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INSTITUTE OF ENGINEERING & TECHNOLOGY

DETAILED LECTURE NOTES

UNIT-6

INTRODUCTION TO PAGE NO.
ELECTROMAGNETISM

Del operator $\rightarrow (\vec{\nabla})$
now marks

$$\vec{\nabla} \equiv \hat{i} \frac{\partial}{\partial x} + \hat{j} \frac{\partial}{\partial y} + \hat{k} \frac{\partial}{\partial z}$$

i) [Gradient] (grad φ) of scalar scalar field \rightarrow
let $\phi = \phi(x, y, z)$ be the scalar field, which
is function of (x, y, z) .

Now change in ϕ is $d\phi \rightarrow$

$$\begin{aligned} d\phi &= \left(\frac{\partial \phi}{\partial x} \right) dx + \left(\frac{\partial \phi}{\partial y} \right) dy + \left(\frac{\partial \phi}{\partial z} \right) dz \\ &= \left(\hat{i} \frac{\partial \phi}{\partial x} + \hat{j} \frac{\partial \phi}{\partial y} + \hat{k} \frac{\partial \phi}{\partial z} \right) \cdot (dx\hat{i} + dy\hat{j} + dz\hat{k}) \end{aligned}$$

$$d\phi = (\vec{\nabla}\phi) \cdot \vec{dl}$$

$$\text{here } \vec{dl} = dx\hat{i} + dy\hat{j} + dz\hat{k}$$

here the quantity

$$\boxed{\vec{\nabla}\phi = \text{grad } \phi = \hat{i} \frac{\partial \phi}{\partial x} + \hat{j} \frac{\partial \phi}{\partial y} + \hat{k} \frac{\partial \phi}{\partial z}} \quad (1)$$

represents the gradient of ϕ , it is
a vector quantity.

Physical Significance \rightarrow since $d\phi = (\vec{E} \cdot \vec{d}) \cdot \vec{dl}$

$$\therefore d\phi = |\vec{E}\phi| |\vec{dl}| \cos\theta$$

$$\Rightarrow \frac{d\phi}{dl} = \nabla\phi \cos\theta. \quad \text{for maximum change in } \phi, \theta \rightarrow 0$$

$$\therefore \boxed{\left(\frac{d\phi}{dl}\right)_{\max} = \vec{\nabla}\phi = \text{grad } \phi} \quad \therefore \cos\theta = 1$$

The gradient $\nabla\phi$, is direction along the normal to the surface. Moreover, thus $\nabla\phi$, represents the maximum change in ϕ .

Divergence ($\vec{\nabla} \cdot \vec{A}$)

Let us consider a vector field \vec{A} , $\vec{A} = A_x \hat{i} + A_y \hat{j} + A_z \hat{k}$

then

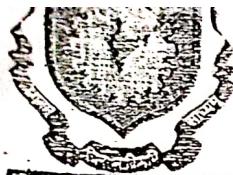
$$\operatorname{div} \vec{A} = (\vec{\nabla} \cdot \vec{A}) = \left(\hat{i} \frac{\partial}{\partial x} + \hat{j} \frac{\partial}{\partial y} + \hat{k} \frac{\partial}{\partial z} \right) \cdot (A_x \hat{i} + A_y \hat{j} + A_z \hat{k}).$$

$$\Rightarrow \boxed{\operatorname{div} \vec{A} = \left(\frac{\partial A_x}{\partial x} + \frac{\partial A_y}{\partial y} + \frac{\partial A_z}{\partial z} \right)}$$

Physical meaning \rightarrow if a volume dV is placed in vector field $\vec{A}(x, y, z)$; the outgoing flux from surface S is given by -

$$\oint_S \vec{A} \cdot d\vec{a}$$

$$\therefore \boxed{\operatorname{div} \vec{A} = \vec{\nabla} \cdot \vec{A} = \iint_S \frac{\vec{A} \cdot d\vec{a}}{dV \rightarrow 0}}$$

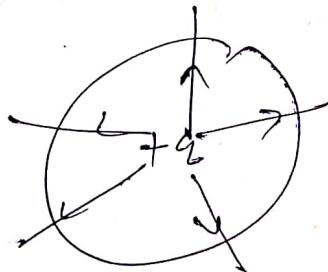


Thus, the net outgoing flux, per unit volume from the closed surface of small volume placed in vector field, is called.

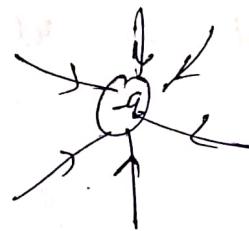
Divergence of that vector field.

Divergence of vector \vec{A} is a measure of how much \vec{A} , spreads out (Diverges), from the point of observation.

