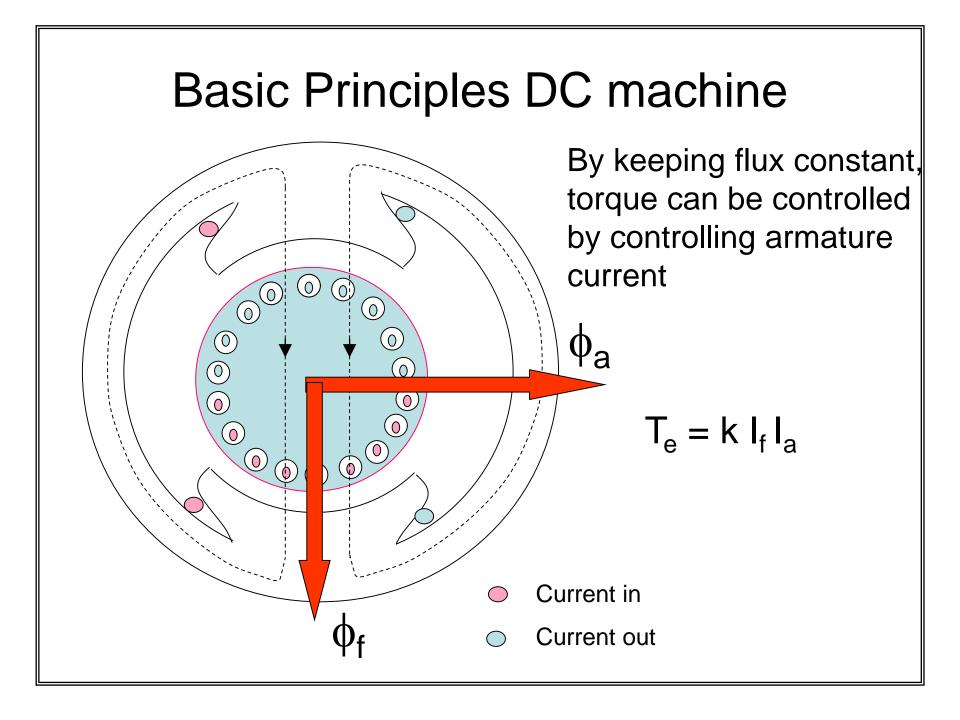
Lecture 24

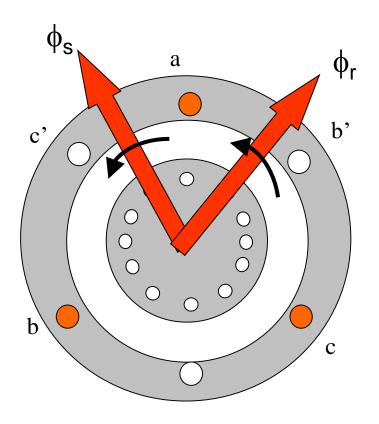
Field Oriented Control

Why FOC?

- IM is superior to DC machine with respect to size, weight, inertia, cost, speed
- DC motor is superior to IM with respect to ease of control
 - High performance with simple control due de-coupling component of torque and flux
- FOC transforms the dynamics of IM to become similar to the DC motor's – decoupling the torque and flux components



Basic Principles of IM



Stator current produce stator flux

Stator flux induces rotor current → produces rotor flux

Interaction between stator and rotor fluxes produces torque

Space angle between stator and rotor fluxes varies with load, and speed

Torque equation:

$$T_{e} = \frac{3}{2} \frac{p}{2} \overline{\psi}_{s} \times \overline{i}_{s}$$

$$T_{e} = \frac{3}{2} \frac{p}{2} \frac{L_{m}}{L_{r}} \overline{\psi}_{r} \times \overline{i}_{s}$$

In d-q axis:

$$T_{e} = \frac{3}{2} \frac{p}{2} \frac{L_{m}}{L_{r}} (\psi_{rd} i_{sq} - \psi_{rq} i_{sd})$$

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Choose a frame such that:

$$\psi_{\rm rd}^{\Psi_{\rm r}} = \left| \overline{\psi}_{\rm r} \right|$$

$$\psi_{rq}^{\psi_r} = 0$$

Choose a frame such that:

$$\psi_{rd}^{\psi_r} = |\overline{\psi}_r|$$

$$\psi_{\, rq}^{\, \psi_{\, r}} \, = 0$$

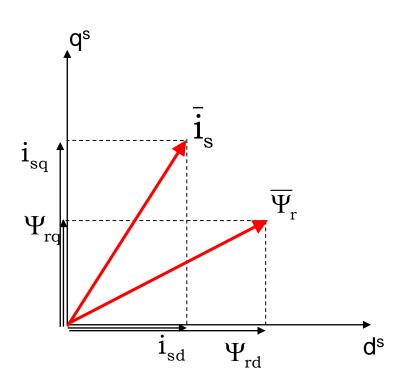
Choose a frame such that:

$$\psi_{rd}^{\Psi_r} = \left| \overline{\psi}_r \right|$$

$$\psi_{rq}^{\psi_r} = 0$$

As seen by stator reference frame:

$$T_{e} = \frac{3}{2} \frac{p}{2} \frac{L_{m}}{L_{r}} (\psi_{rd} i_{sq} - \psi_{rq} i_{sd})$$

