

DC Amplifier

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A DC amplifier has an open loop gain of 1000 and two poles, a dominant one at 1kHz and a high frequency one whose location can be controlled. It is required to connect this amplifier in a negative feedback loop that provides a DC closed loop gain of 10 and a maximally flat response.

1. Find the required value of H .

Solution: Table 1 summarises the given information. The open loop gain can be expressed as

$$G(s) = \frac{G_0}{\left(1 + \frac{s}{p_1}\right)\left(1 + \frac{s}{p_2}\right)} \quad (1.1)$$

$$\Rightarrow G(0) = G_0 \quad (1.2)$$

The closed loop gain

$$T(s) = \frac{G(s)}{1 + G(s)H} \quad (1.3)$$

$$\Rightarrow T(0) = \frac{G_0}{1 + G_0H} \quad (1.4)$$

Substituting from Table 1,

$$\frac{1000}{1 + 1000H} = 10 \quad (1.5)$$

$$\Rightarrow H = 0.099 \quad (1.6)$$

Parameter	Value
dc open loop gain	1000
dominant pole	-1000Hz
insignificant pole	$-p_2$
dc closed loop gain	10

TABLE 1: 1

$$G_0 = 1000 \quad (1.7)$$

$$\text{Therefore, } G(s) = \frac{1000}{\left(1 + \frac{s}{p_1}\right)\left(1 + \frac{s}{p_2}\right)} \quad (1.8)$$

2. Find p_2 .

Solution: From (1.3) and (1.1),

$$T(s) = \frac{p_1 p_2 G_0}{s^2 + (p_1 + p_2)s + (HG_0 + 1)p_1 p_2} \quad (2.1)$$

$$= \frac{K\omega_n^2}{s^2 + 2\zeta\omega_n s + \omega_n^2} \quad (2.2)$$

$$\omega_n = \sqrt{(HG_0 + 1)p_1 p_2}$$

$$\Rightarrow \zeta = \frac{p_1 + p_2}{2\sqrt{(HG_0 + 1)p_1 p_2}} \quad (2.3)$$

using the standard formulation for a second order system. Also, for maximally flat response, the quality factor

$$Q = \frac{1}{2\zeta} = \frac{1}{\sqrt{2}} \quad (2.4)$$

$$\Rightarrow \zeta = \frac{1}{\sqrt{2}} \quad (2.5)$$

$$\Rightarrow \frac{p_1 + p_2}{2\sqrt{(HG_0 + 1)p_1 p_2}} = \frac{1}{\sqrt{2}} \quad (2.6)$$

$$\Rightarrow \sqrt{\frac{p_1}{p_2}} + \sqrt{\frac{p_2}{p_1}} = \sqrt{2(HG_0 + 1)} \quad (2.7)$$

The above equation is of the form

$$x + \frac{1}{x} = a \quad (2.8)$$

$$\Rightarrow x = \frac{a \pm \sqrt{a^2 - 4}}{2} \quad (2.9)$$

where

$$x = \sqrt{\frac{p_2}{p_1}} \quad (2.10)$$

$$a = \sqrt{2(HG_0 + 1)}, \quad (2.11)$$

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Thus, from (2.10), (2.11) and (2.9),

$$p_2 = p_1 \left[\frac{\sqrt{2(HG_0 + 1)} \pm \sqrt{2(HG_0 + 1) - 4}}{2} \right]^2 \quad (2.12)$$

From the following code,

```
codes/ee18btech11005/ee18btech11005_1.py
```

$$p_2 = 1244038.9567529503$$

and 31.734068607786863 (2.13)

