tau = 0$?

Solution

Part A

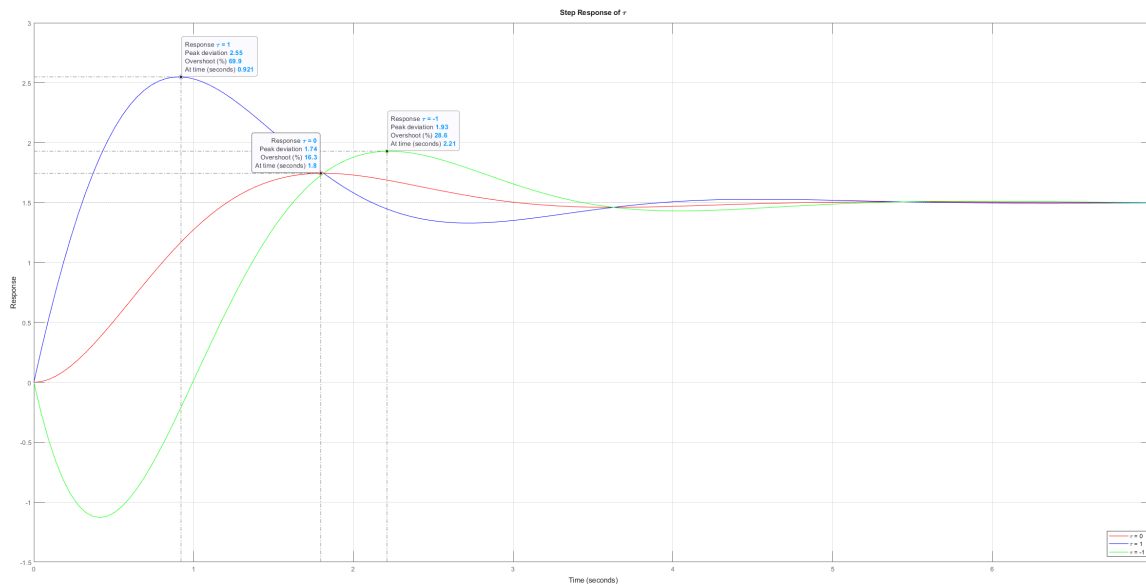


Figure 1: Step Response of τ with labeled Peak Values and Times

Part B

When $\tau = 0$, the transfer function has no zeroes, and the response will be the same as the standard second-order response for complex conjugate poles. When $\tau \neq 0$, the zero of the transfer function will be $z = -\frac{1}{\tau}$. Therefore, when $\tau = -1$, there is a zero in the LHP, and when $\tau = 1$, there is a zero in the RHP. As we discussed in class, the LHP zero will cause a higher peak overshoot and have a faster peak time compared to the standard second-order response. This behavior shows up in the plot, as seen with both $\tau = 1$ and $\tau = -1$.

MATLAB gives poles as $-1 \pm 1.732j$.

$$\begin{aligned}
 t_p &= \frac{\pi}{\omega_d} \\
 &= \frac{\pi}{1.732} \\
 t_p &= 1.81 \text{ sec} \quad \square \\
 M_p &= e^{\sigma t_p} \\
 &= e^{-1.81} = 0.16302 \\
 y_p &= G(0) \times (1 + M_p) \\
 &= \frac{3}{2} (1 + 0.16302) \\
 y_p &= 1.745 \quad \square
 \end{aligned}$$

These values align with the peak response and peak time given by MATLAB for $\tau = 0$.

Code

```

1      s = tf('s');
2      tau = [0, 1, -1];
3      colors = ['r', 'b', 'g'];
4      denom = s^2 + 2*s + 4;
5
6      figure;
7      hold on;
8      for j = 1:length(tau)
9          G = 6 * (tau(j) * s + 1) / denom;
10         step(G, colors(j));
11     end
12
13     grid on;
14     legend('\tau = 0', '\tau = 1', '\tau = -1', Location="southeast");
15     title('Step Response of \tau');
16     xlabel('Time');
17     ylabel('Response');
18     hold off;
19

```

Listing 1: MATLAB code for P01

Problem 2:

1. Repeat P01a if instead the denominator of $G(s)$ is $s^2 + 4s + 4$; label the settling times on the graph instead of the peaks
2. For the $\tau = 0$ case, how does the settling time compare with the approximation discussed in the lecture? From the theory, would you expect to see any overshoot in the step response for this case?
3. For the two cases where $\tau \neq 0$, do either exhibit overshoot? If so, how much? Is this overshoot associated with oscillations in the response?