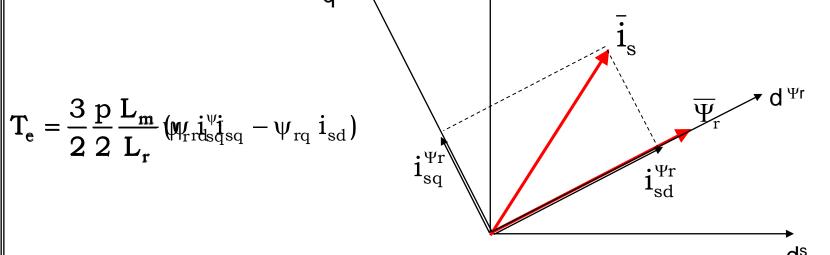


Choose a frame such that:

$$\psi_{rd}^{\Psi_r} = \left| \overline{\psi}_r \right|$$

$$\psi_{rq}^{\psi_r} = 0$$

Rotating reference frame:



To implement rotor flux FOC need to know rotor flux position:

(i) Indirect FOC

Synchronous speed obtain by adding slip speed and rotor speed

Rotor voltage equation:

$$0 = R_r \overline{i}_r^g + \frac{d\overline{\psi}_r^g}{dt} + j(\omega_g - \omega_r) \overline{\psi}_r^g$$

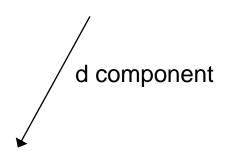
Rotor flux equation:

$$\overline{\psi}_r^g = L_r \overline{i}_r^g + L_m \overline{i}_s^g$$

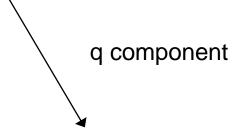
$$0 = \frac{R_r}{L_r} \overline{\psi}_r^g - \frac{L_m R_r}{L_r} \overline{i}_s^g + \frac{d\overline{\psi}_r^g}{dt} + j(\omega_g - \omega_r) \overline{\psi}_r^g$$

$$0 = \frac{R_r}{L_r} \psi_r - \frac{L_m R_r}{L_r} \left(i_{sd}^{\psi_r} + j i_{sq}^{\psi_r} \right) + \frac{d\psi_r}{dt} + j(\omega_{slip}) \psi_r$$

FOC of IM drive - indirect



$$0 = \frac{R_r}{L_r} \psi_r - \frac{L_m R_r}{L_r} i_{sd}^{\psi_r} + \frac{d\psi_r}{dt}$$



$$0 = -\frac{L_{\rm m}R_{\rm r}}{L_{\rm r}}i_{\rm sq}^{\rm \psi r} + (\omega_{\rm slip})\psi_{\rm r}$$

$$O = \frac{R_r}{L_r} \psi_r - \frac{L_m R_r}{L_r} \Big(i_{sd}^{\psi_r} + j i_{sq}^{\psi_r} \Big) + \frac{d\psi_r}{dt} + j(\omega_{slip}) \psi_r$$

FOC of IM drive - indirect

$$O = \frac{R_r}{L_r} \psi_r - \frac{L_m R_r}{L_r} \left(i_{sd}^{\psi_r} + j i_{sq}^{\psi_r} \right) + \frac{d\psi_r}{dt} + j(\omega_{slip}) \psi_r$$

d component

$$0 = \frac{R_r}{L_r} \psi_r - \frac{L_m R_r}{L_r} i_{sd}^{\psi_r} + \frac{d\psi_r}{dt}$$

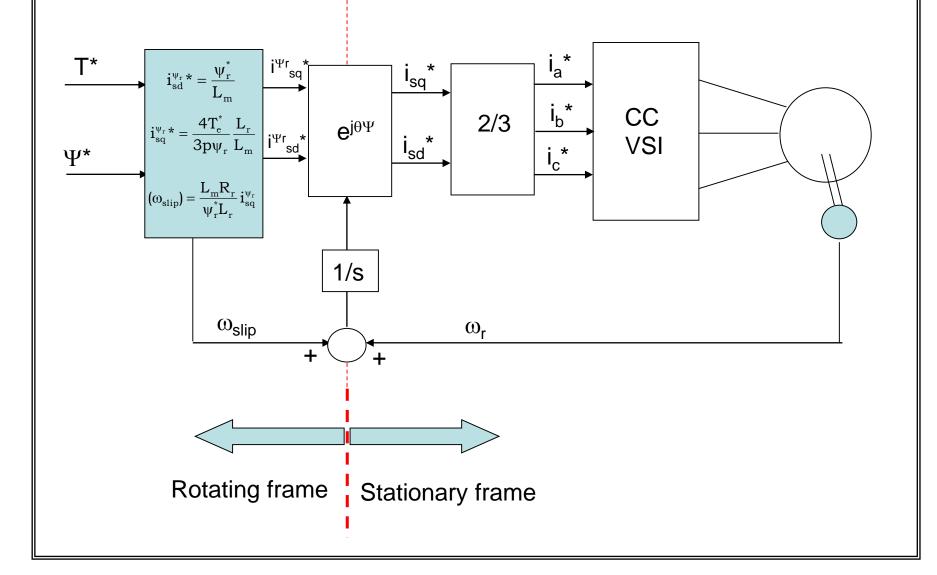
$$i_{sd}^{\psi_r} * = \frac{\psi_r^*}{L_m}$$

