ECE 31033 Project #1: DC—DC Converter

ID Number: 229,506

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Objective

The overall objective of this project was to simulate a step-down DC—DC converter, taking an 800V input and bringing it to a 400V output. In addition, the circuit has a load range of 50 to 250 kW with a switching frequency.

Using the information from above, we were tasked with analytically calculating the inductance and the minimum capacitance for the circuit. With these values, a Forward Euler integration algorithm was implemented to simulate the ideal circuit behavior by numerically solving the differential equations.

The simulation required the use of four MATLAB files, with two of them being functions that were implemented in the other files. The simulation plotted each circuit component's voltages and currents in the transient state and then repeated the process for the steady state, by looking at the last couple of periods. After the plotting was completed, the average value for each waveform was calculated. Finally, the efficiency of the circuit was calculated.

Brief Overview of the MATLAB Files

There were 4 required files for this project. Two of the files were functions and two of the files were scripts. The code for each file can be found after the results section of this document. Instead of pasting the code at the end of the document, each file was exported using a Visual Studio Code extension to preserve formatting and readability.

"sw.m"

This file was a function that created a Fourier series-based triangle wave which was compared to the duty cycle to determine the state of the transistor.

The inputs to this function were the duty cycle and a single instant in time. The output was a Boolean; 0 if the transistor if turned off or 1 if the transistor is turned on.

"buck.m"

This file was a script containing the Forward Euler integration algorithm. The algorithm consisted of a while loop that calculated the instantaneous voltage and current of each component in the circuit.

The script called the function "sw.m", where its output was used to determine if both the transistor and the diode were on or off.

"aver.m"

This file was a function that was used to calculate the average of a waveform by using a Reimann sum and taking the last period of the waveform.

The inputs to this function were the waveform, the period, and the period between the samples. The output is the average value of the waveform.

"buckproc.m"

The final file was a script that acted as a main function. This script contained each of the analytically solved component values while also calling the file "buck.m" to calculate the voltage and currents of each of the waveforms. After calling "buck.m", it was able to call "aver.m" to calculate the average value of each of the waveforms. The script then plotted each of the waveforms in both the transient and steady states using ideal and non-ideal conditions.

Analytical Calculations

Buck Converter Overview

The general schematic of a buck converter can be seen as follows:

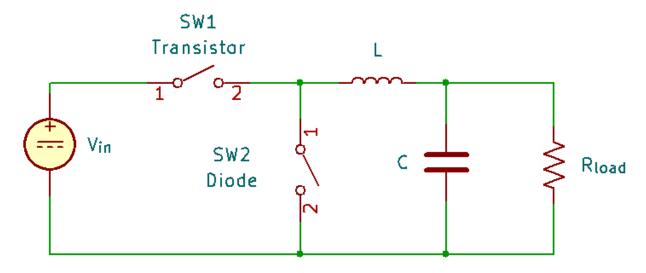


Figure 1: Standard circuit schematic for a buck converter.

The transistor switch and diode switch are opposites to each other; only one can be on at a time. Therefore, the circuit shown in Figure 1 has two configurations.

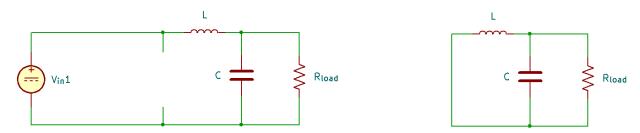


Figure 2: Buck converter schematic for when the transistor is on and for when the diode is on.

With each configuration, we can apply Kirchoff's Voltage and Current laws to determine the values of each of the circuit components.

Component Values

According to the project specifications, we were not given the values for both the inductor and the capacitor. I was able to determine that I would need to solve for the values of the inductor, capacitor, duty cycle, switching period, and finally the heavy and light load resistor.

To create an expression duty cycle, we can use the relationship between the load voltage and input voltage.

$$D = \frac{V_{load}}{V_{in}} = \frac{400}{800} = 0.5$$

Equation 1: Expression to find Duty Cycle.

The expression for switching period is simply the inverse of the switching frequency.

$$T_{sw} = \frac{1}{f_{sw}} = \frac{1}{10000} = 10^{-4} s$$

Equation 2: Expression to find Switching Period.

To calculate the load resistance, we can rearrange Ohm's law and isolate the resistance.

$$P_{load} = \frac{(V_{load})^2}{R_{load}} \rightarrow R_{load} = \frac{(V_{load})^2}{P_{load}}$$

Equation 3: Expression to find Load Resistance.

With this simplified expression, we can solve for both the heavy and light load resistance.

$$R_{load,light} = \frac{(V_{load})^2}{P_{load}} = \frac{(400)^2}{50000} = 3.2\Omega$$

Equation 4: Expression to find Light Load Resistance.

$$R_{load,heavy} = \frac{(V_{load})^2}{P_{load}} = \frac{(400)^2}{250000} = 0.64\Omega$$

Equation 5: Expression to find Heavy Load Resistance.

Next, we can determine an expression for critical inductance. Using this critical inductance value, we can solve for the actual inductor to use with this circuit.

$$L_{crit} = \frac{R_{load,light} \cdot (1 - D)}{2 \cdot f_{sw}} = \frac{(3.2) \cdot (1 - 0.5)}{2 \cdot 10000} = 8e^{-5}H$$

Equation 6: Expression to find Critical Inductance.

$$L = 1.1 \cdot L_{crit} = (1.1) \cdot (8e^{-5}) = 8.8e^{-5}H$$

Equation 7: Expression to find Inductance.

Finally, we can solve for the minimum capacitance, using some of the values that were given in the project specification in addition to ones that we calculated above.

$$C \ge \frac{1}{8L} \left(T_{sw}^2 \cdot (1 - D) \right) \cdot \frac{V_{load}}{\Delta V_{load}}$$

$$\ge \frac{1}{8 \cdot (8.8e^{-5})} \left((10^{-4})^2 \cdot (1 - 0.5) \right) \cdot \frac{400}{10}$$

$$\ge 2.84e^{-4}F$$

Equation 8: Expression to find minimum Capacitance.

The values that were calculated above were used in the Forward Euler integration algorithm to find the instantaneous value of each circuit component.

Fourier Series Triangle Wave

To create a Fourier Series based triangle wave, I needed to calculate the values of the coefficient for each harmonic wave. Using the values for each coefficient, it can be put into a summation. Knowing that the triangle is an even function, we can use the following as the equation for the Fourier Series:

$$x(t) = a_0 + \sum_{k=1}^{\infty} (a_k + \cos(k\omega t))$$

Equation 8: General Fourier Series for an even function.

The coefficient, a_k , can be determined as:

$$a_k = \frac{2}{T_{sw}} \int_{0}^{T_{sw}} (x(t) \cdot \cos(k\omega t)) dt$$

Equation 8: General expression to determine the Fourier Series coefficients.

Equation 8 can be broken into two integrals. The first integral accounts for when the triangle has a positive slope and the second integral accounts for when the triangle has a negative slope.

$$a_k = \frac{2}{T_{sw}} \left(\int_{0}^{T_{sw}} (t \cdot \cos(k\omega t)) dt + \int_{DT_{cw}}^{T_{sw}} (-t \cdot \cos(k\omega t)) dt \right)$$

Equation 9: General expression for the Fourier Series coefficients of a triangle wave.