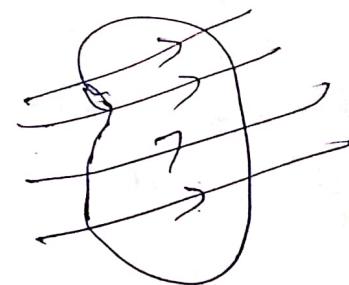
it may be +ive, -ive or zero.



$$\text{Div } \vec{E} = +\text{ive}$$



$$\text{Div } \vec{E} = -\text{ive}$$



$$\text{Div } \vec{E} = 0$$

CURL \vec{A}

$$\text{curl } \vec{A} = \nabla \times \vec{A} = \left(\frac{\partial}{\partial x} + \frac{\partial}{\partial y} + \frac{\partial}{\partial z} \right) \times (A_x \hat{i} + A_y \hat{j} + A_z \hat{k})$$

$$\text{or } \nabla \times \vec{A} = \begin{vmatrix} \hat{i} & \hat{j} & \hat{k} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ A_x & A_y & A_z \end{vmatrix}$$

Physical meaning of curl \vec{A} →

Let us consider a point P, in vector field \vec{A} , and path C, enclosing the point.

Now, we divide the path into small displacement $d\vec{l}$.

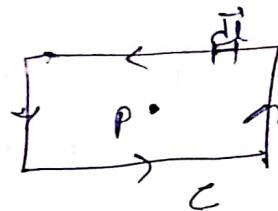
If the surface area enclosed by path C, is small, then \vec{A} remains same on each point of the path.

then $\oint_C \vec{A} \cdot d\vec{l}$ is line integral of \vec{A} , over closed path C. So →

Curl of any vector is defined as the line integral per unit small surface area enclosed by the path, so

$$\text{curl } \vec{A} = \lim_{da \rightarrow 0} \left(\frac{\oint_C \vec{A} \cdot d\vec{l}}{da} \right) \cdot \hat{n}$$

Curl means rotation of in vector \vec{A} .





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DETAILED LECTURE NOTES

PAGE NO.

Causs's Divergence Theorem →

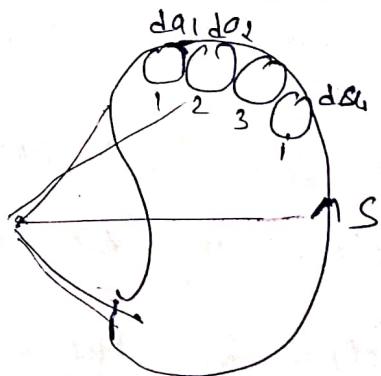
let we consider a vector field \vec{A} . The vol^m enclosed by it V .

If this volume is enclosed by an imaginary surface S .

Volume can be considered as made of many rectangular tetragons.

outgoing flux from each small element -

$$\phi_i = \oint_S \vec{A}_i \cdot d\vec{a}_i \quad \text{--- (1)}$$



∴ total flux from this surface S →

$$\oint_S \vec{A} \cdot d\vec{a} = \sum_i \oint_S \vec{A}_i \cdot d\vec{a}_i \quad \text{--- (2)}$$

divergence of \vec{A} on small area element $d\vec{a}_i$

$$\therefore \operatorname{div} \vec{A}_i = \frac{1}{dV_i} \sum_i \oint_S \vec{A}_i \cdot d\vec{a}_i$$

$dV_i \rightarrow 0$

$$\oint_S \vec{A}_i \cdot d\vec{a}_i = \lim_{dV_i \rightarrow 0} \operatorname{div} \vec{A}_i \cdot dV_i \quad \text{--- (3)}$$

from (2) and (3)

$$\oint_S \vec{A} \cdot d\vec{a} = \sum_i \operatorname{div} \vec{A}_i \cdot dV_i$$

If $dV_i \rightarrow 0$, the summation sign can be replaced by integration sign -

$$\boxed{\oint_S \vec{A} \cdot d\vec{a} = \int_V (\operatorname{div} \vec{A}) dV}$$

Thus, the surface integration of any vector field over a closed surface, is equal to the volume integration of its divergence.

This is called Cauchy's Divergence theorem.

Stokes's Curl Theorem \Rightarrow Let us consider an area enclosed by closed path c in a vector field \vec{A} .

To determine the line integral along the path c , we divide whole surface in small rectangles, and find line integral over each closed path of rectangle, the sum them all.

Let us consider path KLMN,

For each boundary of path KLMN, the path integration is equal and opposite to that of neighbouring path like

$$\text{since } \int_K^L \vec{A} \cdot d\vec{l} = - \int_L^K \vec{A} \cdot d\vec{l}$$

$$\therefore \int_K^L \vec{A} \cdot d\vec{l} + \int_L^K \vec{A} \cdot d\vec{l} = 0$$

The sum of all the integrals over common path becomes zero.

