## Beam Diagrams and Formulas

The following beam diagrams and formulas have been found useful in the design of welded steel structures.

Proper signs, positive (+) and negative (-), are not necessarily indicated in the formulas. The following are suggested:

Shear diagram above reference line is (+)

| |---| |---|

Shear diagram below reference line is (-)

Reaction to left of (+) shear is upward (+)

2 <del>| + V</del>

Reaction to left of (-) shear is downward (-)

-V

Reaction to right of (+) shear is downward (-)

+ V

Reaction to right of (—) shear is upward (+)

Moment above reference line is (+) Compressive bending stresses on top fibers also tends to open up a corner connection

Moment diagram on same side as compressive stress

tends to close corner

Moment below reference line is (—) Compressive bending stresses on bottom fibers also tends to close up a corner connection

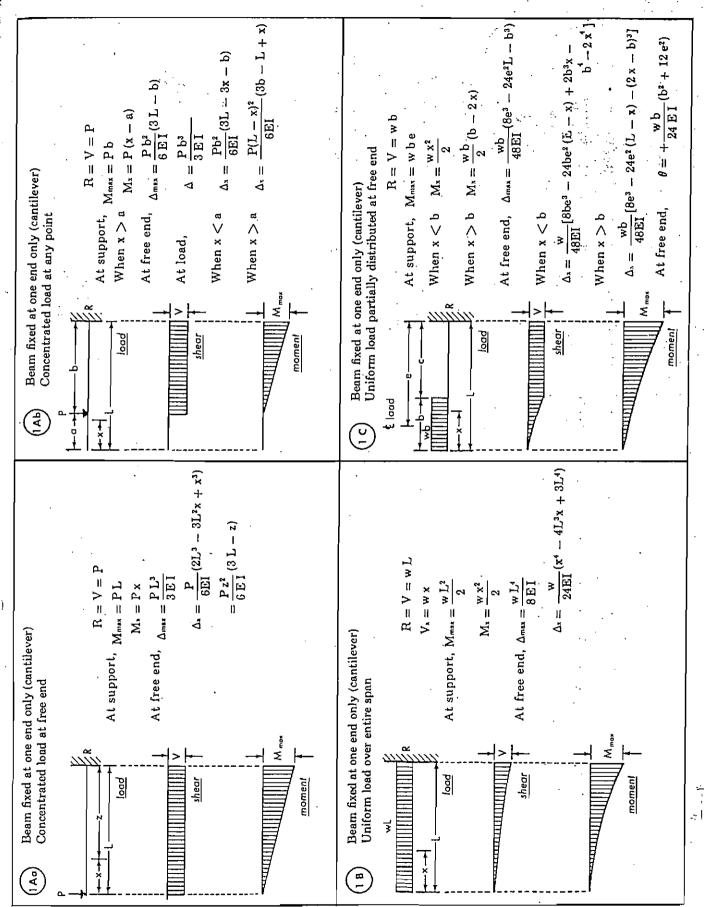
Angle of slope,  $\theta$  clockwise rotation (-), counter-clockwise rotation (+)

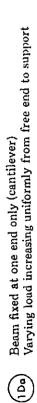
On the next page is a visual index to the various beam diagrams and formulas. As indicated, these are keyed by number to the type of beam and by capital letter to the type of load.

For some conditions, influence curves are included to illustrate the effect of an important variable. These are keyed to the basic beam diagram and are positioned as close as practical to the diagram.

## VISUAL INDEX TO FORMULAS ON FOLLOWING PAGES FOR VARIOUS BEAM-LOAD CONDITIONS

Type of LOAD  Type of BEAM	Cancentrated force	w [][][][][][][][][][][][][][][][][][][]	Uniform load partio' span	W Varying load	Cauple E
Cantilever free fixed	1Ab IP	18	1C [[]]	100 IDb	1E (
guided fixed	2A   + P	28			
Simply supported supported	3Ao PP	38	3C + 1	3D¢ 3D¢	3Eo (M, M <sub>2</sub> ) 3Ec (M, M <sub>2</sub> )
fixed fixed	4A0   1 P   4Ab   1 P   4Ac ( 1 P )	48a	4C	40	4E
supported fixed	5Aa TP	5B	5C 1	5Do 5Db	5E (1)
Single span with averhang	6Aa 1 P	680 T T	6Ca + + + + + + + + + + + + + + + + + + +		
Cantinuaus two span	7Aa T T T	7B 1 1	٠,	7D See odjocent to 39	For other multi-spon lood conditions, see discussion under ①



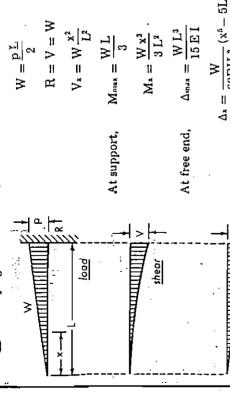


Varying load increasing uniformly from support to free end

≥

Beam fixed at one end only (cartilever)

(1Db)



$$M_{x} = \frac{W x^{2}}{3 L^{2}}.$$
(d) 
$$\Delta_{max} = \frac{W L^{3}}{15 E I}$$

$$\Delta_x = \frac{W}{60 E 1 L^2} \left( x^5 - 5 L^4 x + 4 L^5 \right)$$
 At free end, 
$$\theta = + \frac{W L^2}{12 E I}$$

 $\Delta_x = \frac{W}{60 E 1 L^2} \left[ L^4 (15 x - 11 L) - x^4 (5 L - x) \right]$ 

 $\frac{WL^2}{4 E I}$ 

 $^{-} + = 0$ 

At free end,

¥ gwa ¥

momen

 $M_x = \frac{W x^2}{3L^2} (x - 3L)$ 

 $M_{\text{max}} = \frac{2 \text{ W L}}{2 \text{ M L}}$ 

At support,

000

R = V = W

11 W L3

 $\Delta_{\text{max}} = \frac{1}{60 \text{ E I}}$ 

At free end,

sheor

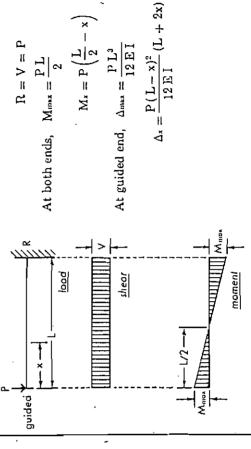


Beam fixed at one end only (cantilever)

moment

Monsent applied at free end

(IE)