q component

$$0 = -\frac{L_{\rm m}R_{\rm r}}{L_{\rm r}}i_{\rm sq}^{\psi_{\rm r}} + (\omega_{\rm slip})\psi_{\rm r}$$

$$(\omega_{\text{slip}}) = \frac{L_{\text{m}}R_{\text{r}}}{\psi_{\text{r}}^*L_{\text{r}}}i_{\text{sq}}^{\psi_{\text{r}}} \qquad i_{\text{sq}}^{\psi_{\text{r}}}* = \frac{4T_{\text{e}}^*}{3p\psi_{\text{r}}}\frac{L_{\text{r}}}{L_{\text{m}}}$$

FOC of IM drive - indirect



(ii) Direct FOC

Rotor flux estimated from motor's terminal variables

Rotor flux can be estimated by:

$$0 = \frac{R_r}{L_r} \overline{\psi}_r - \frac{L_m R_r}{L_r} \overline{i}_s + \frac{d\overline{\psi}_r}{dt} - j\omega_r \overline{\psi}_r^g$$

$$T_{e} = \frac{3}{2} \frac{p}{2} \frac{L_{m}}{L_{r}} \overline{\psi}_{r} \times \overline{i}_{s}$$

Express in stationary frame

(ii) Direct FOC

$$0 = \frac{R_r}{L_r} \overline{\psi}_r - \frac{L_m R_r}{L_r} \overline{i}_s + \frac{d \overline{\psi}_r}{dt} - j \omega_r \overline{\psi}_r^g$$

$$O = \frac{R_{r}}{L_{r}} (\psi_{rd} + j\psi_{rq}) - \frac{L_{m}R_{r}}{L_{r}} (i_{sd} + ji_{sq})\overline{i} + \frac{d(\psi_{rd} + j\psi_{rq})}{dt} - j\omega_{r}(\psi_{rd} + j\psi_{rq})$$

$$\psi_{\rm rd} = \int \left(\frac{R_{\rm r}}{L_{\rm r}} \psi_{\rm rd} - \frac{L_{\rm m} R_{\rm r}}{L_{\rm r}} i_{\rm sd} + \omega_{\rm r} \psi_{\rm rq} \right) dt$$

$$\psi_{\mathrm{rd}} = \int \!\! \left(\frac{R_{\mathrm{r}}}{L_{\mathrm{r}}} \psi_{\mathrm{rd}} - \frac{L_{\mathrm{m}} R_{\mathrm{r}}}{L_{\mathrm{r}}} i_{\mathrm{sd}} + \omega_{\mathrm{r}} \psi_{\mathrm{rq}} \right) \!\! dt \qquad \psi_{\mathrm{rq}} = \int \!\! \left(\frac{R_{\mathrm{r}}}{L_{\mathrm{r}}} \psi_{\mathrm{rq}} - \frac{L_{\mathrm{m}} R_{\mathrm{r}}}{L_{\mathrm{r}}} i_{\mathrm{sq}} - \omega_{\mathrm{r}} \psi_{\mathrm{rd}} \right) \!\! dt$$

$$\Rightarrow \theta_{\Psi} = \frac{\psi_{rq}}{\psi_{rd}} \qquad \Rightarrow \psi_{r} = \sqrt{\psi_{rd}^{2} + \psi_{rq}^{2}}$$

FOC of IM drive - direct i_{sq}^* TC CC $\mathbf{e}^{\mathrm{j} \theta \Psi}$ 2/3 $\Psi_{\mathsf{r}}^{\, \star}$ VSI Ψ_{r} θ_{Ψ} $0 = \frac{R_r}{L_r} \overline{\psi}_r - \frac{L_m R_r}{L_r} \overline{i}_s + \frac{d\overline{\psi}_r}{dt} - j\omega_r \overline{\psi}_r^g$ $T_{e} = \frac{3}{2} \frac{p}{2} \frac{L_{m}}{L_{r}} \overline{\psi}_{r} \times \overline{i}_{s}$ Rotating frame | Stationary frame