Solution

Part A

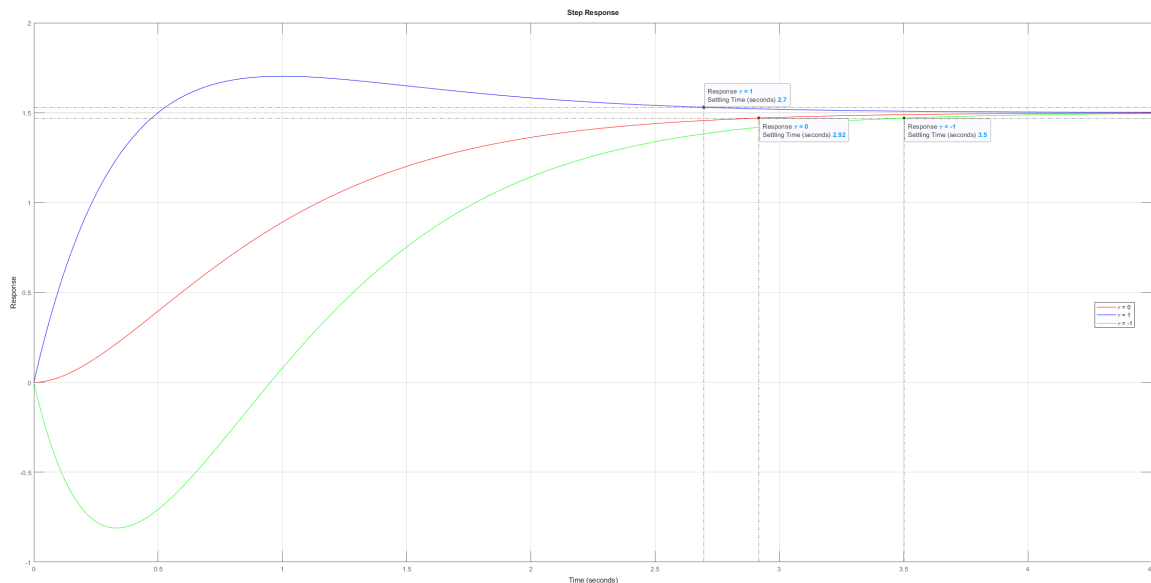


Figure 2: Step Response of τ with labeled Settling Times

Part B

MATLAB gives repeated poles of -2 . For a repeated real pole, the damping ratio will be 1, and settling time will be $\tau_s \approx \frac{6}{|\sigma|} = 3$ sec. MATLAB gave a numerical settling time of 2.92 sec, which differs from the theoretical value we just found, and falls outside of the 2% approximation.

As we discussed in class, when the transfer function has repeated real roots, the system response will not oscillate. Therefore, there will be no overshoot in the response, and will instead act like the standard first-order response.

Part C

When $\tau = 1$, the system response overshoots, with a peak response of 1.7 (0.2 greater than the steady-state response). When $\tau = -1$, the system response undershoots. As stated in P02a, there will be no oscillations.

Code

```
1      denom = s^2 + 4*s + 4;
2
3      figure;
4      hold on;
5      for j = 1:length(tau)
6          G = 6 * (tau(j) * s + 1) / denom;
7          step(G,colors(j));
8      end
9
10     grid on;
11     legend('\tau = 0', '\tau = 1', '\tau = -1', 'Location', 'best');
12     title('Step Response');
13     xlabel('Time');
14     ylabel('Response');
15     hold off;
16
```

Listing 2: MATLAB code for P02

Problem 3:

Use MATLAB to obtain the Bode diagrams for the transfer function:

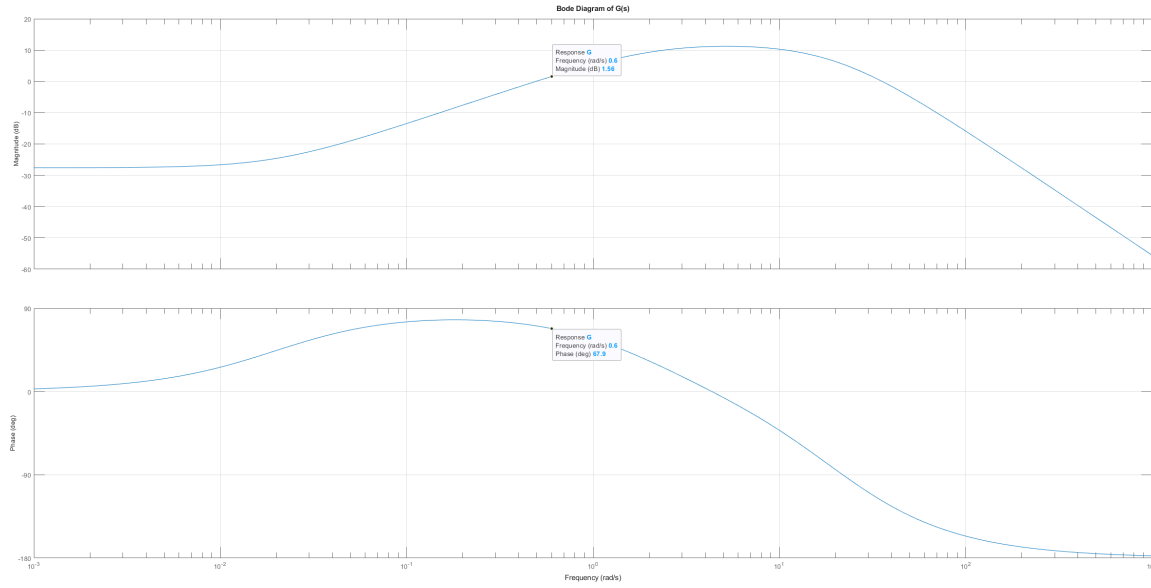
$$G(s) = \frac{5000(s + 0.02)}{3(2 + s)(20 + s)^2}$$

1. If the input to the system is $u(t) = \sin(\frac{6t}{10})$, what does the diagram predict the steady-state output of the system will be? Highlight the point(s) on each diagram you use to calculate this.
2. Analytically verify your result in P03a by explicitly calculating $G(\omega j)$, $|G(\omega j)|$, and $\angle G(\omega j)$ for the appropriate value of ω .
3. If the input to the system is $u(t) = 2\sin(70t + \frac{\pi}{4})$, what do you expect the steady-state output of the system will be? Indicate the point(s) on each diagram you use to calculate this. Repeat P03b for this input.
4. For an input of the form $u(t) = 2\sin(\omega t)$, approximately what range of frequencies ω would result in the largest amplitude oscillations in the steady-state output? Determine from the graph as exactly as possible the actual output amplitude at these frequencies. Verify using the technique in P03b.
5. For the input in P03d, what value of ω will result in the output oscillations lagging the input by 90° ("lag" = negative phase shift)? What will the amplitude of the output oscillations be at this frequency? Use the plot to estimate, then the technique in P03b for precision.

Solution**Part A**

With an input of $u(t) = \sin(\frac{6t}{10})$, we take the points on the Bode Diagram corresponding to $\omega = 0.6 \text{ rad/sec}$.

$$\begin{aligned} \frac{A}{B} &= |G(\omega j)|, \begin{cases} A = |G(\omega j)| \\ B = 1 \end{cases} \\ \phi - \psi &= \angle G(\omega j), \begin{cases} \phi = \angle G(\omega j) \\ \psi = 0 \end{cases} \\ A &= |G(0.6j)| = 1.65 \text{ dB} \\ &= 10^{\frac{1.56}{20}} = 1.197 \\ \phi &= \angle G(0.6j) = 67.9^\circ = 1.185 \text{ rad} \\ y_{ss} &= 1.197 \sin(\frac{3}{5}t + 1.185) \quad \square \end{aligned}$$

Figure 3: Bode Diagrams of $G(s)$ with labeled Steady-State Locations

Part B

$$\begin{aligned}
 G(0.6) &= \frac{5000(s + 0.02)}{3(2 + s)(20 + s)^2} \Big|_{s=0.6} \\
 G(0.6) &= \frac{5000(s + 0.02)}{3(2 + 0.6)(20 + 0.6)^2} = 0.4492 + 1.1094j \\
 |G(0.6)| &= \sqrt{(0.4492)^2 + (1.1094)^2} = 1.197 \\
 \angle G(0.6) &= \tan^{-1}\left(\frac{1.1094}{0.4492}\right) = 1.185 \text{ rad} \\
 y_{ss} &= 1.197 \sin\left(\frac{3}{5}t + 1.185\right) \quad \square
 \end{aligned}$$

This result is the same as the one found in P03a.