The calculus and the algebra used to solve this equation can get quite out of hand. To simplify this expression, Equation 9 was inputted into an online calculator, leaving us with Equation 10.

$$a_k = 2 \cdot \frac{4 \cdot \cos(0.5k\omega t) - 2 \cdot \cos(k\omega t) - 2}{(k\omega t)^2}$$

Equation 10: Final expression for the Fourier Series coefficients of a triangle wave.

We can insert Equation 10 into the summation in Equation 8 to create the triangle wave.

Forward Euler Integration

In the buck converter circuit, there are 5 components: the transistor switch, the diode switch, the inductor, the capacitor, and the resistor. In the Forward Euler integration algorithm, the voltage and the current for each component was calculated.

Switch 1 – The Transistor

When the switch is on, the voltage of Switch 1 is equivalent to the input voltage. If the switch is off, there is no voltage running through the switch.

$$V_{Sw1} = V_{in} \cdot (switch\ state) = 800V \cdot (switch\ state)$$

Equation 11: Expression to find the voltage of Switch 1.

If the switch state is off, the value of the switch state in Equation 11 will become zero. If the switch state is on, the value of the switch state in Equation 11 will become 1. Therefore, the value of switch 1's voltage will be zero if the switch is off and 800 if the switch is on.

The current of the switch is calculated using the relationship between the inductor current and the switch state.

$$i_{Sw1} = i_L \cdot (switch\ state)$$

Equation 12: Expression to find the current of Switch 1.

Like for the voltage, if the switch state is off, the value of the switch state in Equation 12 will become zero. If the switch state is on, the value of the switch state in Equation 12 will become 1. Therefore, the value of switch 2's current will be zero if the switch is off and i_L if the switch is on.

Switch 2 - The Diode

Fundamentally, Switch 2 is like Switch 1 but differs slightly. Neither switch can be turned on or off at the same time. The values for current and voltage are similar.

$$V_{Sw2} = (-V_{load}) \cdot (switch\ state) = (-800) \cdot (switch\ state)$$

Equation 13: Expression to find the voltage of Switch 2.

$$i_{Sw2} = i_L \cdot (1 - switch state)$$

Equation 12: Expression to find the current of Switch 1.

Inductor

If we were to plot the voltage of the inductor, it would look reminiscent of a triangle wave. However, the voltage when the slope is positive and negative are different to each other.

$$V_L^{+ slope} = V_{in} - V_{load} = 800 - 400 = 400$$

 $V_L^{- slope} = -V_{load} = -400$

Equation 13: Expression to find the voltage of the inductor.

To determine the current for the inductor, the Forward Euler integration algorithm was implemented.

$$i_L(t + \Delta t) = i_L(t) \cdot \frac{(switch\ state) \cdot V_{in} - V_{load}(t)}{I_L}$$

Equation 14: Expression for the Forward Euler Integration to find inductor current.

Like with other components, the switch state either returns a 0 or a 1. Therefore, the numerator of the fraction in Equation 14 will resemble either the top or bottom line of Equation 13.

Capacitor

The voltage of the capacitor in this circuit is equivalent to the load voltage. Therefore, we can write the expression for capacitor voltage as:

$$V_C = V_{load}$$

Equation 15: Expression to find the capacitor voltage.

The current of the capacitor can be determined by taking the inductor voltage and subtracting the current through the load.

$$i_C = i_L - \frac{V_{load}}{R_{load}}$$

Equation 16: Expression to find the capacitor current.

Resistor

The value of the load's voltage was given in the project specification, so there was nothing to determine the voltage. To calculate the current through the load, we can rearrange Ohm's law to solve for current.

$$i_{load} = \frac{V_{load}}{R_{load}}$$

Equation 17: Expression to find the current of the load resistor.

The value R_{load} of depends on if the simulation is using heavy conditions or light conditions.

Non-Ideal – Heavy Load

Circuit Differences

In a non-ideal circuit, there are a couple differences to the circuit we saw in Figure 1. Specifically, for this project, each switch has a voltage drop and resistance. With this in mind, we can redraw the circuit to account for these non-idealities.

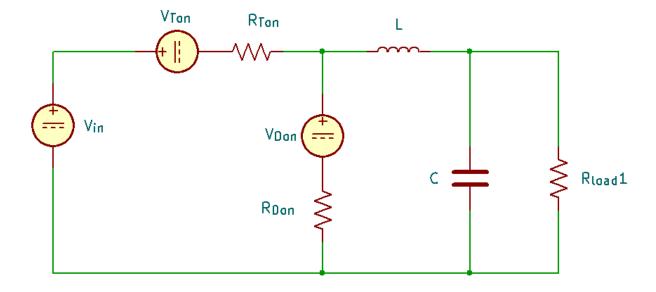


Figure 3: circuit schematic for a buck converter with non-ideal conditions.

Like the ideal conditions, only one switch can be on at a single point in time. Therefore, there are two smaller subcircuits that can be created using the circuit from Figure 3.

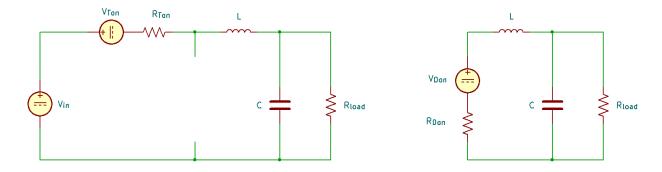


Figure 4: Non ideal Buck Converter schematics.

With these new circuit schematics, we can reapply Kirchoff's Laws to determine any changes to the values of the components or the duty cycle.

Duty Cycle

We know that the average inductor voltage is zero.

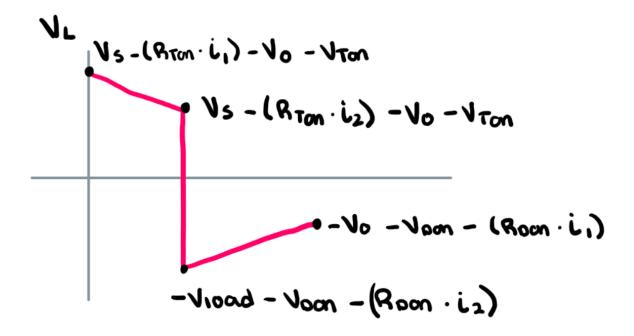


Figure 5: Plot for inductor voltage.

Using Figure 5, we can set up an expression for average inductor voltage.

$$< V_L> = 0 = \frac{1}{T_{sw}} (DT_{sw} \big(V_{in} - V_{T,ON} - i_{L2} R_{T,ON} - V_{load} \big) + \frac{DT_{sw}}{2} \big(-i_{L1} R_{T,ON} \ + \ -i_{C1} R_{T,ON} \big) + \\ (1-D)T_{sw} \big(-V_{D,ON} - i_{L1} R_{D,ON} - V_{load} \big) + \frac{(1-D)T_{sw}}{2} \big(-i_{L2} R_{D,ON} \ + \ i_{L1} R_{D,ON} \big).$$

Equation 18: Expression for average inductor voltage.

