Introduction to Hydrodynamic Analysis with Ansys Aqwa

Appendix Slides

Release 2021 R2



Core Aqwa Programs

Aqwa-Line

• 3-D diffraction & radiation analysis program for wave force and structure response calculations; hydrostatic analysis

Aqwa-Librium

 Structure equilibrium position and force balance calculations; eigen-mode and dynamic stability analysis

Aqwa-Fer

• Spectral analysis of structure motion (wave frequency or/and drift frequency) and mooring tension in irregular waves



Core Aqwa Programs

Aqwa-Naut

 Time domain program for wave frequency structure motion and mooring tension analyses in regular and irregular waves

Aqwa-Drift

 Time domain program for drift frequency and wave frequency structure motion and mooring tension analysis in irregular waves

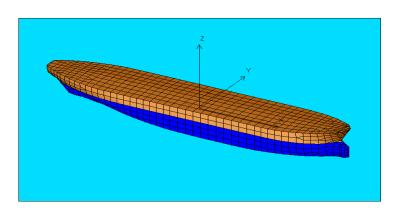
Aqwa Graphical Supervisor (AGS)

Aqwa pre and post processor; on-line analysis



/ Aqwa-Line

- Aqwa-Line is a 3D diffraction and radiation analysis program
- Frequency domain
- Structures are described by a number of panels
- Source distribution approach (boundary integration method)
- A source is placed at the centre of each panel and then the program solves for the source strengths, subject to the boundary conditions (see Aqwa Theory Manual)





Features

- Removal of irregular frequencies by auto-generated lid
- Multi-body hydrodynamic interactions (lid to suppress standing waves)
- Forward speed
- Second order forces
- Mean drift forces:
 - Far field momentum theory
 - Near field pressure-motion integration method
 - Full QTF matrix (difference & sum frequency components)

Aqwa-Line provides hydrodynamic coefficients for use in other programs in the Aqwa suite



General Warnings

Requirements	Reason
Number of diffracting elements should be no more than 30k (12k in 32-bit)	Solution time
Maximum number of total elements is 40k (18k in 32-bit)	Solution time
Normals point out	Modelling Convention
No gaps in between panels	Force balance
Facets cannot cut surface	Solution requirement

Geometric Property Warnings

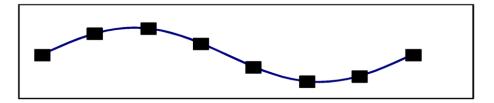
- Area ratio of adjacent elements < 3
- Aspect ratio (AR) > 1/3, where $AR = \frac{area}{longest \ side^2}$. (C = 1 for quadrilateral elements,

C = 2.3 for triangular elements)

- Element centres must be at least one facet radius (r_f) apart, $r_f = \sqrt{\frac{area}{\pi}}$
- Shape factor (parameter for regularity of panel)
- <0.2 = warning
- <0.02 = fatal error
- See Aqwa Theory Manual for more detail

Hydrodynamic warnings

- Minimum wave frequency (rad/s) > $0.001\sqrt{g/d}$
- Distance above sea bed must be > 0.5 r_f
- Longest side < 1/7 wavelength
 - Fatal error if more than 5% fail
- Nodes are not connected to another element = warning



Aqwa-Librium

- Equilibrium position, Static and Dynamic (oscillatory) stability
- Complex ship/offshore structure systems
- Various mooring, fender, pulley, winch, constraints configuration
- Equilibrium estimation under wave, wind and current combination
- Database approach for static catenary mooring line
- Finite element approach for dynamic cable (drag force)
- Iteration approach for determining equilibrium position
- Calculate the eigenvalues of linearized stiffness matrix to obtain static stability
- Eigenvalues of the impedance matrix to give dynamic (oscillatory) stability
- Series of wave spectrums



Aqwa-Librium

Theory in Aqwa-Librium

Equation for determining static equilibrium position

$$X_{j+1} = X_j + \mathbf{K}^{-1}(X_j)F(X_j)$$

- K is the stiffness matrix of the system,
- F is the force matrix
- The program iterates until $\Delta X = |X| + 1 |X|$ is less than a defined tolerance
- Static stability

$$\mathbf{K} X - \lambda X = 0$$

- \bullet Eigenvalue λ (< 0, unstable; = 0, neutral; > 0, stable)