Part C

We repeat the same process as P03a and P03b, but with the points corresponding to $\omega = 70 \text{ rad/sec}$. Repeating P03a:

$$\begin{aligned}
 \frac{A}{B} &= |G(\omega j)|, \begin{cases} A = |G(\omega j)| \\ B = 2 \end{cases} \\
 \phi - \psi &= \angle G(\omega j), \begin{cases} \phi = \angle G(\omega j) \\ \psi = \frac{\pi}{4} \end{cases} \\
 |G(70j)| &= -10 \text{ dB} \\
 &= 10^{\frac{-10}{20}} = 0.316
 \end{aligned}$$

$$\angle G(70j) = -146^\circ = -2.548 \text{ rad}$$

$$A = B|G(\omega j)|$$

$$= 2|G(70j)|$$

$$= 0.632$$

$$\phi = \angle G(\omega j) + \psi$$

$$= \angle G(70j) + \frac{\pi}{4}$$

$$= -2.548 + \frac{\pi}{4} = -1.762 \text{ rad}$$

$$y_{ss} = 0.632 \sin(70t - 1.762) \quad \square$$

Repeating P03b:

$$\begin{aligned} G(70j) &= \frac{5000(s + 0.02)}{3(2 + s)(20 + s)^2} \Big|_{s=70j} \\ &= \frac{5000(70j + 0.02)}{3(2 + 70j)(20 + 70j)^2} = -0.2621 - 0.1735j \end{aligned}$$

$$|G(70j)| = \sqrt{(-0.2621)^2 + (-0.1735)^2} = 0.314$$

$$\angle G(70j) = \pi - \tan^{-1}\left(\frac{-0.1735}{-0.2621}\right) = -2.557 \text{ rad}$$