3. Draw the equivalent circuit system diagram.

Solution: The equivalent circuit system is shown in the figure.3

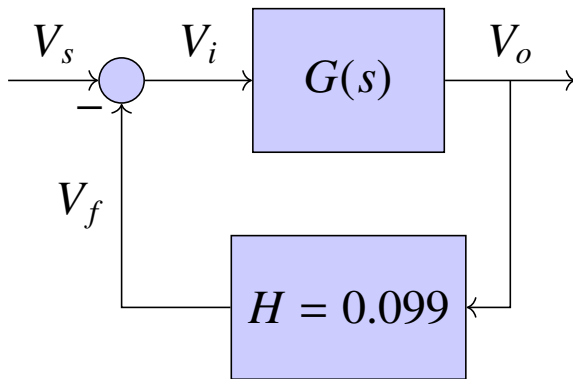


Fig. 3: 1

4. Obtain $G(s)$ and $T(s)$

Solution: Substituting the value of p_2 in (1.1) and (2.1),

$$G(s) = \frac{1000}{(1 + \frac{s}{2\pi 10^3})(1 + \frac{s}{1.244 \times 10^6})} \quad (4.1)$$

$$T(s) = \frac{10}{0.128 \times 10^{-11} s^2 + 1.599 \times 10^{-6} s + 1} \quad (4.2)$$

5. Verify from the Bode plot of above closed loop transfer function that it has maximally flat response.

Solution: The following code generates the bode plot of the transfer function in Fig. 5.

```
codes/ee18btech11005/ee18btech11005_2.py
```

6. Find the step response of $T(s)$

Solution: The following code generates the desired response of in Fig. 6.

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codes/ee18btech11005/ee18btech11005_3.py
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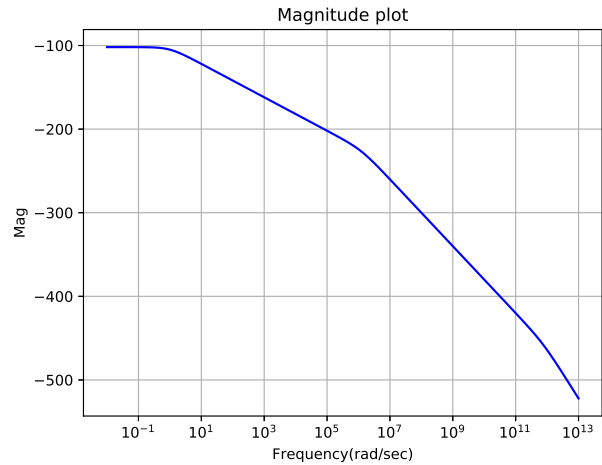


Fig. 5

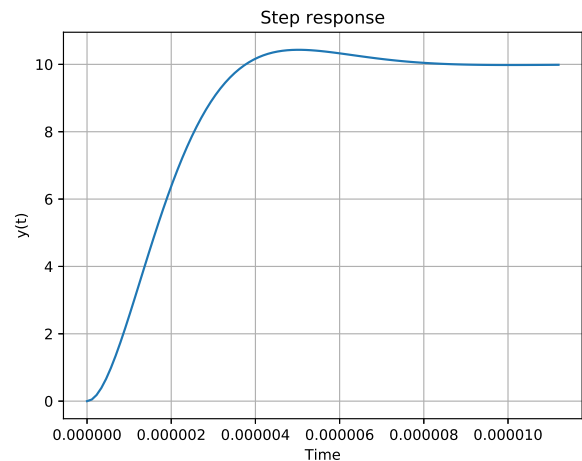


Fig. 6

7. Design a circuit that represents the above transfer function.

Solution: The circuit can be designed using operational amplifiers having negative feedback. Consider the circuit shown in figure.7:1. Assume the gain of all the amplifiers are large. And assume no zero state response. Take the parameters in s-domain.

For the first amplifier,

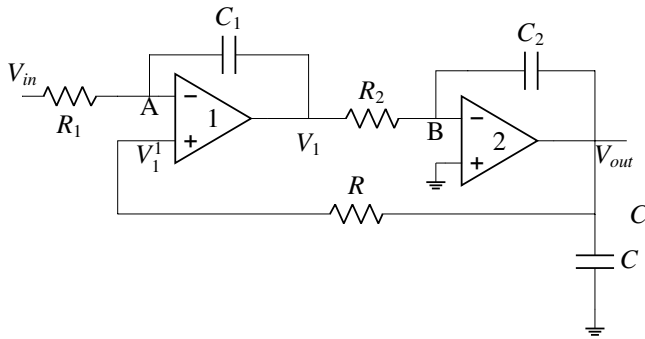


Fig. 7: 1

$$\frac{V_{in} - V_1^1}{R_1} = \frac{V_1^1 - V_1}{\frac{1}{sC_1}} \quad (7.1)$$

$$\frac{V_{in}}{R_1} = \frac{V_1^1}{R_1} + sC_1 V_1^1 - sC_1 V_1 \quad (7.2)$$

$$\frac{V_{in}}{R_1} = V_1^1 \left[sC_1 + \frac{1}{R_1} \right] - sC_1 V_1 \quad (7.3)$$