 $\Delta x = \frac{M_o}{2 \ \mathrm{E} \ \mathrm{I}} \ (L - x)^2$ 

M. L

At free end,

sheor

mament

 $\Delta_{\text{mex}} = \frac{M_u \, L^2}{2 \, E \, I}$ 

At free end,

lood

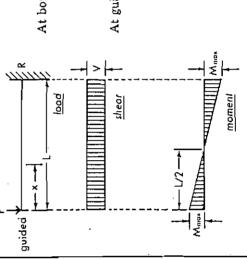
R = V = 0

 $M_{\star} = M_{\omega}$ 

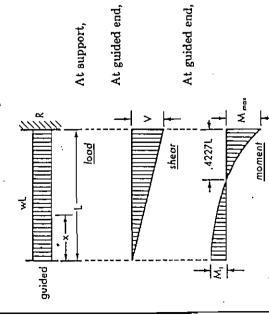
 $M_x = P\left(\frac{L}{2} - x\right)$ 

R = V = P

 $M_{max} = \frac{P L}{2}$ 



Bearn fixed at one end and free but guided at the other end Uniform load over entire span  $\binom{2B}{}$ 

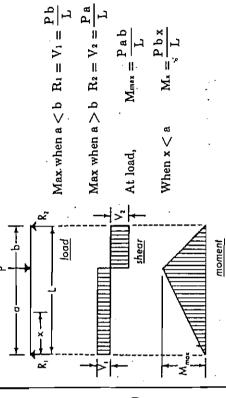


- R = V = wL $M_{max} = \frac{w L^2}{3}$  $V_x = w \; x$
- $M_x = \frac{W}{6} (L^2 3 \, x^2)$

₩ L²

M1 = -

 $W(L^2-x^2)^2$ 24 E I At guided end,  $\Delta_{max} = \frac{w L^4}{24 E I}$ Δ×



 $M_{max} = \frac{Pab}{L}$ 

 $M_x = \frac{P b_x}{V}$ 

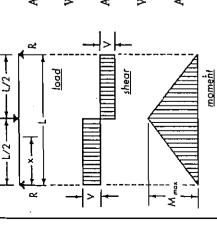
- when a > b  $\Delta_{max} = \frac{Pb}{3EIL} \sqrt{}$  $At \ x = \sqrt{\frac{L^2 - b^2}{}}$
- $\Delta = \frac{P a^2 b^2}{3 \times I L}.$ When x < a At load,

 $R_1=R_2=V=P/2$ 

Beam supported at both ends Concentrated load at mid-span

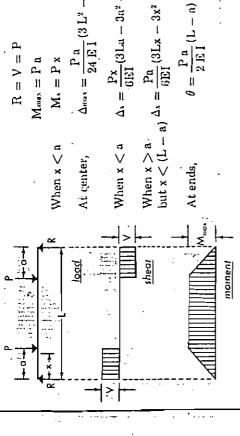
(g Ag

- $\Delta \mathbf{t} = \frac{\mathrm{Pa}}{48\mathrm{EI}} (3\mathrm{L}^2 4\mathrm{a}^2)$ When a < b
- At ends,

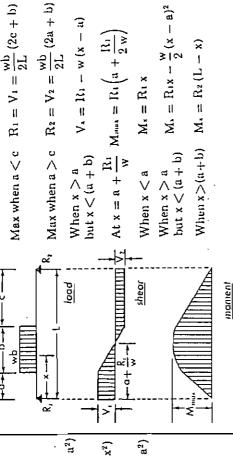


- $\Delta_{\text{mex}} = \frac{P L^3}{48 \ E \ I}$  $M_{max} = \frac{P L}{4}$ When x < L/2  $M_x = \frac{Px}{\sqrt{}}$ At load, At load,
- When  $x < L/2 ~\Delta_x = \frac{P\,x}{48\,E\,I}(3\,L^2 4\,x^2)$ 
  - $\theta_1 = -\frac{1}{16 \times I} = -\theta_2$ At end,





 $\Delta_{\text{max}} = \frac{P \, a}{24 \, \text{E} \, \text{I}} \, (3 \, \text{L}^2 - 4 \, a^2)$  $\Delta_1 = \frac{Px}{6BI}(3La - 3a^2 - x^2)$ When x > a. but  $x < (L - a)^{\Delta x} = \frac{Pa}{6BI} (3Lx - 3x^2 - a^2)$ 



## $M_x = \frac{wbx}{2} - \frac{w}{2} (x - a)^2$ $V_{\lambda} = w \left( a + \frac{b}{2} - x \right)$ $M_{\text{mux}} = \frac{w b}{2} \left( a + \frac{b}{4} \right)$ o ¥ $M_{x} = \frac{w b x}{2}$ R = V =but x < (a + b)When x < a When x > a At center,

 $R_1 = V_1 = \frac{P_1(L-a) + P_2b}{1}$ 

Beam supported at both ends Two unequal concentrated loads, unequally spaced from ends

(3 A d)

<u>ا</u> کے

 $P_{13} + P_{2}(L - b)$ 

 $R_2 = V_2 =$ 

000

 $V_s=R_1\stackrel{.}{-}P_1$ 

 $M_1 = R_1 a$  $M_2 = R_2 b$  $M_s = R_{1,x}$ 

<u>ت</u>ر.

When a = c

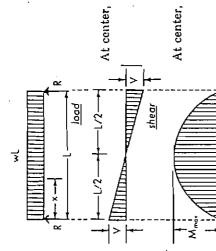
 $\Delta_1 = \frac{wb}{384EI} (-+8L^3 - 4b^2L + b^3)$ At center,

Max when R2<P2 Max when R1 < P1 but x < (L - b)When x > a When x < a sheor

but x < (L - b)  $M_x = R_1 x - P_1 (x)$ When x > a

Also see formulas on page 8

Beam supported at both ends Uniform load over entire span (38)



$$R = V = \frac{wL}{2}$$
$$V_{c} = w\left(\frac{L}{2} - x\right)$$

$$M_{\text{niox}} = \frac{\sqrt{2}}{8}$$

$$M_{x} = \frac{w L^{2}}{8}$$

$$M_x = \frac{w x}{2} (L - x)$$

$$\Delta_{\text{max}} = \frac{5 \text{ w L}^4}{384 \text{ E I}}$$

$$\Delta_{\text{x}} = \frac{\text{wx}}{24 \text{EI}} (L^3 - 2 \text{Lx}^2 + \text{x}^3)$$