Thus, sum only comes from the integration over boundary C, ..

$$\therefore \oint_C \vec{A} \cdot d\vec{l} = \sum_i \oint_{dC} \vec{A} \cdot d\vec{l}_i \quad \text{--- (1)}$$

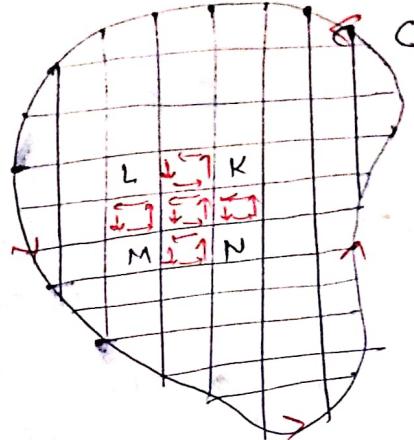
As we know the curl over the small path (with zero)

$$\therefore \text{curl } \vec{A} = \lim_{dai_i \rightarrow 0} \left[\frac{1}{dai_i} \sum_i \oint_{dC} \vec{A} \cdot d\vec{l}_i \right] \hat{n}$$

$$\therefore \oint_{dC} \vec{A} \cdot d\vec{l}_i = \lim_{dai_i \rightarrow 0} \text{curl } \vec{A} \cdot \hat{n} dai_i \quad \text{--- (2)}$$

∴ from (1) and (2)

$$\oint_C \vec{A} \cdot d\vec{l} = \lim_{dai_i \rightarrow 0} \sum_i (\vec{r} \times \vec{A}) \cdot \hat{n} dai_i$$



for small surface element $\rightarrow \Sigma \rightarrow \int$

$$\boxed{\int_C \vec{A} \cdot d\vec{l} = \int_S (\vec{A} \times \hat{n}) \cdot d\vec{a}} \quad \left\{ \begin{array}{l} \hat{n} da \\ = \frac{d\vec{a}}{da} \end{array} \right.$$

\Rightarrow Thus the line integration of any vector along the closed path is equal to the surface integration of curl of that surface vector, over the surface enclosed by the path.

This is called Stoke's curl Theorem.

Gauss Law of Electrostatic \rightarrow

According to this law \rightarrow the net electric flux through a closed surface, is equal to ratio of the charge enclosed by that surface, and ϵ_0 .

$$\boxed{\phi_E = \frac{q}{\epsilon_0}} \quad \text{---(1)} \quad \text{or} \quad \phi_E = \frac{1}{\epsilon_0} \int_V p \cdot dV \quad \text{---(2)}$$

where $p \rightarrow$ is the volume charge density.

eqⁿ (2) is Gauss law in integral form.

Now, from the definition of flux

$\phi_E = \int_S \vec{E} \cdot d\vec{a}$ ---(3) if the surface S is divided into small area element $d\vec{a}$.

$$\text{then } dp = \vec{E} \cdot d\vec{a}$$

From Gauss divergence theorem

$$\oint_S \vec{E} \cdot d\vec{\sigma} = \int_V (\nabla \cdot \vec{E}) dv - \textcircled{3}$$

From eqn $\textcircled{2}$ and $\textcircled{3}$

$$\frac{1}{\epsilon_0} \oint_V P \cdot d\vec{v} = \int_V (\nabla \cdot \vec{E}) dv$$

$$\Rightarrow \frac{P}{\epsilon_0} = \nabla \cdot \vec{E} \Rightarrow \boxed{\nabla \cdot \vec{D} = P} - \textcircled{4}$$

Eqn $\textcircled{4}$ represents the
Gauss law in differential form.

$\left. \begin{array}{l} \text{as } \vec{D} = \epsilon \vec{E} \\ \text{electric displacement} \\ \text{vector} \end{array} \right\}$

Now as we know $\nabla \times \vec{E} = -\nabla v$

\therefore from $\textcircled{4}$ $D = -\epsilon \nabla v$

$$\nabla \cdot (-\epsilon \nabla v) = P_v$$

$$\Rightarrow -\nabla^2 v = \frac{P_v}{\epsilon} \Rightarrow \boxed{\nabla^2 v = -\frac{P_v}{\epsilon}} - \textcircled{5}$$

Eqn $\textcircled{5}$ is known as
Poisson's Equation.

Now for charge free region $P_v = 0$

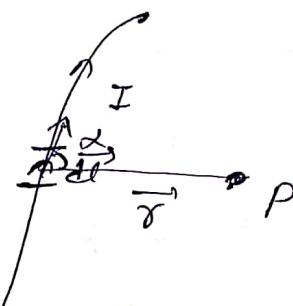
$$\boxed{\nabla^2 v = 0} - \textcircled{6}$$

This eqn is known as
Laplace Equation.

Bio - Savart law \rightarrow This law is used to determine the resultant magnetic field \vec{B} at position r in 3-D space generated by a steady current. [Steady-current means a continuous flow of charge, which does not change with time].