Using algebra, we can simplify the equation to eliminate some variables and solve for the duty cycle, D.

$$D = \frac{V_{D,ON} + V_{load} + \frac{R_{D,ON} \cdot V_{load}}{R_{load}}}{V_{in} - V_{T,ON} + V_{D,ON} + \frac{R_{D,ON} \cdot V_{load}}{R_{load}} - \frac{R_{T,ON} \cdot V_{load}}{R_{load}}} = \frac{1 + 400 + \frac{0.01 \cdot 400}{0.64}}{800} = 0.509625$$

Equation 19: Expression for non-ideal duty cycle.

Using this expression for non-ideal duty cycle, we can use it to solve for the voltages and the currents for each of the components.

Efficiency

Efficiency can be determined by dividing the output power by the input power.

$$\eta = \frac{P_{out}}{P_{in}}$$

Equation 20: Expression for finding the efficiency of a circuit.

Maximum and Minimum Inductor Current

To find $i_{L,max}$ and $i_{L,min}$, we must first solve for the load voltage. By rearranging Equation 19, we can determine an expression for load voltage.

$$V_{load} = \frac{D \cdot V_{in}}{\frac{D \cdot R_{T,ON}}{R_{load}} + \frac{(1 - D) \cdot R_{D,ON}}{R_{load}}}$$

Equation 21: Expression to find load voltage under non-ideal conditions.

Like the ideal conditions, the graph for inductor current ranges resembles a triangle wave, with the lowest value being $i_{L,min}$ and the highest value being $i_{L,max}$. By applying Kirchoff's voltage and current laws, to Figure 4, we can determine values for the maximum and minimum inductor current, specifically by looking at the slope for each side of the triangle. This process leads to a system of equations which can be simplified using both calculus and basic algebra, but by using some linear algebra and an online matrix calculator, we can easily determine the forms for $i_{L,min}$ and $i_{L,max}$.

$$\begin{bmatrix} -e^{\frac{-R_{T,ON\cdot D\cdot T_{SW}}}{L}} & 1 \\ 1 & -e^{\frac{-R_{T,ON\cdot (1-D)\cdot T_{SW}}}{L}} \end{bmatrix} \begin{bmatrix} i_{L,min} \\ i_{L,max} \end{bmatrix} = \begin{bmatrix} \frac{V_{in} - V_{load} - V_{T,ON}}{R_{T,ON}} \cdot (1 - e^{\frac{-R_{T,ON\cdot (1-D)\cdot T_{SW}}}{L}}) \\ \frac{V_{in} - V_{load} - V_{T,ON}}{R_{T,ON}} \cdot (1 - e^{\frac{-R_{T,ON\cdot (1-D)\cdot T_{SW}}}{L}}) \end{bmatrix}$$

Equation 22: Expression to solve the minimum and maximum inductor current.

Results

Ideal – Heavy Load

Once the code for "buck.m" was complete, I was able to run "buckproc.m" to test my Forward Euler integration algorithm. This was done by plotting each of the voltages and currents for each component in both the transient state and steady state.

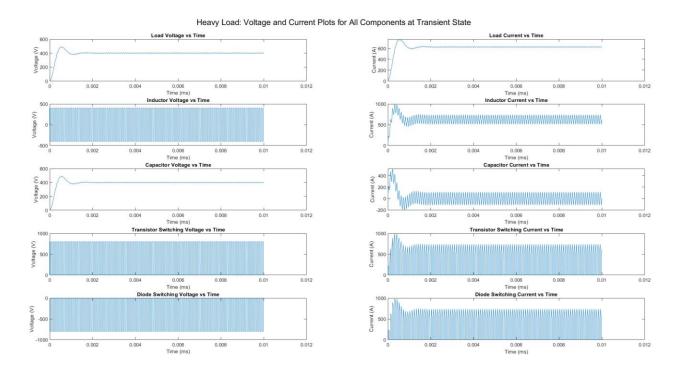


Figure 6: Voltage and Current graphs for each component at transient state.

From the graph for load voltage, load current, inductor current, and capacitor voltage, we can see that the values fluctuate for a small period before reaching steady state.

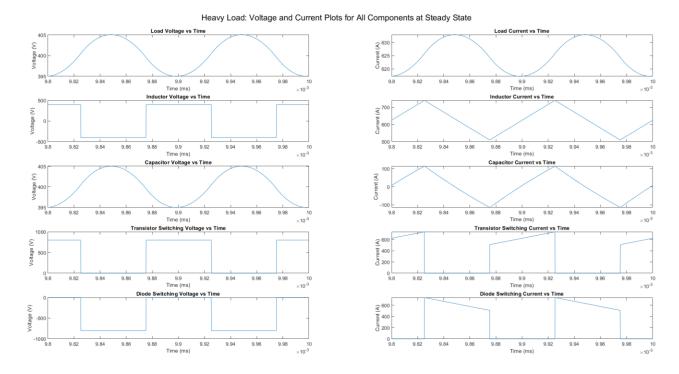


Figure 7: Voltage and Current graphs for each component at steady state.

In "buckproc.m", a separate section of code was written to plot the last two periods of each waveform. This was done to make each waveform's graph easier to read. With the number of periods being reduced, we can see where each waveform averages out to.

Instead of reading each of the graphs and estimating what the average of each waveform is, "buckproc.m" calls "aver.m" to display the average of each waveform onto the console.

Component	Voltage (V) Current		
Load Resistor	400.0307	625.0479	
Inductor	7.59E-15	625.0319	
Capacitor	400.0307	-0.016048	
Transistor	400	312.6551	
Diode	-400	312.606	

Table 1: Average Voltage and Current for each circuit component under heavy load.

If we use Equation 20 to solve the efficiency of the circuit, we find that the efficiency of circuit is 99.9657%.

Ideal – Light Load

When the simulation was complete for the heavy load, "buckproc.m" was able to focus on the light load. Like before, the script plotted each component's voltages and currents in the transient state.

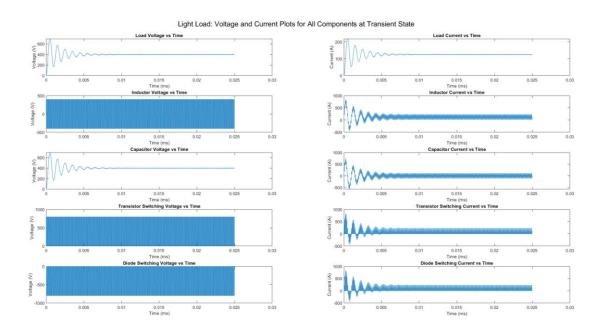


Figure 8: Voltage and Current graphs for each component at transient state.

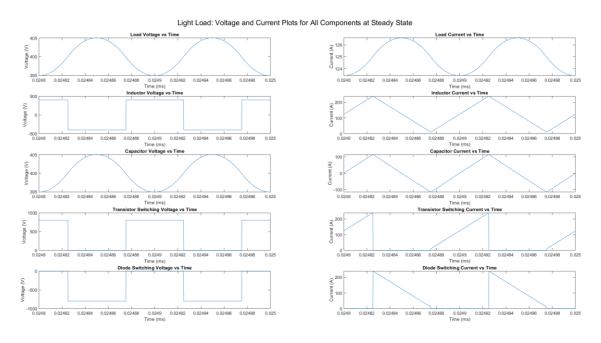


Figure 9: Voltage and Current graphs for each component at steady state.