$$W = \frac{PL}{2}$$

$$R_1 = V_1 = \frac{W}{3}$$

$$R_2 = V_2 (m_{MA}) = \frac{W}{3}$$

$$V_4 = \frac{W}{3} - \frac{W}{L^2}$$

At x = L/
$$\sqrt{3}$$
 = .5744 L  
 $M_{max} = \frac{2 W L}{9 \sqrt{3}}$  = .1283 W ]

momen

 $\theta = \frac{w L^3}{24 \to I}$ 

At ends,

moment

Benm supported at both ends Varying load, increasing uniformly to center

(g)

$$M_1 = \frac{W_X}{3L^2}(L^2 - x^2)$$

$$At x = L \sqrt{1 - \sqrt{8/15}} = .5193 L$$

$$\Delta_{max} = .01304 \frac{W L^3}{E I}$$

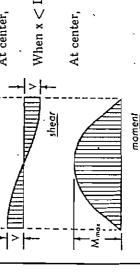
 $\Delta_{\mathbf{z}} = \frac{\mathbf{v} \cdot \mathbf{x}}{180 \times 1 L^2} (3 \times \mathbf{z})$ 

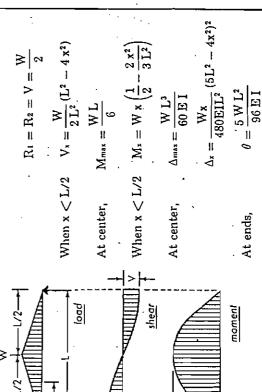
At center,

At center, 
$$\Delta_L = \frac{5 \text{ W L}^3}{384 \text{ EI}}$$

$$\theta_1 = -\frac{7 \text{ W L}^2}{180 \text{ EI}}$$
At ends, 
$$\theta_2 = +\frac{8 \text{ W L}^2}{180 \text{ EI}}$$

At ends, 
$$\begin{cases} \theta_1 = -\frac{7 \text{ W}}{180} \\ \theta_2 = +\frac{8 \text{ W}}{180} \end{cases}$$





$\theta_1 = -\frac{7 \text{ W L}^2}{180 \text{ E I}}$ $\theta_2 = +\frac{8 \text{ W L}^2}{180 \text{ E I}}$	
At ends,	
•	

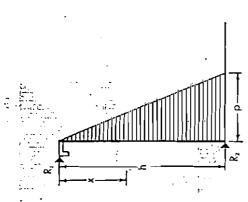
BEAM FORMULAS APPLIED TO SIDE OF TANK, BIN OR HOPPER

(p = pressure, psi; m = width of norm considered)



300

(dx)



 $R_1 = \frac{p h m}{}$ 

$$M_{max} = \frac{p h^2 m}{9 \sqrt{3}} = .0642 p h^2 m$$
 $M_x = \frac{p x m}{\sqrt{3}} (h^2 - x^2)$ 

$$(\Delta_1 = \frac{5 \, \mathrm{ph}^4 \, \mathrm{m}}{768 \, \mathrm{E} \, \mathrm{I}}$$

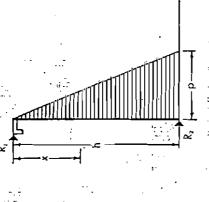
(\* These values are within 98%

of maximum.)

 $V_{max} = \frac{m h}{6} (p_1 + 2 p_2)$ 

$$\Delta x = \frac{p \times m}{360 \text{ E I h}} (3 x^4 - 10 \text{ h}^2)$$

$$\Delta_{\text{max}} = .00652 \frac{p \text{ h}^4 \text{ m}}{\text{E I}}$$



 $R_2 = \frac{p h m}{\tilde{n}} = V_{max}$ 

$$f_{\text{max}} = \frac{p \cdot r \cdot m}{9 \sqrt{3}} = .0642 \text{ p h}^2 \text{ n}$$

$$M_x = \frac{p \cdot x \cdot m}{6 \cdot h} (h^2 \cdot - x^2)$$

$$(\Delta t_{1} = \frac{5 \, \text{p} \, h^{4} \, \text{m}}{768 \, \text{E} \, \text{I}}$$

$$\Delta x = \frac{p \, x \, \text{m}}{360 \, \text{E} \, \text{I} \, \text{h}} (3 \, x^{4} - 10 \, h^{2} \, x^{2} + 7 \, h^{4})$$

$$\Delta_{\text{max}} = .00652 \frac{\text{p h}^4 \text{ m}}{\text{E I}}$$
(at x = .5193 h)

Also see formulas on page 7

Maximum bending moment is least when

$$a = .57 \text{ h}$$
  
 $b = .43 \text{ h}$ 

 $\Delta U = \frac{5 \, h^4 \, m}{768 \, E \, I} \, (p_1 + p_2) ^{-4}$ 

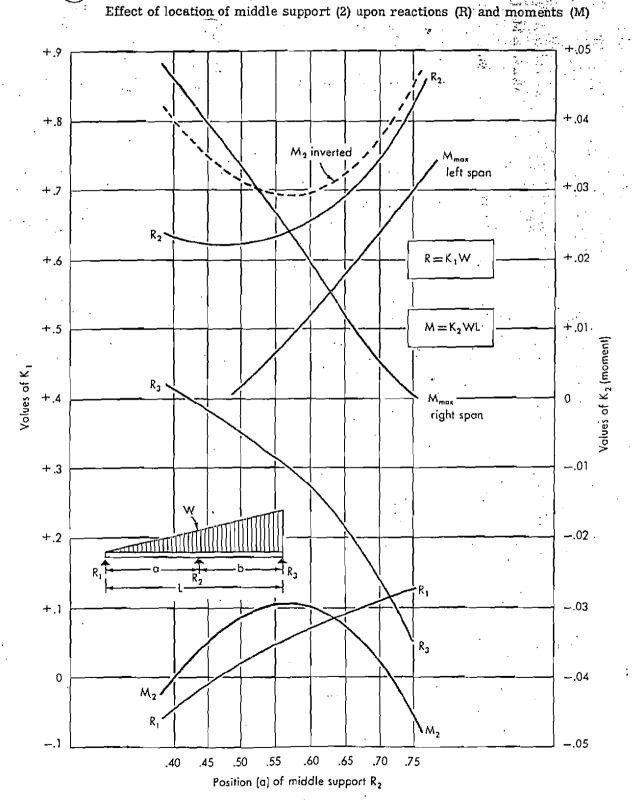
 $M_{4.} = \frac{h^2 m}{16} (p_1 + p_2)$ 