Let us consider a wire carrying a current I , we want to find out

magnetic field at point P , which is r distant \vec{r} , by from wire.



We divide wire into small length elements. Let we take a small length element dl , the direction of dl is in direction of \hat{r} .

Now the magnetic field at P , due to current flow in element dl , is dB

$$dB \propto \frac{I}{r^2}$$

$$\Rightarrow dB = \frac{\mu_0}{4\pi} \frac{I dl \sin\theta}{r^2}$$

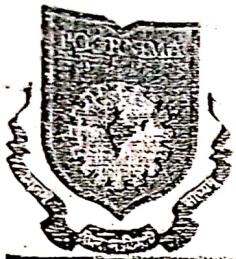
$$dB \propto dl$$

$$dB = \frac{\mu_0}{4\pi} \frac{I \vec{dl} \times \hat{r}}{r^2}$$

$$\text{here } \hat{r} = \frac{\vec{r}}{|\vec{r}|}$$

is unit vector.

$$B = \int dB = \frac{\mu_0}{4\pi} \int I \frac{\vec{dl} \times \vec{r}}{r^3}$$



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DETAILED LECTURE NOTES

PAGE NO.

The sources of light from which phase difference between the waves from them reaching at any point in space does not change with time rather remains constant, are known as coherent source.

This property of the waves is known as coherence. It is an important property of waves which refers to the connection betⁿ the phase of light waves.

Coherence effect are mainly divided into two categories.

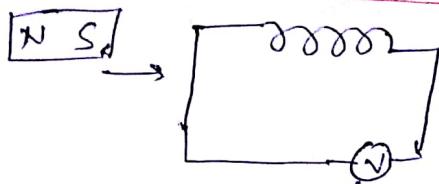
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Faraday's law of Electromagnetic Induction →

According to this law - when magnetic flux linked with any circuit changes, an e.m.f., is induced in the circuit, and this induced e.m.f., is proportional to the rate of change of magnetic flux linked with the circuit.

and direction of this e.m.f. is always opposite to the charges responsible for its production

$$\boxed{e \propto \frac{d\phi}{dt}, e = -\frac{\partial \phi}{\partial t}}$$



Ampere's circuital law → according to this law -

Line integral of magnetic field over a closed path is equal to μ_0 times the net current passes through the closed path. -

$$\boxed{\oint \vec{B} \cdot d\vec{l} = \mu_0 \sum I}$$

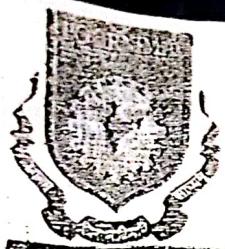
Displacement current → In electromagnetism, a displacement current is a quantity, defined in terms of the rate of change of electric displacement field.

If we have a varying magnetic field linked with a conductor, then electric field induced in conductor will also vary.

Thus due to change in electric field, a current caused a current, known as displacement current

$$I_D = \frac{\partial D}{\partial t} = \epsilon \frac{\partial E}{\partial t}$$

This current is not due to moving charges, it is due to the varying electric field.



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DETAILED LECTURE NOTES

PAGE NO.

Maxwell's Equation

1. first eqn is based on Causs's law for electric field.

According to it

$$\oint_S \vec{E} \cdot d\vec{a} = \frac{Q}{\epsilon_0} \quad \text{--- (1)}$$

if charge inside the closed path is continuously distributed the ρ - is volume charge density defined as - $Q = \int_V \rho dV \quad \text{--- (2)}$

from Eqn (1) and Eqn (2) -
$$\oint_S \vec{E} \cdot d\vec{a} = \frac{1}{\epsilon_0} \int_V \rho dV \quad \text{--- (3)}$$

Eqn (3) is integral form of Maxwell's eqn.

Now, according to Causs divergence theorem-

$$\oint_S \vec{E} \cdot d\vec{a} = \int_V (\nabla \cdot \vec{E}) dV$$

$$\therefore \int_V (\nabla \cdot \vec{E}) dV = \frac{1}{\epsilon_0} \int_V \rho dV$$

$$\Rightarrow \nabla \cdot \vec{E} = \frac{\rho}{\epsilon_0} \Rightarrow \text{div } \vec{E} = \frac{\rho}{\epsilon_0}$$

This is the differential form of Maxwell's Eqⁿ.

from displacement vector $\vec{D} = \epsilon \vec{E}$

$$\therefore \nabla \cdot (\epsilon \vec{E}) = \rho \Rightarrow \boxed{\nabla \cdot \vec{D} = \rho}$$

for free space $\rho = J = 0$

$$\therefore \nabla \cdot \vec{E} = 0$$

$$\boxed{\nabla \cdot \vec{D} = 0}$$

Maxwell's Second Eqⁿ \rightarrow This Eqⁿ is derived from Gauss law for magnetic field.