Like the heavy load, the script plots the last two periods of each waveform to increase the readability.

Component	Voltage (V) Current (A		
Load Resistor	400.0307	625.0479	
Inductor	7.59E-15	625.0319	
Capacitor	400.0307	-0.016048	
Transistor	400 312.655		
Diode	-400	312.606	

Table 2: Average Voltage and Current for each circuit component under heavy load.

The efficiency of the circuit under light load comes out to 99.8114%.

Non-Ideal – Heavy Load

The final section of "buckproc.m" completed the calculations and plotting for the non-ideal situation. Unlike the previous two sections, this section of the code only focused on calculating values for the load voltage, inductor current, in addition to the current, voltage, and power of each switch.

The code in "buck.m" had to be slightly altered in order to incorporate the non-idealities of the circuit, such as the voltage drop and inherent resistance for each switch.

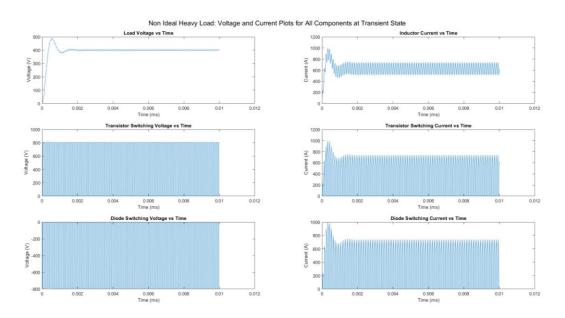


Figure 10: Voltage and Current graphs for each component at transient state.

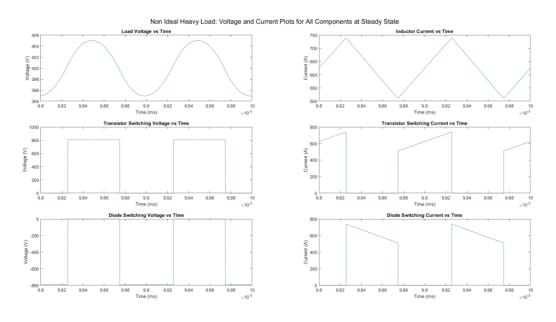


Figure 11: Voltage and Current graphs for each component at steady state.

Each of the components that were plotted share a similar shape to both ideal cases. However, some of the values are slightly different from what were seen in the ideal cases.

Component	Voltage (V)	Current (A)	Power (W)
Load Resistor	399.9508	Х	х
Inductor	х	624.9231	х
Transistor	396.3574	318.2797	2330.834
Diode	-403.5082	306.6434	2243.2617

Table 3: Average Voltage, Current, and Power for each circuit component under heavy load.

As we can see from Table 3, each component has slightly different values to the ones seen in both Table 1 and Table 2. These different values are most likely due to the non-idealities from both switches.

Using Equation 20, we find that the efficiency of the non-ideal circuit is 98.1559%.

From Table 3, we find that the power loss from the transistor is 2330.834 W and the power loss from the diode is 2243.2617 W.

Project #1\aver.m

25

```
% ID Number: 229,506
1
2
   % ECE 31033 - Project #1
3
   % aver.m
5
   % The fourth file (aver.m) contains a function you create to compute the average of
   % a waveform. Specifically, the function is of the form
6
7
            function av = aver(x,T,dt)
   % where x is the waveform to be averaged, T is its period, and dt is the period of time
8
9
   % between samples. This function must use the last period of the input waveform to
   % calculate the average.
10
11
   function av = aver(x, T, dt)
12
13
        location = length(x);
14
        av = 0;
        time = 0;
15
16
        while (time <= T)</pre>
17
18
            av = av + dt * (x(location));
19
            time = time + dt;
            location = location - 1;
20
21
        end
22
23
        av = av / T;
24
   end
```

Project #1\sw.m

```
1 % ID Number: 229,506
2
   % ECE 31033 - Project #1
3 % sw.m
4
5
   % The first file (sw.m) contains a function (sw) that accepts the duty cycle D, and a
   % single instant of time as an input, and outputs the state (on/off) of the transistor
6
7
   % at that time instant as an output. A Fourier series-based triangle wave that you
   % create within this function should be compared with the duty cycle D to
8
9
   % determine the state of the transistor. The output of the function is a 1 if the
   % transistor is to be turned on. It is a value of 0 if it is turned off.
10
11
12
   function state = sw(D, t)
13
       T_sw = 1 / 10000;
14
15
        W = 2 * pi / T sw;
16
17
        a k = 0;
        triangle_wave = 0.5;
18
19
        N = 200; % Number of Fourier terms.
20
21
22
        k = 1;
23
        while k <= N
            z = k * w * T sw; % Temporary variable; to simplify code for the coefficient.
24
25
            a k = (2 * (4 * cos(0.5 * z) - 2 * cos(z) - 2)) / (z^2);
26
27
            triangle_wave = triangle_wave + a_k * cos(k * w * t);
28
            k = k + 1;
29
        end
30
31
        if D >= triangle wave
32
            state = 1;
33
        else
34
            state = 0;
35
        end
36 end
```