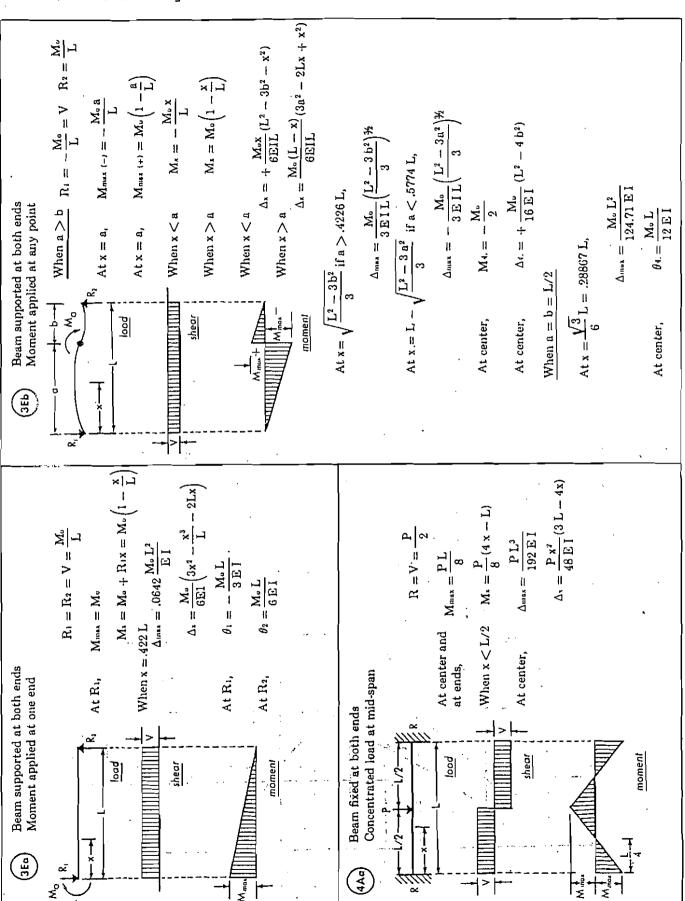
(negative proment at middle support, 2)  $M_{\text{max}} = .0147 \text{ ph}^2 \text{ m}$ 

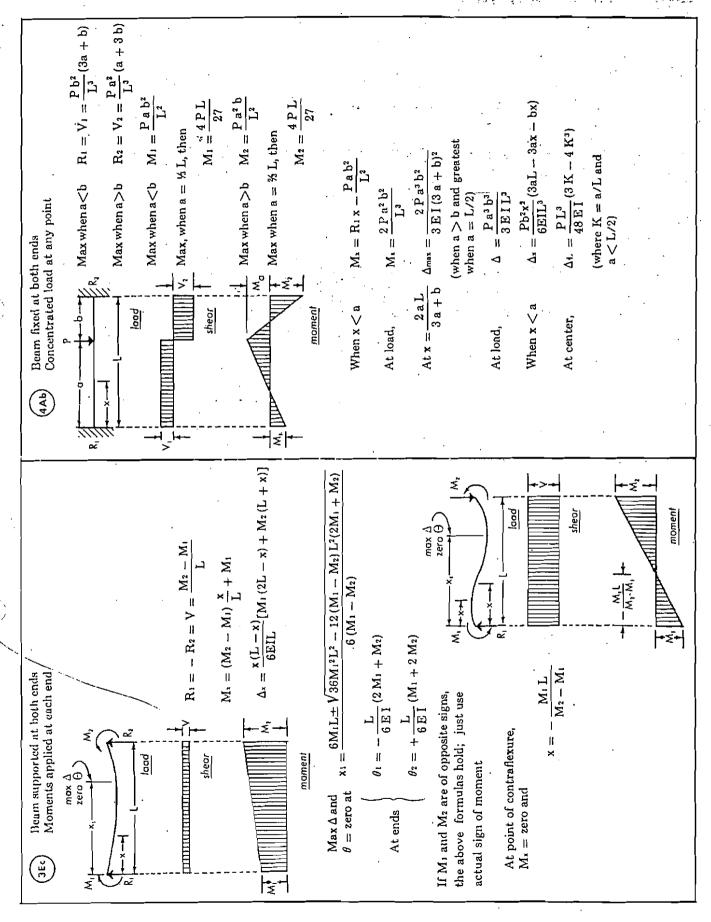
$$R_1 = + .030 \text{ ph m}$$
  
 $R_2 = + .320 \text{ ph m}$   
 $R_3 = + .150 \text{ ph m}$ 

$$V_{max} = +.188 \, \text{p h m}$$
(at middle support, 2)

Influence Lines

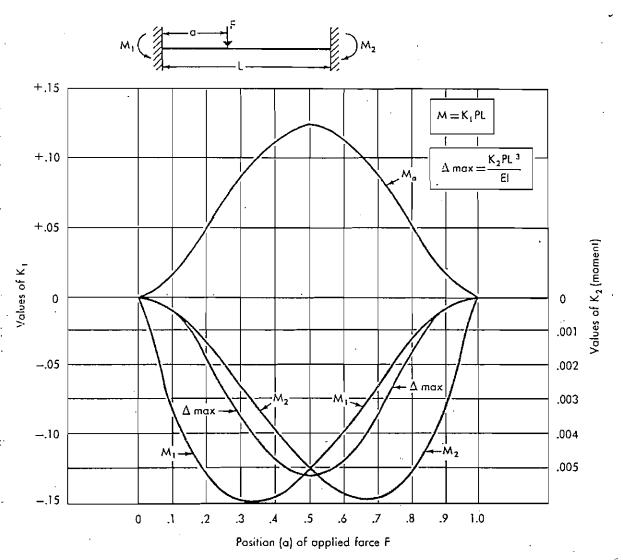




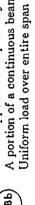


Influence Lines

Effect of position of force (F) upon moments  $\rm M_{a},\ M_{1}, M_{2}$  and upon  $\Delta_{max}$ 



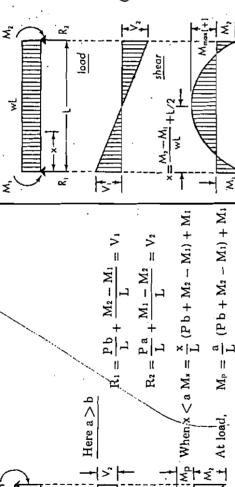
8.1-13



Beam supported and partially restrained at both ends

Concentrated load at any point

(4 A c)