According to this law - net outgoing flux from any closed surface is always zero. [b'coz the magnetic field lines always form closed loops].

$$\text{since } \phi_B = 0 \quad \text{or} \quad \oint \vec{B} \cdot d\vec{a} = 0$$

S

This is the integral form of Maxwell's IInd Eqⁿ.
From Gauss Divergence theorem -

$$\oint_S \vec{B} \cdot d\vec{a} = \int_V (\nabla \cdot \vec{B}) dV = 0 \Rightarrow \boxed{\nabla \cdot \vec{B} = 0}$$

This is differential form of Maxwell IInd Eqⁿ.



This equation prove that monopole does not exist in nature.

Maxwell's Third Equation

This Equation is derived from Faraday's law of electromagnetic induction.

According to this law, - whenever magnetic flux linked with a circuit, changes, an e.m.f. is induced in the circuit and this induced e.m.f. is directly proportional to the rate of change of magnetic flux linked with the circuit.

$$e \propto \frac{d\phi_B}{dt}$$

or $e = -\frac{d\phi_B}{dt} \quad \text{--- } ①$

This e.m.f. is defined as the work done in carrying a unit positive charge around a open loop. Thus

$$e = \int_{C^0} \vec{E} \cdot d\vec{l} \quad \text{--- } ②$$

a) we know the magnetic field - $\phi_B = \oint_S \vec{B} \cdot d\vec{a}$ flux \rightarrow ③

$$\therefore \oint_C \vec{E} \cdot d\vec{x} = -\frac{\partial}{\partial t} \oint_S \vec{B} \cdot d\vec{a}$$

$$\Rightarrow \boxed{\oint_C \vec{E} \cdot d\vec{l} = \oint_S \left(-\frac{\partial \vec{B}}{\partial t} \right) \cdot d\vec{a}} \rightarrow ④$$

This is the integral form of Maxwell's third eqn.
from Stoke's curl theorem -

$$\oint_C \vec{E} \cdot d\vec{x} = \oint_S (\nabla \times \vec{E}) \cdot d\vec{a}$$

$$\therefore \oint_S (\nabla \times \vec{E}) \cdot d\vec{a} = \oint_S \left(-\frac{\partial \vec{B}}{\partial t} \right) \cdot d\vec{a}$$

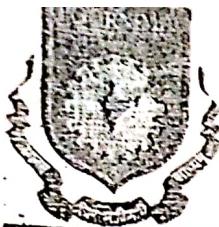
$$\Rightarrow \boxed{\nabla \times \vec{E} = -\frac{\partial \vec{B}}{\partial t}} \text{ or } \boxed{\text{curl } \vec{E} = -\frac{\partial \vec{B}}{\partial t}}$$

This is differential form of Maxwell's third eqn.

for static field $\frac{\partial \vec{B}}{\partial t} = 0 = \frac{\partial \vec{E}}{\partial t}$

$$\therefore \nabla \times \vec{E} = 0$$

$$\text{or } \oint_S \vec{E} \cdot d\vec{l} = 0$$



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DETAILED LECTURE NOTES

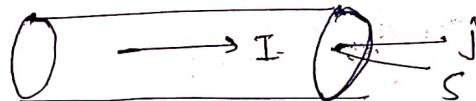
PAGE NO.

Equation of continuity \rightarrow

$$\text{As we know } I = \int_S \vec{J} \cdot d\vec{a} \quad \text{---(1)}$$

if we consider a current carrying conductor, and ρ be the volume charge density, then the total charge in the volume V is

$$q = \oint_V \rho_v \cdot dv$$



$$\therefore I = -\frac{dq}{dt} = -\frac{d}{dt} \int_V \rho \cdot dv \quad \text{---(2)}$$

from eqⁿ (1) and eqⁿ (2)

$$\oint_S \vec{J} \cdot d\vec{a} = -\frac{d}{dt} \int_V \rho \cdot dv \quad \text{---(3)}$$

from Gauss Divergence theorem -

$$\oint_S \vec{J} \cdot d\vec{a} = \int_V (\nabla \cdot \vec{J}) \cdot dv \quad \text{---(4)}$$

from (3) and (4)

$$\int_V (\nabla \cdot \vec{J}) \cdot dv = -\frac{d}{dt} \int_V \rho \cdot dv$$

$$\Rightarrow \boxed{\nabla \cdot \vec{J} = \nabla \cdot \vec{J} = -\frac{\partial \rho}{\partial t}}$$

$$\Rightarrow \boxed{\nabla \cdot \vec{F} + \frac{dp}{dt} = 0}$$

This eqⁿ is known as equation of continuity and represents the physical fact of conservation for charge.