Project #1\buck.m

```
% ID Number: 229,506
 1
   % ECE 31033 - Project #1
 2
 3 % buck.m
 4
 5 % The file (buck.m) contains the Forward Euler integration algorithm within a while
    % loop (FOR LOOPS ARE NOT ALLOWED). buck is not a function. The file buck.m only
 6
 7
    % contains a single while loop (i.e. while (t(k) < tend)) to solve for all circuit voltages
    % and currents of your buck converter. Within the while loop, you will call the
 8
 9
    % function sw at each time instant to determine the value of your transistor gate
    % (on or off). Voltages of currents and voltages of circuit components must be
10
11
    % determined within the while loop.
    while t vec(k) < tend</pre>
12
13
        if (ideal boolean) % If the circuit is ideal.
14
            switch_state(k) = sw(D, t_vec(k)); % calling sw.m
15
            % Inductor Current and Load Voltage Calculation
16
17
            i_L_{vec(k+1)} = i_L_{vec(k)} + dt * ((switch_state(k)) * V_in - V_load_{vec(k)}) / L;
    %i L
18
            V load vec(k+1) = V load vec(k) + dt * ((i L <math>vec(k) - (V load <math>vec(k) / R load)) / C);
    %V load
19
20
            % Switch 1 and 2: Voltage and Current Calculations
21
            if(switch_state(k))
22
                23
                 i_switch1(k+1) = i_L_vec(k+1) * switch_state(k);
24
25
                V switch2(k+1) = 0;
                 i_switch2(k+1) = 0;
26
27
28
                V_L_{vec}(k+1) = V_{in} - V_{load_avg};
29
            else
                 V switch1(k+1) = 0;
30
31
                 i_switch1(k+1) = 0;
32
33
                V \text{ switch2}(k+1) = -1 * V \text{ in};
34
                 i_switch2(k+1) = i_L_vec(k) * (1 - switch_state(k));
35
                 V_L_{vec(k+1)} = -1 * V_{load_avg};
36
37
            end
38
39
            % Capacitor: Voltage and Current Calculations
40
            i_C_{vec(k+1)} = i_L_{vec(k)} - (V_{load_{vec(k)}} / R_{load});
            V \in V(k+1) = V \text{ load } V(k+1);
41
42
            % Load: Current Calculation
43
            i load vec(k+1) = V load <math>vec(k+1) / R load;
44
45
        else % If the circuit is non ideal.
46
            switch_state(k) = sw(D_non_ideal, t_vec(k)); % calling sw.m
47
48
49
            if(switch state(k))
                 i_L \cdot vec(k+1) = i_L \cdot vec(k) + dt * ((V_in - V_T_on - V_load_vec(k) - (R_T_on * V_t))
50
    i_L_{vec}(k))) \overline{/} \overline{L};
                           %i L
```

```
i L vec(k+1) = i L vec(k) + dt * ((V in - V T on - V load vec(k) - (R T on * V load vec(k) - (
51
                    i_L_{vec(k))} \overline{7} \overline{L});
                                                                                                                                %i L
52
                                                                              % Switch 1: Voltage and Current Calculations
53
54
                                                                              V_switch1(k+1) = 0;
                                                                               i_switch1(k+1) = i_L_vec(k+1);
55
                                                                               P_switch1(k+1) = (R_T_on * i_L_vec(k+1) + V_T_on) * i_L_vec(k+1);
56
57
                                                                              % Switch 2: Voltage and Current Calculations
58
59
                                                                              V_switch2(k+1) = V_D_on + (R_D_on * i_L_vec(k+1)) - V_in;
60
                                                                               i \text{ switch2}(k+1) = 0;
61
                                                           else
62
                                                                                i_L_{vec}(k+1) = i_L_{vec}(k) + dt * ((-1 * V_{load_{vec}}(k) - V_{load_{vec}}(k) - V_{load_{vec}}(k) + (R_{load_{vec}}(k) + V_{load_{vec}}(k) +
                    i_L_vec(k)))) / L;
63
                                                                              % Switch 1: Voltage and Current Calculations
64
65
                                                                              V_switch1(k+1) = V_in + (R_D_on * i_L_vec(k+1)) + V_D_on;
                                                                              i switch1(k+1) = 0;
66
67
                                                                              % Switch 2: Voltage and Current Calculations
68
69
                                                                              V switch2(k+1) = 0;
70
                                                                               i_switch2(k+1) = i_L_vec(k+1);
                                                                               P_switch2(k+1) = (R_D_on * i_L_vec(k+1) + V_D_on) * i_L_vec(k+1);
71
72
                                                           end
73
74
                                                           V load vec(k+1) = V load vec(k) + dt * ((i L <math>vec(k) - (V load <math>vec(k) / R load)) / C);
                   %V_load
75
                                       end
76
77
                                       % Increment the time and index
                                       t \operatorname{vec}(k + 1) = t \operatorname{vec}(k) + dt;
78
79
                                       k = k + 1;
                  end
80
```