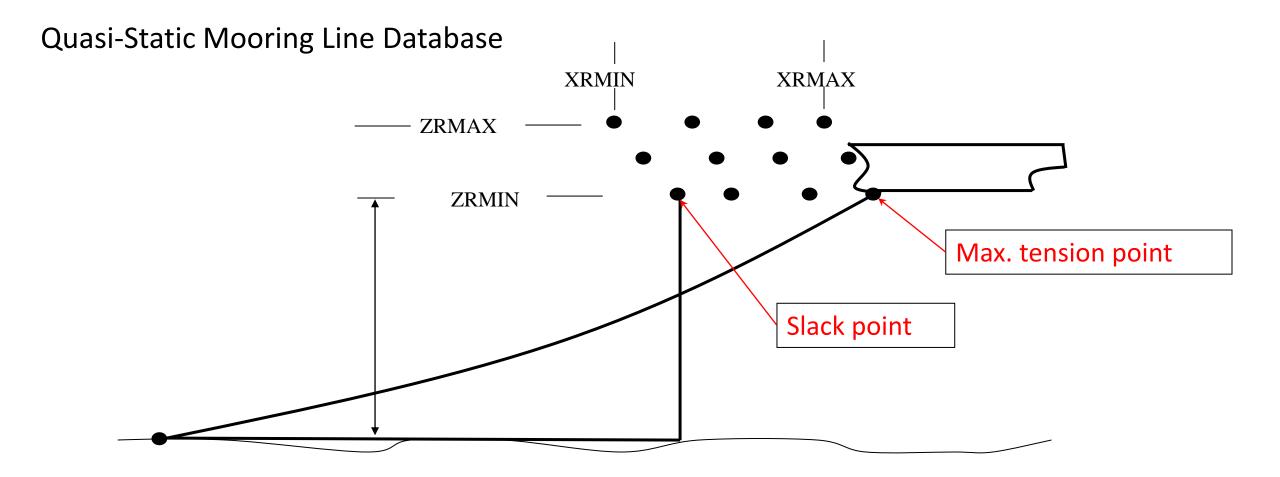
Dynamic stability
$$\begin{bmatrix} \mathbf{M}^{-1}\mathbf{C} & \mathbf{M}^{-1}\mathbf{K} \\ \mathbf{I} & \mathbf{0} \end{bmatrix} \begin{bmatrix} \mathbf{\bar{X}} \\ X \end{bmatrix} + \lambda \begin{bmatrix} \mathbf{\bar{X}} \\ X \end{bmatrix} = 0,$$

© Eigenvalue
$$\lambda$$
 (from $M\ddot{X} + C\dot{X} + KX = 0$, $X = e^{\lambda t}$, $\lambda = f + ig$)

- f < 0, stable (converging oscillations)</p>
- $\mathbf{\Phi}$ f > 0 and g = 0, unstable (steady oscillations)
- $\mathbf{\Phi}$ f > 0 and g \neq 0, unstable (oscillatory divergence)



Mooring Lines



Aqwa-Fer

- Principally for calculating the significant response of amplitudes in irregular waves
 - Frequency domain program
 - Linearized stiffness matrix / damping to obtain the transfer function and response spectrum
 - Simple, inexpensive approach to make systematic parameter study
 - Series of wave spectrums and mooring configurations





Typical applications:

- Calculation of wave frequency RAOs for uncoupled/coupled moored structures.
- Calculation of significant motions and tensions for the system due to wave frequency (high frequency) excitation.
- Calculation of significant motions and tensions for the system due to drift frequency (low frequency) excitation.
- Calculation of significant motions and tensions for the system due to wave frequency and drift frequency excitation combined.



Aqwa-Fer

Theory in Aqwa-Fer

• Response spectrum in irregular waves

$$S_{x_i x_i}(\omega) = \sum_{j} [\text{mod}(H_{ij}(\omega)F_j(\omega))]^2 S(\omega)$$

 $S_{xixi}(\omega)$: response spectrum in i-th degree of freedom,

 $H_{ii}(\omega)$: receptance matrix defined as

$$H_{ii}(\omega) = \left[-\omega^2 (M_s + M_a(\omega)) - i\omega B(\omega) + C\right]^{-1}$$

 $F_i(\omega)$: frequency dependent force (in j-th degree of freedom) on the structure

 $S(\omega)$: the wave spectrum

Aqwa-Fer

Linearization in Fer

Stiffness: stiffness (hydrostatic, mooring etc.) at the initial position
(= the static equilibrium position with RDEP option)

Damping: catenary cable drag is linearized using the RMS velocity, when NLID used

$$F_D = (C_D. |V_{RMS}|).V$$

wind drag is always linearized

current hull drag is linearized when LDRG option used

1st order hydrodynamic damping

any other input damping (fender, constraints)