~~Maxwell's fourth eqⁿ~~

This eqⁿ is based upon Ampere's circuital law, also to this law - line integral of magnetic field over a closed path is equal to all lines the net current passes through the closed path.

$$\oint_C \vec{B} \cdot d\vec{l} = \mu \Sigma I \quad \text{--- (1)}$$

$$\text{as we know } \Sigma I = \oint_S \vec{F} \cdot d\vec{a} \quad \text{--- (2)}$$

$$\therefore \oint_C \vec{B} \cdot d\vec{l} = \mu \oint_S \vec{F} \cdot d\vec{a}$$

$$\text{from Stokes' law theorem} - \oint_C \vec{B} \cdot d\vec{l} = \oint_S (\vec{E} \times \vec{B}) \cdot d\vec{a}$$

$$\therefore \text{from (2) and (3)} \quad \text{--- (3)}$$

$$\Rightarrow \nabla \times \vec{B} = \mu \vec{F} \quad \text{--- (4)}$$

Eqⁿ (4) is valid only for steady close current. For changing electric field it does not holds true b'coz if we take divergence of eqⁿ (4) -

$$\nabla \cdot (\nabla \times \vec{B}) = \nabla \cdot \vec{F}$$



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DETAILED LECTURE NOTES

PAGE NO.

$$\text{Since } \nabla \cdot (\vec{E} \times \vec{A}) = 0 \quad \text{div}(\text{curl } \vec{A}) = 0$$

$$\therefore \vec{E} \cdot (\vec{\nabla} \times \vec{B}) = 0$$

$$\therefore \vec{E} \cdot \vec{J} = 0 \quad - \textcircled{5}$$

But from eqⁿ of continuity $\nabla \cdot \vec{J} + \frac{\partial P}{\partial t} = 0$

so. eqⁿ ⑤ is conflicts with the equation of continuity $\text{div } \vec{J} = - \frac{\partial P}{\partial t}$

Thus here it is clear that Ampere's law relates magnetic field to the steady current only.

while for the current, produces due to change in electric field w.r.t. to time this law is not valid.

Maxwell removed this inconsistency by giving a suggestion that total current density is made of two types of currents -

1) free current density J_f due to motion of free charges.

2) Displacement current J_D due to change in electric field.

$$\text{Eqn } ⑤ \quad \vec{J} = \vec{J}_f + \vec{J}_d$$

becomes

$$\vec{\nabla} \times \vec{B} = \mu (\vec{J}_f + \vec{J}_d)$$

$$\text{On taking divergence} \quad \vec{\nabla} \cdot (\vec{\nabla} \times \vec{B}) = \mu (\nabla \cdot \vec{J}_f + \nabla \cdot \vec{J}_d)$$

$$\therefore \vec{\nabla} \cdot \vec{J}_f = - \nabla \cdot \vec{J}_d$$

$$\text{but from Eqn of continuity} \quad \nabla \cdot \vec{J}_f + \frac{\partial P}{\partial t} = 0$$

$$\therefore \nabla \cdot \vec{J}_f = - \frac{\partial P}{\partial t}$$

$$\Rightarrow \nabla \cdot \vec{J}_d = \frac{\partial P}{\partial t}$$

$$\text{or } \nabla \cdot \vec{J}_d = \frac{\partial}{\partial t} (\nabla \cdot \vec{D}).$$

$$\left. \begin{array}{l} \nabla \cdot \vec{D} = P \\ \text{Maxwell's 1st eqn} \end{array} \right\}$$

$$\Rightarrow \vec{J}_d = \frac{\partial \vec{D}}{\partial t} \quad \text{--- (6)}$$

Eqn ⑥ represents the displacement current, which is due to change in electric field. Now Maxwell's forth eqn becomes. (corr. to true.)

$$\vec{\nabla} \times \vec{B} = \mu (\vec{J}_f + \vec{J}_d).$$

$$\Rightarrow \vec{\nabla} \times \vec{B} = \mu \vec{J}_f + \mu \frac{\partial \vec{D}}{\partial t}$$

$$\Rightarrow \boxed{\vec{\nabla} \times \vec{B} = \mu \vec{J}_f + \mu \epsilon \frac{\partial \vec{E}}{\partial t}}$$

Subtracting eqⁿ (2) from eqⁿ (3) →

$$\vec{E} \cdot (\vec{B} \times \vec{H}) - \vec{H} \cdot (\vec{E} \times \vec{E}) = E \frac{\partial}{\partial t} (\epsilon_0 F) + H \frac{\partial (\mu_0 H)}{\partial t}$$

$$\therefore \vec{\nabla} \cdot (\vec{E} \times \vec{H}) = -\frac{1}{2} \frac{\partial}{\partial t} (E^2 + \mu_0 H^2) \quad \left. \begin{array}{l} (4) \\ \vec{A} \cdot (\vec{B} \times \vec{C}) \\ = \vec{B} (\vec{C} \times \vec{A}) - \vec{C} (\vec{A} \times \vec{B}) \end{array} \right\}$$