Project #1\buckproc.m

```
1 % ID Number: 229,506
   % ECE 31033 - Project #1
 2
   % buckproc.m
 3
 4
   % The file buckproc.m first contains the circuit parameter values (i.e. L, C, fsw, time
   % step, initial conditions etc.). Only the initial value of your circuit voltages and
 6
   % currents should be pre-established (i.e. Vload(1)=0). It then invokes buck. Finally,
 8
   % it performs your plotting and any post-processing calculations that are done
   % using the simulated data (such as computing average values, efficiency, etc.).
10 | %% Ideal - Given Values
11 V in = 800;
12 V load avg = 400;
13 V_load_ripple = 10;
14 P_load_light = 50000;
15 P load heavy = 250000;
16 frequency = 10000;
17
18 | ideal boolean = 1; % = 0 if non ideal, = 1 if ideal; here, it is ON.
19
20 | %% Ideal - Calculated Values
   T sw = 1 / frequency;
21
   D = V load avg / V in; % Duty Cycle
22
23
   R load light = (V load avg^2) / P load light;
24
25
    R_load_heavy = (V_load_avg^2) / P_load_heavy;
26
   L crit = (R load light * (1 - D)) / (2 * frequency);
27
28
   L = L_crit * 1.1;
29
30
   C = (V_load_avg / V_load_ripple) * (T_sw^2 * (1 - D)) / (8 * L);
31
32
   I load light = V load avg / R load light;
33
   I load heavy = V load avg / R load heavy;
34
   i L1 light = (V \text{ load avg } / \text{ R load light}) - (1 - D) * T sw * V load avg / (2 * L);
35
   i_L2_light = (V_load_avg / R_load_light) + (1 - D) * T_sw * V_load_avg / (2 * L);
36
37
38 i L1 heavy= (V load avg / R load heavy) - (1 - D) * T sw * V load avg / (2 * L);
39
    i_L2_{heavy} = (V_{load_avg} / R_{load_heavy}) + (1 - D) * T_sw * V_{load_avg} / (2 * L);
40
41 %% Buck Intialization - Heavy Load
42 % Initializing Values
43 k = 1;
44 t = 0;
45
   dt = 1e-7;
46
47
   tend = 100 * T_sw;
48
49 % Zero Vectors (used in buck)
50 t_vec = [0];
51 switch state = [0];
52
53 V_L_vec = [0];
```

```
54 | i L vec = [0];
55
 56 V C vec = [0];
57 | i C vec = [0];
58
59 V_load_vec = [0];
60 | i_load_vec = [0];
61
62 V switch1 = [0];
63 | i switch1 = [0];
64
65 V switch2 = [0];
66
    i \text{ switch2} = [0];
67
68
    %% Running Buck - Using R_load_heavy
69
     R load = R load heavy;
     disp('Running buck for heavy load.');
70
71
     buck
72
73
     %% Post-processing Calculations (computing avg values, efficiency, etc)
     disp("----")
74
75
     disp("Heavy Averages:")
76
77
     V_load_avg_func_H = aver(V_load_vec, T_sw, dt);
78
     disp(" V_load Average: " + V_load_avg_func_H);
79
80
     i_load_avg_func_H = aver(i_load_vec, T_sw, dt);
     disp(" i_load Average: " + i_load_avg_func_H);
81
82
    V_L_func_H = aver(V_L_vec, T_sw, dt);
83
    disp(" V_L Average: " + V_L_func_H);
84
85
     i_L_func_H = aver(i_L_vec, T_sw, dt);
86
     disp(" i_L Average: " + i_L_func_H);
87
88
    V_C_func_H = aver(V_C_vec, T_sw, dt);
89
90
     disp(" V_C Average: " + V_C_func_H);
91
     i_C_func_H = aver(i_C_vec, T_sw, dt);
92
93
     disp(" i C Average: " + i C func H);
94
95
     V_sw1_func_H = aver(V_switch1, T_sw, dt);
     disp(" V_sw1 Average: " + V_sw1_func_H);
96
97
98
     i_sw1_func_H = aver(i_switch1, T_sw, dt);
     disp(" i_sw1 Average: " + i_sw1_func_H);
99
100
     V_sw2_func_H = aver(V_switch2, T_sw, dt);
101
     disp(" V_sw2 Average: " + V_sw2_func_H);
102
103
104
     i_sw2_func_H = aver(i_switch2, T_sw, dt);
105
     disp(" i_sw2 Average: " + i_sw2_func_H);
106
107
     P out H = (V \text{ load avg func } H^2) / R \text{ load};
     P_in_H = V_in * i_sw1_func_H;
108
109 | eff_H = P_out_H / P_in_H;
```

```
110
    disp("Efficiency for Light Load: " + (eff_H * 100) + "%.");
111
    disp("----")
112
113
114 | %% Plotting - Heavy Load - Transient
115 % Plots for the transient to steady state
116 | figure;
117 sgtitle("Heavy Load: Voltage and Current Plots for All Components at Transient State");
118 % Plots for the Load
119 | subplot(5,2,1);
120 plot(t_vec, V_load_vec);
121 | title('Load Voltage vs Time');
122 | xlabel('Time (ms)');
123 | ylabel('Voltage (V)');
124
125 subplot(5,2,2);
126 plot(t_vec, i_load_vec);
127 | title('Load Current vs Time');
128 xlabel('Time (ms)');
129 ylabel('Current (A)');
130
131 % Plots for the Inductor
132 subplot(5,2,3);
133 plot(t_vec, V_L_vec);
134 | title('Inductor Voltage vs Time');
135 | xlabel('Time (ms)');
136 | ylabel('Voltage (V)');
137
138 | subplot(5,2,4);
139 | plot(t_vec, i_L_vec);
140 | title('Inductor Current vs Time');
141 xlabel('Time (ms)');
142 | ylabel('Current (A)');
143
144 % Plots for the Capacitor
145 subplot(5,2,5);
146 plot(t_vec, V_C_vec);
147 | title('Capacitor Voltage vs Time');
148 | xlabel('Time (ms)');
149 | ylabel('Voltage (V)');
150
151 subplot(5,2,6);
152 plot(t_vec, i_C_vec);
153 title('Capacitor Current vs Time');
154 xlabel('Time (ms)');
155 ylabel('Current (A)');
156
157 % Plots for Switch 1
158 | subplot(5,2,7);
159
    plot(t_vec, V_switch1);
160 | title('Transistor Switching Voltage vs Time');
161 xlabel('Time (ms)');
162 | ylabel('Voltage (V)');
163
164 | subplot(5,2,8);
165 plot(t vec, i switch1);
```

```
166 | title('Transistor Switching Current vs Time');
    xlabel('Time (ms)');
167
168 | ylabel('Current (A)');
169
170 % Plots for Switch 2
171 subplot(5,2,9);
172 | plot(t_vec, V_switch2);
173 | title('Diode Switching Voltage vs Time');
174 xlabel('Time (ms)');
175 | ylabel('Voltage (V)');
176
177 subplot(5,2,10);
178
    plot(t_vec, i_switch2);
179 | title('Diode Switching Current vs Time');
180 | xlabel('Time (ms)');
181 | ylabel('Current (A)');
182
183 | %% Plotting - Heavy Load - Steady State
184
    periods_to_plot = 2;
185
186 | points_per_period = round(T_sw / dt); % Points per period
187
    total_periods = floor(tend / T_sw); % Total number of periods in the simulation
188
189
     start_index = max(1, (total_periods - periods_to_plot) * points_per_period + 1);
190
     end_index = min(length(t_vec), total_periods * points_per_period);
191
192
    range to plot = start index:end index;
193
194 | %% Plot
195 | figure;
196 sgtitle("Heavy Load: Voltage and Current Plots for All Components at Steady State");
197 % Plots for the Load
198 subplot(5,2,1);
199 plot(t vec(range to plot), V load vec(range to plot));
200 | title('Load Voltage vs Time');
201 xlabel('Time (ms)');
202 | ylabel('Voltage (V)');
203
204 | subplot(5,2,2);
205 | plot(t_vec(range_to_plot), i_load_vec(range_to_plot));
206 | title('Load Current vs Time');
207 xlabel('Time (ms)');
208 ylabel('Current (A)');
209
210 % Plots for the Inductor
211 subplot(5,2,3);
212 | plot(t_vec(range_to_plot), V_L_vec(range_to_plot));
213 | title('Inductor Voltage vs Time');
214 xlabel('Time (ms)');
215
    ylabel('Voltage (V)');
216
217 | subplot(5,2,4);
218 | plot(t_vec(range_to_plot), i_L_vec(range_to_plot));
219 | title('Inductor Current vs Time');
220 xlabel('Time (ms)');