 $M_1 - M_2$ 

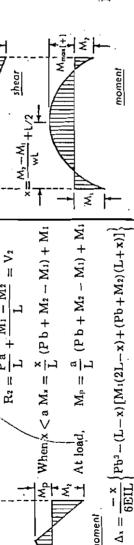
 $R_2 = \frac{Pa}{-1} +$ 

shear

 $Pb + M_2 - M_1$ 

Here a > b

laad



M, At load,

ž

moment

When x < a

<u>۲</u>,

M1 - M2

Use actual signs of moment
$$V_1 = \frac{M_1 - M_1}{V_1 + wL}$$

$$M_{x} = \frac{M_{1} - M_{2}}{L} + \frac{WL}{2}$$

$$M_{x} = \frac{WX}{2}(L - x) + M_{1}$$

 $+ M_2 \frac{x}{L}$ 

When 
$$x = \frac{M_2 - M_1}{wL} + \frac{L}{2}$$

$$M_{\text{max (+)}} = \frac{wL^2}{8} + \frac{M_1 + M_2}{2}$$

 $(M_2 - M_1)^2$ 

 $2wL^2$ 

 $V_x = w \left( \frac{L}{2} - x \right)$ 

 $M_{\text{max}} = \frac{1}{12}$ 

At ends,

load

¥ Ľ

×Γ,

Mill

At center,

 $R = V = \frac{w L}{v}$ 

Uniform load over entire span

Beam fixed at both ends

(489)

$$x^{2} - x \left[ \frac{2(M_{2} - M_{1})}{wL} + L \right] + \frac{2}{w} (M_{x} - M_{1}) = 0$$
and  $x = \frac{b \pm \sqrt{b^{2} - 4ac}}{c}$ 

$$x = \frac{-b \pm \sqrt{b^2 - 4a}}{a^2}$$

$$x = \frac{-b \pm \sqrt{b^2 - 4}}{2a}$$

$$= \frac{-b \pm \sqrt{b^2 - 4}}{2a}$$

$$= \frac{-b \pm \sqrt{b^2 - a^2}}{2a}$$

$$\frac{-b \pm \sqrt{b^2 - 4}}{2a}$$

$$= \frac{w x^2}{24 \text{ Ft I}} (L - x)^2$$

 $M_x = \frac{w}{12} (6Lx - L^2 - 6x^2)$ 

$$x = \frac{w x^2}{24 E I} (L - x)^2$$

$$\Delta_{\mathrm{x}} = rac{\mathrm{w} \, \mathrm{x}^2}{24 \, \mathrm{E} \, \mathrm{I}} \, (\mathrm{L} - \mathrm{x})^2$$

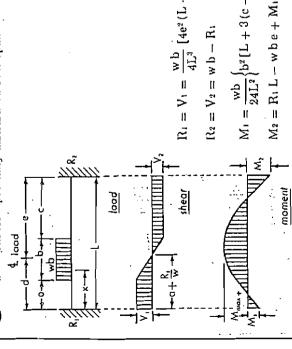
$$\Delta_{\text{max}} = \frac{\text{w L}^4}{384 \text{ E I}}$$
$$\Delta_{\text{x}} = \frac{\text{w x}^2}{24 \text{ E I}} (L - \text{x})^2$$

moment

At center,



(4c)



$$R_1 = V_1 = \frac{w b}{4L^3} \left[ 4e^2 \left( L + 2d \right) - b^2 \left( c - n \right) \right]$$

$$M_1 = \frac{wb}{24L^2} \left\{ b^2 \left[ L + 3(c - a) \right] - 24 e^2 d \right\}$$

$$At x = a + \frac{R_1}{w}$$

$$M_{\text{into}} : (+) = M_1 + R_1 \left( n + \frac{R_1}{2 w} \right)$$
When  $x < a$   $M_1 = M_1 + R_1 x$ 

When 
$$x > a$$
  $Mx = M_1 + R_1 x - \frac{w}{2} (x - a)^2$  but  $x < (a + b)$ 

but 
$$x < (3 + 5)$$
 2 ...  
When  $x < a$   $\Delta_1 = \frac{1}{GEI} (3M_1x^2 + R_1x^3)$ 

When 
$$x > a$$
 i  $\Delta_x = \frac{1}{24EI} \left[ 12M_1x^2 + 4R_1x^3 - w(x - u)^4 \right]$ 

Monient applied at any point 
$$R_{1} = -\frac{6}{L^{3}} \frac{M_{0} \cdot a \cdot b}{L^{3}} = V$$

$$R_{1} = -\frac{6}{L^{3}} \frac{M_{0} \cdot a \cdot b}{L^{3}} = V$$

$$R_{2} = +\frac{6}{L^{3}} \frac{M_{0} \cdot a \cdot b}{L^{3}} = V$$

$$R_{3} = -\frac{M_{0} \cdot b}{L^{3}} (L - 3a)$$

$$V = -\frac{M_{0} \cdot b}{L^{2}} (L - 3a)$$

# $M_{max}(-) = M_{max}(+) - M_0$

## $M_{\text{max 1+1}} = M_{\text{u}} \left[ -\frac{6a^2b}{L^3} - \frac{b}{L^2} (L - 3a) + 1 \right]$ At x = a (right side),

At 
$$x = \frac{-2 M_1}{R_1} = -\frac{L (L - 3 a)}{3 a}$$

if 
$$a > L/3$$
  $\Delta_{max}(t_1) = + \frac{M_0 b (L - 3 a)^3}{54 E I a^2}$   
At  $x = L/3 b$   $\Delta_{max}(t_2) = - \frac{M_0 a (2 L - 3 a)^3}{64 E I a^2}$ 

$$i(a < 2L/3) \Delta_{max}(-) = -\frac{54 E I L^2}{M_{\odot} k_{\odot} k_{\odot}^2}$$

When 
$$x < a$$
  $\Delta_x = -\frac{M_a b x^2}{2 B I L^2} \left(L - 3a + \frac{2 a x}{L}\right)$ 

When x > a 
$$\Delta_s = \frac{M_o \, a \, (L - x)^2}{2 \, E \, I \, L^2} \left( 3 \, a - 2 \, L + 2 \, b \right)$$
At center,  $M_b = -\frac{M_o}{L^2} \left[ 3 \, a \, b + b \, (L - 3 \, a) \right]$ 