$$A = B|G(\omega j)|$$

$$= 2|G(70j)|$$

$$= 0.628$$

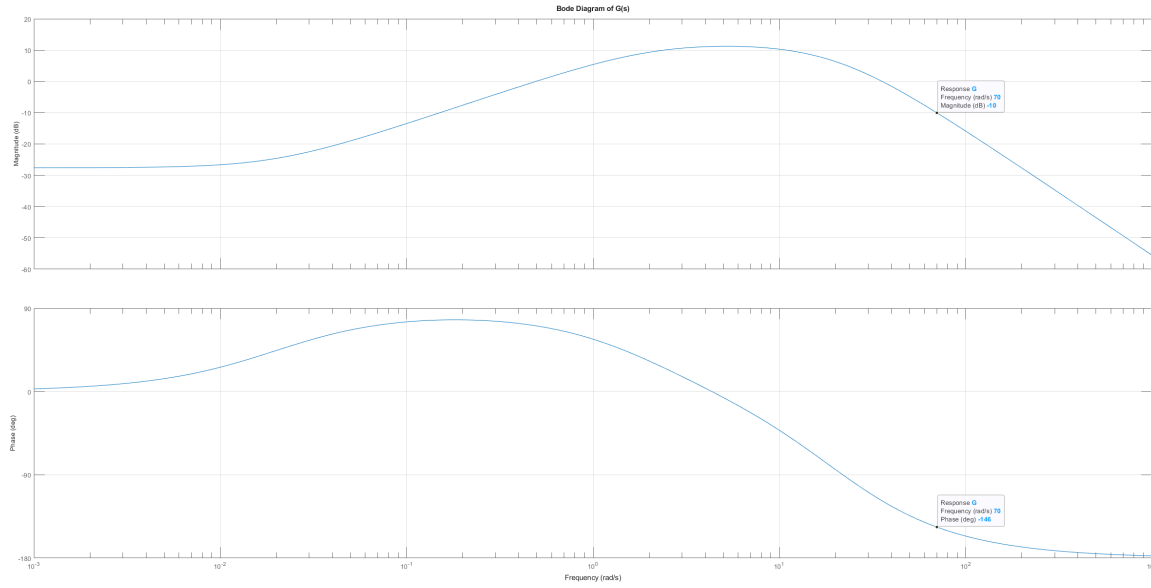
$$\phi = \angle G(\omega j) + \psi$$

$$= \angle G(70j) + \frac{\pi}{4}$$

$$= -2.557 + \frac{\pi}{4} = -1.771 \text{ rad}$$

$$y_{ss} = 0.628 \sin(70t - 1.771) \quad \square$$

We get approximately the same answers from the Bode Diagram and numerical analysis.

Figure 4: Bode Diagrams of $G(s)$ with labeled Steady-State Locations

Part D

As A relies on $|G(\omega j)|$ and B , with constant B , A (the amplitude of the steady-state oscillation) reaches its maximum when $|G(\omega j)|$ is at its maximum. We can get this value from the Bode Diagram. **MATLAB** gives this value as 11.2 dB at $\omega = 5.22$ rad/sec.

$$|G(5.22j)| = 10^{\frac{11.2}{20}} = 3.63$$

$$A = B|G(\omega j)|$$

$$= 2|G(5.22j)|$$

$$A = 7.26 \quad \square$$

Verifying analytically:

$$\begin{aligned} G(5.22j) &= \frac{5000(s + 0.02)}{3(2 + s)(20 + s)^2} \Big|_{s=5.22j} \\ &= \frac{5000(5.22j + 0.02)}{3(2 + 5.22j)(20 + 5.22j)^2} = 3.603 - 0.539j \end{aligned}$$

$$|G(5.22j)| = \sqrt{(3.603)^2 + (-0.539)^2} = 3.643$$

$$A = B|G(\omega j)|$$

$$= 2|G(5.22j)|$$

$$A = 7.286 \quad \square$$

We get approximately the same answers from the Bode Magnitude Diagram and numerical analysis, with a maximum amplitude of 7.3 at $\omega = 5.22$ rad/sec.

Part E

With an input of $u(t) = 2 \sin(\omega t)$, $\psi = 0 \implies \phi = \angle G(\omega j)$. MATLAB gives $\angle G(\omega j) = -90^\circ$ when $\omega = 21.9 \text{ rad/sec}$. We now use the Bode Magnitude Diagram to find the amplitude at $\omega = 21.9 \text{ rad/sec}$ as 5.52 dB.

$$\begin{aligned}
 |G(21.9j)| &= 10^{\frac{5.52}{20}} = 1.888 \\
 A &= B|G(\omega j)| \\
 &= 2|G(21.9j)| \\
 A &= 3.7 \quad \square
 \end{aligned}$$

Verifying analytically:

$$\begin{aligned}
 G(21.9j) &= \frac{5000(s + 0.02)}{3(2 + s)(20 + s)^2} \Big|_{s=21.9j} \\
 &= \frac{5000(21.9j + 0.02)}{3(2 + 21.9j)(20 + 21.9j)^2} = -1.887j \\
 |G(21.9j)| &= \sqrt{(-1.887)^2} = 1.887 \\
 A &= B|G(\omega j)| \\
 &= 2|G(21.9j)| \\
 A &= 3.774 \quad \square
 \end{aligned}$$

We get approximately the same answers from the Bode Magnitude Diagram and numerical analysis, with an amplitude of 3.8 when there is 90° lag in the oscillations.

Code

```

1      G = (5000 * (s + 0.02))/(3 * (2 + s) * (20 + s)^2);
2      w = logspace(-3, 3, 10000);
3      figure;
4      bode(G,w);
5      grid on;
6      title('Bode Diagram of G(s)');
7

```

Listing 3: MATLAB code for P03

Problem 4:

1. Give the Bode form for the transfer function in P03. Identify the Bode gain numerically. Discuss how and why this gain agrees with the "starting" (low frequency) magnitude shown on the left side of the Bode magnitude plot in P03.
2. Use the `bodemag` function in `MATLAB` to get just the Bode magnitude diagram for the transfer function in P03, put a grid on it, and print out this plot (use `orient landscape` just before printing to get a plot that fills the page horizontally). Sketch on top of this diagram the straight-line approximation using the technique described in class. Comment on the accuracy of this approximation.