221 ylabel('Current (A)');
```

```
222
223 | % Plots for the Capacitor
224 subplot(5,2,5);
225 plot(t vec(range to plot), V C vec(range to plot));
226 title('Capacitor Voltage vs Time');
227 xlabel('Time (ms)');
228 ylabel('Voltage (V)');
229
230 subplot(5,2,6);
231 plot(t_vec(range_to_plot), i_C_vec(range_to_plot));
232 title('Capacitor Current vs Time');
233 xlabel('Time (ms)');
234 | ylabel('Current (A)');
235
236 % Plots for Switch 1
237 subplot(5,2,7);
238 plot(t_vec(range_to_plot), V_switch1(range_to_plot));
239 | title('Transistor Switching Voltage vs Time');
240 xlabel('Time (ms)');
241 ylabel('Voltage (V)');
242
243 subplot(5,2,8);
244 | plot(t_vec(range_to_plot), i_switch1(range_to_plot));
245 | title('Transistor Switching Current vs Time');
246 xlabel('Time (ms)');
   ylabel('Current (A)');
247
248
249 % Plots for Switch 2
250 subplot(5,2,9);
251 plot(t_vec(range_to_plot), V_switch2(range_to_plot));
252 | title('Diode Switching Voltage vs Time');
253 xlabel('Time (ms)');
254 ylabel('Voltage (V)');
255
256 | subplot(5,2,10);
257 | plot(t_vec(range_to_plot), i_switch2(range_to_plot));
258 title('Diode Switching Current vs Time');
259 xlabel('Time (ms)');
260 ylabel('Current (A)');
261
262
    263 | %% Buck Intialization - Light Load
264 % Initializing Values
265 k = 1;
266 t = 0;
267 \mid dt = 1e-7;
268
269 | \text{tend} = 250 * T_sw;
270
271 % Zero Vectors (used in buck)
272 t vec = [0];
273 | switch state = [0];
274
275 | V L vec = [0];
276 | i L vec = [0];
277
```

```
278 | V C vec = [0];
279
    i C vec = [0];
280
281 V load vec = [0];
282
    i_load_vec = [0];
283
284 \vee switch1 = \lceil 0 \rceil;
285
    i_switch1 = [0];
286
287
    V switch2 = [0];
288
    i_switch2 = [0];
289
290
    %% Running Buck - Using R_load_light
291
    R_load = R_load_light;
292
    disp('Running buck for light load.');
293
    buck
294
295
    %% Post-processing Calculations (computing avg values, efficiency, etc)
    disp("-----
296
297
    disp("Light Averages:")
298
299
    V_load_avg_func_L = aver(V_load_vec, T_sw, dt);
    disp(" V load Average: " + V load avg func L);
300
301
    i_load_avg_func_L = aver(i_load_vec, T_sw, dt);
302
303
    disp(" i_load Average: " + i_load_avg_func_L);
304
305
    V_L_func_L = aver(V_L_vec, T_sw, dt);
306
    disp(" V L Average: " + V L func L);
307
308
    i_L_func_L = aver(i_L_vec, T_sw, dt);
    disp(" i L Average: " + i L func L);
309
310
    V C func L = aver(V C vec, T sw, dt);
311
312
    disp(" V_C Average: " + V_C_func_L);
313
314
    i_C_func_L = aver(i_C_vec, T_sw, dt);
315
    disp(" i C Average: " + i C func L);
316
317
    V sw1 func L = aver(V switch1, T sw, dt);
    disp(" V_sw1 Average: " + V_sw1_func_L);
318
319
320
    i sw1 func L = aver(i switch1, T sw, dt);
321
    disp(" i_sw1 Average: " + i_sw1_func_L);
322
323
    V_sw2_func_L = aver(V_switch2, T_sw, dt);
324
    disp(" V_sw2 Average: " + V_sw2_func_L);
325
326
    i_sw2_func_L = aver(i_switch2, T_sw, dt);
327
    disp(" i_sw2 Average: " + i_sw2_func_L);
328
329
    P_out_L = (V_load_avg_func_L^2) / R_load;
330 \mid P in L = V in * i sw1 func L;
    eff_L = P_out_L / P_in_L;
331
332
333 disp("Efficiency for Light Load: " + (eff L * 100) + "%.");
```

```
334 | disp("----")
335 | %% Plotting - Light Load - Transient
336 % Plots for the transient to steady state
337 | figure;
338 sgtitle("Light Load: Voltage and Current Plots for All Components at Transient State");
339 % Plots for the Load
340 subplot(5,2,1);
341 plot(t_vec, V_load_vec);
342 | title('Load Voltage vs Time');
343 | xlabel('Time (ms)');
344 ylabel('Voltage (V)');
345
346 subplot(5,2,2);
347 plot(t_vec, i_load_vec);
348 | title('Load Current vs Time');
349 | xlabel('Time (ms)');
350 ylabel('Current (A)');
351
352 % Plots for the Inductor
353 subplot(5,2,3);
354 plot(t_vec, V_L_vec);
355 title('Inductor Voltage vs Time');
356 xlabel('Time (ms)');
357
   ylabel('Voltage (V)');
358
359 subplot(5,2,4);
360 | plot(t_vec, i_L_vec);
   title('Inductor Current vs Time');
361
362 xlabel('Time (ms)');
363 ylabel('Current (A)');
364
365 % Plots for the Capacitor
366 subplot(5,2,5);
367 | plot(t_vec, V_C_vec);
368 | title('Capacitor Voltage vs Time');
369 xlabel('Time (ms)');
370 ylabel('Voltage (V)');
371
372 | subplot(5,2,6);
373 | plot(t_vec, i_C_vec);
374 | title('Capacitor Current vs Time');
375 xlabel('Time (ms)');
376 | ylabel('Current (A)');
377
378 % Plots for Switch 1
379 subplot(5,2,7);
380 plot(t_vec, V_switch1);
381 | title('Transistor Switching Voltage vs Time');
382 xlabel('Time (ms)');
383
   ylabel('Voltage (V)');
384
385 | subplot(5,2,8);
386 plot(t_vec, i_switch1);
387 | title('Transistor Switching Current vs Time');
388 xlabel('Time (ms)');
389 ylabel('Current (A)');
```

```
390
391 % Plots for Switch 2
392 | subplot(5,2,9);
393 plot(t vec, V switch2);
394 | title('Diode Switching Voltage vs Time');
395 xlabel('Time (ms)');
396 | ylabel('Voltage (V)');
397
398 | subplot(5,2,10);
399 plot(t_vec, i_switch2);
    title('Diode Switching Current vs Time');
400
401 xlabel('Time (ms)');
402
    ylabel('Current (A)');
403
404
    %% Plotting - Light Load - Steady State
405
    periods to plot = 2;
406
407
    points per period = round(T sw / dt); % Points per period
    total periods = floor(tend / T sw); % Total number of periods in the simulation
408
409
    start index = \max(1, (total periods - periods to plot) * points per period + 1);
410
411
    end_index = min(length(t_vec), total_periods * points_per_period);
412
413
    range to plot = start index:end index;
414
    %% Plot
415
416 | figure;
    sgtitle("Light Load: Voltage and Current Plots for All Components at Steady State");
417
418 % Plots for the Load
419 subplot(5,2,1);
420 plot(t vec(range to plot), V load vec(range to plot));
421 | title('Load Voltage vs Time');
422 xlabel('Time (ms)');
423 ylabel('Voltage (V)');
424
425 | subplot(5,2,2);
426
    plot(t_vec(range_to_plot), i_load_vec(range_to_plot));
427 | title('Load Current vs Time');
428 xlabel('Time (ms)');
429 vlabel('Current (A)');
430
431 % Plots for the Inductor
432 subplot(5,2,3);
433 plot(t_vec(range_to_plot), V_L_vec(range_to_plot));
434 | title('Inductor Voltage vs Time');
    xlabel('Time (ms)');
435
436 ylabel('Voltage (V)');
437
438 | subplot(5,2,4);
439
    plot(t_vec(range_to_plot), i_L_vec(range_to_plot));
440 | title('Inductor Current vs Time');
441
    xlabel('Time (ms)');
442 | ylabel('Current (A)');
443
444 % Plots for the Capacitor
445 | subplot(5,2,5);
```

```
446 | plot(t vec(range to plot), V C vec(range to plot));
447
    title('Capacitor Voltage vs Time');
448 xlabel('Time (ms)');
    ylabel('Voltage (V)');
449
450
451
    subplot(5,2,6);
452
    plot(t_vec(range_to_plot), i_C_vec(range_to_plot));
453 | title('Capacitor Current vs Time');