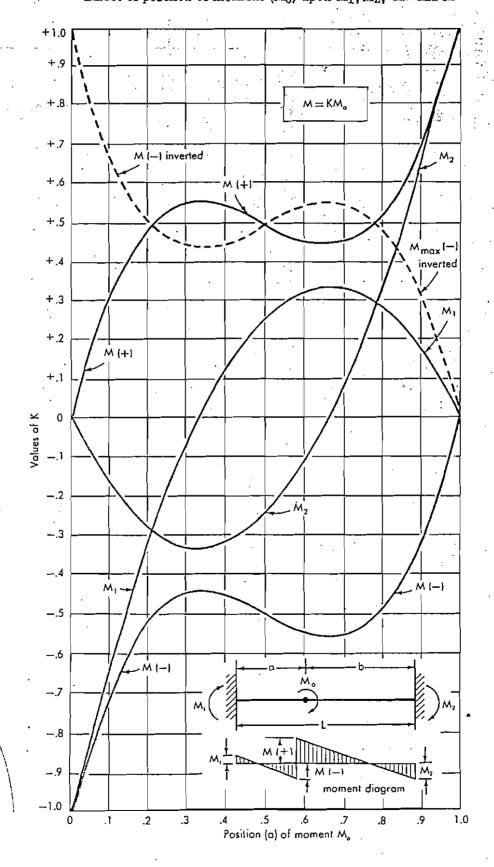
2bx

At center, 
$$\Delta_{\rm L} = -\frac{M_{\rm u}\,b}{8\,E\,I}\,(L-2\,a) \ . \label{eq:lambda}$$

Greatest maximum deflection 
$$\Delta$$
 when a = .2324  $L_{\Delta_{max}}$  = \_\_.01615 M.  $L^2$ 

Influence Lines

Effect of position of moment (M<sub>0</sub>) upon M<sub>1</sub>, M<sub>2</sub>, M+ and M-

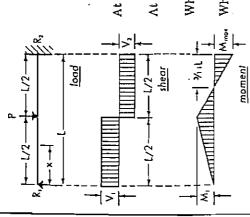


٥. Δ max = .01615 M<sub>o</sub>L<sup>2</sup> when a = .2324Lat x = .4342Lœ KM<sub>°</sub>L² 핍 ó . II Position (a) of moment Mo Solid line = actual deflection curves of member Dotted line = influence line, max  $\Delta$ max deflection  $\Delta_{\max}$  for a given position (a) of  $M_a$ Influence line for +.006 +.002 0 -.002 -.010 -.012 -.016 -.006 -.004 Yalues of K

(4E) influence Line for Maximum Deflection

1

Beam fixed at one end and supported at the other end Concentrated load at mid-span (5A<sub>9</sub>)



$$R_1 = V_1 = \frac{5P}{16}$$

$$R_2 = V_{2 \text{ max}} = \frac{11P}{16}$$
,  $M_{\text{max}} = \frac{3PL}{16}$ 

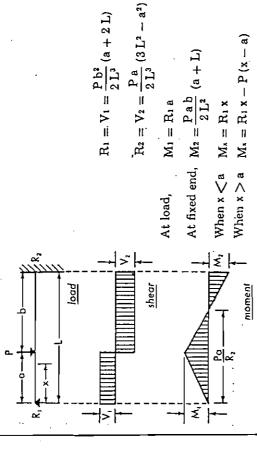
 $\frac{11 \text{ x}}{16}$ 

At 
$$x = L\sqrt{.2} = .4472 L$$
, 
$$\Delta_{\text{max}} = \frac{PL^3}{48El\sqrt{5}} = .009317 \frac{PL^3}{El}$$

At load, 
$$\Delta = \frac{7 P L^3}{768 E I}$$
 When x < L/2 
$$\Delta_x = \frac{P x}{96 E I} (3 L^2 - 5 x^2)$$

When x < L/2

When 
$$x > L/2$$
  $\Delta_x = \frac{P}{96BI} (x - L)^2 (11x - 2L)$ 



At 
$$x = L \frac{L^2 + a^2}{3L^2 - a^2}$$

$$\Delta_{\text{max}} = \frac{Pa (L^2 - a^2)^3}{3EI (3L^2 - a^2)^2} \text{ when}$$

$$At x = L \sqrt{\frac{a}{2L + a}}$$

$$\Delta_{\text{mos}} = \frac{\text{Pab}^2}{6\text{EI}} \sqrt{\frac{a}{2\text{L} + a}} \quad \text{when}$$

$$\Delta = \frac{\text{Pa}^2 b^3}{12\text{EIL}^3} (3\text{L} + a)$$

When 
$$x < a$$
  $\Delta_x = \frac{Pb^2x}{12BIL^3} (3aL^2 - 2Lx^2 - ax^2)$ 

At load,

When 
$$x > a$$
  $\Delta_x = \frac{Pa}{12 \text{BIL}^3} (L - x)^2 (3L^2 x - a^2 x - 2a^2 L)$ 

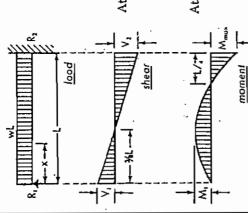
$$x > a$$
  $\Delta_x = \frac{Pa}{12BIL^3} (L - x)^2 (3L^2 x - a^2 x - a^2 x)^2$ 

Beam fixed at one end and supported at the other end Uniform load over entire span (5B)

Beam fixed at one end and supported at the other end

(30)

load over entire span 
$$R_1 = 1$$



$$R_1 = V_1 = \frac{3 w L}{8}$$

$$R_2 = V_2 = \frac{5 w L}{8}$$

 $V_x = R_1 - wx$ 

$$M_{\text{nex}} = \frac{w L^2}{8}$$
At x = 3/8 L,  $M_1 = \frac{9}{128} \text{ w L}^2$ 

M<sub>1</sub> = 
$$\frac{3}{128}$$
 w L<sup>2</sup>  
M<sub>x</sub> = R<sub>1</sub> x -  $\frac{w x^2}{2}$ 

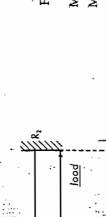
At 
$$x = \frac{1}{16} (1 + \sqrt{33}) = .4215 L$$
,

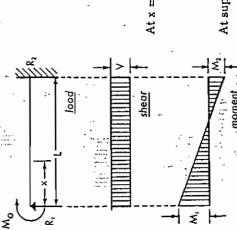
$$\Delta_{\text{max}} = \frac{w L^4}{185 E I}$$

$$\Delta_{\text{x}} = \frac{wx}{48EI} (L^3 - 3Lx^2 + 2x^2)$$

$$= \frac{wx}{48EI} (L^3 - 3Lx^2 + \theta_1) = \frac{wL^3}{48EI}$$

2E)





$$R_1 = R_2 = V = \frac{3 M_o}{2 L}$$
 $M_1 = M_o$ 
 $M_2 = 1/2 M_o$ 
 $M_A = \frac{M_o}{2 L} (2 L - 3x)$ 