Integrating eqⁿ (4) over a volume V, then

$$\int (\vec{\nabla} \cdot (\vec{E} \times \vec{H})) dV = -\frac{\partial}{\partial t} \int \left(\frac{E^2}{2} + \frac{\mu_0 H^2}{2} \right) dV$$

from Gauss divergence theorem

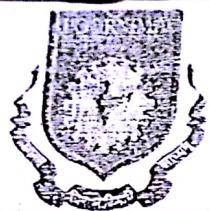
$$\boxed{\int_S (\vec{E} \times \vec{H}) \cdot d\vec{s} = -\frac{\partial}{\partial t} \int \left(\frac{E^2}{2} + \frac{\mu_0 H^2}{2} \right) dV} \quad (5)$$

The R.H.S. of eqⁿ (5), represents the rate of change of total EM Energy, Therefore the L.H.S. should also represents the flux of total energy passing per unit time from a closed surface bounding the field and it is denoted by \vec{P} (Poynting vector).

$$\Rightarrow \vec{P} = \vec{E} \times \vec{H} \text{ watt/m}^2 = \frac{\text{energy}}{\text{time} \times \text{area}}$$

The \vec{P} , has the dimensions of $\frac{\text{energy}}{\text{area} \times \text{time}}$ and hence is interpreted

as the rate at which the energy flows through unit area of surface. This statement is termed as Poynting theorem and represents the law of conservation of Energy.



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DETAILED LECTURE NOTES

PAGE NO.

Energy flow Due to plane EM wave -
Poynting vector

As EM waves propagates through space from one point to another they transport energy with them.

Let the em wave propagates through free space - $\sigma = \rho = J = 0$

$$\therefore \nabla \times \vec{E} = - \frac{\partial \vec{B}}{\partial t} \quad \text{---(1)}$$

$$\left\{ \begin{array}{l} \vec{D} = \epsilon \vec{E} \\ \vec{B} = \mu_0 \vec{H} \end{array} \right.$$

On taking divergence dot product with \vec{H}

$$\vec{H} \cdot (\nabla \times \vec{E}) = - H \cdot \frac{\partial (\mu_0 \vec{H})}{\partial t} \quad \text{---(2)}$$

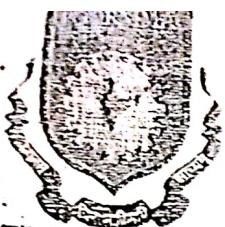
similarly from Maxwell fourth eqⁿ

$$\nabla \times \vec{B} = \mu J + \mu \frac{\partial \vec{D}}{\partial t} \quad \left\{ \begin{array}{l} J = 0 \\ B = \mu H \end{array} \right.$$

$$\nabla \times \vec{H} = \frac{\partial \vec{D}}{\partial t}$$

Dot product with \vec{E}

$$\vec{E} \cdot (\nabla \times \vec{H}) = \vec{E} \cdot \frac{\partial (\epsilon \vec{E})}{\partial t} \quad \text{---(3)}$$



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DETAILED LECTURE NOTES

PAGE NO.

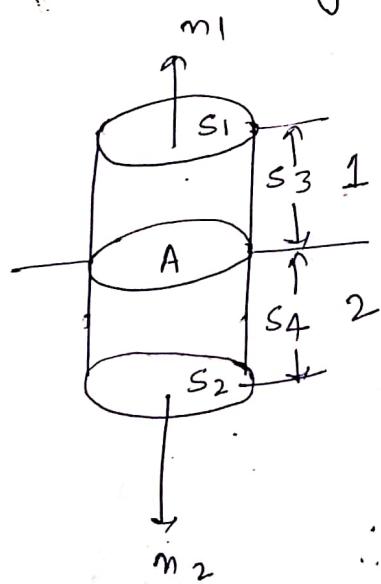
Boundary conditions for electric magnetic field vector (\vec{E} , \vec{D} , \vec{B} and \vec{H})

We shall consider the behaviour of EM waves at the boundaries between different media.

A boundary means - the end of one region and the beginning of the other.

By study boundary conditions - we study the behaviour of tangential and normal component of EM field vector at the boundary surfaces.