454
   xlabel('Time (ms)');
   ylabel('Current (A)');
455
456
457 % Plots for Switch 1
458
    subplot(5,2,7);
459
    plot(t_vec(range_to_plot), V_switch1(range_to_plot));
460
    title('Transistor Switching Voltage vs Time');
461
    xlabel('Time (ms)');
    ylabel('Voltage (V)');
462
463
464
    subplot(5,2,8);
465
    plot(t_vec(range_to_plot), i_switch1(range_to_plot));
466 | title('Transistor Switching Current vs Time');
467
    xlabel('Time (ms)');
   ylabel('Current (A)');
468
469
470 % Plots for Switch 2
471
    subplot(5,2,9);
472
   plot(t_vec(range_to_plot), V_switch2(range_to_plot));
473
    title('Diode Switching Voltage vs Time');
474
   xlabel('Time (ms)');
    ylabel('Voltage (V)');
475
476
477
    subplot(5,2,10);
478
    plot(t_vec(range_to_plot), i_switch2(range_to_plot));
479 | title('Diode Switching Current vs Time');
480
    xlabel('Time (ms)');
    ylabel('Current (A)');
481
482
483
   %% Non Ideal - Given Values
484
485
   V T on = 1;
486
   V D on = 1;
487
    R_T_on = 0.01;
488
   R D on = 0.01;
489
490
    ideal_boolean = 0; % = 0 if non ideal, = 1 if ideal; here, it is OFF.
491
492 | %% Non Ideal - Calculated Values
493
    R load = R load heavy;
494
    D_non_ideal = (V_D_on + V_load_avg + (R_D_on * V_load_avg / R_load));
495
    D_non_ideal = D_non_ideal / (V_in - V_T_on + V_D_on + (R_D_on * V_load_avg / R_load) -
    (R_T_on * V_load_avg / R_load));
496
    i_L1_NI = (V_load_avg / R_load) - (((1 - D_non_ideal) * T_sw * V_load_avg) / (2 * L));
497
498
    i_L2_NI = (V_load_avg / R_load) + (((1 - D_non_ideal) * T_sw * V_load_avg) / (2 * L));
499
500 \ %% Buck Intialization - Heavy Load
```

```
501 % Initializing Values
502 \mid k = 1;
503 t = 0;
504 \mid dt = 1e-7;
505
    tend = 100 * T_sw;
506
507
508 % Zero Vectors (used in buck)
509 t vec = [0];
510 | switch_state = [0];
511
512 V L vec = [0];
513 | i_L_{vec} = [0];
514
515 | V C vec = [0];
516 \mid i_C_{vec} = [0];
517
518 \mid V load vec = \lceil 0 \rceil;
519 | i_load_vec = [0];
520
521 V switch1 = [0];
522 \mid i_switch1 = [0];
523
524 V_switch2 = [0];
525 \mid i_switch2 = [0];
526
527 P switch1 = [0]; % Power loss across the transistor; new for non-ideal calculations.
     P switch2 = [0]; % Power loss across the diode; new for non-ideal calculations.
528
529
530 %% Running Buck - Using R load heavy
    R_load = R_load_heavy;
531
     disp('Running buck for heavy load and non ideal conditions.');
532
533
    buck
534
535
    %% Post-processing Calculations (computing avg values, efficiency, etc)
536
     disp("----")
     disp("Non Ideal Averages:")
537
538
    V_load_avg_func_NI = aver(V_load_vec, T_sw, dt);
539
    disp(" V load Average: " + V load avg func NI);
540
541
     i_L_func_NI = aver(i_L_vec, T_sw, dt);
542
     disp(" i_L Average: " + i_L_func_NI);
543
544
545
    V_sw1_func_NI = aver(V_switch1, T_sw, dt);
     disp(" V_sw1 Average: " + V_sw1_func_NI);
546
547
    i_sw1_func_NI = aver(i_switch1, T_sw, dt);
548
    disp(" i_sw1 Average: " + i_sw1_func_NI);
549
550
551
    V sw2 func NI = aver(V switch2, T sw, dt);
552
    disp(" V_sw2 Average: " + V_sw2_func_NI);
553
554 i sw2 func NI = aver(i switch2, T sw, dt);
555
    disp(" i_sw2 Average: " + i_sw2_func_NI);
556
```

```
557 P sw1 func NI = aver(P switch1, T sw, dt);
558 disp(" P sw1 Average: " + V sw2 func NI);
559
560 P sw2 func NI = aver(P switch2, T sw, dt);
561 | disp(" P_sw2 Average: " + i_sw2_func_NI);
562
563 P out NI = (V load avg func NI^2) / R load;
564 | P_in_NI = V_in * i_sw1_func_NI;
565 | eff NI = P out NI / P in NI;
566
567
    disp("Efficiency for Non-Ideal: " + (eff_NI * 100) + "%.");
568 disp("Transistor Power Loss: " + P sw1 func NI);
569 disp("Diode Power Loss: " + P_sw2_func_NI);
570 | disp("----")
    %% Plotting - Non Ideal Heavy Load - Transient
571
572 | % Plots for the transient to steady state
573 | figure;
574 sgtitle("Non Ideal Heavy Load: Voltage and Current Plots for All Components at Transient
    State");
575 % Plots for the Load
576 subplot(3,2,1);
577 plot(t_vec, V_load_vec);
578 | title('Load Voltage vs Time');
579 xlabel('Time (ms)');
580 | ylabel('Voltage (V)');
581
582 | subplot(3,2,2);
583 | plot(t_vec, i_L_vec);
584 | title('Inductor Current vs Time');
585 xlabel('Time (ms)');
586 ylabel('Current (A)');
587
588 % Plots for Switch 1
589 | subplot(3,2,3);
590 plot(t_vec, V_switch1);
591 | title('Transistor Switching Voltage vs Time');
592 | xlabel('Time (ms)');
593 ylabel('Voltage (V)');
594
595 | subplot(3,2,4);
596 plot(t vec, i switch1);
597 | title('Transistor Switching Current vs Time');
598 xlabel('Time (ms)');
599
    ylabel('Current (A)');
600
601 % Plots for Switch 2
602 | subplot(3,2,5);
603 plot(t_vec, V_switch2);
604 | title('Diode Switching Voltage vs Time');
605
    xlabel('Time (ms)');
606
    ylabel('Voltage (V)');
607
608 | subplot(3,2,6);
609 plot(t_vec, i_switch2);
610 title('Diode Switching Current vs Time');
611 | xlabel('Time (ms)');
```

```
612 | ylabel('Current (A)');
613
614 | %% Plotting - Heavy Load - Steady State
615
    periods to plot = 2;
616
    points_per_period = round(T_sw / dt); % Points per period
617
618
    total periods = floor(tend / T sw); % Total number of periods in the simulation
619
620
    start index = \max(1, (total periods - periods to plot) * points per period + 1);
    end index = min(length(t vec), total periods * points per period);
621
622
    range to plot = start index:end index;
623
624
625
   %% Plot
626
    figure;
627
    sgtitle("Non Ideal Heavy Load: Voltage and Current Plots for All Components at Steady State")
628 % Plots for the Load
629 subplot(3,2,1);
630 plot(t_vec(range_to_plot), V_load_vec(range_to_plot));
631 | title('Load Voltage vs Time');
632 xlabel('Time (ms)');
633 | ylabel('Voltage (V)');
634
635 | subplot(3,2,2);
636 plot(t_vec(range_to_plot), i_L_vec(range_to_plot));
   title('Inductor Current vs Time');
637
638 xlabel('Time (ms)');
   ylabel('Current (A)');
639
640
641 % Plots for Switch 1
642 subplot(3,2,3);
643 plot(t_vec(range_to_plot), V_switch1(range_to_plot));
644 | title('Transistor Switching Voltage vs Time');
645 xlabel('Time (ms)');
   ylabel('Voltage (V)');
646
647
648
    subplot(3,2,4);
649 plot(t vec(range to plot), i switch1(range to plot));
650 title('Transistor Switching Current vs Time');
651 xlabel('Time (ms)');
   ylabel('Current (A)');
652
653
654 % Plots for Switch 2
655 | subplot(3,2,5);
   plot(t_vec(range_to_plot), V_switch2(range_to_plot));
656
    title('Diode Switching Voltage vs Time');
657
658 xlabel('Time (ms)');
659
    ylabel('Voltage (V)');
660
661
    subplot(3,2,6);
662 plot(t vec(range to plot), i switch2(range to plot));
663 | title('Diode Switching Current vs Time');
664 xlabel('Time (ms)');
665 ylabel('Current (A)');
```