At 
$$x = L/3$$
,  $\Delta_{\text{nux}} = \frac{M_0 L^2}{27 \, \text{EI}}$ 

$$\Delta_x = \frac{M_0 \, x}{4 \, \text{EIL}} \, (L - \frac{M_0$$

When 
$$x < a$$
  $M_t = R_1 x$   
When  $x > a$   $M_x = R_1 x - \frac{w}{2} (x - a)^2$   
but  $x < (a+b)$ 

When 
$$x > (a + b)$$
  $M_x = R_1 x - w b (x - d)$   
but  $x < L$ 

When 
$$x < a$$
  $\Delta_x = \frac{x}{24EI} [4R_1(x^2 - 3L^2) + wb(b^2 + 12e^2)]$ 

When 
$$x > a$$
  $\Delta_x = \frac{1}{24EI} [4R_{1X}(x^2 - 3L^2) + wbx (b^2 + 12e^2) - w (x - a)^4]$   
When  $x > (a + b)$   $\Delta_x = \frac{1}{24EI} [3M_{max}(L - x)^2 + R_2(L - x)^3]$ 

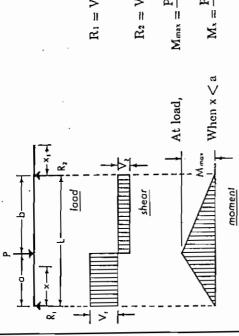
When x > (a + b) 
$$\cdot$$
  $\Delta_x = \frac{1}{6EI} \left[ 3 M_{\text{max}} (L-x)^2 + R_2 \, (L-x)^3 \right]$  but x  $< L$ 

orted end, 
$$\theta = -\frac{M_o L}{4 E I}$$

Single span, simply supported beam, with overhang Concentrated load at any point between supports (6Ag

(

(6 Ab)



$$R_1 = V_1 \begin{pmatrix} \max \\ \text{when} \end{pmatrix} = \frac{P b}{L}$$

$$R_2 = V_2 \begin{pmatrix} \max \\ \text{when} \end{pmatrix} = \frac{P a}{L}$$

$$P a b$$

$$At x = \sqrt{\frac{a(a+2b)}{3}}$$

Pbx

$$\Delta_{\text{max}} = \frac{\text{Pab}(a+2b)\sqrt{3a(a+2b)}}{27\text{EIL}} \text{ when}$$

$$\Delta = \frac{\text{Pa}^2 \text{ b}^2}{3\text{EIL}}$$

At load, 
$$\Delta = \frac{Pa^{*}b^{*}}{3 E I L}$$
When x < a 
$$\Delta_{x} = \frac{Pb x}{6 E I L} (L^{2} - b^{2} - x^{2})$$

When 
$$x>a$$
  $\Delta_x=\frac{Pa\left(L-x\right)}{6BIL}\left(2Lx-x^2-a^2\right)$  For overhang,  $\Delta_{x1}=-\frac{Pabx_1}{6BIL}\left(L+a\right)$ 

When x > a

TATE OF THE PARTY IN THE PARTY	D A Y	İ	1	$M_{x1} = P(a - x_1)$
(4,7,00)		Between supports, Mx		For overhang,
	1 -	~	- 1	

mamen

Between supports at 
$$x = L/\sqrt{3}$$
,  $= ...$   $\Delta_{max} = -\frac{PaL^2}{9\sqrt{3}EI}$ 

For overhang 
$$x_1 = a$$
, 
$$\Delta_{max} = \frac{Pa^2}{3 E I} (L + a)$$

Between 
$$\Delta_x = -\frac{Pax}{6EIL}(L^2 - x^2)$$
 supports,

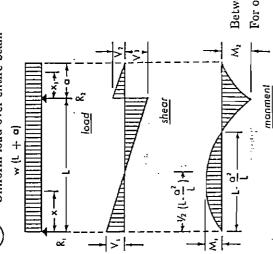
For overhang, 
$$\Delta_{x1} = \frac{Px_1}{6EI} (2aL + 3ax_1 - x_1^2)$$



Single span beam, overhanging at both ends

Uniform load over entire beam

(agh



 $R_1 = V_1 = \frac{w}{2L} (L^2 - a^2)$  $R_2 = V_2 + V_3 = \frac{w}{2L} (L + a)^2$ 

$$V_2 = w a$$

$$V_3 = \frac{w}{2 L} (L^2 + a^2)$$

 $Vx_1 = w(a - x_1)$ Between supports,  $V_x = R_1 - w x$ For overhang,

 $V_x = w (x - L/2)$ moment

 $R = V_1 + V_2 = w (a + L/2)$ 

 $V_{x,i} = w x_i$ 

For overhang, 
$$M_{x1} = \frac{w x_1^2}{2}$$
At support,  $M = \frac{w a^2}{9}$ 

Between supports,  $M_x = \frac{w}{2} (L x - x^2 - a^2)$ 

At center, 
$$M\iota = \frac{w}{R}(L^2 - 4a^2)$$

 $\Delta = \frac{wa}{24EI} (L^3 - 6a^2L - 3a^3)$  $\Delta_{\rm L} = \frac{\rm wL^2}{384\,\rm BI}\,(5\rm L^2\!-\!24a^2)$ At ends,

Between supports,  $\Delta_x = \frac{w \, x}{24 \, \mathrm{BH}} (L^4 - 2 \, L^2 \, x^2 + L \, x^3 - 2 \, a^2 \, L^2 + 2 \, a^2 \, x^2)$ 

Between supports,  $\dot{M}_x = \frac{wx}{2L} \left( L^2 - a^2 - x L \right)$ 

 $M_2 = \frac{w a^2}{2}$ 

For overhang,  $M_{x1} = \frac{w}{2} (a - x_1)^2$ 

 $\Delta_{x1} = \frac{w \, x_1}{24 \, E \, I} \, (4n^2 \, L - L^3 + 6u^2 \, x_1 - 4 \, a \, x_1^2 + x_1^3)$ 

For overhang,

 $\Delta = \frac{wa}{24 \text{ E} 1} (3 a^3 + 4 a^2 \text{ L} - \text{L}^3)$ 

At free end,

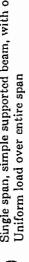
When a = .414 L,  $M_1 = M_2 = .08579 \text{ w L}^2$ 