(i) Boundary condition for $\vec{B} \rightarrow$



at we consider two media 1 and 2, in a box having four surfaces S_1, S_2, S_3 and S_4 .

from Maxwell's IInd eqⁿ -

$$\nabla \cdot \vec{B} = 0$$

$$\oint_S \nabla \cdot \vec{B} \cdot d\vec{V} = 0$$

Cauchy divergence theorem -

$$\oint_S \vec{B} \cdot \vec{n} ds = 0$$

- (1)

Applying eqn (1) for all surfaces of the box -

$$\int_{S_1} \vec{B}_1 \cdot \vec{n}_1 dS_1 + \int_{S_2} \vec{B}_2 \cdot \vec{n}_2 dS_2 + \int_{S_3} \vec{B}_1 \cdot \vec{n}_1 dS_3 + \int_{S_4} \vec{B}_2 \cdot \vec{n}_2 dS_4 = 0$$

At the boundary ; the height of the box approaches zero , and S_1 and S_2 approaches same area A , and contribution from S_3 and $S_4 \rightarrow 0$

$$\Rightarrow \int_A (\vec{B}_1 \cdot \vec{n}_1 + \vec{B}_2 \cdot \vec{n}_2) dA = 0 \quad \text{as } \vec{n}_1 = -\vec{n}_2$$

$\therefore B_1 \cdot n_1 = B_2 \cdot n_1$

$$\Rightarrow B_{1n} = B_{2n}$$

i.e. the nor normal component of magnetic induction is continuous across the boundary.

⑨ Boundary condition of Displacement vector $\vec{D} \rightarrow$
from Maxwell's Eqn $\rightarrow \nabla \cdot \vec{D} = P$

$$\int_V (\nabla \cdot \vec{D}) dV = \int_V P dV$$

from Gauss Divergence theorem -

$$\oint_S (\vec{D} \cdot \hat{n}) dS = \int_V P dV \quad \text{for all surfaces of the box -}$$

$$\int_{S_1} \vec{D}_1 \cdot \vec{n}_1 dS + \int_{S_2} \vec{D}_2 \cdot \vec{n}_2 dS + \int_{S_3} \vec{D}_1 \cdot \vec{n}_1 dS + \int_{S_4} \vec{D}_2 \cdot \vec{n}_2 dS = \int_V P dV$$

at boundary $S_1 = S_2 = A$ and contribution from S_3 and $S_4 \rightarrow 0$

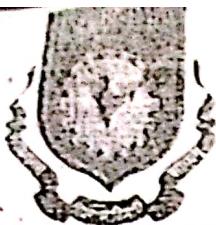
$$\text{Now } \int_V P dV = \int_S \sigma dA = \sigma \cdot A$$

$$\therefore \int_{S_1} \vec{D}_1 \cdot \vec{n}_1 dS + \int_{S_2} \vec{D}_2 \cdot \vec{n}_2 dS = \sigma A$$

Thus the normal

$$\Rightarrow A(D_1 \cdot n_1 - D_2 \cdot n_2) = \sigma \text{ component of electric}$$

$$\Rightarrow D_1 n_1 - D_2 n_2 = \sigma \text{ displacement vector is not continuous across the interface and changes by an amount equal to surface current density at the interface .}$$



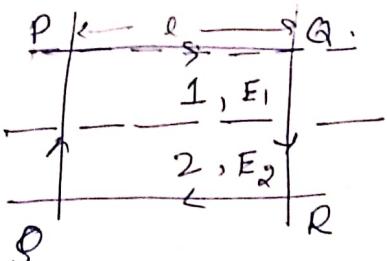
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DETAILED LECTURE NOTES

PAGE NO.

③ Boundary condition for \vec{E} - let us consider a rectangular loop PARS bounding the surface S from Maxwell eqn -



$$\nabla \times \vec{E} = -\frac{\partial \vec{B}}{\partial t}$$

$$\text{Now } \int_S (\nabla \times \vec{E}) \cdot \hat{n} ds = - \int_S \frac{\partial \vec{B}}{\partial t} \cdot \hat{n} ds.$$

using Stoke's theorem

$$\int_{\text{PQRS}} \vec{E} \cdot d\vec{l} = - \int_S \frac{\partial \vec{B}}{\partial t} \cdot \hat{n} ds$$

$$\therefore \int_{PA} \vec{E}_1 \cdot d\vec{l} + \int_{RS} \vec{E}_2 \cdot d\vec{l} + \text{contribution from sides QR and SP}$$

At boundary the height of the loop is zero.

so contribution from sides QR and PS will be zero. and $\int \vec{B} \cdot \hat{n} ds \rightarrow 0$ b'coz no flux can be enclosed when $S_h \rightarrow 0$

$$\therefore \int_{PA} \vec{E}_1 \cdot d\vec{l} + \int_{RS} \vec{E}_2 \cdot d\vec{l} = 0$$

$$\vec{E}_1 \cdot \vec{PQ} - \vec{E}_2 \cdot \vec{RS} = 0 \Rightarrow \boxed{\vec{E}_{1f} = \vec{E}_{2f}}$$

Now \vec{E}_1 and \vec{E}_2 are since ($\vec{P}\vec{B} = -\vec{R}$)
the tangential component of the electric field
in two media.

Thus, the tangential component of \vec{E} , are
continuous across the interface.