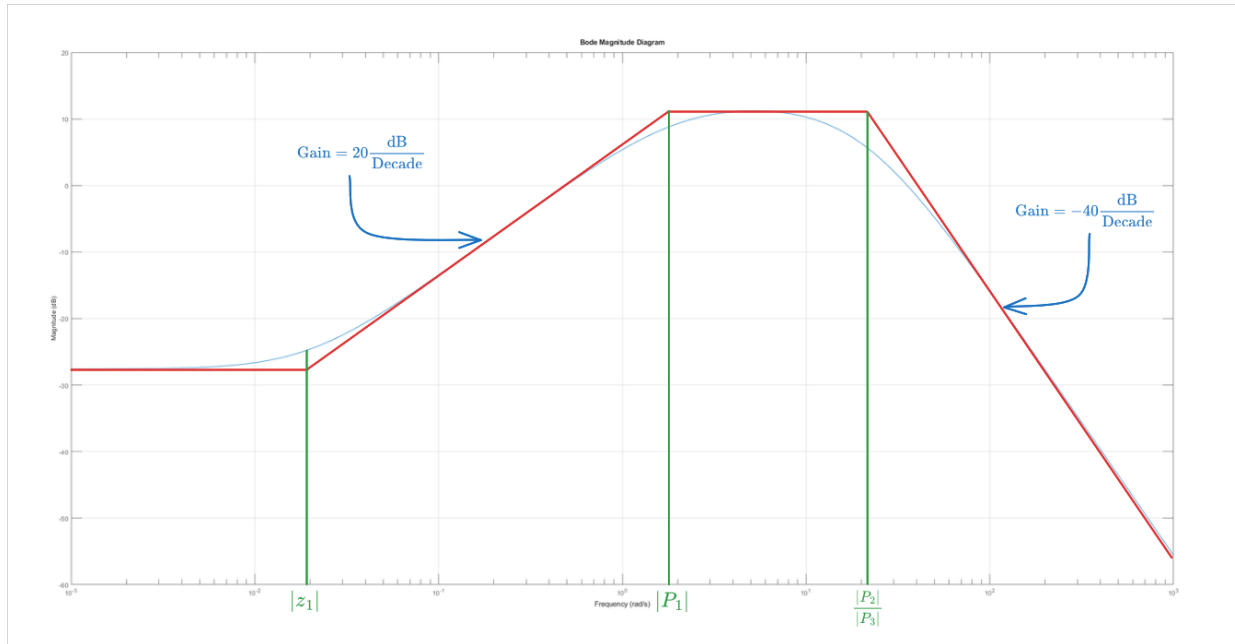
Solution**Part A**

$$\begin{aligned}
 N = 0 &\implies K_B = G(0) \\
 G(0) &= \left. \frac{5000(s + 0.02)}{3(2 + s)(20 + s)^2} \right|_{s=0} \\
 &= \frac{5000(0 + 0.02)}{3(2 + 0)(20 + 0)^2} = 0.0417 \\
 A_{\text{vdB}} &= 20 \log(K_B) \\
 &= 20 \log(0.0417) \\
 A_{\text{vdB}} &= -27.6 \text{ dB} \quad \square
 \end{aligned}$$

The Bode Gain for the transfer function is -27.6 dB , which agrees with the starting magnitude on the Bode Magnitude Diagram from `MATLAB`. This is due to $\omega \rightarrow 0$ on the left axis of the plot, causing the transfer function to be approximately constant.

Part B

The straight-line approximation is reasonably accurate, following the overall behavior pretty well. However, near the zeroes and the poles, the approximation fails, modeling the effects as sudden instead of gradual, creating sharp corners where there should be smooth curves.

Figure 5: Bode Magnitude Diagram of $G(s)$ with sketched Straight-Line Approximation

Code

```

1  f1 = figure;
2  bodemag(G);
3  grid on;
4  orient landscape;
5  title('Bode Magnitude Diagram');
6

```

Listing 4: MATLAB code for P04