$$V_{in} = V_1^1 (sC_1 R_1 + 1) - sC_1 R_1 V_1 \quad (7.4)$$

For the second amplifier,

$$\frac{V_1 - V_b}{R_2} = (V_b - V_{out})sC_2 \quad (7.5)$$

$$\text{Since, } V_b = 0 \quad (7.6)$$

$$\Rightarrow V_1 = -sC_2 R_2 V_{out} \quad (7.7)$$

Voltage division at node C.,

$$\frac{V_1^1}{V_{out}} = \frac{1 + \frac{1}{sC}}{\frac{1}{sC}} \quad (7.8)$$

$$\Rightarrow V_1^1 = (sCR + 1)V_{out} \quad (7.9)$$

From eq:(7.4) ,eq:(7.7) ,eq:(7.9)

$$V_{in} = ((sCR + 1)(sC_1 R_1 + 1) + s^2 C_1 R_1 C_2 R_2) V_{out} \quad (7.10)$$

$$(7.11)$$

$$\frac{V_{in}}{V_{out}} = s^2 (CRC_1 R_1 + C_1 R_1 C_2 R_2) + s(CR + C_1 R_1) + 1$$

$$\frac{V_{out}}{V_{in}} = \frac{1}{s^2 (CRC_1 R_1 + C_1 R_1 C_2 R_2) + s(CR + C_1 R_1) + 1} \quad (7.12)$$

Comparing the equation.(4.2) and equation.(7.12)

$$C_1 R_1 (CR + C_2 R_2) = 0.128 \times 10^{-11} \quad (7.13)$$

$$CR + C_1 R_1 = 1.599 \times 10^{-6} \quad (7.14)$$

$$\text{Let, } CR = 10^{-6} \quad (7.15)$$

$$\Rightarrow C_1 R_1 = 0.599 \times 10^{-6} \quad (7.16)$$

$$0.599 \times 10^{-6} (10^{-6} + C_2 R_2) = 0.128 \times 10^{-11} \quad (7.17)$$

$$C_2 R_2 = 0.681 \times 10^{-6} \quad (7.18)$$

The parameters can be chosen as shown in the TABLE:7

The final circuit is shown in the figure.7

Parameter	Value
R_1	1000 Ω
R_2	1000 Ω
R	1000 Ω
C_1	0.1 nF
C_2	0.681 nF
C	0.599 nF