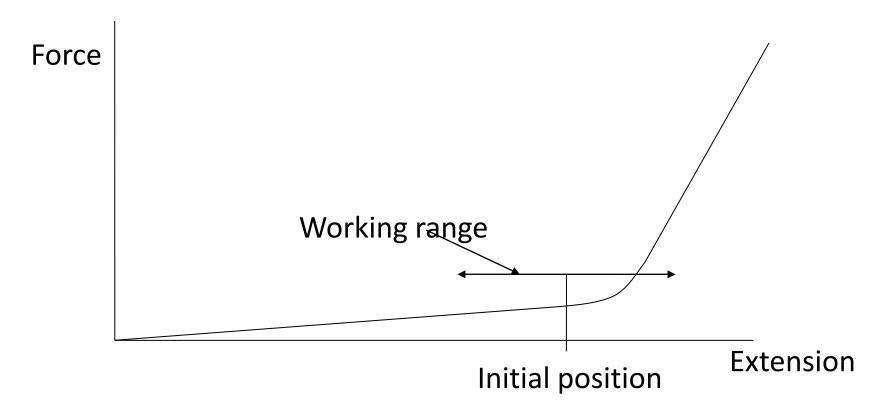
• Forces: 1st and 2nd order wave forces





Aqwa-Fer Mooring Stiffness Linearization

Typical Force-Extension curve for catenary mooring



Aqwa-Fer uses stiffness (i.e. slope) at initial position Aqwa-Drift/Naut uses changing stiffness over working range



- Aqwa-Drift and Aqwa-Naut are time-domain simulation programs
- For a series of time-steps they:
 - calculate the total force on the structure
 - calculate the acceleration
 - find the new position of the structure
- A two stage predictor/corrector integration scheme is used



Equations of motion in time domain

$$M_s \ddot{X}(t) = F(t)$$

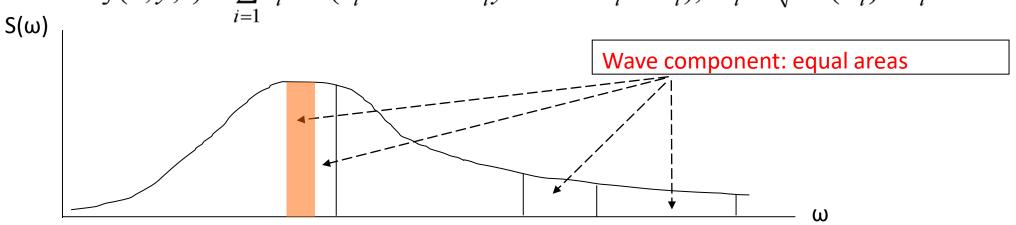
- F(t) is the total force on the structure, including
 - Incident wave force
 - Diffraction force
 - Drift force
 - Mooring force
 - Radiation force (damping)
 - •
- The equations of motion are solved in convolution integral form

$$[\mathbf{M}_{s} + \mathbf{M}_{a}(\infty)] \ddot{X}(t) = KX(t) + \int_{0}^{t} \mathbf{h}(t-\tau) \ddot{X}(\tau) d\tau + F_{1}(t)$$

Simulation of irregular waves

- Wave spectra processing:
 - Spectrum is split into sections of equal area for integration
 - Wave components are defined with frequency at the centre of the section (Max. 200)
 - Wave components are added together with random phase angles

$$\zeta(x, y, t) = \sum_{i=1}^{N} a_i \cos(k_i x \cos\theta + k_i y \sin\theta - \omega_i t + \varepsilon_i), \quad a_i = \sqrt{2S(\omega_i)\Delta\omega_i}$$



Drift vs. Naut

Drift	Naut
Irregular waves only	Regular or Irregular waves
Linear hydrostatic stiffness (mean water surface)	Non-linear hydrostatics and incident wave forces (instantaneous wave surface)
2 nd order drift forces	2 nd order incident wave (omits drift forces but some 2 nd order effects)

Summary

Linearity in Aqwa Programs

	Hydro- Statics	Diff / Radiation	Froude- Krylov	Drift Force	Mooring Force	Drag
Line	LIN	LIN	LIN	2 nd order	-	-
Librium eqm	NON	LIN	LIN	2 nd order	NON	Linearised
Librium stability	LIN	LIN	LIN	2 nd order	LIN	Linearised
Fer	LIN	LIN	LIN	2 nd order	LIN	Linearised
Drift	LIN	LIN	LIN	2 nd order	NON	NON
Naut	NON	LIN	NON	-	NON	NON