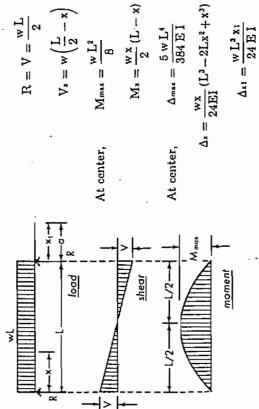
At center, 
$$\Delta t = \frac{\text{wL}^2}{384131}$$
 When  $a = .207 \times \text{total length}$ 

$$M = M_{\rm c} = \frac{w L^2}{16}$$

When 
$$a = .207 \times 100$$
 to or  $a = .354 \text{ L}$ 

Single span, simple supported beam, with overhang Uniform load over entire span (<sup>0</sup>ပွဲ





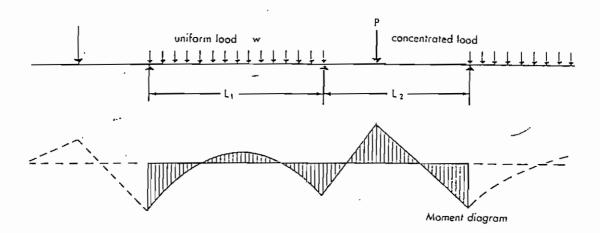
beam, with overhang	$R_1 = V_1 = \frac{w a^2}{2L}$	. ∠ . ∠	For overnang, $V_{x1} = w (a - x_1)$ At $R_2$ , $M_{max} = \frac{w a^2}{2}$ .	Between supports, $M_x = \frac{w  a^2  x}{2  L}$ For overhang, $M_{x1} = \frac{w}{2}  (a - x_1)^2$	
Single span, simply supported beam, with overhang Uniform load on overhang	R + x +	, , , , , , , , , , , , , , , , , , ,	shear	M move I	

$\Delta_{\text{max}} = -\frac{\text{w a}^2 L^2}{18\sqrt{3} \text{ E I}}$	$\Delta_{\text{max}} = \frac{w a^3}{24 E I} (4 L + 3 a)$	-
$At x = L/\sqrt{3},$	At free end,	

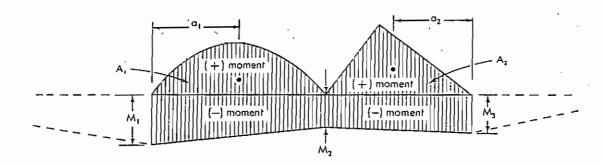
Between supports, 
$$\Delta_x = -\frac{w \, a^2 \, x}{12 \, E \, I \, L} \, (L^2 - x^2)$$
  
For overhang,  $\Delta_{x1} = \frac{w x_1}{24 E I} \, (4 a^2 L + 6 a^2 x_1 - 4 a x_1^2 + x_1^3)$ 

### THEORY OF THREE MOMENTS

Consider the following continuous beam:



The above moment diagram may be considered as made up of two parts: the positive moment due to the applied loads, and the negative moment due to the restraining end moments over the supports.



For any two adjacent spans, the following relationship is true:

$$+ \frac{M_1 L_1}{6 E I_1} + \frac{M_2}{3 E} \left( \frac{L_1}{I_1} + \frac{L_2}{I_2} \right) + \frac{M_3 L_2}{6 E I_2} + \frac{A_1 a_1}{E I_1 L_1} + \frac{A_2 a_2}{E I_2 L_2} = 0$$

where:

M<sub>1</sub>, M<sub>2</sub>, and M<sub>3</sub> are the end moments at the 1st, 2nd, and 3rd supports.

L1 and L2 are the lengths of the 1st and 2nd span.

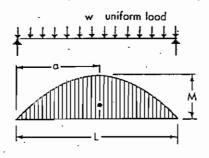
I1 and I2 are the moments of inertia of the 1st and 2nd span.

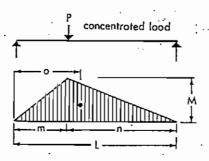
A<sub>1</sub> and A<sub>2</sub> are the areas under the positive moment diagrams of the 1st and 2nd span.

and arare the distance of the centroids of the areas of the positive moment diagrams to the 1st and 3rd outer supports.

By writing this equation for each successive pair of spans, all of the moments may be found.

The moment diagram for a simply supported, uniformly loaded beam is a parabola; and a concentrated load produces a triangular moment diagram. The following shows the area and distance to the centroid of these areas.





Ares

A = 2/3 M L

Distance to centroid

a = L/2

Area

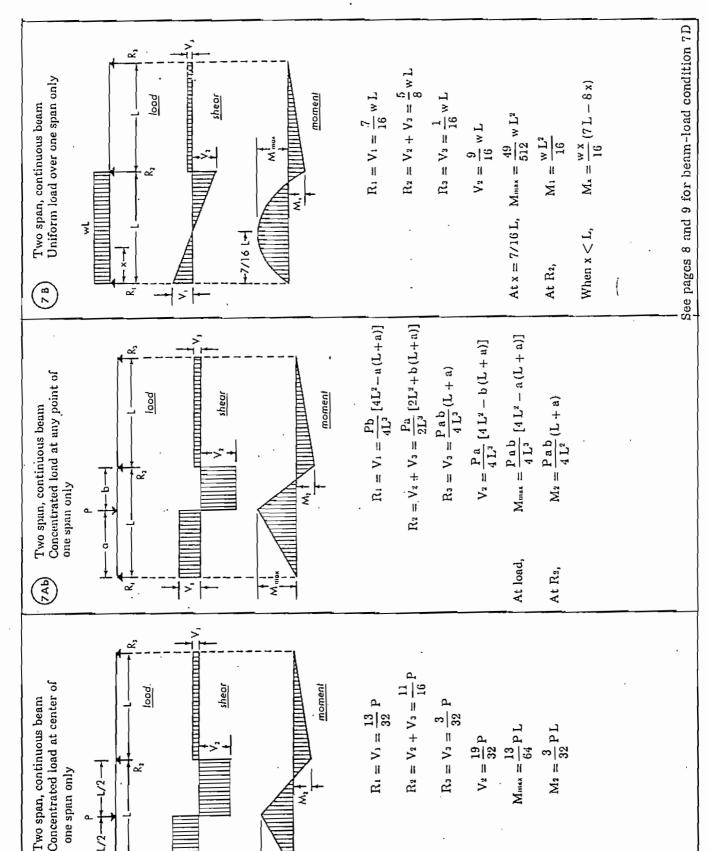
A = 1/2 M L

Distance to centroid

$$a = \frac{m + L}{2}$$

121

(7 Aa)



At load,

At R2,