TABLE 7

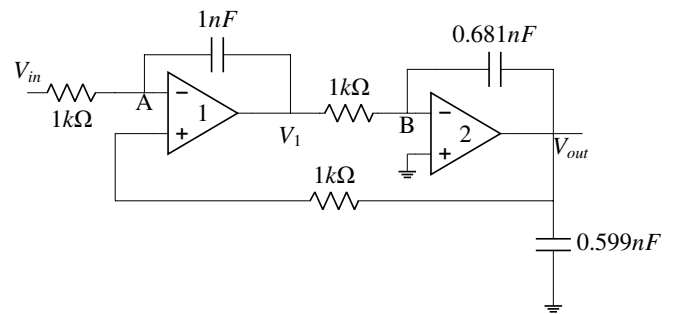


Fig. 7

8. Draw the block diagram of the closed loop system.

Solution: The block diagram is shown in figure.8

9. Find H_2 .

Solution: H_2 can be calculated as follows.,

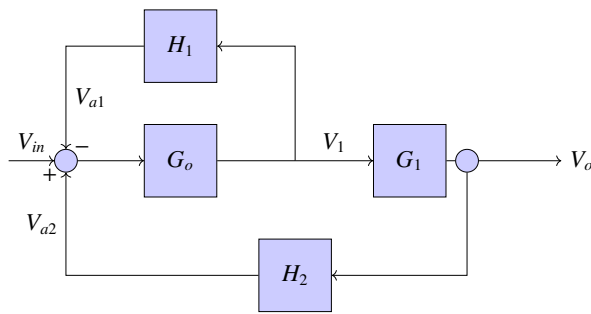


Fig. 8

$$H_2 = \frac{V_{a2}}{V_o} \quad (9.1)$$

$$(9.2)$$

But from the figure.7.,

$$\frac{V_{a2}}{V_o} = \frac{V_1^1}{V_o} \quad (9.3)$$

$$\frac{V_{a2}}{V_o} = \frac{R + \frac{1}{sC}}{\frac{1}{sC}} \quad (9.4)$$

$$\frac{V_{a2}}{V_o} = 1 + sCR \quad (9.5)$$

$$H_2 = 1 + sCR \quad (9.6)$$

10. Find equivalent open loop gain of the system without positive feedback.

Solution: The figure.10 shows the equivalent block diagram.

The resultant open loop gain after removing

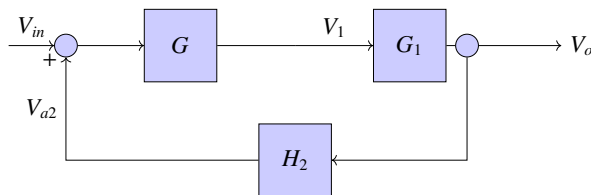


Fig. 10

positive feedback is GG_1 . Where G can be calculated as follows.,

$$G = \frac{G_o}{1 + G_o H_1} \quad (10.1)$$

$$G = \frac{1}{\frac{1}{G_o} + H_1} \quad (10.2)$$

Since, G_o is very large.,

$$G \approx \frac{1}{H_1} \quad (10.3)$$

For finding H_2 ., ground V_{in} .,

$$H_1 = \frac{V_{a1}}{V_1} \quad (10.4)$$

$$H_1 = \frac{R_1}{R_1 + \frac{1}{sC_1}} \quad (10.5)$$

$$H_1 = \frac{sC_1 R_1}{sC_1 R_1 + 1} \quad (10.6)$$

Finding G_1 .,

$$G_1 = \frac{V_o}{V_1} \quad (10.7)$$

$$G_1 = -\frac{1}{sC_2 R_2} \quad (10.8)$$

Therefore., The open loop gain without positive feedback is given by.,

$$OLG = GG_1 \quad (10.9)$$

$$OLG = \frac{G_1}{H_1} \quad (10.10)$$

$$OLG = -\frac{\frac{1}{sC_2 R_2}}{\frac{sC_1 R_1}{sC_1 R_1 + 1}} \quad (10.11)$$

$$OLG = -\frac{sC_1 R_1 + 1}{s^2 C_1 R_1 C_2 R_2} \quad (10.12)$$

11. Find the approximate closed loop transfer function.

Solution: The overall system is in positive feedback. The closed loop transfer function is given by.,

$$T(s) = \frac{OLG}{1 - OLG \times H_2} \quad (11.1)$$

$$T(s) = \frac{\frac{sC_1 R_1 + 1}{s^2 C_1 R_1 C_2 R_2}}{1 + \left[\frac{sC_1 R_1 + 1}{s^2 C_1 R_1 C_2 R_2} \right] (1 + sCR)} \quad (11.2)$$

$$T(s) = \frac{sC_1 R_1 + 1}{s^2 C_1 R_1 C_2 R_2 + (sC_1 R_1 + 1)(sCR + 1)} \quad (11.3)$$

Since $C_1 R_1$ is very small compared to 1. We can assume the zero lies far away from origin.

$$T(s) \approx \frac{1}{s^2 C_1 R_1 C_2 R_2 + (sC_1 R_1 + 1)(sCR + 1)} \quad (11.4)$$

The above equation is similar to equation.7.12
Hence verified.

12. Find the block diagram and circuit diagram for H_2 .

Solution: The block diagram is shown in figure.12 The circuit diagram is shown in the

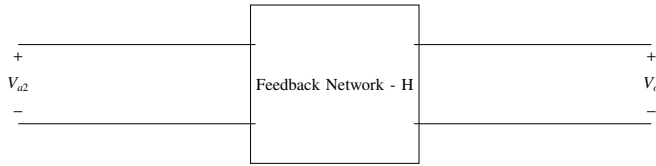


Fig. 12: Block diagram

fig.12

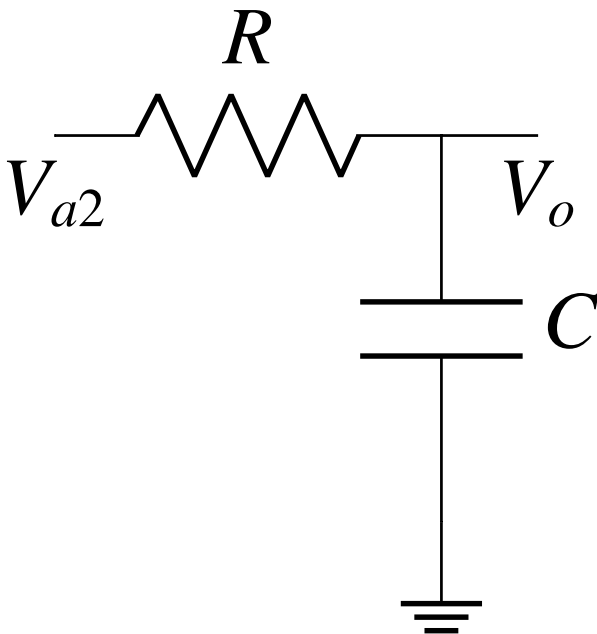


Fig. 12: Circuit diagram

13. Draw the block diagram for open loop gain GG_1 and find R_{11} and R_{22} .

Solution: The figure.13 Finding R_{11} ., short V_o

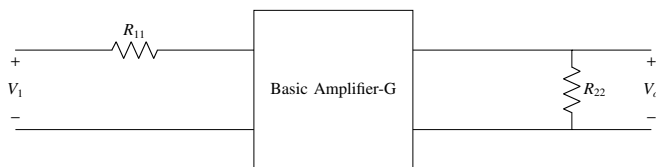


Fig. 13: Circuit diagram

to ground.,

$$R_{11} = R \quad (13.1)$$

Finding R_{22} ., short V_{a2} to ground.,

$$R_{22} = R \parallel \frac{1}{sC} \quad (13.2)$$

14. Verify the closed loop DC gain using NGSPICE simulator.

Solution: The following README file gives the procedure to be followed.

`codes/ee18btech11005/spice/README`

From equation.4.2. The DC closed loop gain is 10.

The following netlist file, gives the DC gain of the closed loop function.

`codes/ee18btech11005/spice/gvv_ngspice.net`

We can observe from simulation that the value of DC closed loop gain is 9.997.

Error analysis:-

ERROR in DC GAIN = $10 - 9.993 = 0.007$
Thus, the predicted value in ngspice is almost accurate. Therefore, the value is verified using ngspice.

15. Verify the step response of the output from ngspice simulation.

Solution: The following netlist file does the transient analysis and store the V_{out} values with respect to time in a dat file.

`codes/ee18btech11005/spice/gvv_ngspice.net`

Following python code is to plot the step response.

`codes/ee18btech11005/spice/
ee18btech11005_spice.py`

The step response obtained is shown in the figure.15. The graph has steady state value equal to 10.

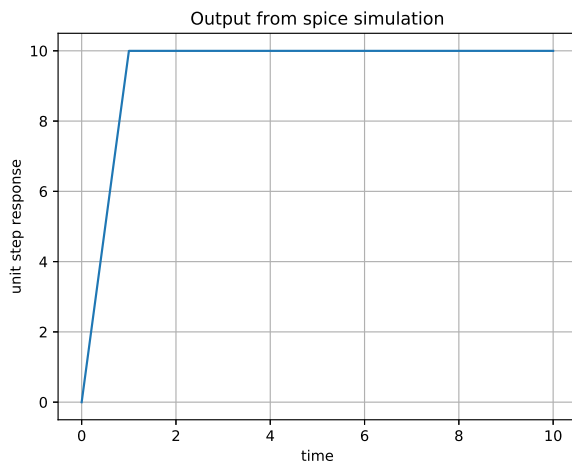


Fig. 15